NASA TECHNICAL MEMORANDUM

(NASA-TH-X-72822) HYPERSONIC RESEARCH ENGINE/AEROTHERMODYNAMIC INTEGRATION MODEL, EXPERIMENTAL RESULTS. VOLUME 2: MACH 6 PERFORMANCE (NASA) 426 P HC 7. CSCL 21E N76-27238

Unclas G3/07 44617_

HYPERSONIC RESEARCH ENGINE/AEROTHERMODYNAMIC

INTEGRATION MODEL - EXPERIMENTAL RESULTS

· Volume II - Mach 6 Performance

by

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(Contract No. NAS1-6666)

April 1976

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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
LANGLEY RESEARCH CENTER, HAMPTON, VIRGINIA

NATIONAL TECHNICAL INFORMATION SERVICE
US DEPARTMENT OF COMMERCE
SPRINGFIELD, VA 22161

12H

1 Report No.	2 Government Accession No	3 Recipient's Catalog No
NASA TM X-72822		
4 Title and Subtitle HYPERSONIC RESEARCH ENGINE	Z/AEROTHERMODYNAMIC	5 Report Date April 1976
INTEGRATION MODEL - EXPERI	MENTAL RESULTS	6 Performing Organization Code
Volume II - Mach 6 Perform	nance	3745
7 Author(s)		8 Performing Organization Report No.
Earl H. Andrews, Jr.; Erne		
Engineering Staff, AiRese	earch Manutacturing Compa	10 Work Unit No
9 Performing Organization Name and Address	- 0.10	505-05-41-03
NASA Langley Research Cent Hampton, VA 23665	er	11 Contract or Grait No NAST-6666
		13 Type of Report and Period Covered
12 Sponsoring Agency Name and Address		Technical Memorandum
National Aeronautics and S	Space Administration	14 Sponsoring Agency Cide
Washington, D.C. 20546		the oppositional agency of the
15 Supplementary Notes		
Special technical informat	tion release, not planne	d for formal NASA Publication.
Special becomied involved	tion refease, not prainte	2 . of forma. There is an income
16 Abstract		
	Research Engine (HRF) Pr	oject was initiated in 1967
for the purpose of advanct	ing the technology of ai	rbreathing propulsion for
hypersonic flight. A larg	re component (inlet, com	bustor, and nozzle) and structures
development program was er	ncompassed by the projec	t. The component development pro-
gram was culminated in 19.	/4 WITH THE TESTS OF d T decignated the Aerother	ull-scale (18 in. diameter cowl and modynamic Integration Model (AIM),
in the NASA Lewis Research	h Center. Plum Brook Sta	tion Hypersonic Tunnel Facility
' at Mach numbers of 5, 6, a	and 7. AIM tests descri	ptions, data results, and analysis
results have been previous	sly documented. Four re	ports document computer program
analysis results of the Al	im experimental engine p	erformance. Enough information nal analysis and/or additional
or different interpretation	on of the AIM data. The	present report (Volume II) pre-
sents computer program res	sults for the Mach 6 per	formance tests. Program results
are contained in three add	ditional volumes that ha	ve the following subtitles:
Volume I - Mach 6 Cor	monont Intogration	
	Component Integration an	d Performance
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17 Key Words 'Suggested by Author(s))	18 Distribut	ion Statement
Propulsion	ŀ	
Scramjets Engine Performance		Unclassified - Unlimited
Hypersonic Propulsion		OHE COOPE TO CHITTING ON
Hydrogen Fuel		grane -
	Security Classif (of this page)	21 No of Pages 22 Price
Unclassified	Unclassified	424 \$10.50° ⁴ \

HYPERSONIC RESEARCH ENGINE/AEROTHERMODYNAMIC INTEGRATION MODEL - EXPERIMENTAL RESULTS

Volume II - Mach 6 Performance

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SUMMARY

An extensive aerothermodynamic development program for the purpose of advancing the technology of airbreathing propulsion for hypersonic flight has been conducted by NASA in the form of the Hypersonic Research Engine (HRE) Project. The engine components (inlet, combustor, and nozzle) aerothermodynamic development program culminated in the testing of an engine which integrated these components and allowed assessment of engine performance at Mach numbers of 5, 6, and 7. This engine was termed the Aerothermodynamic Integration Model (AIM) and was a water-cooled, hydrogen-fueled, full-scale configuration of the HRE design concept, 18 inches in diameter at the cowl lip and 87 inches long.

Descriptions of the AIM tests and a computer program used in the engine performance analyses, as well as data results and analyses, have been previously documented. All of the results of the engine performance computer program, including enough information to enable additional analysis or interpretation of the data, are reported in four volumes. Volume I present's Mach 6 component integration results that were obtained with supersonic combustion. During the integration tests, inlet unstart limits were determined for fuel injection from the first stage fuel injectors only and for multi-stage fuel injection. Optimization of the fuel injector combination that would yield the best combustion and engine performance was attempted. Volume II (present report) presents Mach 6 engine performance results during supersonic and subsonic combustion modes. Combustion mode transition was successfully performed, exit surveys made, and effects of altitude, angle of attack, and inlet spike position were determined during these tests. Volume III presents Mach 7 component integration and engine performance results with supersonic combustion modes. Fuel injector optimization was again attempted, exit surveys made, and the effects of low free-stream total temperature, free-stream oxygen content, and angle of attack were studied during these tests. Volume IV presents Mach 5 component integration and engine performance results with supersonic and subsonic combustion modes. Combustion mode transition was successfully demonstrated, exit surveys made, and effects of free-stream total temperature, free-stream oxygen content, and angle of attack were investigated during these tests.

INTRODUCTION

The NASA Hypersonic Research Engine (HRE) Project was undertaken to design, develop, and construct a hypersonic research ramjet engine for high performance and to flight test the developed concept on the X-15-2A airplane over the speed range from Mach 3 to 8. It should be emphasized that from the beginning the design was specified to be a research ramjet engine to conduct meaningful experiments and was in no sense intended to be a small-scale prototype of a propulsion system for any particular mission.

About one year after the development phase of the HRE program was underway, the X-15 program was phased out; as a result, adjustments to the project plan and scope were necessitated, which were, however, effected without detriment to achievement of the basic project objectives. The result of the adjustment was that ground testing became the major experimental effort for the HRE program. Engine aerothermodynamic components (inlet, combustor, and nozzle) were developed in separate ground-test programs. Results of the development tests are documented in references 1 through 3. Regeneratively cooled engine structures were also included in the ground-testing program. Tests of the hydrogen-cooled engine structure progressed from small panels and problem area components in laboratory setups to wind-tunnel tests at Mach 6.7 of a full-scale, flight-weight engine termed the Structure Assembly Model (SAM). Results of this program, which was completed in May 1971, are reported in reference 4. Culmination of all the HRE development testing was the engine tests of what was termed the Aerothermodynamic Integration Model (AIM). The purpose of the tests of this full-scale, watercooled, hydrogen-fueled engine was to integrate the aerothermodynamic components and to assess the engine performance at Mach numbers of 5, 6, and 7. Successful tests of the AIM were completed in April 1974.

The AIM employed the HRE design concept of an axisymmetric engine, 18 inches in diameter at the cowl lip and 87 inches long. Versatility was incorporated into the AIM to allow: (1) inlet spike translation for optimum air flow and inlet internal contraction ratio variation; and (2) hydrogen fuel injection for tailored fuel distribution for proper heat release in a diverging combustor, and to change the mode of combustion from supersonic to subsonic or vice versa. The AIM tests are reported in reference 5 and data results of the tests have been analyzed in terms of engine performance by use of a computer program (ref. 6) generated during the HRE program. Results of these analyses are reported in references 7 through 9.

The purpose of the present reports (herein and refs. 10 to 12) is to present experimental engine performance results obtained from computer program analyses of the test data. These results contain the free-stream conditions, pressure distributions, fuel injection configuration and rate, etc., that should enable additional analysis or interpretation of results other than those previously reported. It

should be noted that all units are in U.S. Customary Units because the data results from the HRE contracts, which were initiated in May 1965 with a follow-on effort in February 1967, were under that system. Because of the cost that would have been incurred if the contractors had been required to change to the metric system, the U.S. Customary Units were retained through the HRE contractual effort; this procedure is consistent with the guidelines for conversion established by NASA.

SYMBOLS

All units are in U.S. Customary Units because of the reason noted above.

A area, ft.²

M Mach number

P or p pressure, psia

r radius, in.

 R_{Cl} cowl lip radius at 120 tangent point (see table 3), in.

x longitudinal distance from inlet spike virtual tip (see table 3), in.

longitudinal distance from inlet spike virtual tip to the cowl lip l20 tangent point (see table 3), in.

Δx longitudinal distance inlet centerbody moved from inlet physical close-off, in.

 $\Delta\Delta x$ difference between an actual x_{CL} value and the Mach 6 x_{CL} value of 34.884 in., in.

T temperature, OR

 α angle of attack, deg.

fuel equivalence ratio; value of unity is for stoichiometric combustion (subscript symbols or notations, such as ϕ_{1A} or ER1A, represent the values for the designated fuel injector (e.g., 1A), EROA is the sum of all ϕ -values).

Subscripts:

0 free stream

ref. reference condition

th throat

T total

APPARATUS

Experimental Tests

Experimental tests of the HRE/AIM were conducted in the Plum Brook Hypersonic Tunnel Facility (HTF) (figs. 1(a) and 1(b)) at nominal Mach numbers of 5, 6, and 7. The AIM is shown partially installed in the HTF in the photographs of figures 1(c) and 1(d). During the tests the engine was nearly completely enshrouded except for an 11-inch gap between the facility nozzle exit and the front of the shroud as depicted in the schematic of figure 1(e). This test configuration was suggested by results of a subscale tunnel starting investigation reported in reference 13.

A description of the facility and the results of calibration tests are presented in reference 14. The test facility used an induction-heated, drilled-core graphite storage bed to raise the temperature of nitrogen to a nominal 4960° R at a maximum design pressure of 1200 psia. The nitrogen was mixed with ambient-temperature oxygen to produce synthetic air. Diluent nitrogen was added with the oxygen in the mixture at tunnel Mach numbers below 7 to control free-stream total temperature and to supply the correct weight flow. Because of facility heater deterioration and a lack of time to implement necessary repairs, true temperature simulation of 3700° R at Mach 7 was not achieved; a maximum temperature of about 3100° R was obtained.

The original test plan is summarized in table 1. Because of testing problems and limitations in facility schedule, the test plan was altered to provide a maximum of data to meet the test objectives. Details of the AIM tests are described in reference 5. General test conditions, results, and remarks of the AIM tests were tabulated in references 5 and 9 and are presented herein as table 2. All tests (reading numbers in second column) are listed including the tests that were aborted because of tunnel starting or other problems. Run numbers were assigned to AIM reading numbers or groups of AIM reading numbers with the same test objective (some readings represent zero success, partial success, or are reruns of others) to provide a means for a cross-check with the original plan.

Model

The HRE/AIM was a full-scale (18 inches in diameter at the cowl and 87 inches long), water-cooled, hydrogen-fueled research engine. Details of the design and fabrication of the AIM have been reported in references 16 through 29. The design is described generally in references 5 and 9, and some difficulties encountered with the AIM during the tests are discussed in reference 5.

A schematic of the AIM is presented in figure 2 and the coordinates are listed in table 3. The AIM incorporated a mixed compression inlet with a translating spike that enabled the close-off of the engine (an early HRE program

requirement). The inlet was designed for spike translation to the most open position for Mach 4 to 6 operation with spillage occurring up to Mach 6. At Mach 6 "shock-on-lip" occurred, and from Mach 6 to 8 the spike was designed to translate to maintain shock-on-lip over this Mach number range. An "upsloping throat" was incorporated in the inlet which enabled the inlet to not only maintain shock-on-lip with spike translation for Mach 6 to 8, but also to have increased inlet contraction ratio with increased Mach number. The combustor was designed with diverging walls and the area distribution is shown in figure 3(a) with fuel injector locations indicated. Figure 3(b) presents a sketch of the combustor with the locations of the staged fuel injectors and two sets of ignitors indicated (a third set of ignitors planned for the outerbody at an x-station of 54.38 inches was not installed). The set of ignitors at an x-station of 42.0 inches malfunctioned and use was discontinued (see fig. 3(b)) about midway in the Mach 6 test program (see discussion in ref. 5). Injectors 1A, 1B, 1C, 4, 2A, and 2C were designed to allow optimum distribution of the fuel in the combustor to obtain a fuel equivalence ratio, ϕ , of unity during the supersonic combustion mode. During the supersonic combustion mode, it was desired to inject the maximum amount of fuel from the first-stage injectors (IA and IB) without unstarting the inlet; all of the fuel was designed to be injected from injectors 1A and 1B at Mach 8. Injectors 3A and 3B were designed for use in the subsonic combustion mode. The locations are tabulated in figure 3(b) for the designed Mach 6 inlet operating position; cowl lip positions other than the Mach 6 position (because of spike translation) result in different x-station values for the injectors and ignitors on the outer wall and also for injector 3B. These changes are accounted for in the performance results presented herein.

Instrumentation

Planned instrumentation for the AIM is documented in reference 15. All of the instrumentation planned was not used because of facility instrumentation recording channel limitations or damages to instrumentation in inaccessible places during the AIM final assembly or during AIM repairs at the test site. A list of all planned instrumentation is presented in table 4 (obtained from ref. 5) with notations indicating the items not installed or damaged, the recording channel numbers for each item used, and the ranges of the pressure transducers or thermocouples.

Method of Calculation

A computer program that incorporated methods described in reference 15 was used in reducing the data from the AIM tests to engineering units. Listings of this program were checked for accuracy and determination of steady-state conditions. Times of interest were selected from each run and the information from the engineering units computer program was used in a performance analysis computer program which incorporated methods described in reference 6. After the erroneous surface pressures were eliminated, the remaining pressures at each station were averaged by the performance computer program which then performed surface-pressure integration by linear interpolation and determined the skinfriction coefficients. Chemical equilibria of the synthetic air and fuel-air mixtures were calculated by the program using methods described in reference 30.

Description of Performance Program Methods

General.- Several methods were used to establish validity of critical parameters, such as the wind tunnel Mach number. The first method used curves generated from instrumentation rakes installed during calibration of the wind tunnel. The second method used measured values of wind tunnel total pressure and temperature, and pitot pressure at the spike tip along with real-gas, normal-shock solution to calculate the wind tunnel Mach number. The third method used measured values of wind tunnel total temperature, spike-tip pitot pressure, and spike cone surface pressure, along with the real-gas, normal-and conical-shock solutions, to calculate the wind tunnel Mach number. Calculations made utilizing each of the three methods indicated good agreement. After confidence was established in the three methods, the use of the third method was discontinued, since it required excessive computer time. Additional information concerning tunnel Mach number determination is contained in reference 9.

The conditions at the inlet throat were determined by computing the momentum and total enthalpy from the pressure forces and accounting for friction and heat losses incurred on the inlet spike and the internal surfaces. The inlet mass flow ratio and additive drag were determined from theoretical calculations (ref. 31). Pressures used in these calculations were obtained as follows: (1) for conditions where inlet start was obtained ($M_{th} > 1$), the calculated mass-momentum-average static pressure was used, and the measured static pressures at the throat were not used; and (2) for conditions where inlet unstart was experienced ($M_{th} \le 1$), the average of the measured static pressures at the throat was used with the Mach number constrained to unity to calculate spillage and additive drag.

For both cases above, the flow was analytically expanded (isentropically) from the inlet throat conditions to the freestream static pressure in order to determine the hypothetical static enthalpy and associated velocity which are required to compute the inlet kinetic energy efficiency and the inlet process efficiency (as required under the contract statement of work). Also the flow was analytically compressed (isentropically) from the inlet throat conditions until the calculated total enthalpy matched the known total enthalpy after heat loss. For a started inlet, a side calculation was made by isentropically expanding the flow to an area which was arbitrarily set 10 percent larger than the throat area (for flow stability). At this point, the flow was passed through a normal shock. The limiting subsonic pressure recovery for the inlet and the corresponding kinetic energy and process efficiencies were then determined from conditions downstream of the normal shock. These inlet performance parameters were considered of interest as indicators of the overall inlet performance and of flow conditions prior to inlet unstart.

Two methods were used to calculate conditions at the combustor stations:
(1) up to the first station where fuel was injected, the mass-momentum-averaged static pressure that satisfied the state, continuity, momentum, and energy equations was calculated; and (2) at stations downstream of the first fuel injector the average of the measured innerbody and outerbody pressures was used, and the combustor efficiency was calculated to satisfy the conservation equations. For these methods it was assumed that the flow area equals the geometric duct

area (no flow separation). The amount of hydrogen required to react in order to satisfy the measured static pressure, the duct area, the heat loss, and the conservation equations is computed by the program. Of the total hydrogen injected or present in the flow at a given station, the amount which reacts has been named "real" hydrogen and is used in the equilibrium chemistry process being completed. The hydrogen which is not reacting has been named "inert" hydrogen. The concept of real and inert hydrogen and the station-wise conversion from inert to real is simply a bookkeeping procedure in the program which simulates or "models" the mixing process. The inert hydrogen is assumed to have the properties of an inert gas, not to react with other species, and not to dissociate.

The combustor throat was defined as the point of minimum-flow area between the struts in the subsonic combustion mode and at the strut exit plane in the supersonic combustion mode. When the computed one-dimensional Mach number at the assumed combustor exit was found to be less than 0.95, the computation was considered to improperly represent the subsonic combustor flow situation in that the flow must have reached a sonic point further downstream. With the area increasing added combustion (heat release) downstream of the assumed combustor exit station is implied. Therefore, a side calculation was made of the combustor efficiency required to produce sonic velocity at the assumed combustor exit station, as if this added heat release occurred prior to the assumed combustor exit station. For this condition, the performance program printout shows results under the heading SONIC THROAT (e.g., reading 94, time 150.342 sec).

The regeneratively cooled combustor performance ("COMBUSTOR REGEN" in the performance program printout) was simulated by recalculating the total enthalpy at the combustor exit as the sum of the free-stream enthalpy of the synthetic air, the enthalpy of the hydrogen fuel at 50° R, and the absolute value of the heat loss through all the engine surfaces wetted by the internal flow stream. Using this total enthalpy, the stream total pressure, and the same combustion efficiency, the combustor exit static-state properties were also computed.

Nozzle performance was obtained by isentropically expanding the flow from the actual and regeneratively cooled combustor exits to the nozzle exit area and to ambient pressure ("NOZZLE AE" and "NOZZLE PO" in the performance program printout). The flow was then isentropically expanded from the actual combustor throat to those nozzle stations representing the locations of pressure taps, and the local skin-friction coefficients were calculated using the Spalding-Chi correlation. The nozzle vacuum stream thrust coefficient was also computed. This coefficient is arbitrarily defined in previous HRE documents (e.g., refs. 3 and 15) as the ratio of the actual nozzle exit total momentum (stream thrust) divided by the theoretical nozzle exit total momentum where the flow was isentropically expanded from the combustor exit conditions to the nozzle exit area (512.389 in 2). The actual nozzle exit total momentum was determined by taking the combustor exit total momentum and adding (or subtracting) the pressure force, the friction force, and one-half of the calculated drag force (onehalf of strut assumed to be charged to the nozzle component). The hypothetical static enthalpy resulting from the computed isentropic expansion from the combustor exit conditions to the free-stream static pressure was used to calculate the nozzle kinetic energy and process efficiencies.

Side calculations were made of a fictitious stagnation combustion process (constant pressure and zero velocity) with 100 percent combustion efficiency and no loss to the walls (denoted in the performance program printout as "FICTIVE COMBUSTOR"), followed by an isentropic expansion to ambient pressure to obtain the combustor effectiveness. Also to obtain the combustor effectiveness, the flow at the combustor exit was expanded to free-stream static pressure and the total momentum at this pressure was determined. The combustor effectiveness (ref. 15) is then the change in total momentum for the actual combustor process from the combustor entrance condition to the expanded (free-stream static pressure) condition divided by the change in total momentum for the fictitious process mentioned above from the combustor entrance condition to the expanded (free-stream static pressure) condition. Side calculations were also made of a fictitious nozzle to determine the static and total conditions ("FICTIVE NOZZLE" in the performance program printout) required to match the actual vacuum specific impulse at the nozzle exit.

Calculation of cooling load distribution. For the AIM tests, the heat loss distribution was determined from the differences between the skin thermocouples inbedded in the engine surfaces and the cooling water temperatures. Standard heat-transfer equations were used to obtain local heat losses. These losses were then adjusted linearly with the overall heat loss as measured by the overall water temperature rise. The detailed equations and procedures used for these computations are presented in reference 9.

Tare forces.- Purge nitrogen was injected in the AIM cavity between the non-metric "windshield" shroud and the metric outerbody to assure that hot tunnel gases did not enter into this cavity. This method produced a large tare force which was of the same order of magnitude as the engine net thrust. An effort was made to reduce and even control the tare force by suitable control of the pressures in two parts of the cavity. This tare-force control concept was, however, not achieved. Since the thrust is considered the most important measurement in evaluating the engine performance, special tare-force calibration tests were made and the results carefully correlated in order to determine the correction for the measured thrust. The method and procedures are described in detail in references 5 and 9.

External drag. - The external drag was calculated from the summation of pressure and friction forces acting on the external metric surfaces of the AIM. The method and procedures are described in reference 9.

Strut force calculation. The performance program was originally programmed to calculate strut force based on a theoretical calculation, assuming uniform flow ahead of the strut. This force should be a drag term since, theoretically, pressures downstream of the maximum strut blockage should be lower than upstream. However, test data indicate that this is only true with subsonic combustion. Upon examination of the test data, it appeared that measured static pressures between struts on both the inner and outer walls (there were no measurements along the strut surfaces) could be used to represent the forces occurring on the strut surface. Thus, a pressure integral was used to determine the strut force and a calculation was also made for strut base pressure as discussed in reference 9.

Performance correction for regeneratively cooled system. The AIM incorporated a water-cooled jacket in which heat was rejected and not recovered. In order to compensate for this heat loss, hydrogen fuel was heated up to 1500°R to simulate a regeneratively cooled system. The deficiency of energy in the system in terms of theoretical energy release was less than 10 percent in all cases.

In order to correct this deficiency, the performance computer program (ref. 6) incorporated a side calculation in which the energy deficiency, because of the heat loss through internal surfaces, was added to the stream at the combustor exit with no total pressure change. The flow was then expanded to the nozzle exit with measured nozzle efficiency. The differences between the heat added to fuel and the internal cooling loss are presented for several tests in reference 9 as table 6.6-1.

Performance correction for inlet total temperature.— Because of the facility heater deterioration, the true temperature simulation of 3700° R at Mach 7 was not achieved (the test Mach number was generally about 7.25 requiring a simulation temperature of about 3960° R). It is known that the effect of decreasing total temperature is to increase the engine performance. Therefore, it is necessary to correct the measured performance for Mach 7 (ref. 11) to properly account for deviations in test conditions. Theoretical calculations indicate that, at Mach 7, a decrease of 560° R would increase the thrust coefficient by 5 percent and the specific impulse by 3.5 percent. The accomplishment of this correction in the performance computer program (ref. 6) employed the methods discussed in reference 9.

Determination of tunnel gas composition. The oxygen-to-nitrogen ratio was determined from the flow measurements of oxygen, diluent nitrogen, and nitrogen entering the storage heater, and checked by gas samples taken through two aspirating thermocouple probes $180^{\rm O}$ apart in the facility nozzle entrance prior to each run. The samples were collected in high-pressure bottles and later analyzed on a mass-spectrometer. The measured compositions for each run are presented in reference 9 as table 6.8-1. The one-dimensional performance computer program (ref. 6) used only the N2 and O2 values.

RESULTS

Selected points of interest of the HRE/AIM test data have been analyzed by use of the one-dimensional performance analysis computer program (ref. 6). The amount of material generated requires four volumes. Mach 6 engine performance results are presented herein. Mach 6 component integration results, Mach 7 component integration and engine performance results, and Mach 5 component integration and engine performance results are presented in references 10 to 12, respectively. All of these results were used in references 7 through 9 in the discussion of the results of the AIM test program.

Selected Test Points for Performance Analysis

Details of the AIM tests were discussed in reference 5 which included a list of all the HRE/AIM tests; this list is contained herein as table 1 (included in each volume). The individual AIM tests were recorded as consecutive reading numbers that extended through number 97 for a total operation time of 112 minutes with 41.5 minutes of combustor operations. About 60 successful tests are noted in the first column of table 2.

Reference 5 documented the fuel injection schedules, both planned and measured, for the successful tests. The measured fuel injection schedules for the successful Mach 6 engine performance tests are contained herein for convenience in figure 4. Such plots were reviewed and points (run time) of interest were selected for performance analysis. The selected points were listed in reference 9 and are included in table 5(a) for the results presented in reference 10, table 5(b) for the results presented herein, and tables 5(c) and 5(d) for the results presented in references 11 and 12, respectively, where the times correspond to the abscissa in figure 4. The first column of table 5 indicates the page number of the initial page of the data for a given test point (specific time of a reading number). Table 5 indicates the general test conditions and fuel injection equivalence ratios, ϕ , for the first-, second-, and third stage injectors and the accumulative ϕ -value. Also, the use of ignitors is indicated and the general purpose of the test is noted.

Vagaries in the test program that should be noted (table 5, last column) are:

- (1) Fuel equivalence ratio values, ϕ , in table 5 for reading 93 are lower than the values indicated by the fuel injection schedule (fig. 4(a) of ref. 12). In preparation for the performance analysis, the tunnel measured oxygen content was found to be about 34 percent instead of the standard 21 percent; therefore, the fuel equivalence ratios were corrected to account for the difference in the available oxygen for combustion.
- (2) Time 235 seconds in reading 90 is for an inlet unstart condition. With an unstart, the captured mass flow is, of course, greatly decreased, and since the fuel flow rate is still high, the ϕ -value would be high as indicated, therefore this time is not very meaningful.
- (3) At Mach 7 the agreement between computed thrust (a function of \$\int pda\$) and measured thrust was not nearly as favorable as experienced for Mach 6. Examination of the surface static pressure distributions on the outer combustor surface in the vicinity of the pressure rise indicated some pressure instrumentation to be faulty. For reading 89, more reasonable values were substituted for the measured pressures and the performance recomputed. The recomputation was performed for two different times, 316.47 and 327.27 seconds (see table 5(c)), and the results indicate a much more favorable agreement between the computed and measured thrust. The channel numbers in which new pressure values were substituted are noted on the first page of the results for these two times. A more detailed discussion of this exercise is contained in reference 9 (section 7.7.2 Mach 7 Performance).

- (4) Times 264.04, 274.84, and 275.74 seconds of reading 96 had a fuel flow measurement malfunction that indicated no fuel flow from injector 1B. Injector 1B manifold pressure, however, indicated flow to exist at pressure levels about equal to planned pressure levels (ϕ -values about the same as for injector 1A). The performance calculations for these times of reading 96 erroneously used only fuel flow from injector 1A.
- (5) At time 313.54 seconds, also of reading 96, the test chamber pressure was noted to be high, thus yielding unrealistically high pressures on the AIM nozzle shroud and plug that would, of course, contribute erroneously to increased engine thrust.

Description of Performance Computer Results

The selected points listed in table 5 were analyzed using the performance computer program described in reference 6. As noted in the Method of Computation section, the AIM test data were reduced to engineering units and reviewed for erroneous data. Such data were "coded out" in the performance computer program. Table 6 indicates the channels that were coded out. The COXX indicates the code outs for a reading number, e.g., for reading 33, CO33 is indicated. Channels that are coded out are listed adjacent to the notation KODSEL, e.g., for reading 33 the first and last of 85 coded out channels are 60 and 399, respectively. The locations and type of measurement for the listed channels may be determined by referring to table 4.

Several points (run time) of interest were selected for each run as indicated in table 5. The page numbers indicated in the first column of table 5 are output listings of the performance computer program (ref. 6). For each time of interest there are seven or eight pages of computer output_listings. On each of these pages a standard heading exists: READING number (test number); BLOCK number (numbered sequentially and corresponding to recording times of test data); TIME (of data recording, seconds); MACH number (in wind tunnel); PT (total pressure in wind tunnel, psia); TT (total temperature in wind tunnel, OR); and PAGE number.

Station flow parameters.- A summary of flow parameters at each calculation station in the AIM is contained on pages 1, 2, and 3. Each station is headed by a station designator (i.e., WIND TUNNEL, INLET THROAT, COMBUSTOR, etc.), followed by three integers (the zero following the combustor designator is meaningless). The first integer denotes the station number, the second denotes the combustor station, and the third denotes the number of interations required to converge on a solution. The third integer may assume values between 0-21, 100-121, and 200-221. A value of the third integer equal to 21 denotes that the mass flow was too great or the flow area too small to obtain a solution, 121 denotes that the solution for total conditions did not converge in 21 interations and 200-221 denotes that the mass flow was too small or the flow area too large to obtain a solution. When both solutions for static and total conditions have converged, the third integer may assume the values 1-20 or 101-120 depending upon which solution (static or total) required the larger number of interations. Columns 2-8 have two rows of values for each station; total and static conditions in first and second rows, respectively.

Most of the station designators are self-explanatory. The first appearance of the designators WIND TUNNEL and SPIKE TIP NS (NS = NORMAL SHOCK) reports conditions in wind tunnel and upstream of the spike tip based on a wind tunnel Mach number determined from calibration runs. The second appearance of these designators reports these conditions based on a wind-tunnel Mach number calculated from the total and pitot pressures and the total temperature of the synthetic air applied to the normal shock equations. The designators INLET UPNRSK and INLET DNNRSK denote conditions upstream and downstream of a normal shock positioned at a fictitious flow area 1.10 times the flow area at the inlet throat. The designator COMBUSTOR REGEN denotes, for cases with fuel flow, conditions at the combustor throat simulating a regeneratively cooled ramjet. In some cases (e.g., reading 94 time 150.342 sec) the designator SONIC THROAT appears ahead of the COMBUSTOR REGEN. This denotes the results discussed in section entitled "Description of Performance Program Methods." NOZZLE AE and NOZZLE PO report conditions when the flow is expanded isentropically to the nozzle exit area and to the wind-tunnel static pressure, respectively. NOZZLE AE REGEN and NOZZLE PO REGEN denote, for cases with fuel flow, conditions at the nozzle exit simulating a regeneratively cooled ramjet. FICTIVE COMBUSTOR denotes stagnation combustion conditions (zero velocity and constant pressure) with combustor efficiency equal to unity. FICTIVE NOZZLE reports conditions required to match the actual momentum and nozzle exit area.

Definition and units of parameters in the SUMMARY REPORT, pages 1-3 in the computer listings, are listed below:

P - pressure, psia
T - temperature, OR
H - enthalpy*, Btu/lb
GAMMA - specific heat ratio
MOLWT - molecular weight
SONV - conic velocity, ft/sec
MACH - Mach number
VEL - flow velocity, ft/sec
S - entropy, Btu/lb_m-OR

W/A - flow rate per unit area, lb_m/sq in W - flow rate, lb_m/sec A/AC - mass flow ratio MØMTM - flow momentum, lb_f Q - dynamic pressure, lb_f/sq in IVAC - vacuum specific impulse, lb_f-sec/lb_m PHI - equivalence ratio (see discussion in Ramjet Performance section) ETAC - combustor efficiency

$$\sum_{i} \int_{0}^{T} C_{p,i} dT \quad \sigma_{i}(T) = \sum_{i} H_{f,i}^{298} + \int_{298}^{T} C_{p,i} dT \quad \sigma_{i}(T)$$

$$- \sum_{i} H_{f,i}^{298} + \int_{298}^{300} C_{p,i} dT \quad \sigma_{i}(T) + \sum_{i} \int_{0}^{300} C_{p,i} dT \quad \sigma_{i}(T)$$

where: $C_{p,j}$ is specific heat at constant pressure, Btu/lb_m - OR, and $\sigma_i(T)$ is the mass fraction of the specie i as a function of temperature and H_f is fuel enthalpy.

^{*}Two values were reported. The first value (column 4) was the JANNAF-based enthalpy. The value in parentheses (column 5) was the enthalpy potential or the sensible enthalpy based on the equation

Cooling and surface-pressure parameters. - Surface pressures, cumulative surface-pressure integrals, cumulative cooling losses, cumulative surface area, and pressure ratios for axial distances from the AIM virtual spike tip are listed on pages 4 and 5.

Definitions and units of the parameters are as follows:

```
XABS - axial distance from virtual spike tip, in P-IB - surface pressure on innerbody, psia P-ØB - pressure on cowl inner surface, psia PDA - cumulative surface-pressure integral, \int_{0}^{\chi} \text{ABS}_{PdA}, \text{lbf} \text{Df} \text{ODA} \text{ODA} \text{Coling loss}, \text{Btu/sec} \text{Q-IB} - cumulative cooling loss from innerbody, \text{Btu/sec} \text{Q-ØB} - cumulative cooling loss from outerbody, \text{Btu/sec} \text{CAWALL} - cumulative surface area, sq in P-IB/PSØ - innerbody static to wind-tunnel static-pressure ratio POB/PSØ - outerbody surface static to wind-tunnel static-pressure ratio POB/PSØ - outerbody surface static to wind-tunnel static-pressure ratio POB/PTØ - outerbody surface static to wind-tunnel total-pressure ratio
```

<u>Drag and heat-transfer coefficients</u>.- Longitudinal values of drag force and drag and heat-transfer coefficients are listed on page 6 (for some cases on page 6 and 7). Definition and units of the parameters are as follows:

```
X - axial distance from spike virtual tip, in DDRAG - incremental frictional drag force, lf_f CDRAG - cumulative frictional drag force, lf_f Cp - friction-drag coefficient HC - heat-transfer coefficient, f_f Btu/(sec-sq ft-OR)
```

Ramjet performance.— AIM performance parameters and pertinent information are contained on page 7 (page 8 for some cases). The performance parameters are generally self-explanatory; detailed discussion about the methods of computation are presented in references 6 and 9. Parameters listed below STATIONS are presented since they are related (except for the inlet throat) to the cowl leading-edge station. The NOMINAL COWL LEADING EDGE refers to the χ_{CL} (table 3) value for the Mach 6 design operating position. SPIKE TRANSLATION is the recorded distance between the nominal and the actual χ_{CL} value (this distance is designated as $\Delta\Delta x$ in symbols and used in figure 3(a)); all dimensions other than those for the inlet spike are corrected by this amount.

The fuel injectors and their corrected stations in inches are shown. A letter in the VALVE column indicates the injectors that were in use during the respective time. Table 5 indicates the general fuel equivalence ratio values for the various injector stages. The actual fuel equivalence ratio, however, for each injector can be determined by noting the step increases in the PHI column on the output, pages 1-3, for the respective time (ignore 0.01 or 0.02 changes); the step difference at the combustor station corresponding to the indicated injector station is the ϕ -value for the respective injector.

SUMMARY OF TESTS

The Hypersonic Research Engine/Aerothermodynamic Integration Model was tested in the NASA Hypersonic Tunnel Facility at the Plum Brook Station of the NASA Lewis Research Center. Synthetic air (heated nitrogen with proper amount of oxygen added) was delivered by the facility at nominal Mach numbers of 5, 6, and 7. The Mach 5 and 6 tests were conducted at true air temperature while Mach 7 tests were conducted at Mach 6 temperature (3000° R) because of heater deficiency. Changes in total temperature and instream oxygen content at Mach 5 and 7 were also explored. The hydrogen fuel was heated up to 1500° R prior to injection to simulate a regeneratively cooled system.

The engine testing was completed with an accumulated actual running time of about 112 minutes with 41.5 minutes of combustor operation. The important achievements realized from this test program which advanced the state-of-the-art in hypersonic propulsion were discussed in detail in reference 9 and are:

1. Realistic engine performance levels for hypersonic flight were obtained from Mach 5 to 7.

Test Mach <u>No.</u>	Equivalence Ratio	Internal Thrust Coefficient	Internal Specific Impulse
5.1	1.0	0.910	2740
6.0	1.0	0.735	2360
7.25	1.0	0.570	2170

- 2. Engine inlet performance agreed well with theoretical prediction. Combustor efficiency of 95 percent was achieved. Nozzle vacuum thrust coefficient was lower than predicted.
- 3. The interaction effects in staged fuel injection were very important in achieving auto-ignition, high combustor efficiency, and overall performance. High supersonic combustor efficiency in a diverging duct was difficult to achieve. The strong stage interaction effects discovered during these tests may be used to great advantage in future designs.
- 4. The "transonic combustion" or "mixed combustion mode" was the most efficient heat addition process in the range of Mach numbers and temperatures tested in this program.
- 5. The effects of ignitors, altitudes, spike translation, fuel schedules, angle of attack, step and struts, inlet gas composition, inlet total temperature, and component interactions were investigated and correlated.

- 6. Stable subsonic and supersonic combustion and convertibility over a range of fuel equivalence ratios at Mach 5 and 6 was demonstrated.
- 7. The overall cooling load and its distribution as compared with theoretical prediction was determined.
- 8. Experience was acquired in free jet testing in a ground test facility with large model blockage and combustion.

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Table 1. - Summary of planned HRE/AIM wind tunnel tests.

(obtained from ref. 9 and 15)

RUN	но	PTO, PSIA	ŢŢŌ, °R	'n	FUEL Systems	FUEL SCHED,	INLET	COMBUSTION MODE	RUN TYPE AND PURPOSE
,	6	466	1500	0	-	-	4 23	-	Purge force, nominal case
2	6	466	1500	0	_	-	1 90	-	Purge force, effect of spike position
3	6	466	1500	3	-	-	4 23	-	Purge force, effect of angle of attack
4	6	466	2000	0	-	-	4 23	-	Operation checkout, effect of higher TTO
5	6	466	3000	0	-	-	0, 1 71, 2.52 4 23, aft stop	-	Airflow calibration, effect of altitude
6	6	930	2946	0	-	-	0, 1 71, 2.52 4.23, aft stop	-	Airflow calibration, nominal case
'	6	930	2946	3	-	-	0, 171, 2 52 4 23, aft stop	-	Airflow calibration, effect of angle of attack
8	6	930 930	2946	٩	la, ib	' '	4 23	Supersonic	Inlet-combustor performance, ignition and inlet unstart limits
10	٥	930	2946	0	la, lb, 2a, 2c	2	4 23	Supersonic	Inlet-combustor performance, injector optimization
11	6	930	2946 °	0	1c, 4, 2a, 2c	2	4 23	Supersonic	Inlet-combustor performance, injector optimization
12		930	2946	٥	ia, ib, ic, 4 TBO	3	4 23	Supersonic	Inlet-combustor performance, injector optimization
13	6	466	3000	0	ia, ib, 2a, 2c	TBD 2	4.23 4.23	Supersonic	Inlet-combustor performance, injector optimization
14	6	700	3000	0		2	4 23	Supersonic	Injet-combustor performance, effect of altitude
15	6	930	2946	0	la, lb, 2a, 2c la, lb, 2a, 2c	2	Aft stop	Supersonic Supersonic	Inlat-combustor performance affact of altitude
16	6	930	2946	o	la, 16, 2a, 2c	2	2 52		Inlet-combustor performance, effect of spike position
17	٠	930	2946	0	la, lb, 2a, 2c	2	171	Supersonic Supersonic	Inlet-combustor performance, effect of spike position Inlet-combustor performance effect of spike position
18	١	930	2946	o	3a, 3b	4	4 23	Subsonic	Inlet-combustor performance, subsonic combustion
19	6	930	2946	0	3a, 3b	5	4 23	Subsonic & transition	Engine performance, subsonic combustion and transition
20	6	930	2946	0	la, Ib, 2a, 2c	2	4 23	Supersonic	Engine performance, nomina) case
21	6	466	2946	0	la, lb, 2a, 2c	2	4.23	Supersonic	Engine performance effect of altitude
22	6	930	2946	3	îa, Ib, 2a, 2c	2	4.23	Supersonic	Engine performance, effect of angle of attack
23	7	520	1500	o	-	- (2 88		Purge force
24	7	520	3965	0	-	-	2 34, 2 88 3.24		Airflow calibration, effect of altitude
25	7	1000	3840	0	-	-	1 78, 2,88 3 24	-	Airflow calibration, nominal case
26	7	1000 520 &	3840	3	-	-	2 34, 2 88 3 24	•	Airflow calibration, effect of angle of attack
-]	1000	3965 3840	0	la, ib	6	2.88	Supersonic	Inlet-combustor performance, Egnition and inlet unstart limits
28	7	1000	3840	٥	ia, lb, 2a, 2d	7	2 88	Supersonic	Inlet-combustor performance injector optimization
30	7	1000	3840 3840	0	lc, 4, 2a, 2c	8	2 88	Supersonic	Injet-combustor performance, injector optimization
31	,	1000	3840	0	la, lb, lc, 4 TBD	TED	2.88	Supersonic Supersonic	Inlat-combustor performance, injector optimization
32	7	522	3965	0	la, 15, 28, 2c	7	2 88		Inlet-combustor performance injector Optimization
33	,	700	3965	٥	la, 16, 28, 20	,	2 88	Supersonic	Inlat-combustor performance, effect of altitude
34	7	1000	3840	0	la, lb, 2m, 2c	7	3 24	Supersonic	Inlet-combustor performance, effect of altitude , Inlet-combustor performance, affect of spike position
35	,	1000	3840	o	la, Ib, 2a, 2c	7	2 34	Supersonic	Inlet-combustor performance, effect of spike position
36	,	1000	3840	ŏ	ia, ib, 2a, 2c	7	1 98	Supersonic	Inlet-combustor performance, effect of spike position
37	,	1000		ŏ	la, ib, 2a, 2c	·	2 88	Supersonic	Engine performance, nominal case
38	7	522	3965	0	la, 1b, 2a, 2c	,	2 68	Supersonic	
39	7	1000	3840	3	la, lb, 2a, 2c	7	2 88	Supersonic	Engine performance, effect of angle of attack
40	5	445	1500	1	la, 16, 2a, 2c	- 1	4 23	•	Purge force
41	5	206	2210	0	la, lb, 2a, 2c	J	4 23	-	Airflow calibration
42	5	41.5	2210	٥	la, lb, 2a, 2c	9	4 23	Supersonic	Inlet-combustor performance, nominal case effect of altitude
43	5	415	2210	0	la, 16, 2a, 2c	TBD	4 23	Supersonic	Inlet-combustor performance, and ignitor flow rate
44	5	415	2210	٥	la, lb, 2a, 2c	9	4 23	Supersonic	Engine performance, supersonic combustion
45	5	415	2210	٥	3a, 3b	10	4.23	Subsenic	Engine performance, subsonic combustion
46	5	415	2210	3	ia, Ib, 2a, 2c	11	4 23	Subsonic & Supersonic	Engine performance, effect of angle of attack

			1	inlet Condi	ilon	inlet		*	<u> </u>	T in	ie.			
Run	Reading		Hach		- 0.	Spike Position,	Fuel Injectors	Tunnel	- Au			ful		
Χο	Ho	Date	No	P _{TO} , Psia	T ₁₀ , °A	Δx , in.	Used	Config	Hin	Sec	Hin	Sec	Objective of Test	Comments
1	I through 5	9/14/72	-	-	•	•	-	A	-	-	-	-	Pro-run reference No-airflow engine Purge system calibration	Data not valid due to mechanical Interference between AIN and outer cowl body
2	6	10/31/72	6	466	1500/2100	4.266	.	۸	-	3	-	-	Facility and engine checkout	Test terminated due to cooling system overpressure abort system failure
3	7	11/1	6	466	1500	4 266	•	4	2	26	-	-	Same as run 2	Tunnel nozzie started iniet started Strong shocks in test section Cell pressure ≈ 2 0 psis
4	8	11/2	6	466	1500	4 266	-	A	٠	5	-	1	Establish facility operational procedure	Test aborted due to facility problem (TAFP)
5	9	11/16	6	466	1500	4 266	•	81	-	-	-	•	Same as run 4	Facility shroud extended and washer added to assist tunnel start (TAFP)
	10	11/16	6	466	1500	4 266				-	-	-	Samo as run 4	TAFP
	11	11/16	6	466	1500	4 266	-		2	39	-	99	Same as run 4	Mozzle start and inlet start obtained Call pressure — 1 2 paia Wadge nozzle pressure changed from 50 to 60 psia Ho Improvement in call pressure
6	12	11/21	6	466	2250	3 962	-	81		-	-	-	Same as run 4	TAFP
	13	11/21	6	466	2250	3 962	-		1	07	-	-	Same as run 4	Wedge nozzie pressure 55 to 90 psig. No tunnel nozzie start Nozzie started when inlet closed for shutdown
7	14	11/21	6	466	2950	3 962	•	81	•	34	-		Same as run 4	TAFP
8	15	12/8/72	6	466	2950	4 266	•		_	16	-	<u> </u>	Same as run 4	TAFP
9	16	1/18/73	6	466	2800	4 266	10, 4	81	-	35	<u> </u>	<u> </u>	Same as run 4	First combustion attempt TAFP
			Э	-	**		1C, 4		1	06	<u> </u>	<u> </u>	Same as run 4	Nozzle start not obtained TAFP
	18	,	,	,	,	•	1C, 4		1	00	-	-	Same as run 4	Nozzie start obtained by cycling inlet spike open and closed inlet start obtained Fuel ramped to equivalence ratio = .25 prior to tunnel unstart and TAFP
10	19	2/2	6	466	2950	0 99/ 4 00	-	81	•	13	•	-	Same as run 4	Nozzle start with inlet partially open (å x = 0 99) TAFP. Ho fuel injected
11	20	2/2	6	466	2950	0 99/ 4 00	1C, 4	81		02	·		Same as run 4	No start at AX = 0.99 Nozzle started by cycling inlet spike Combustor lit causing tunnel unstart
12	21	2/15/73	6	750	3000	0 99/ 4 00	-	Ç1		•	·	-	Establish facility operational procedure	Jet pump installed Test aborted due to freezing of coolant supply system
13	22	2/21	6	750	3000	0 99/ 4 90	-	C1	•	22	_	-	Same as run 12 above	Jet pump used for this test Nazzle start obtained Unstart experienced when inlet was opened Test aborted manually, Nozzle restart noted during shutdown
14	23	2/21	6	750	3000	0 99/ 4.00	•	CI	-	58	•	-	Same as run 12 above	Jet pump and wedge nozzie inlet pressure variad Nozzie start was not obtained Use of jet pump did not affect test chamber pressure Seals between AIN support struts and facility shrout blown out
15	24	2/23	6	750	3000	0 99/ 4 00	-	CZ	-	•	-	-	Same as run 12 above	Jet pump inactivated TAFP
	25	2/23	6	750	3000	0 99/ 4 00	•	CZ	•	•	-	•	Same as run 12 above	TAFP
	26	2/23	6	750	3000	0 99/ 4 00	1A 18	C2	•	49	-	-	Same as run 12 above	Nozzle start and engine start obtained Fuel Injected for 4 seconds prior to nozzle unstart Unstart attributed to excessive fuel injected caused by facility valve malfunction
16	27	3/1	6	930	3100	0 99/ 4 00	<u>-</u>	C2	1	42	•	•	Some as run 12 above	Nozzle start and inlet start obtained. Jet pump inactivated Fuel was injected engine inlet unstart experienced 12 seconds later. Inlet start reestablished and fuel again injected inlet unstart experienced 9 seconds later. Test was manually aborted. Cowl leading edge assembly separated from the outer body. Cause of the separation was attributed to failure of the screw heads. The failure was caused by overheating of the screw heads resulting from ingesting the hot tunnel environmen into this area. Ingestion of tunnel ambient was the result of a shock standing on the AIH cowl. Additional diagnostic instrumentation was installed in the facility shroud and diffuser.
17	28	3/16	6	930	3100	0 99/ 4 00	1A 18	B2	1	11	-	-	Establish facility operational procedure to obtain hypersonic airflow	Tunnel configuration same as config B except washer inside diameter changed to 44 5 inches Tunnel unstart observed 19 seconds after fuel introduced Start reastablished Test manually aborted 3 seconds later when excessive heating of HEC-All cowl leading edge assembly mount flange was noted Excessive heating of the external skin of the AlM was noted

^{*} see figure 5-9, reference 5

Table 2. - Continued.

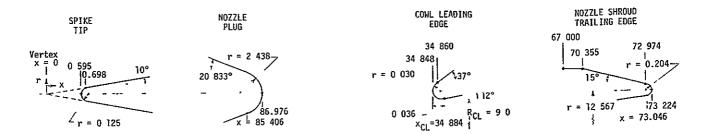
						Inlet		Ι		Tin	ne -			
- 1				let Condition		Spike	fuel Injector	Tunnel	Ru	n	Use	ful]	
Run No	Reading No	Date	Hach No.	P _{TO} , Psia	TTO, OR	Δx,in.	Used	Config	Hin	Sec	Hin	Sec	Objective of Test	Comments
18	29	3/22	6	930	3100	0 99/ 4 00	1A, 18	Č1	-	36		Ŀ	Same as run 17 above	Re-run of reading 23 with seal repaired
19	30	4/27	6	750	2000	0, 99/ 4 00	Fuel Injec not planned	٥	1	16	2	-	Same as run 17 above	Shroud inlet washer replaced with cone-cylinder and 15° conical diffuser inlet contraction replaced with 7° cone, tunnel nozzle did not start
20	31	4/30	6	750	2000	0 99/ 4 00	Fuel Injec not planned	E	-	51	•	-	Establish operational procedure	First run with fully started tunnel Shroud inlet cone cylinder replaced with priginal 46 in diameter washer Tunnel start obtained when inlet spike was cycled twice, supersunic flow in diffuser Test terminated when target conditions achieved due to limited supply of nitrogen Test call pressure was 1 2 psia
21	32	4/30	6	750	2000	0 99/ 4 00	Fuel injec not plenned	Ē	,	42	-	-	Determine effect of varying wedge nozzle flow	Tunnel config identical to run 20 Tunnel start obtained when inlet spike cycled twice Test cell pressure of 1 0 psia obtained Wedge nozzie has negligible effect on cell pressure
22	33	5/4	6	750		0 99/ 4 00	18, 25	E	1	2.5	-	-	Investigate inlet unstart limit with first stage combustion	First successful supersonic combustion run intentional inlet unstart when first stage equivalence ratio reached 0 3% No second stage fuel added 0-ring between the outerbody and the cowl leading edge extruded
23	34	5/15/73	6	750/ 930	3000	0 99/ 4 00	1A,18,2A, 3A	E	2	08	•	-	Checkout AlM and facility. Fuel rich at P _{TO} = 750 psia gm 1 0 at P _{TO} = 930 psia	Tunnel start and inlet start obtained \$\phi\$ of 135 set at \$P_0 = 150 ps ia and \$\phi\$ of 100 set at \$P_0 = 930 ps ia Facility fuel control value for injector it oscillated kun proved Ain and tunnel can operate at \$\phi\$ > 10 Erosion of ≥1cconium oxide coating on outer coub body crossover manifold noted Erosion caused by carbon dust in tunnel flow
24	35	5/16/73	6	750	3000	0 59/ 4 00	FA 1B 2A, 2C	E	•	25	-	-	Sheckout AiM and facility Design in- jector locations	Test was aborted when engine inlet unstart was observed three seconds after initiation of fuel injection. The engine unstart was result of injecting excessive fuel, caused by malfunction of facility control valve. Inspection of the unit revealed that the coulant leak on the spike assembly had progressed, and repair was necessary.
25	36	5/24	6	750	3000	0 99/ 4 00	1A 1B 2A 20	€	2	19	1	38	Demonstrate operation with design injector location and determine auto ignition limit	First good run with design injector locations. Auto ignition obtained at $\phi = 0.55$, first stage did not light unt ' second stage fuel added. Overall ϕ remped to 1.0 with first stage ϕ held at 0.24
26	37	5/30/73	6	750	3000	0 99/ 4 00	-	E	-	•	-	-	Determine effect of First stage & on com- bustor performance	Test aborted due to maifunction of the steam ejector system
	38	5/30	6	750	3000	0 99/ 4 00	1A, IB 2A, 20	E	-	47	-	26	Determine offect of first stage ¢ on com- bustor performance	Tast abarted when inlet unstarted Malfunction of the facility fuel control value resulted in injecting accessive fuel into injector ZC 3 shell cracks in spike skin an region of ignitura found in post run inspection Cracks repaired to prevent water loak into combustor
	39 thru 48	-	-	-	-	-	•	£	<u> </u>	-	-	-	Purge system calibration test	
27	49	10/4/73	6	750	3000		-	E	-	•	*	-	Combustor optimization	TAFP
	50	10/5/73	6	750	3000	-	-	€	2	39	2	09	Combustor optimization Combustor optimization	Fuel control problems encountered
	51	10/5/73	6	750	3000	0 99/ 4 00	1A, 1B 2A 2	ļ	ļ	1	<u> </u>	ļ.		Investigating performance improvement due to injecting fuel close
28	52	10/10/73	6	750	3000	0.99/ 4 00	1A, 18, 2C, 4	E	1	21		50	Combustor optimization	to inlet inlet unstarted at overall ϕ of 83
	53	10/10	-	-	-	•	-	E	-	-	-	-	Purge system callbration test Evacuated test call	
29	54	10/11/73	6	750	3000	0 99/ 4 00	1A, 13, 2A, 2	G E	3	04	2	13	Combustor optimization	Attempt to determine effect of first stage ¢ and thrust on performance. Auto ignition obtained at ¢ = ,54 Data taken with ignitors on and off to determine effect on performance inspection of unit revealed excessive coolant leak at spike/ignitor body interface. Repair necessary. Tunnel operating procedure modified to reduce water ingestion into AIH well pressure taps.
Ì	55	10/17/74	-	-	-	-	-	ε	-	T-	-	-	Furge system calibration evacuated test cell	·
30	56	11/2/73	6	750	3000	-	-	Ē	-	-	-	-	Combustor optimization	Effect of fuel split between 1st and second stage injectors at overall $\phi=1$ 0 investigated. Also all second stage fuel added from innerbody side (system 2C). Fuel system purges turned off to determine effect on combustor wall pressure distribution found thrust measurement affected by thermal expansion of fuel manifold 18. Inlet unstarted at overall ϕ of 10 with first stage $\phi=0.36$ Cavity pressure tap PA2 repaired for this run Encountered fuel control problems

	•		Ţ,	viet Conditio		Inlet				Υi	me.			
Run	Reading		Hach			Spike Position.	Fuel Injectors	Tunnet	, P	un	Us	eful	1	
No.	No.	Date	No	P _{TO} , Psia	T _{TO} , [©] R	Δx , in.	Used	Config.	Ain	Sec	Hin	Sec	Objective of Test	Comments
	57	11/2/73	6	750	3000	0 99/ 4,00	1A, 18, 2A 2C	E	-	-	-	-		
	58	11/7/74	-	-	-	-	-	ε	`-	-	 -	-	Purge system callbration	Detarmine offect of thermal expansion of fuel manifold 18.
31	59	11/8/73	6	750	3000	-	-		-	-	-	-	Combustor optimization	TAFP
	60	11/8/73	6	750	3000	0,99/ 4 00	1A, 16, 2A, 2C	E	2	34	2	04	Combustor optimization	Overall 6 held constant while amount of fuel from innerbody and outerbody injectors varied Fuel temperature com- pensation added to fuel control
32	61	11/13/73	6	750	3000	0,99/ 1 72/ 2 52	1A, 1B, 2A, 2C	E	2	50	2	21	Datermine offact of spike position on engine performance	Injet massflow ratios of 0.81 and 0.58 ran by varying the injet spike position. AlM wall pressure distribution measured with fuelding purge flow shut off. Reworked section of the innerton assembly burned and damaged during combustion, damaged section (was removed Operational procedure modified to prevent further damage.
33	62	11/20/73	6	930/ 466	3000			E					Performance test	TAFP
	63	11/21/73	6	930/ 466	3000	0 99/ 4 00	1A, IB, 2A, 2C		2	59	1	52	Performence test	Tunnel total pressure varied to determine effect of altitude on performance
34	64	11/28/73	6	750	3000	0 99/ 4 00	18,2A,2C, 3A,30	ε	3	38	2	35	Subsonic-supersonic combustor mode transition	Transition from subsonic to supersonic combustion mode domonstrated inspection of unit revealed coolant was flowing into the 18 fuel manifold and a nickel plated section of the innerbody had bilistered. Separation at the spike skirt-spike body has progressed to approximately 10 inches Forward facing step at the interface of the cowl leading edge assembly and the outerbody had prograssed to approximately 065 Inches Larger fuel matering venturi installed in fuel system E
35	65	12/11/73	6	750	3000	4 00	1A, 18, 2A, 2C	E	2	52	1	44	Supersonic combustion with instrumentation rig	Instrumentation rake installed Rake caused tunnel to unstart at g = 1 05 Exhaust gas sampling data taken
	66	12/14	-	-		-		€	•	•	-	-	Purge system calibration	TAFP
	67	12/14	-		-	-	-		-	-	-	-	Purge system callbration	No purge force calibration with cell evacuated
36	68	12/14/73	6	750	3000	-	•		•	-	-	•		Time of steady state fuel flow increased to 20 seconds to allow one sampling data to stabilize
:	69	12/14/73	6	750	3000	4 00	1A, 18, 2A, 2C	E	3	20	2	17	Supersonic combustion	One tunnel unstart experienced mear and of run. Several tunnel unstarts prevented by shutting off fuel incipient unstart detacted by monitoring luminescent normal shock position in T Y view of tunnel.
37	70	12/19/73	6	750	3000		•	E	•	•	-	-	Determine effects of angle of attack	Test terminated prematurely due to frozen vent valve
	71	12/19/73	6	750	3000	4 00	1A, 18, 2A, 2C		J	56	2	29		Cowl leading edge assembly removed after this run to remove facing step noted after reading 64
	72												Purge system calibration	Calibration with 1B fuel injector manifold heated test cell evacuated.
47	73.74.75	1/22/74	7	1000	3200	-	-	F	-	-	-	•	Mach 7 facility check- out	Test aborted due to facility problems (TAFP)
	76	1/23/74	7	1000	3200	-	-	F		-	-1	$\overline{}$	Hach 7 facility check- out	TAFP
	77	1/23/74	7	1000	3200	2 57	-	F	2	-	-	-	Mach 7 facility check- out	Actempt to start tunnel at Hach 7 unsuccessful Secondary steem eyector used wedge nozzle pressure varied, inlet spike essembly translated
48	78	1/25/74	7	1000	3500	2 57	•	G	2	-	-	-	Hach 7 facility check- out	Test aborted while attempting tunnel start TAFP Unusual amount of carbon dust deposited on AlM
49	79	2/15/74	7	1000	3100	-	-	G1		-	-	-	Facility check-out	Alk moved aft 5 5 inches
- 1	80	2/15/74	7	1000	3100	2 57	-	61		-	-		Facility check-out	TAFP (dewar water system frozen),
	81	2/20/74	7	1000	3300	2 57	2A, 2C	G2	2	38	-	-	Facility check-out	Blowout doors installed in tunnel closure. Tunnel started when wedge nottle pressure reduced. Tunnel unstarted when combustor lit. Restart not obtained due to change in wedge nozzle inlet pressure.
50	82	2/22/74	7	1000	3300	-	-	G2					Facility check-out	TAFP Seal around outer cowl body support damaged
	83	2/22/74	7	1000	3300	2 57	•	G2	2	05	Ξ	\equiv	Facility check-out	Tunnel start not obtained
51	84,85,86 87	2/28/74	7	1000	3300	-		62		\equiv	Ξ	\equiv	Facility check-out	TAFP
		2/28/74	17	1000	3300	2 57	1A, 1B, 2A		-2	46	\neg	30	Facility check-out	Tunnel nozzle started. Unstarted at φ ≈ 0 8

Table 2. - Concluded.

Γ	·		1			Inlet		ı —		— <u> </u>				
				et Condition		Spike Position,	Fuel Injectors	7		lun	_	ful	1	_
Run No	Reading No	Date	No No	P _{TO} , Psia	τ _{το} , ^ο ε	Δx , in.	Used	Config.	Hin	Sec	Kin	Sec	Objective of Test	Comments
52	88	2/28	7	1000	3100	2 57	1A, 18, 2A, 2C	F	2	45	1	31	Combustion evaluation	First successful Mach 7 run Tunnel closure removed Diffuser seal repaired Effect of fuel injection location investigated Row 2 ignitors on, Outer cowl body support damaged by carbon particles in tunnel flow due to failure of carbon part in facility heater Shroud inlet pressure rake hit and damaged Repaired outer cowl body support and water cooled protective wedge installed Coolent leak at the interface of spike skirt and spike body noted at angular location 270° in addition to leak at 180 dogrees noted in Rdg 64 Leak at 180° progressed to approximately 125 inches Cowl leading edge tip radius and spike tip damaged by particles Damaged areas reworked
53	89	3/15/74	7	1000	3000	2 57	1A, 18, 2A, 2C, 4	F	3	•	2	02	Combustor optimization	Performance measured with various fuel injection schemes T _{TO} varied during run lightors on Test terminated prematurely due to failure of transducer in fuel control causing fuel control valve to fully open Abhormal amount of carbon dust observed in tunnel flow. Cowi leading edge tip radius and spike tip again damaged. Tip section repaired
54	90	3/8/75	7	1000	3000	2.57	1A, 18, 1C, 4	F	3	09	1	16	Combustar aptimization	Second stage fuel injection closer to inlet (injectors IC, 4) inlet unstarts encountered
55	91	3/12/74	7	1000	3000	2,57	1A, 18,2C, 4	F	2	52	1	32	Effect of angle of attack	Tunnel start improved at angle of attack. Tunnel started at Pro = 850 psla. 3 Inlet unstarts encountered due to excessive 1st stage fuel. Total coolant leak into combustor estimated to be 5 0 gpm.
56	92	3/18/74	7	1000	2900	2 57	1A, 18, 2C, 4	F	3	50	2	30	Combustor performance with instrumentation rake installed.	instrumentation rake blockage had adverse effect on tunnel start, inlet spike stroked twice to start tunnel Oxygen content of tunnel flow varied while AIM exhaust gas sampling data taken
57	93	3/27/74	5	415	2210	4 0	1A, 18, 2A, 3A, 3B	F	0	85	•	-	Facility check-out	First Mach 5 run Subsonic combustion data obtained. Run terminated prematurely (TAFP)
58	94	3/28/74	5	(a) 415	2210	4 00	1A, 18 2A. 3A.38	F					Combustor optimization	Subsonic and supersonic combustion and transition demonstrated Four unstarts experienced, three unstarts attributed to high
				(b) 300	3000	4 00	IA, 18, 2A, 3A, 38		2	25	2	01		cell pressure one to injecting excessive fuel intentionally into the AIM Hore carbon in tunnel flow Cowl leading edge
			<u> </u>	(c) 206	2210	4.00	1A, 1B, 2A 3A 3B							and spike tip damaged Both reworked.
59	95	3/29/74	5	415	2210	4 00	1A, 18, 2A, 2C	F						All comments made for Rdg 94 applicable for this run, except combustion was limited to supersonic combustion made. Four
				300	3000	4 00	1A, 15, 2A,		3	41	3	20	Combustor optimization	engine unstarts experienced. Three unstarts were attributed to facility conditions and the other to programmed to determine
				206	2210	4 00	1A 18,2A, 2C							infot unstart limit
60	96	4/15	5	415	2210	4.00	1A, 18, 2A, 3A, 38	F					Evaluate effects of angle of attack	Subsonic and supersonic combustion and transition demonstrated at angle of attack intentional engine unstart obtained when
				300 206	3000 2210	4.00 4.00								excessive fuel was injected in supersonic combustion mode
61	97	4/22	5	206/ 415	2210	4.00	2A, 3A, 3B	F					Combustor performance with instrumentation rake installed	Combustor exit flow conditions surveyed Gas sampling data taken Blockage of instrumentation rake had adverse effect on tunnel operation

Table 3 - AIM aerodynamic coordinates (Mach 6 cowl position, $x_{CL} = 34844$ in)

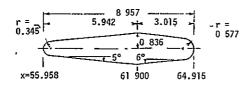


a) Centerbody

	-
x, 1n	r, in
0.595	0 0 90°
0 698	0 123) st line
18 360	3 237 / 10°
19 304	3 411
20 443	3 633
21.691	3 885
22.830	4.122
23 850	4.338 4.782
25 875	4 985
26 766 27 900	5 256
28 904	5 518
29 655	5 726.
30 360	5 726 } 15 819°
32,760	6 660
34 080	
37 710	7-140 8 607) 22 0°
38 070	8 734 i
38 538	B 874
38.826	8 942
39 132	9 000
39 780	9.096
40.500	9 180- 5 645° Throat
42 000	9 318
43.400	9 415
44 000	9 452
45.000	9 518
46 000	9 578
47 000	9 624
47 600	9 650
48.400	9.670
55 760	9 670 End of
55 760	,p,, ,
61.900	9 406 Thermal throat, 9 406
65 740	0 072
67 553 85 406	9.072 2.278) 20.833°
85 406 86.976	0.0 900
00.970	<u> </u>

c) Internal struts (6)

1



b) Outerbody

	b) outerbody
x, 1n	r, In
40 894 36 750 36 250 36 000 35 750 35 437 34 860	11 611 10 103 9 975 9.808 9 685 9 487 9 053 37°
34 848 34 884 35 397 35 874 36 171 36 414 36 765 37 494 40 500 40 894 41 894 42 894 43 894 44 894 45 760 57 000 58 700 61 900 66 220 66 740 67 740 68 740 67 740 68 740 67 740 68 740 67 72 260 72 260 72 980 72 980 73 224 72 974 70 355 67 000	9.029 90° 9 000 12° 9 104 9 192 10° 9.241 9 278 8° 9 322 9 398 9 695 5 645° 9 720 9 810 9 890 9 960 10.132 10.873 10 955 11 000 11 022 11 022 - Thermal 11 022 throat 11 042 11.132 11 348 11 572 11 773 11 989 12 146 12 249 12 349 12 357 12.365 12 567 90° 12 791 13 493 13 493

(d) Cowl lip design positions

	x _{CL} , in	∆x, ın	× _{CL} /R _{CL}
Close off	39 150	0 0	4 350
Inlet start	38 160	0 990	4 240
Mach 8	36 990	2 160	4 110
Mach 7	35 270	2.880	4 030
Mach 4 - 6	34 884	4 266	3 876

Table 4. - HRE/AIM Instrumentation (obtained from ref. 5).

(a) Coding for instrumentation list.

The code for the instrumentation listed in the "Identification" column is as follows. Sample, $S-P-14.492-0^{0}$ [I'-90-3 (A-B-C-D-E-F).

"A" designates the component on which the instrumentation is located

S = inlet spike assembly

I = innerbody assembly

NP = nozzle plug assembly

CO = cowl leading edge assembly (outside)

C = cowl leading edge assembly (combustor side)

0 = outerbody

N = nozzle shroud (combustor side)

NO = nozzle shroud (outside)

CE = combustor exit

EF = engine airflow-metering duct

F = fluids

"B" designates type of instrumentation

P = pressure

T = temperature

"C" designates the location of the instrumentation in terms of station, with the inlet spike assembly positioned for testing at Mach 6 condition.

"D" designates the angular location in degrees and minutes.

"E" designates position of the pressure pickup with respect to airflow in degrees, or, if the instrument is a temperature sensor, it designates the thermocouple:

CA = chromel aiumel

CuC = copper constantan

P/rh = platinum-platinum/rhodium

"F" designates the leg through which the leads are brought out.

An "X" anywhere in the Identification Code indicates that the parameter was not applicable.

xxx/yy in the "Reading No." column indicates the Channel No. (xxx) on which the parameter was recorded, and the rated capacity (yy) of the transducer used.

The "N/U" Code in the "Reading No." Column indicates channels that were not used.

"LeRC Sys" - recorded on separate system, therefore no channel number.

Table 4. - Continued.

(b) Instrumentation list.

easure-											READI	NG HUME	ER												
ent lumber	Identification	31	33	34	36	37	38	51	57	61	63	64	65	69	70	73	78	84	88	89	91	92	93	96	97
s	5-P - 0 595 - 0 - 0-3	121/25		- *	<u> </u>			ŀ																	
·\$ ·\$	S-P - 14 492 - 0°11' - 90-3 ' S-P - 14 483 - 271°8' - 90-3	N/U 123/10:		*		123/10		.					l												
-S	S-P - 14 473 - 180°5' - 90-3	N/0		*	_	,,,,,,																			_
~S	S-P = 14 4 = 90 = 90	Not Rou				l				l													1		i
-S -S	S-P - 30 695 - 359°36' - 90-3 S-P - 35 085 - 359°34' - 90-3	125/10			ŀ	1																			l
	S-P - 35 071 - 269°35' - 90-3	127/10	il l		1			1	l			i		l		1			1	li			ľ		
-\$_	S-P - 35 071 - 179°28' - 90-3	259/25			1		į .		Ì	ļ								1							
0-\$ 1-\$	S-P - 35 079 - 89°23' - 90-3 S-P - 35 580 - 359°32' - 90-3	260/10 261/10				ļ			·	1					i i			l	ŀ						1
2~S	S-P - 36 077 - 3590341 - 90-3	262/10			i			1		l	1	i	i	ļ			1		ŧ	i 1					Į.
3~5	S-P - 36 487 - 3590301 - 90-3	263/10	ii I		!		İ	1	1	1			1	1			Į.	İ] [[
4-S 5-S	S-P - 36 476 - 269031 - 90-3 S-P - 36 476 - 179027 - 90-3	264/10 265/25			ļ		İ			1	į		l	Į.				[l			1 !	!		
5-3 6-8	S-P - 36 482 - 89°29' - 90-3	266/15			ļ	ļ	ļ	├ ─-		 		<u> </u>			-	266/10-					ļ		-		
	S-P - 36 984 - 3590321 - 90-3	128/10			 	 				 	 			 		\vdash	 				├──		128/15		 - -
8-\$ 9-\$	S-P - 37 5 - 0 - 90-3 S-P - 38 0 - 0 - 90-3	-Not Ro			l	1	l	1	1		l	l	i	l	1	1		1	1	l	1	1	1	1	i i
0-5	S-P - 38 017 - 269°27' - 90-3	122/10			<u> </u>				ļ	ļ		<u> </u>				 		 		-	 	-	122/15		┤╼╾
1-S	S-P - 38 001 - 179°23' - 90	Hot Ros			i	İ	ŀ	ļ.				i		l	l '	1	i			l	•	i	1	i	1
2-S 3-S	S-P - 38 00 - 270 - 90 S-P - 38 5 - 0 - 90	Not Rai		ł	1	1	į	l l	}	1		ļ]	1		1	l	İ	1		!	1	1	
+-S	S-P - 39 024 - 359°25' - 90-4	129/20		 -		<u> </u>	├──	ļ	ļ	ļ	 			 			 			ļ	<u> </u>	-	129/25		╌
5-S	S-P - 39 011 - 269025' - 90-4	N/U	hI			l	1	ł	ļ.	1		1	ł	1	1	1			i	l				l	1
6-5 7-5	S-P - 38 996 - 179°23' - 90-4 S-P - 39 0 - 270° - 90	N/U Not Ro	U I	1	ŀ	١,	1	1	1	1	1		1	1	1	l		1	1	ĺ	[Ì		İ	
B-5	S-P - 39 497 - 3590241 - 90-4	130/25					ļ	ļ		-		├	 	↓		130/15		 	├─-	├ ──	ļ		130/25	<u> </u>	┥╼-
9-5	S-P - 40 027 - 359°24° - 90-4	131/25		<u></u>	1	1	ŀ		1		1	1	i	1	1		1		l		l			ł	1
0-5 1-5	S-P - 40 023 - 269°28' - 90-4 S-P - 40 015 - 179°25' - 90-4	132/25				<u> </u>	l				267/50	<u> </u>			<u> </u>	267/25			ļ	<u> </u>	ļ <u> </u>			Ь—	↓.
2-5	S-P- 40 015 - 89020' - 90-4	133/25			Τ	1		1	I	1	120,,,,0	l .	i		1			1	i	1	1	ŀ	1	ļ	1
3-5	S-P - 41-498 - 359030' - 90-4	134/75			 	-	 	+		 		 	├ ─	+	 	134/25		┼──	 -	ļ	134/50		134/75	1	╁╌╸
4-5 5-5	S-P - 42 464 - 359028' - 90-4 S-P - 43.7 - 0 - 90	135/75 Not Ro			-	+		· · · · ·		1		· · · ·				135/50			1	-		-	135/75		1
5-3 6-5	S-P - 43.7 - 90 - 90	Not Ro			F	1	Ì		1	1	l		i		l		Į.	1	i i	l .	ļ	1	1	1	ļ
r-s	S-P - 43.7 - 180 - 90	Hot Ro	uted	l]	1	1	1	1	l	ŀ	1			ŀ	1	l	1	1	ĺ	1	}		1
3-S 3-S	S-P = 43 7 = 270 = 90 S-P = 44 796 = 359*28' = 90-4	Not Ro		ľ	1		l	i.	1	1	l	l			١.	136/50	1	l	<u> </u>	<u>.</u>	136/75	Í			۱.
-3 3-5	S-P - 44 796 - 359°28' - 90-4 S-P - 45 0 - 0 - 90	136/75 Not Ros			1	\vdash										1 30/50					(1)0//5			I	
I-S	S-P - 47 315 - 359°28' - 90-4	268/75	⊢		 	 			 -		268/100	·[-	268/50			┼	 	 		268/75		-
-5	S-P - 47 301 - 269°22' - 90-4	137/75		 	1	 			 	 	 	+	 	┪	-	137/50		1 .	1	1			137/75 138/75		
3-5 4-5	S-P - 47 289 - 179015' - 90-4 S-P - 47 309 - 89020' - 90-4	138/75 139/75				1										- 138/50 - 139/50			Ι				139/75		—
5-5	S-P - 48 109 - 3590281 - 90-4	269/75			 	ļ	├ ─	├ ──	├	┤	269/100	ı]- -	 	 	-	269/50		 	+	1		·	269/75		1
6- s 7- s	S-T - 24 0 - 359°45' - S-T - 37 789 - 359°30' - CA-3	Not Ro			1		1		1	1		1	1	1				1]	İ		1	1	i	1
/-3 8-\$	S-T - 38 017 - 354035' - CA-3	303/50 N/U	1	*	1	1	1	1	1	1	Ì	1	1	1		1	1	1	1	l		1	1		1
9-\$	S-T - 40 021 - 3540301 - CA-4	305/50		1	l	1	1	1	1	1		1	1	l		1		1	1	l .		1	1	1	
0-S	S-T - 41 965 - 359030' - CA-4	306/50		*	1	1		1	1	1		1	1	1		1		1	l	1	1	1	1	i	1
1~S 2~S	S-T - 44 796 - 354027' - CA-4 LVDT (Spike Position)	307/50	Day = 4	, 372 la	chas		1	i i	1	1			1	1]	1	1	1]	1	1		1	
	1	1	Ĩ .	1	Ĭ		1	1	1	1]		1	1	1	1		1	1	1	1	
			<u>l</u> l	١		1	1		1	1]	1	1	1	1	-	1		1	1			1	
7-1	Load Cet1	1 277/30	00 lb =	20MA	-	 *	1		<u> </u>	<u> </u>		Щ.		J	1	ــــــــــــــــــــــــــــــــــــــ	J	<u></u>	<u> </u>					Ь	 5-

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Table 4. - Continued,

Measure-											REA	DING NU	MBER												
ment Humber	identification	31	33	34	36	37	38	51	57	61	63	64	65	69	70	73	78	84	88	89	91	92	93	96	97
1-1	1-P - 54 519 - 3590491 - 90-3	143/20 -							<u> </u>	 	143/25	143/50			ļ			ļ	ļ	ļ	<u> </u>	 -	143/100		-
2-1	I-P - 54 529 - 269049' - 90-3	N/U		H/U	186/50					 						· · · · ·							186/100		┢╾
3-1	1-2 - 54 512 - 179941 - 90-3	141/75 -		10.74	101/00		 -		 	1	 					141/50				 	 	-	141/75		-
4-1 5-1	1-P - 54 514 - 90° 0' - 90-4 1-P - 56 004 - 0°48' - 90-4	H/U 271/75		H/U	191/50											271/50							191/100 271/100		
6-1	I-P - 56 0 - 32°30' - 90		t Routed		i										1	,,,,,,,,		1			1		.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		1
7-1	I-P - 56 0 - 178°30' - 90	[No	ot Routed	ļ.	i		1		1	1	i	İ		ĺ	1		1	1		1	ļ	1	1		
8-1 9-1	1-P - 56 0	270/75 -	ot Routed		1]	1		J	<u>.l</u>		l		<u> </u>	270/20					<u> </u>	i	270/50		L
10-1	1-T - 54 0 - 0		t Routed					1	1	Ι΄				I		12,00,20					[270750		Г
11-1	i-r - 55 25 - 0	l k	t Routed	ŀ	1		i	l	1	l	1				i	l		1		ļ	į	1			i
11-1 12-1 13-1	-T - 60 0		t Routed	ŀ	i l		1	1	1	1	1				1	1			l i	i	•				į .
14-1	1-T - 60 019 - 120° 0' - CA-4	308/50 m 290/50 m		L				i	1	!	1			l	l	!	l	i	i	i	-	1	1		l
15-1		309/50 m	~		i l			1	Į.	1	i				1	l	Ì				1	į į			
										·	·	ــــــــــــــــــــــــــــــــــــــ		····			Ц	L			·	<u> </u>			1

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Noasure-		L	********								REA	DING HU	NBER							~					
ment Humber	Identification	31	33	34	36	37	38	51	57	61	63	64	65	69	70	73	78	84	88	89	91	92	93	96	97
2-HP	RP-P - 66.640 - 59°54' - 90-4 RP-P - 68.080 - 119°38' - 90-4	145/10 ~														144/10							144/25 - 145/20 -		=
4-HP	MP-P - 69.405 - 180° 8' - 90-4 MP-P - 70.790 - 240°12' - 90-4 MP-P - 70 465 - 300°12' - 90-4	147/10			}																				
6-HP 7-HP	MP-P - 74 550 - 0010' - 90-4 MP-P - 77 400 - 600 0' - 90-4 MP-P - 81.295 - 1200 8' - 90-4	149/10]																				
9-HP 10-HP	NP-P - 84.105 - 180° 5' - 90-4 NP-P - 86.967 - € - x-4	152/10						·								1									
12-67	HP-T - 68 080 - 124 ⁰ 15' - CA-3 HP-T - 70 790 - 245 ⁰ 12' - CA-3 HP-T - 74 45 - 5	311/50 av	Routed	i				ł	İ]											
14-NP	NP-T - 81. 300 - 1250 81 - CA-4	312/50 EV	 *		1				1			l		1		1	1								1

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Table 4. - Continued.

easure-											REA	M SHIP	MEER												
mber	Identification	31	33	34	36	37	38	51	57	61	63	64	65	69	70	73	78	84	88	89	91	92	93	96	9
1-C0 2-C0			-•							T	<u> </u>														
3-CO	CO-P - 35 544 - 262°56' - 90-	155/25		K/U	156/15							==	N/U	155/25 156/15	155/15						-	N/U	155/15 156/15	125/20	
4-00 5-00		157/25		1/0	158/10				 	-	 	-	11	157/25 158/10		N/U	N/U	N/U	N/U	157/25- 158/10	-	11.	157/15 158/10	-	Ħ
6-C0 7-CD	CO-P - 37 OH4 - 173° S' - 90-	159/15	\dashv											159/15								11	159/15		11
8-co	CO-P - 37 044 - 3530 2' - 90-	161/15		V/U	160/10									160/10		W/U	M/U 161/10	N/U	N/U	160/10 161/10			160/10 161/10		П
9-C0 10-C0		163/15		K/U	162/10			 	├	-		-		162/10		W/U		N/U	N/U	162/10			162/10		11
11-CO 12-CO	CO-P - 39.004 - 2630 1' - 90-	N/U		1/ U	164/10								11	163/15 164/10									163/15 164/10		11
13-00	CO-P - 40.509 - 830 6' - 90-	165/15		1/1	166/10						166/15		1 1	165/15 166/15		165/10 N/U	H/U	N/U	N/U	166/15			165/10 166/15] [
14- co 15-co	CO-P - 40 507 - 1730 6' - 90-1 CO-P - 40 504 - 2630 4' - 90-1	167/15		_					 	-	100,13	-		167/15		167/10			17.7			N/U	167/10	`	N/U
16-CO	CO-P - 40 500 - 3530 5' - 90-	169/15	~~~					L	└ ─	<u> </u>				169/15		M/U	N/U	M/U	N/U	169/15		N/U	169/15	169/20	N/U
17~CO 18~CO		170/15		/u	171/10					<u> </u>		-	1	170/15		- 1				170/15 171/10			170/15 171/10		1
19-CO 20-CO	CO-P - 40 600 - 210° 3' - 110- CO-P - 40 249 - 330° 1' - 135-				172/10								11	172/10	_					172/10			172/10	_	11
t1-co .	CO-P - 40.654 - 330" 0" - 110-	M/U		1/0	174/10								11	173/15 174/10		H/U	N/U	N/U	N/U	173/15 174/10		H/U	173/15 174/10		K/U
2-C0 3-C0	CO-P - 40 004 - 00 5' - 110-1 CO-P - 40 364 - 359057' - 75-			K/U	175/25 176/10				 			-				M/U	M //1	N/U	N/U	176/10	-		1,1,1		1
4-00		177/15			1700 10							-		177/15		N/U	N/U	N/U	N/U	177/15	-	N/U	177/15	176/15	jn/u
16-CO	CO-P - 40 656 - 1800 5' - 110-	179/15	`		179/25						178/20		M/U M/U	178/20 179/25				N/U N/U	K/U K/U	178/20 179/25		M/U	178/20 179/25		מיאון ו
31-C 32-C	C-P - 35 514 - 359058' - 90-	181/50							<u> </u>	<u> </u>						-	180/25 181/25			- 1,51.23		-	180/50		-
33-C 34-C	C-P - 36 685 - 0º 8' - 90-4	182/50	\dashv														102/25						181/50 182/50		▭
35-C	C-P - 37.034 - 00 81 - 90-4	183/50		=													183/25 184/25						183/50 184/50		
36-C 37-C		185/50		_				<u> </u>				 -	 	 		-	105/25					-	105/50		-
38-c 39-c	C-P - 37 -034 - 2700 7' - 90	Demogr	4	- 1											1						ŀ	1			l
+0-C	C-P - 38.044 - 00101 - 86-1	187/50	=														187/25 186/25					_	187/50 188/50		-
41-C 42-C		189/50						_					-			-	109/25						189/50		\vdash
4-C	C-P - 38.041 - 2100 71 - 86-1	N/U -	**										· · · · ·			-	190/25	<u> </u>		———	i	-	190/50		
5-C	C-P = 39.014 = CO 5' - 94-1	192/50												<u> </u>		=	192/25 193/25				 	-	192/50		-
6-C 7-C		194/50	- +	\dashv												-	194/25			-	194/50		193/50		⊏
0-C	C-F - 39 014 - 2700 0' - 94-1	195/50-1-	<u></u>			~	,		ļ		L						195/25				<u> </u>		195/50		L.
9-C		196/50									\vdash			 	 	-	196/25	 —					196/50		
1-C 2-C	C-F - 40 00 - 90° 7' - 90-4	N/U		- 1													197/25	!				_	197/50		
3-C	C-P - 40 004 - 2700 51 - 90	199/50 — Demage	8												 	-	199/25		_		-		199/50		-
H-C S-C	C-T - 39 014 - 70 C' - CA-4	314/50 EV		Ī]	1															l	.			1
56-C	C-T - 39.994 - 7º 8' - CA-4	316/50 m/					i							1			[l]
57-C 58-C	C-T - 40.0 - 900 - CA C-T - 40 004 - 1800 7' - CA-	M/U - Not Ro	betu.														İ				Ī	[]	i		
9-c	C-T - 40 000 - 2770 4' - CA- CO-T - 36 544 - 3530 2' - CA-	292/50		-				 -	H/U			<u> </u>													N/U
1-00	CO-T - 38.504 - 0 CA	Hot Ro		- 1		i			Į.				l	i	I		l i		1 1		Ι.	Ι' Ι			ı

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Table 4. - Continued.

Seasure- ment											READ	ING NU	BEA												
umber	Identification	31	33	34	36	37	38	51	57	61	63	64	65	69	70	73	78	84	88	89	91	92	93	96	9
-0	0-P - 41 06 - 000' - 110-4	201/75 -				<u> </u>		L		ļ <u>.</u>							201/50								-
	0-P - 41-06 - 180°0' - 110-4	272/75 -	 	 	ļ <u></u> -	Ь—	 -	 									272/50					-	272/75		-
	0-P - 41 06 - 21000 - 110-3		 	H/U	228/75	<u> </u>	┝──		├	}		——				-	228/50	_							╌
		H/U			· · · · · · · · · · · · · · · · · · ·	-	N/U	200/75		┢──							200/50								-
	0-P - 43 786 - 100° - 90-4		 	+	 			 	├─		202/100						202/50						202/75	-	-
		N/U	1	1			ט/א	203/75			203/100					_	203/50					_	203/75		1
0		204/75 -	 	 		1	ט/א	205/75		 	_				_	_	204/50					-	204/75 205/75		Ι.
		N/U 206/75		$\overline{}$			יייין	205/15									206/50						206/75		
	0-P - 47 016 - 100' - 90-4	273/75 ~		1							273/100						273/50						273/75		
		207/75 -									2/3/100					l	207/50						207/75		
		N/Ú		1			N/U	219/50									20// 50					-	219/75		
		N/U	*	1		T	}'''	- ' ' ' ' '																	
-0	0-P - 49 005 - 27000' - 90-3	N/U	-	↓ ——		-	H/U	198/50	<u> </u>		198/15	598/75					198/50						198/75		├
-0		H/U				├ ──																			-
		208/75 ~	 -	 				ļ		ļ						-	208/50					-	200/75		-
	0-P - 50 411 - 90° - 90-4	K/U	 	1	ļ	-	N/U	221/50				221/75				-	221/50		-				221/75		-
	0-P - 50 411 - 180 - 90-4	N/U	 	+	·						├				 						\vdash				₩
	0-P - 50 411 - 270° - 90-3	N/U		 		 		 		 					 										-
	0-P - 50 505 - 10 - 90-4	H/U	 	 	 		 																		-
	0-P - 52 506 - 0° - 90-3	209/75			···-	 	 	 									209/50	ļ			l	-	209/100		
		210/75 -		+	 	 			-					_			210/50	· · · · ·					210/100		1.
	0-P - 53 006 - 90° - 90-4	H/U		1	1		H/U	211/25		_	211/30	****				-	211/50					_	211/100		N/I
		212/75 N/U	H/U ~	1		· · · · ·	N/U	212/25		_	212/30						212/50						212/100		1"'
		214/75 -	1	1			וייין ן	114/45			212/30						214/50						214/100		
		215/75	1														215/50						215/100		\Box
	D-P - 57 451 - 00 - 90-3	H/U					N/U	213/25			213/30				Ĭ		213/50						213/100		-
		216/75	1		L		,,,,	2,3,23			21,37,30						216/50						216/75		-
		N/U	!	4	ļ	└	!	ļ	 	!					 		-10,00	_	_				2.0773		-
		217/50-	 			ļ	 	ļ <u>-</u>	├ ──	↓		217/75	<u> </u>	├		-	217/25		-			-	217/75		₩-
		218/50 -	 		ļ	 	 	 	├ ──	├──		218/75	├	├		├	218/25						218/75		┾
	0-P - 51 881 - 110° - 90-4	N/U	┼	-				 	 	 	-									_					┼~
	0-P - 61 881 - 180° - 90-3	220/75	 	ļ		├	—			 -	 				├──	₩	220/50	_				-	220/75		+-
	0-P - 61 874 - 290° - 90-3	N/U	┼──	+	 	╌	 	 		 					 	 									=
-0	0-P - 62 976 - 0° - 90-4	N/U	+	 		 									<u> </u>					· · · · · · · · · · · · · · · · · · ·					口
-0	0-P - 63 974 - 00 - 90-4	H/U	 	T		1				r	1				I						_			"	1
	0-P - 64 975 - 1º - 90-4	222/20 -	1	1	222/50		T		T	1	1						222/15		·			-	222/75		-
	0-T - 41 978 - 00 - CA-3 0-T - 42 581 - 00 - CA-3	317/50mv				!	1	!	i	!	1			l	!		1					l i			1
-0 -0		318/50av		1	1	I	l	1	!	I	1			l			I							l	1
-0	0-T - 45 234 - 3590 - CA-	319/50mv 320/50mv		1	į .	l	i		i	1	1	l			ľ		1				1			l	
	0-T - 46 507 - 00 - CA-3	289/50mV		1	ì	I	I	ŀ	1	1	1			l	l	'	1				l	1		i	1
	D-T - 46 510 - 900 - CA-4	293/50m				ı	I	l	1	1				ĺ	l	l					l			I	1
	D-T - 46 520 - 1800 - CA-3	294/50m		1		I	I	ı	1	1				l	l	Ī					1			1	1
	0-T - 46 491 - 2700 - CA-3	295/50m		1		l	1	l]	f			1	1		l	l .		.		1]	1
-0	0-Y - 47 016 - 3590 - CA-3	321/50m		1		1	1	!	ı	1	1 3		l	l	1	1					ł		•	1	1
	0-T - 48 0 - 00 - CA-	Not Rout	ted	1		1	1	I	ł	l .	1	l	ŀ	i		l					ŀ			l	1
- 0	0-T - 49 005 - 359° - CA-3	322/50av 323/50av	<u>ا المار</u>	1	ļ	1	1	I	1	1	I	l	ŀ	i	ŀ	1		1			I			l	1
-0	0-T - 50 005 - 00 - CA-3	323/50mv	4	1		1		I	l		1	1	I	I	I	ł					I	1		i	i
	0-T - 50 014 - 90° - CA	Not Rout	ted	1		1	l	l	l	I	1	l]	l						1			l	1
2-0	0-T - 50 014 - 1800 - CA-4	296/50av	/ *	1	1	1	l	I	l		l]	1	I	l	1	1		l	i			I	1
	L	I	<u>.</u>	.1	1	1	I	ı	I	ı	1	I	l	1	i -	l	1	l l		r :	i	l l		ı	1

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Heasure-						_					READ	ING HUMB	ER					, , , , ,							
ment Number	Identification	31	33	34	36	37	38	51	57	61	63	64	65	69	70	73	78	84	88	89	91	92	93	96	97
51-0 55-0 55-0 55-0 58-0 60-0 61-0 63-0 65-0 65-0 68-0	0-T - 52 910 - 00 - CA-4 0-T - 52 996 - 3590 - CA-3 0-T - 54 0 - 00 - CA- 0-T - 56 00 - 00 - CA- 0-T - 56 00 - 1200 - CA- 0-T - 56 00 - 2400 - CA- 0-T - 56 00 - 2400 - CA- 0-T - 57 010 - 00 - CA- 0-T - 57 970 - 00 - CA- 0-T - 59 976 - 00 - CA- 0-T - 59 976 - 00 - CA- 10-T - 62 474 - 00 - CA- 10-T - 62 474 - 1200 - CA- 10-T - 63 970 - 00 - CA- 10-T - 63 970 - 00 - CA- 10-T - 63 970 - 00 - CA- 10-T - 63 970 - 00 - CA- 10-T - 63 970 - 00 - CA- 10-T - 64 474 - 2400 - CA- 10-T - 63 970 - 00 - CA- 10-T - 64 474 - 2400 - CA- 10-T - 64 474 - 2400 - CA- 10-T - 64 475 - 00 - CA- 10-T - 64 475 - 00 - CA-	Not Routs 324/50mv 325/50mv 325/50mv 326/50mv Not Rout-Not Rout-Not Rout-1327/50mv 328/50mv 328/50mv 331/50mv 3	ed ed																						

"Cantinuous to end

READING HUMBER Beasure 91 92 93 96 97 88 89 78 84 ment Number 64 65 69 70 73 37 38 5 t 57 36 Identification 33 34 N-P - 66 635 - 298°55' - 80-3 223/20 N-P - 67 305 - 240° - 78-3 224/15 N-P - 67 305 - 240° - 78-3 224/15 N-P - 68 18 - 180° - 180° - 30 224/15 N-P - 68 800 - 118°49' - 90-3 225/10 N-P - 69 605 - 58°53' - 90-3 N/U - 100° 223/25 223/10 2-N 2-N 3-N 4-H 5-N 6-K 7-H 8-N 9-N N/U - 226/10 230/15 230/25 11-H 12-N 13-N 14-N 15-H £ 89694

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READING NUMBER Measure! 96 97 91 92 84 88 89 93 64 69 70 73 78 63 65 38 51 57 61 36 31 33 34 37 Number Identification | NO-P - 70 921 - 180°12' - 90-4 | 233/10 | NO-P - 70 917 - 330°8' - 90-3 | 234/10 | NO-P - 70 917 - 330°8' - 90-3 | 234/10 | NO-P - 71 940 - 134°53' - 90-4 | 235/10 | NO-P - 71 054 - 150°10' - 90-4 | 237/10 | NO-P - 71 978 - 0°11' - 90-4 | 237/10 | NO-P - 71 956 - 180°12' - 90-4 | 239/10 | NO-P - 71 956 - 180°12' - 90-4 | 239/10 | NO-P - 71 956 - 180°12' - 90-3 | 243/10 | NO-P - 71 956 - 180°13' - 90-3 | N/U | NO-P - 71 956 - 192°23' - 90-3 | N/U | NO-P - 71 956 - 192°23' - 90-3 | N/U | NO-P - 71 956 - 192°33' - 90-3 | 242/10 | NO-P - 71 956 - 20°13' - 90-3 | 243/10 | NO-P - 71 956 - 20°13' - 90-3 | 243/10 | NO-P - 71 956 - 30°10' | 90-3 | 243/10 | NO-P - 71 970 - 330°8' - 90-3 | 245/10 | NO-P - 71 971 - 340°85' - 90-4 | 247/10 | NO-P - 71 970 - 353°35' - 90-4 | 249/10 | NO-P - 72 430 - 150°11' - 60-4 | 250/10 | N/U N/U 233/10 233/10 234/10 n/u N/U R/U 16-NO 17-NO 18-NO H/U N/U 235/10 N/U 235/10 H/U 154/15 N/U 237/10 N/U 19-10 237/10 N/U N/U N/U 20-NO 21-NO 22-NO 23-NO 24-NO N/U 239/10 N/U H/U 239/10 R/U 168/15 N/U 242/10 R/U 242/10 N/U N/O N/U 243/10 N/U 243/10 H/U 243/10 245/10 29-NO 246/10 247/10 30-NO 31-NO 32-NO 247/10 249/10 249/10 250/10 33-HD 250/10

#Continuous to and

\$ 89718

Table 4. - Continued.

Measure-											READ.	ING HUM	ER												
Number	fdentification	31	33	34	36	37	38	51	57	61	63	64	65	69	70	73	78	84	88	89	91	92	93	96	97
	GCB - P - 66 34 - X - 180-X S-P - 1A - 172 - X-3 S-P - 1A - 25 - X-3	251/10 N/U 244/20	1)	- :				73/300																	
	S-P - 10 - 175 - X-3 S-P - 10 - 25 - X-3 S-P - 20 - 175 - X-4	H/U			23/600	211/500	N/U	74/300	_						 							, .			
6-F 7-F 8-F	S-P + 2C - 25 - X-4 1-P - 38	H/U	124/500		24/500		·	76/300	=				·		-										==
10-F 11-F	0-P - 18 - 90 - x-4 10-P - 18 - 270 - x-3 10-P - 4 - 90 - x-4	240/20 241/20 N/U	ė <u> —</u>	- 1/			l	77/300 78/300																	
13-F 14-F	0-P - 4 - 270 - x-x 0-P - 2A - 90 - x-x 0-P - 2A - 270 - x-3	Not Ro Not Ro N/U ←	uted				÷	79/500	<u> </u>																
16-F	0-P - 3A - 90 - X-4 0-P - 3A - 270 - X-3 15-T - 1A - 188 - CA-3	N/U N/U 53/50		123/500				80/300										:-							==
18-F 19-F 20-F 21-F 23-F 24-F 25-F 26-F 27-F 28-F 29-F	S-T - 1A - 30 - CA-3 S-T - 1C - 180 - CA-4 S-T - 1C - 30 - CA-4 S-T - 2C - 180 - CA-3 S-T - 2C - 30 - CA-3 1-T - 38 - 90 - CA-4 1-T - 38 - 270 - CA-4 0-T - 18 - 90 - CA-4 0-T - 18 - 20 - CA-3 0-T - 2A - 90 - CA-4 0-T - 2A - 270 - CA-3 0-T - 4 - 90 - CA-4 0-T - 4 - 90 - CA-4 0-T - 4 - 90 - CA-4 0-T - 4 - 90 - CA-4	\$4/50 \$5/50 \$6/50 \$7/50 \$9/50 60/50 61/50 62/50 63/50 64/50 65/50 66/50		*																					
33-F 34-F 35-F	0-T - 3A - 270 - CA-3 S-P - IGN 0 ₂ - X - X-3 S-P - IGN 0 ₂ 0-P - IGN 0 ₂ - X - X-4 0-P - IGN 0 ₂	68/50 248/30 Hot Ro 236/30	0 ' uted 0														·			_			236/500		
37-F	S-P - IGN H ₂ - X - X-4 S-P - IGN H ₃	Not Ro 252/30 Not Ro	ļ																				252/500	-	
39-F	0-P - IGN H ₂ - X - X-4 0-P - IGN H ₂	253/30 Not Ra	·																				253/500	-	
41-F 42-F 43-F	S-P - H ₂ O IN (TIP) - X - X-4 1-P - H ₂ O IN (TIP) - X - X-4 ST-P - H ₂ O IN (LE) - X - X-4		ly Monit	pred																					
	ST-P - H ₂ O IN (SIDE) - X - X-4 D-P - H ₂ O IN - X - X-3																								:

*Continuous to end

Measure∙ ment		[READ	HG HUM	SER												
Number	(dent) figation	31	33	34	36	37	38	51	57	61	63	64	65	69	70	73	78	84	88	89	91	92	93	96	97
46-F	OC-P - H20 IN (A) - x - x-4		Γ.																						
47-F	OC-P - H ₂ O IN (B) - X - X-4	[1		Ì		i	1	1	İ		İ		1		1				i			l	
48-F	OC-P - HOO IN (C) - X - X-4	1						1		1		i	i		1	1		!		Į.			•	1	
49 - F	OC-P - H2O IN (D) - X - X-4					l		1	ĺ		i				ì						1			i	i
50-F	S-P - H ₂ 0 OUT (TIP) - X - X-4	ļ		1 :		l		1	1								-]	ŀ
51-F	1-P - H ₂ O OUT - x - x-3		1					ł	l														1		
52-F	ST-P - H,0 OUT (LE) - X - X-3	Yisually	'Hon i	tored	1		1	ł	l														1	1	
53-F	ST-P - HO OUT (SIDE) -x >-3		1			ì		ł	i									i		i					1
54-F	0-Р-Н-0 ОИТ -х-х-з			.			ļ	1	i	ŀ						ŀ					ļ		l	ŀ	
55-F	OC-P - H ₂ O OUT (A) - X - X-3					l			i		1	į			1	1		l			ŀ		l	i	
56-F	OC-P - H_O OUT (8) - X - X-3		1] -	ł	l	t	i				1			1		l.		ļ	ļ	1	
57-F	OC-P - H20 OUT (C) - X - X-3]		l		١,		ĺ		1	i	l		ĺ	•				ļ	1
	OC-P - H_O OUT (D) - X - X-3				İ				l	ľ		ł			1	ļ				1		l			
_	5-AT - H_D OUT - X - CuC-4 /			<u> </u>	<u> </u>			L	L _	L	L			386/5mv			<u> </u>		L		ļ <u>.</u>	<u> </u>			
	S-AT - H_0 IN - X- CUC-4	370/∆5™	11_	ļ <u></u> _	L	1	L	L	L.	L	L			387/5mv			ļ		<u></u> _		1	L	L	1	
	1-AT - H-0 OUT - X - Euc 3 !		ľ	<u> </u>					L	L	L			370/5m											
	1-4T - HaD IN - X - CUC-4	371/aTSm	ν)	1				L	L	I			_	371/5/7			Ī			<u> </u>		1	-		
	ST-AT - H.O OUT LE - X - CuC-3}		ľ	<u></u>										37173	366/5m	!					1	T	T	1	
	ST-AT - HO IN LE - X - CUC-3	372/ATSm	{}				1 -	1	T					_	367/5m	I .	1		r—	Γ			T	1	
	ST-AT - H,0 OLT (SIDE) -x-cuc-31				[T	<u> </u>	Γ	1					368/5m		 	i — —	r	I		1		T	
	ST-AT - H,0 IN (SIDE) -X-CUC-4	373/ _A T5m	`} <i>`</i>	T	,	T -		T	i						369/5m	1	·		1	l	1	† 	†	1	
	0-AT - H ₂ 0 DUT - X - CuC-3							1		-					2037 SIII	ĭ	T		 		T		1		
	0-AT - H20 IN - X - CUE-3	374/6TSm	11 _	Γ		T	Ţ	1 -		1 -	-			372/5mv			T					1	1		
	HYD-P - IN - X - X-X 1		1 -]		T	1	1	1	i			373/5mv			1					t		† 	
65-F	HYD-P - QUT - X - X-X (Visually	Moni	tored			1		1		1				1	1	1	1	ļ			i			İ
66-F 66-F	ΔT1B - 40 6 - 3 - CuC-4 ΔT1A - 35 75 - 356 - CuC-3	375/AT5m	.į —	 	├		 	 -		-				374/5mv			├──		 				 -		
67 - F	ATIB - 40 6 - 181 - CuC-4	376/6T5m	11:										_	375/5mv 376/5mv										<u> </u>	
67-Г 68-F	ΔT1A - 35 75 - 176 - CuC-3 β ΔT20 - 55 6 - 357 - CuC-3 β	מוכום/טוג	ĭ! —	 	 			 	 					377/5mv	·		 	ļ		├	 		 		
68-F	ATZC - 40 5 - 5 - Cuc-4	377/ ₄ 75m	√{=											-	352/5m 353/5m						<u> </u>			<u> </u>	
	AT20 - 55 6 - 177 - Cuc-4 (378/ _A TSm	_iإ	├	·		 	 	 -	ļ		 -		388/5mv	·	-		ļ <u>.</u>						ļ	
	ΔT2C - 40 5 - 178 - CuC-4 } ΔT3F - 66 2 - 356 - CuC-3	_	1;-			<u> </u>		 	 	<u> </u>				389/5mv	359/5m		<u> </u>		_	-		 	 	 	-
70-F	AT3E - 55 6 - 355 - CuC-3 /	379/ <u>6</u> 15m	۲۱ —	 		 									358/5m	<i>-</i>								-	\Box
	ΔT3F - 66 19 - 176 - CuC-4 } ΔT3E - 55 6 - 175 - CuC-4 }	380/ <u>a</u> 75m	√{ <u> </u>	<u> </u>	-		 -	 	 				 		351/5m		├				 -	 	 	 	-
72-F	∆T4H - 72 36 - 356 - CuC-4 \	381/ATSm	J}=	-		二二				<u> </u>				378/5mv	350/5m	=	=						1		
	AT4G - 66 68 - 356 - CuC-4 f AT4H - 72 36 - 176 - CuC-4 l		17.	┼	 		 	 		 -		 		379/5m	·]	 	 	 			 	 	 	 	-
73-F	AT46 - 66 68 - 176 - Cuc-4	382/AT5m	.{Τ				<u> </u>			l		<u> </u>		380/5mv 381/5mv			1		ļ 	 	 	 	1	1	_

Table 4. - Continued.

Heasure-											READ	THE NUM	BER												
ment Number	identification	31	33	34	36	37	38	51	57	61	63	61,	65	69	70	73	78	84	88	89	91	92	93	96	97
74 - F	ATSJ - 40 0 - 4 - CUC-3 }	383/AT50	ļ , į —				 								361/5mv 363/5mv										<u>_</u>
74-F 75-F	Δ15K - 47 84 - 357 - CuC-3 Δ15J - 40 0 - 184 - CuC-4 }	· -	1 ! =												354/5m										-
75-F	AT5K - 47 84 - 181 - CuC-41	384/ ₀ T5n	γ{	 	 					 	 -		 		355/5m	 									
76-F	AT6H - 50 8 - 358 - CuC-3 [385/ATS	l, į ⊤	l	 										364/5m 365/5m	:									
	ATGL - 48 58 - 357 - CuC+31	1	11.												356/5m										_
77-F	ATEL - 48 58 - 181 - CUC-41	386/675	Υ{	 		 			 		 		 		357/5m	 	 	 							├-
	ΔT7P - 66 10 - 356 - CuC-3)	387/AT50	₩{ <u></u>											382/5mv 383/5mv	i	匸									
19-F	ΔT7N - 50 8 - 354 - CuC-3 ΔT7P - 66 10 - 176 - CuC-41	i	l 1 —		 						<u> </u>			384/5mv				<u> </u>				ļ	<u> </u>		-
79-F	AT7N - 50 8 - 174 - CUC-4 /	388/ ₀ 75n	~ } ~	 	i –			-			 			385/5mv		-	 -	 							 -
	0-AT - H20 OUT - X - X-4	389/475	₩ { _											360/5mv											
30-F	0- <u>л</u> т - н ₂ 0 ін - х - х-4 ў		1 '-	 	1			 		 			_	362/5#W	<u> </u>	 		· · · ·			<u> </u>		-		_
)1-F	0-Р - H ₂ 0 DUT - X - X-3 {	1	1	! .	ļ.				l	1	1	l	1		1		İ			1	l	1	1	ì	1
82-F	D-P - H-O IN - X - X-4	Visually	Honi	tored	i	1 .		ŀ	1	1	i	ł	ļ	t	1	ļ			Ι.			1			1
83-F	1-T - H ₂ 0 - 52 8 - 27 - CA-3	390/5mv	ļ	- *	1			i	İ	1	1				l	ŀ					1	i		l	1
	1-T - H-0 - 57 8 - 30 - CA-4	391/50V		 -	 	ļ. <u> </u>					ļ	 			391/5m	 	 					 			┢
	PURGE CAVITY PA-1-X - X - X-3	254/25	<u> </u>	ļ <u>.</u>	ļ	ļ		254/50		ļ	ļ											⊢—			┝
86-F	PURGE CAVITY PA-2-X - X - X-3	255/25		-	255/50	 -				 	 	 	 	 	-	 									-
	PURGE CAVITY PB-1-X - X - X-3 PURGE CAVITY P8-2-X - X - X-3	256/25 257/25	1	1	1	ŀ		1		1	!		1	l	1						ŀ	ļ		1	İ
	INNER BODY CAV PRES - X - X-4	258/50	Ш		1	Ī		1	ļ	1	}		1	1	1	ŀ	ł	ļ			ļ.	l		1	ı
	INNER BODY CAV TEMP - X-X-CA-	69/5	Ц_	<u> </u>	Ì				l	i			1								l	1		1	1
	PURGE CAVITY TAI - X - X - CA-	394/5mv 395/5mv	П		i	ŀ			1	1	}		1								ĺ				1
93-F	PURGE CAVITY TB1 - X - X - CA-	396/5mv	П		1			ļ		1	İ	İ	l		i		:		i	l				ł	1
	PURGE CAVITY TB2 - X - X - CA-	397/5mv	Ι'	l	Į.			1	1	1	l		1	l .		!	i r		ł	Ì		i		İ	ı
95-F 96-F	,	N/U N/U		1	ì		Ī		i	1	ŀ	ļ	ļ.	į.	ł	ì	:					l			L
97~F		N/U		1	ł					ł		[l	ŀ		ţ		ĺ	l		l			ı
98-F		N/U N/U	1	1		ŀ	!		1	l	l	İ		1	i	1	;			1	ŀ	i		1	1
99~F 00+F	PURGE CAVITY	70/50	١,		1	1				1	1	l		l		1		1			1	1			ı
01-F	PURGE CAVITY	71/50	}	+	1	l					1	l		l	I					i	i	}		l	
102-F	PURGE CAVITY	72/50	<u>1′</u>	1	<u> </u>	<u> </u>	L	l	<u> </u>	L	1	L	ــــــــــــــــــــــــــــــــــــــ	<u> 1</u>	<u> </u>	<u> </u>			L	L	<u> </u>	<u> </u>	l	L	<u> </u>

*Continuous to end

(b) Concluded

			READING NUMBER	-
leasurement Number	1dentification	65	92	97
1CE 1	CE-PT - 66 74 - 0 - 00 - X	155/75	155/50	155/75
2	CE-PS - 67 04 - 0 - 13 - 7	156/50	156/15	156/50
3	CE-PS - 67 04 - 0 - 109 - x	157/50	157/15	157/50
í.	CE-PS - 67 04 - 0 - 193 - x	158/50	158/15	158/50
Š	CE-PS - 67 04 - 0 - 283 - λ	159/50	159/15	159/50
á l	CE-PT - 66 74 - 110 - 00 - X	160/75	160/50	160/75
7	CE-PS - 67 04 - 110 - 18 - X	161/50	161/15	
á l	CE-PS - 67 04 - 110 - 108 - X	162/50	162/15	161/50
9	CE-PS - 67 04 - 110 - 198 - X	163/50		162/50
10			163/15	163/50
11	CE-PS - 67 04 - 110 - 288 - X	164/50	164/15	164/50
	CE-PT - 66 74 - 180 - 00 - X	165/75	165/50	165/75
12	CE-PS - 67 04 - 180 - 1 - X	166/50	166/15	166/50
13 14 15 16	CE-PS - 67 04 - 180 - 91 - X	167/50	167/15	167/50
14	CE-PS - 67 04 - 180 - 181 - x	169/50	169/15	169/50
ış (CE-PS - 67 04 - 180 - 271 - x	170/50	170/15	170/50
16	CE-PT - 66.74 - 280 - 00 - x	171/75	171/50	- 171/75
17	CE-PS - 67 04 - 280 - 355 - X	172/50	172/15	172/50
18	CE-PS - 67 04 - 280 - 85 - X	173/50	173/15	173/50
19	CE-PS - 67 J4 - 280 - 175 - X	174/50	174/15	174/50
20	CE-PS - 67 04 - 280 - 265 - X	177/50	177/15	177/50
21	CE-PT - 66.74 - 330 - 00 - X	178/75	178/50	177/50
22	CE-PS - 67 04 - 330 - 3 - X	179/50	179/15	
23	CE-PS - 67 04 - 330 - 93 - X	233/50	233/15	179/50
24	CE-PS - 67 04 - 330 - 183 - X		233/15	233/50
23 24 25 26 27 28		234/50	234/15	234/50
52		235/50	235/15	235/50
40	GE-G-GS - 30 - X - X	LeRC sys	Lerc	LeRC
*/	CE-G-TT - 30 - P/R - X	Leac sys	124/20	124/20
20	CE-G-RT - 30 - C/A - X	LeRC sys	142/20	142/20
29 30 31	CE-G-PT - 30 - X - X	237/75	237/50	237/75
30	CE-G-PS - 30 - X - X	238/60	238/30	238/60
31	CE-G-GS - 70 - X - X	LeRC sys	LeRC	LeRC
32	CE-G-TT - 70 - P/R - X	LeRC sys	81/20	81/20
33	CE-G-RT - 70 - CA - X	LeRC sys	231/20	23 1/10
34	CE-G-PT - 70 - X - X	239/75	239/50	239/75
35	CE-G-PS + 70 - x + x	242/60	242/30	242/60
32 33 34 35 36 37 38 39	CE-G-GS - 170 - x - x	LeRC sys	LeRC	LeRC
37	CE-G-TT - 170 - x - x	LeRC sys	82/20	82/20
38	CE-G-RT - 170 - X - X	LeRC sys	244/20	244/10
39	CE-G-PT - 170 - x - x	243/75	243/50	243/75
40	CE-G-PS - 170 - X - X	245/60	245/30	245/60
41	CE-G-GS - 260 - X - X	LeRC sys	Lerc	LeRC
42	CE-G-TT - 260 - X - X	LeRC Sys	345/20	Lenc
43	CE-G-RT - 260 - X - X	LeRC sys	Lerc	
43 44 45 46 47 48	CE-G-PT - 260 - X - X	246/75	246/50	Leac
LE	CE-G-PS - 260 - X - X			246/75
1 31		247/60	247/30	47/60
10	CE-G-GS - 350 - x - x	LeRC sys	LeRC	LeRC
7/	CE-G-TT - 350 - X - X	LeRC sys	346/20	LeRC
40 to	CE-G-RT - 350 - X - X	LeRC sys	140/20	140/20
49 50	CE-G-PT - 350 - X - X	249/75	249/50	249/75
50 [CE-G-PS - 350 - X - X	250/60	250/50	250/60

Table 5. - Summary of HRE/AIM test points used for analyses.

(a) Mach 6 component integration results;

*					P _{To} ,	т,	χ.			,				
Page	Read Numb		Time	H _o	psia	on	X _{CL} ,	۱.,	ار1/∮₁	Inj.2/φ ₂	Inj.3/ø ₂	ϕ_{T}	Ignitors	Purpose & Remarks
No.	ĺ	1	\$ 1 me	L	base	_ ^	In.	α		- 2	3	<u> </u>	1, 2, 3	
	37	**	126.95	6.0	750	3000	35.2	00	0	٥	0	0	No	No fuel injection
	Ī	_	161.15		1	+	 	+	1A,1B/.24	0	0	0.24	1,2	1st stage only
_			168.0	 -	+{-	 	+	╁╂╴	1A,1B/-3	0	0	0.30	1	1st stage only
				\vdash	 	+	╀╌╂╌	╀					<u> </u>	<u></u>
	y		174.65	Y	T	7	₹	₩.	1A,18/.36	0	0	0.36	Y	Max. ∅, engine unstart
57	34	į.	98.15	6.0	750	3000	35.2	00	0	0	0	0	1,2	
65			104.45	,					1A,18/.20	0	0	0.20		1st stage only
73			148.55						1A,1B/.23	2A/.58	0	0.81		1st and 2nd stages
81			181.85		1		П	П	1A,1B/.21	2A/.56	3A/.39	1.16		Max. Ø, 3 stages
89	Ý	· 1	196.25		940	1	1	14	1A,18/.15	2A/.44	3A/.32	0.91	- 	Max. Ø, 3 stages
				()				1.0						
	- 36			6.0	750	3000	35.2	100	0	0	0	0	No	Auto ignition
		a	· · · · · · · · · · · · · · · · · · ·	-	+	+	++	┼╀	1A,1B/.26		0	0.26		
97			132.68	┵	 	1-1-	11	+	·····	2A,2C/.34	0	0.59		
106	 		144.38	₩.	 	11	11	\coprod		2A,2C/.49	0	0.73	 	
115	╙		158.78	$\sqcup \bot$				$\perp \perp$	·	2A,2C/.69	0	0.92		
124	į į	L	173.18		♦	•	1	₩.	1A,18/-22	2A,2C/.75	0	0.97		•
133	38	3	96.24	6.0	750	3000	35.2	00	0	0	0	0	No	
141	Ιή	-	107.05		17	T	 	+	1A,18/.33	0	0	0.33		1st stage only
150			113.35	╁┼	┼┼	┼╌╁╴	╂┼	++-	0	20/.38	0	0.38	 	2nd stage only transient
158	H		116.95	1	┼╁	+	╁	╁	1A,18/ 18		· · · · · · · · · · · · · · · · · · ·	0 85	 - -	data
			110.95	7	×	, v		<u> </u>	IA, 107 10	207.07		0 03		3 4464
167	52	2	165.93	6.0	750	3000	35.2	O°	0	0	0	0	No	Ø1A,1B and Ø4,2C
175	-		172.23					П	1A,18/.24	4,2C/.26	0	0.50		
183			180.33	П				П	1A,18/.20	4,2C/.41	0	0.61		
191	ý	,	189.33	4	1	1	1	4	1A,1B/.20	4,2C/.53	0	0.73	V	ý
			150 10	(0	750	2000	35.3	00	0	0	a	0	No	Constant Ø1A,1B, Ø2A,2C
199	54	+	156.46	6.0	750	3000	35-2	1	1				NO	
207			185.26	╁		-	++	++-		2A,2C/.64	0	0.85	 	ramped up 3 times
215	ļļ		200.56	$oldsymbol{\downarrow}$	+		₩-	-1-1-	1A,1B/-23	2A,2C/.43	0		ļ	
223	lacksquare		222 16	┦.		$\bot \bot$	$\perp \perp$	11	<u> </u>	2A,2C/.25	0	0.49	[
231			235.66	$\perp \perp$	1-1	$\bot \bot$	┦-	11		2A,2C/.52	0	0.76	₩	
239			253.66	Ц.		$\perp \perp$	$\bot \bot$	11		2A,2C/.60		0.78	1.2	
247	1 9	<u> </u>	280.66	₩.	₩.	1 *	₩.	*	1A,1B/.20	2A,2C/.61	0	0.81	No	V
255	5	7	195.11	6.0	750	3000	35.2	00	0	0	0	0	No	Optimized performance
263	ĺ		207.71		11	11		T	1A,18/.21	2A,2C/.73	0	0.94		
27/	1 1		234 71	++	++	+ +	+-	++	 	2A,2C/.60		0.92		
279	╁═┤		265.31		++	╅═╂╌	1-1-	+		2A,2C/.36		0.57		
287	┨	,	287.81	4	++	 	++	╅	 			0.74	+	
						—								
295	6	0	155.69	6.0	750	3000	35-2	00	0	0	0	0	No	Variation of fuel schedule
303			178.19	$\perp \perp$	$\perp \perp$	$\perp \perp$	$\perp \perp$	$\bot \bot$		2A,2C/.64		0.85		
311			186.29						1A,1B/.22	2A,2C/.65	0	0.87		
319			202.49	$oxed{\Box}$			$\perp \Gamma$	\prod	1A,1B/.21	2A,2C/.65	0	0.86		
327			223.19					\prod	1A/.21	2A,2C/.66	0	0.87		
335			230.39	П				П	1A,1B/.21	2A,2C/.67	0	0.88		
343	1 1		241.19	$\top \top$	 	11		$\top \!\!\!\! \top$	18/.19	2A,2C/.68		0.87		
35/	1 1		249.29	11	1-1-	\top	11	11	1B/.24	2A,2C/.68		0.92		
359	1 1		258.29	11	11	11	11	11	0	2A,2C/.76		0.76		
367		,	264.59	 	+ +	+ +	+ 1	+1	0	2A,2C/.80		0.80		
10/			1207009	▼		<u> </u>	₹	▼	L	1,0, 100	<u>. </u>		 Y	<u> </u>

^{*}Reference 10

^{**} Because of insufficient valid engine surface pressure measurements, performance results were not obtained.

a Listings not available.

Table 5. - Continued.

(b) Mach 6 engine performance results.

Page	Rea Num	ding ber	Time	Мо	PT	o o	PT o		CL'	α	Inj 1/ø ₁	Inj.2/\$ ₂	Inj.3/ø ₃	φ _τ	Ign: tors 1, 2, 3	Purpose & Remarks
55	6	1	178.86	6.0	75	0	3000	1	6.7	00	0	0	0	0	No	Effect of spike position
63	i		198 66				Ť	Ť	Ť	İΤ	1A,1B/-13	2A,2C/,36	0	0.49		
72			205.86		1		\dashv	┪	1	\sqcap		2A,2C/.49	0	0.64		
81			212.16			П		†	1	\sqcap	1A,18/ 15	2A,2C/.61	0	0.76		
90			222.06		1	П		+	+	1	1A,1B/ 14	2A,2C/.73	0	0.87		+
99			231.06			П	\top	3	7 5	00	0	0	0	0	No	Effect of spike position
108			243.66		\top	П	1	1	T	Т	1A,18/.30	0	0	0.30		
117			246 36			П		T	1		1A,18/.30	2A,2C/ 47	0	0.77		
126			251 76					T		П	1A,18/.29	2A,2C/.65	0	0.94		
135			262 56								1A,18/ 27	2A,2C/ 96	0	1 13		High test cell and
144	, ý		273.36	+			Ť	I	•	*	1A,18/.26	2A,2C/115	0	1 41	₩ -{	AIM nozz. pressure
153	63	, 	186.15	6.0	93		3000	, ,	5.2	ó°	0	Ö	0	-	No	Effect of altitude
161	<u>-</u> i		192 45	- T	 	\vdash	<u> </u>	+	Ť	Ť	<u> </u>	2A,2C/.56	0	0 80		and or and code
169		\dashv	216.75	$\vdash \vdash$	+-1	,	+	+	+-	H	1A,1B/ 24	2A,2C/.76	0	1 00	 	
177			249.15	+	47	; - 	\dashv	+	+-	\vdash	0	0	0	0	 	
185	1	,	275.25	-	47		+	+	+	+	I	2A,2C/.73	0	0 99	 	
								+		.0	<u> </u>					
193	64	+	156.11	6.0	75	Ů.	3000	<u>' 3</u>	5.2	0_	0	0	0	0	No	Subsonic-supersonic
201	\dashv		167 81	-	\vdash			1	╄	1	18/.24	2A,2C/ 77	0	1 01		transition
209			202 01	-	\vdash	Н	\dashv	1	_	4	0	0	3A,38/.85	0.85		
217			239 81	-	┦		_	+	╀-	4	1B/.23	2A,2C/1J1	0	1.34		
225			261.43		₩	\vdash	_	+	╄-	+	1B/-24	0	3A,38/ 8	1.04		
233	ý		293 81	♥	1-4			\pm	<u>*</u>	•	18/.26	2A,2C/.8	0	1.06	Ÿ	<u> </u>
241	6	5	164.03	60	75	0	3000) 3	5.2	00	0	0	0	0	No	Supersonic combustion
249			174.83					\perp			1A,1B/.23	0	0	0.23		with instrumentation rig,
257			180,23								14,18/.24	2A,2C/.34	0	0.58		gas sampling
265			196.43					${\mathbb L}$			1A,1B/.24	2A,2C/.59	0	0.83		
273		Ì	201.83					Τ			1A,1B/.24	2A,2t/.80	0	1.04		
281			218.03			П	Т	Τ			1A,1B/-27	2A,2C/ 76	0	1 03		
289			235.13	•		Д		T	T	Ť	1A,1B/.25	2A,2E/.79	0	1.04	•	
297	69	-	177.00	6.0	75	، ا	3000	1/3	5.2	00	0	0	0	0	No	Supersonic combustion
305		$\neg \uparrow$	198.60	\top		\sqcap		ť	Т	Т	1A,18/.22	0	G	0.22		with instrumentation rig,
313	_		212.10			П	十	1	\top	+	}	2A,2C/.48	0	0 48		gas sampling
321			226.50		\sqcap		1	1		+		2A,2C/.59	0	0.82		
329		\neg	256.20	\neg		\Box	1	†		1	1A,18/.22	2A,2C/ 69	0	0.91		
337	ý		265.20	Ŧ			•	I	V	1	1A,1B/-23	2A,2C/.79	0	1.02	•	
345	71	\neg	160 54	6.0	75	. 	3000	1,	5 2	30	10	0	0	0	No	Angle of attack perform-
353	';		171.39		1	-+	1	+	1	Ť	1A,18/.22		0	0.22	- "	ance
			174.94	-	╁	-	+	┿	\vdash	┿			0	0.53		
361 369			193.84	-	╁╌┥	-	+	+	+	╁		2A,2C/.59	· · · · · · · · · · · · · · · · · · ·	0.83		
	-+	\dashv	207 34	+	H	1		+-	╅┥	+		2A,2C/ 81		1.05	-1-1	
377 385	+	+	248.74	+	╁╌┨	\dashv		╁	+	+	0	2A,2C/1.33		1.33	 	
393	\dashv	-	266.74	+	$\vdash \vdash$	\dashv	+	╁	H	╫	0	2A,2C/.87		0.87		
			270.34	+	$\vdash \vdash$	\dashv	+	╁	+	╬	0	2A,2C/.87		0.87		
12 () ·		- 1	-17-		1 1	- 1	i	1	1 1	Ŀ	, v			0.07	Il	1
401 409			284.74			7		Т	\blacksquare	Т	0	2A,2C/.66	0	0.66		

*Herein

Table 5. - Continued.

(c) Mach 7 component integration and engine performance results.

Page*		_		Γ		PT	,	P _{To} ,	٦	7						r	·	 	·····
No.		dıng ber	Time	М	0	ps	ia j	o _R 'o	X i n		ď	1nj.1/ø ₁	inj.2/\$2	Inj.3/ø ₃	$\phi_{\overline{1}}$!gni 1, 2	tors 2,3	Purpose	& Remarks
54	8	8	236.40	7.	25	10	00	3160	36.	.6	o°	0	0	0	0	2	2	Exploratory	run
62	-		245.40					3170	П	_		1A,18/.30	0	0	0.30	1	<u> </u>	<u> </u>	
70			261.60		П			3250	П	十		1A,18/.42	0	0	0.42	f	<u> </u>		
78			269.70		П			3280		1		1A,18/.55	0	0	0.55	l			
86			270.60			-		3270		1		1A,18/.57		0	0.57		<u> </u>		
94			271.50		П			3270	П	7		1A,1B/.58	0	0	0.58	_	_		
102			278.70					3270	Ħ	十		1A,4/.16	2A,2C/.70	G	0.86	·	\vdash		
111			285.90		П			3250	П	1		1A,4/.31	2A,2C/.60	0	0.91	<u></u>			
120			294.00	_				3200		+		1A,4/.28	2A,2C/ 57	0	0 85	<u> </u>	1		
129			299.40		Г			3150		7		1A,4/.45	2A,2C/.46	0	0.91	_			
138			305.70			-	,	3090		<u>, </u>		14,4/.49	2A,2C/.41	0	0.90	Ι,		,	,
10-	ρ	9	250 77	7.		10	20	1790	36.	7	o	0	0	0	0	<u> </u>	lo	Effect of 1	AL T
147	-			7		<u>.،</u>		3160	30,	4	_	1A,1B/.32	2A,2C/.47	0	0 79			GILEGE OL 1	то то
155			283.17	۲ <u>٬</u>	-	\vdash	-	3270	┝╌┩	+		1A,18/.34		0	0 89			<u> </u>	
173			290.37	├	H		Н	3270	$\vdash \vdash$	╅	\dashv	0	2A,2C/.75		0.75	<u> </u>	ļ		
181		$\vdash \dashv$	294.87	├	Н	 	Н	3310	H	+		0	2A,2C/./3	0	0.75	├	 		
189			304.77	┝┈	Н	-		3290	H	╌┼		0	2A,2C/.59		0.59		 		
197			310.17	-	Н	Н	-	3060	H	-+		1A,18/.32		0	0.89	-			
206, 232		**	316.47	7.	<u></u>	\vdash	_	2720		+		1A,1B/.29		0	0.83		 		
215,241		**	327.27	7.		-	-	2410	\vdash	-		1A,18/.28		0	0.82	<u> </u>	 	 	
224	,	TT	352.47	7.	_			3300	┝╏		-	1A,18/.36		0	0.02	 :	<u> </u>	l	<u> </u>
									- 8							<u> </u>	<u> </u>		<u></u> _
249	9	0	197.22	7.	25	10	00	3000	36.	.6	00	0	0	0	0		lo	Optimizatio	h
257			206.22	L			L,		Ш			1A,18/.48		0	0.48	2	<u> </u>	<u></u>	
265			212.52		Ш					_		1A,1B/.49		0	0.54				
273			217.02	L		_				_		1A,1B/.48		0	0.82				
281			230.52	_					Ш	_		1A,1B/.26	L	0	0.77	L		L	
289			235.02	L					Ш	_].		1A,18/.79	L	0	1.98		<u> </u>	Inlet u	nstarted
297			246.72	<u> </u>		_				_		1A/.51	0	0	0.51	L			<u></u> _
305			247.62	<u> </u>	_	ш	_		*	4		1A/.55	0	0	0 55	1			<u> </u>
313	9	11	175.65	7.	25	10	00	3100	36	6	30	1A,1B/.39	0	0	0.39	2	!	Angle of at	tack
321		1	180.15		П				П	7	\neg	1A,18/.47	0	0	0.47	2			
329		\Box	186.45							7		0	0	0	0	N	lo		
337		П	190.05	Г	П		П		П	1		1A,1B/.51	4/.13	0	0.64	2			
345		\sqcap	203.55			Π			П	7		1A,18/.52	0	0	0.52		Γ		
353			216.15							_†		18/.27	4.2C/.34	0	0 61				
361			224.25	$[\]$						T		1B/.28	4,20/50	9.	0 78				
369			226 95							T		18/ 28	4,2C/.45	0	0.73				
377			229.65	<u> </u>					Π	T		18/.33	4,2C/.39	0	0.72		[
385			235.95				\Box	•		丁		18/.29	20/.41	0	0.70				
393)2	186.87	7	3.8	10	00	2050	36.	1	0	0	0	0	0	N.	lo	Supersonic	combustion
401	┌	-	205.77		Ī	۳	Ť	2850	۳	+	<u> </u>	1A,1B/.48		0	0.72			with instru	mentation rig,
			227.37	/.	- 7	\vdash	١.	2050	╀┼┤	-		1A,18/.50	:	0	0.72	<u> </u>		gas samplin content eff	
409	\vdash	\vdash	248.07	-	Н	-	۱	$\vdash \vdash$	⊢┤	+		18/.33	4,20/.58	0	0.91	 	ļ	CONTENC ELL	
425	 	$\vdash \dashv$	290.37	7.	25		-	3000	╟╌╢	+	_	10/-33 1A, lb/-47	4,2C/.55	0	1.12	<u> </u>			
	۳.	╆┤	312.87	7.				3000	╌┤			1A,18/.36		0	0.85		 		
433	L	<u> </u>	12.0/	<u> </u>	د>			3000				14,16/.30	4,267.49	<u> </u>	0.05	1	<u> </u>	L	

^{*}Reference 11

^{**} Recomputations were made with surface pressure substitutions

Table 5. - Continued.

(d) Mach 5 component integration and engine performance results:

Page*	Rea Num	dıng ber	Time	H		P _T ,		•	X _{CL} ,		≀ոյ 1/ φ ₁	inj 2/ø ₂	ln ₃ .3/φ ₂	Ø _T	Ignitors	Purpose & Remarks
						psia	╁┈		110.	α	<u> </u>			-7	1, 2, 3	
<u>54</u>	9.	3	134.03	5.1	1	420 -	21	00	35.2	00		0	0	0	No	No fuel injection
62			142.13	Щ	<u> </u>	4_	<u> </u>	Щ		<u> </u>	0	2A/.29	0	0 29	2	2nd stage only
70			150.23	Ц	_					<u></u>	0	2A/.31	3A,3B/.25	0 56		Subsonic combustion
78			158.33	Ц	ᆚ		$oldsymbol{ol}}}}}}}}}}}}}$				0	0	3A,3B/.60	0.60		and 02 content effect
86			162.83	Ц	┵	4_		Ш		<u>Ļ</u>	0	0	3A,3B/ 71	0.71		
94_			174.53		\perp						0	0	3A,3B/ 49	0.49		
102			182.63	. ♦		<u> </u>				<u> </u>	0	0	3A,3B/.35	0.35	•	•
110	<u></u>	4	134.14	5.1	1	420	22	30	35 2	00	0	0	0	0	No	Subsonic combustion
118	1		140 44	T	+	1	\vdash	M		\vdash	0	2A/ 49	0	0 49	2	
126			150 34	-	+	7				1	0	2A/.49	3A,3B/.47	0 96		
134			157.54	\vdash	╅	+-	\vdash		-	1-	0	0	3A,3B/1.03		 - -	
142			163 84	一	┪	 	H	-		+-	0	0	3A,3B/1 19			
150			180 04	\sqcap	+	┪┈	\vdash	\vdash		\vdash	0	0	3A.3B/ 59		 	
158	-		214 24	\vdash	+	300	20	40	\dashv	\vdash	0	2A/ 53	0	0 53	\vdash	Effect of T _{TO}
166			215.14	\vdash	+	T	 ~			┼	0	2A/.53	0	0 53	++	
174			218.74	\vdash	┰	┿	\vdash	$\vdash \vdash$	\dashv	┼	0	2A/.54	3A,38/-5	1.04	 	High test cell and
183			231.34	\dashv	+	╁╴	\vdash	\vdash		┼	1A,18/ 15	0	0	0.15	++	AIM nozz. pressures
191		-	233 14	\vdash	+	+-	H		-	 	1A,18/ 25	0	0	0.25		
199	- +		234 04	1	╁	-	┼┤		-	┼		0	0			
•••				_	+		<u> </u>				1A,18/.27	0		0.27		<u> </u>
207	9!	5	129.55			300	24	30	35.2	00	0	0	0	8	No	Supersonic combustion
215			140 35	5.1			30	80			1A,18/.16	0	0	0.16	2	
223			160 15				29	40			1A,18/.18	2A,2C/.68	0	0.86		
23/			169.15		L	1			L		1A,18/.19	2A,2C/.83	0	1.02		
239	- 1		189 85								0	2A,2C/ 99	0	0 99		
247			196.15								0	2A,2C/.86	0	0.86		
255			204.25			\perp			\Box		0	2A,2C/.71	0	0 71		
263			211.45								0	2A,2C/.58	0	0.58		
27/	Ī		217.75			T					0	2A,2C/.70	0	0.70		
279			228 55	1	1	1	П				1A,18/.22	2A,2C/.63	0	0.85	1	
287			241 15		1	T	П	$\overline{}$			0	0	0	0	No	
295	Ţ		252.85	\Box	1	320	28	00			1A,18/.18	2A,2C/.70	0	0.88	2	
303			289.75	7	1	310	28	90			0	2A,2C/.86	0	0.86		AIM nozz. press. hi
311	\neg	- "	310.45		1	+20	22	30	\neg		0	2A,2C/.66	0	0 66		Effect of T _{TO}
319	+		317 65	+	1	+20	22	30	-	1	0	2A,2C/.51	0	0.51		†
				<i>-</i> 1	Τ,	420	22	20	35 2	20	0		0	0	No	Anala of attack and
327	96		134 44	3.1	+	120	22.	-	35 2	-	0	0 2A/ 38	0		2	Angle of attack perform-
336	-			-	十	╂—	\vdash		-	-		2A/.45		0 38		ance
344			150.64		╀	╂—	⊢┤		+	\vdash	0		3A,3B/.38			
352	_		165 94	-+	+-	+-		\dashv		\vdash	0	0	3A,3B/.87		 	
360			172 24	-	+-	-	┞╌┤	\dashv	-	H	0	0	3A,38/-59			
368			180 34	-	1	<u> </u>	<u> </u>		_ _		0	0			<u> </u>	
376	_		244.24	-		300	29	_	-	\vdash	0	0	0	0	No No	
384			264 04	\perp	14	+20	22	50 J		\sqcup	1A,18/.10		0	0.10	2	Fuel flow meas.
392			274.84	\perp			\square	ļ		Ш	TA,18/.21	0	0	0 21	2 >	malfunction; 1A
400]	275.74	j¯							1A,18/.20	0	0	0 20	2 J	flow only indicated
408			294.64					\Box			0	0	0	0	No	
700		_	313.54	_		- T-	-			. – –	0	0	3A,3B/.77	0.77	2	High test cell and

Table 5. - Concluded.

(d) Concluded.

Page No.	Reading Number	Time	Мо	P _{To} ,	P _{To}	_ ^	CL'	α	inj.1/ø ₁	inj.2/\$ ₂	1nj.3/ø ₃	φ _T	Ignitors 1, 2, 3	Purpose & Remarks
425	97	135.71	5.1	210	2100	3	5.2	00	0	0	0	0	No	Subsonic combustion with
433		156.41			2200				0	2A/.51	3A,38/.49	0.90	2	instrumentation rig and
442		160.91						П	0	2A/.32	3A,3B/.24	0.56		gas sampling probes
451		182.51							0	0	3A,38/.50	0.50		
459		201.41						П	0	0	3A,3B/.67	0.67		
467		224.81		1					0	0	3A,3B/ 86	0.86		
476		252.71		420		T	Г	П	0	2A/.50	3A,3B/.43	0.93		
485		271 61							0	2A/.43	3A,3B/.34	0.77		
494		295.91							0	0	3A,3B/ 74	0.74		
502		317.51						П	0	0	3A,3B/.90	0.90		
510		322.01				1	T		0	0	3A,3B/1.07	1.07	1	High test cell and
518		325.61					-		0	0	3A,3B/1.08	1.08	1	AIM nozz. pressure

^{*}Reference 12

```
0000000 PROCDEF C033
0000100 KDOSEL 60, 65, 67, 83, 84, 85, 86, 87, 88, 91, 92,123,124,148,154,156,158,160,162,164
0000200 KDOSEL 165,166,168,171,172,174,175,176,180,181,182,183,186,191,206
0000300 KDOSEL 208,212,226,228,230,231,235,239,240,241,244,248,249,290,292
0000400 KDOSEL 305,306,507,308,309,310,311,312,313,314,315,316,317,318,319
0000500 KDOSEL 320,321,322,323,324,325,326,327,328,329,330,331,332,333,334
0000600 KDOSEL 335,336,337,338
0000700 KDOSEL 399
0000800 QUALIFY AIRLETT
0000900 AT 3(2);SET VAL(11, INITRO)=.73448,VAL(11,10XY)=.26552;DISPLAY VAL(11,INITRO),VAL(11,IOXY)
0001000 QUALIFY STAPRS
0001100 AT 320(2);DISPLAY 'INPUT PSI(1,1), THEN TYPE GO¹
0000000 PROCDEF C034
000100 KDOSEL 166,163,171,172,174,176,180,181,182,183,186,191,195,199,201
0000000 KDOSEL 166,168,171,172,174,176,180,181,182,183,186,191,195,199,201
0000300 KDOSEL 166,163,171,172,174,176,180,181,182,183,186,191,195,199,201
0000300 KDOSEL 305,306,307,308,309,310,311,312,313,314,315,316,317,318,319
0000600 KDOSEL 320,321,322,323,324,325,326,327,328,329,330,331,332,334,335
0000600 KDOSEL 330,321,322,323,324,325,326,327,328,329,330,331,332,334,335
0000600 KDOSEL 336,337,338
0000700 KDOSEL 376,237,338
0000700 KDOSEL 376,237,338
0000800 QUALIFY AINLETT
0000900 AT 3(2);SET VAL(11,INITRO)=.73448,VAL(11,IOXY)=.26552;DISPLAY VAL(11,INITRO),VAL(11,IOXY)
  C033
   CO 33
  C033
  Ç033
 CO33
 CO 33
CO 33
CO 33
 CO33
CO33
 CO34
CO34
CO34
 CO34
CO34
 CO34
 C034
C034
                                   0000900 AT 3(2);SET VAL(11, INITRO)=.73448, VAL(11, IOXY)=.26552;DISPLAY VAL(11, INITRO), VAL(11, IOXY)
0000000 PROCDEF CO36
  CO 34
 CQ36
  C036
                                    0000100 KDOSEL 60, 65, 66, 67,123,124,144,154,156,158,160,162,164,166,168,171,172,174,181
 C036
C036
                                    0030500 QUALIFY AINLETT
0CG0600 AT 3(2),SET VAL(11, INITRO)=.73%48,VAL(11, 10XY)=.26552;DISPLAY VAL(11, INITRO),VAL(11, IOXY)
C000000 PROCDEF C038
  C036
 CO36
                                COCCOOD PROCOSE CO38

CCOOLOG ROOSEL 60, 65, 66, 67,123,124,144,154,168,174,181,182,186,191,195,199,201,206,228

CCOOLOG ROOSEL 300,231,236,240,241,244,248,249,252,290,292,294,305,310,312,313

GCCOJOD ROOSEL 314,315,319,320

CCOGGGO ROOSEL 314,315,319,320

CCOGGGO ROOSEL 399

GCOCOOLOG ROOSEL 399

GCOCOOLOG ROOSEL 314,315,319,320

CCOGGGO ROOSEL 399

CCOCOCO QUALIFY AINLETT

CCOCOCOOLOG ROOSEL 320,241,241,181,180,-.73448,VAL(11,10XY)-.26552;DISPLAY VAL(11,INITRO),VAL(11,IOXY)

OCCOCOOLOG ROOSEL 65, 66, 67,124,137,139,141,158,165,168,178,181,182,195,199,200,201,206,208

GCCCOOLOG ROOSEL 65, 66, 67,124,137,139,141,158,165,168,178,181,182,195,199,200,201,206,208

GCCCOOLOG ROOSEL 226,230,249,252,289,290,292,294,305,313,314,315,320,329,399

DCCCOOLOG ROOSEL 65, 66, 67,124,137,139,141,158,165,168,178,181,182,195,199,200,201,206,226,230

CCOCCOO ROOSEL 249,252,268,289,290,292,294,305,313,314,315,319,320,329,399

CCOCCOO ROOSEL 249,252,268,289,290,292,294,305,313,314,315,319,320,329,399

CCOCCOO ROOSEL 249,252,268,289,290,292,294,305,313,314,315,319,320,329,399

CCOCCOO ROOSEL 262,65,66,74,124,137,139,141,158,165,168,178,181,182,195,199,200,201,206,226,230

CCOCCOO ROOSEL 269,252,268,289,290,292,294,305,313,314,315,319,320,329,399

CCOCCOO ROOSEL 62,65,66,74,124,137,139,158,166,168,172,179,181,182,183,187,100,195,199
 C038
C038
C038
 CO38
 C038
 C038
 CO38
CO52
CO52
 CO 52
 CO 52
 C054
  C054
 CO54
 CO54
                                   C000100 KD0SEL 62, 65, 66, 74,124,137,139,158,160,168,172,179,181,182,183,187,190,195,199
C000200 KD0SEL 201,296,226,230,248,249,252,289,290,292,294,305,313,314,315,320,321
C000300 KD0SEL 329
 CO57
CO57
 CO57
CO57
                                 0000400 XDOSEL 399
0000500 QUALIFY AINLETT
0000600 AT 3(2),SET VAL(11, INITRO)=.73613, VAL(11, IOXY)=.26387,DISPLAY VAL(11, INITRO), VAL(11, IOXY)
C000000 PROCDEF C060
0000100 KDOSEL 62, 65, 66, 74,124,137,139,158,160,168,172,179,181,182,183,187,190,195,199
0000200 KDOSEL 201,205,225,230,248,249,252,289,290,292,294,305,313,314,315,319,320
00003C3 KDOSEL 321,329
0000400 KDOSEL 329
C057
C057
 C060
 0300
C060
                                   0000500 QUALIFY AINLETT
0000500 AT 3(2);SET VAL(11, INITRO)=.73613, VAL(11, IOXY)=.26387;DISPLAY VAL(11, INITRO), VAL(11, IOXY)
 0800
                               000500 QUALIFY AINLETT
000600 AT 3(2);SET VAL(11, INITRO)=.73613, VAL(11, IOXY)=.26387;DISPLAY VAL(11, INITRO), VAL(11, IOXY)
000000 PROCDEF COB1
0000100 KDOSEL 62, 65, 66, 74,124,137,139,158,160,168,172,179,181,182,183,187,190,195,199
0000200 KDOSEL 201, 206, 226,230,248,249,252,289,290,292,294,305,313,314,315,319,320
0000300 KDOSEL 321,329
0000400 KDOSEL 321,329
0000500 QUALIFY AINLETT
000600 AT 3(2);SET VAL(11, INITRO)=.73928, VAL(11, IOXY)=.26072,DISPLAY VAL(11, INITRO), VAL(11, IOXY)
0000000 PROCDEF CO63
0000100 KDOSEL 62, 65, 66, 74,124,137,139,158,160,168,172,179,181,182,183,187,190,195,197
0000200 KDOSEL 199,201,206,226,230,248,249,252,289,290,292,294,305,313,314,315,319
0000400 KDOSEL 320,321,329
0000400 KDOSEL 320,321,329
0000400 KDOSEL 320,321,329
0000400 KDOSEL 320,321,329,399
0000500 QUALIFY AINLETT
0000600 KDOSEL 124,137,139,148,158,160,168,172,179,181,182,183,187,190,195
0000200 KDOSEL 62, 65, 66, 74
0000100 KDOSEL 124,137,139,148,158,160,168,172,179,181,182,183,187,190,195
0000200 KDOSEL 127,199,201,206,226,230,248,249,252,289,290,292,294,305,313,314,315
0000300 CKDOSEL 199,201,206,226,230,248,249,252,289,290,292,294,305,313,314,315
0000300 KDOSEL 199,201,206,226,230,248,249,252,289,290,292,294,305,313,314,315
0000300 KDOSEL 199,201,206,226,230,248,249,252,289,290,292,294,305,313,314,315
0000300 KDOSEL 199,201,206,226,230,248,249,252,289,290,292,294,305,313,314,315
0000000 ROCCEF CO65
0000100 KDOSEL 52, 65, 66, 74,137,139,181,182,183,187,188,190,195,197,199,201,206,226,230
0000100 KDOSEL 52, 65, 66, 74,137,139,181,182,183,187,188,190,195,197,199,201,206,226,230
0000100 KDOSEL 52, 65, 66, 74,137,139,181,182,183,187,188,190,195,197,199,201,206,226,230
0000100 KDOSEL 248,252,289,290,292,294,305,313,314,315,320,321,329,399
0000400 QUALIFY AINLETT
0000500 AT 3(2);SET VAL(11, INITRO)=.76751,VAL(11, IOXY)=.23249;DISPLAY VAL(11, INITRO),VAL(11, IOXY)
0000000 PROCCEF CO65
 C060
C061
C061
C061
C061
C051
 C063
C063
C063
C063
C064
C064
 C064
C064
C064
C064
C064
 C065
COSS
C065
C065
                                   0000500 AT 3(2);SET VAL(11, INITRO)=.76751, VAL(11, IOXY)=.23249;DISPLAY VAL(11, INITRO), VAL(11, IOXY)
                                  BODODOO PROCDEE CO69
C069
                                  0000100 KDOSEL 62, 65, 65, 74,137,139,181,182,183,187,190,195,197,199,201,206,226,230,248,252
0000200 KDOSEL 289,290,292,294,305,313,314,315,320,321,322,329,399
C059
                                  0000400 QUALLEY ALCII, INITRO)-.76479, VALCII, IOXY)-.23521; DISPLAY VALCII, INITRO), VALCII, IOXY)
```



```
0000100 KDOSEL 53, 62, 65, 66, 74,124,137,139,158,160,172,179,181,182,183,187,190,195,197,199
0000200 KDOSEL 201,206,226,230,248,249,252,289,290,292,294,305,313,314,315,320,321,322,329,399
CO71
C071
C071
C071
                                                               QUALIFY AINLETT
AT 3(2);SET VAL(11, INITRO)=.75452, VAL(11, IOXY)=.24548;DISPLAY VAL(11, INITRO), VAL(11, IOXY)
PROCDEF CO88
C071
C088
                                 0000600
                              0000000 PROCDEF CO88
0000100 KDOSEL 19, 22, 23, 54, 55, 60, 62, 64, 67, 74, 95,124,137,139,157,158,160
0000200 KDOSEL 162,165,166,169,170,171,172,173,174,175,176,177,178,179,181
0000300 KDOSEL 182,183,182,190,195,197,199,206,226,227,230,235,241,248,249
0000400 KDOSEL 250,252,278,289,290,292,294,305,313,314,315,320,321,329,349
0000500 KDOSEL 353,365,367,368,369,370,374,375,378,379,382,388,394,395,399
0000400 QUALIFY AINLETT
0000900 AT 3(2);SET VAL(11,INITRO)=.75328,VAL(11,IOXY)=.24672;DISPLAY VAL(11,INITRO),VAL(11,IOXY)
0001100 QUALIFY ANOZ
0001100 AT 360(3):SET DRAGEX==0.5*00AC;DISPLAY DRAGEX_PRAGEX_PSIATM_*DRAGEX = -0.5*00*AC*
 CO8 8
  CO88
 C088
 CO88
  C088
  C088
                                0001100 AT 350(3);SET DRAGEX=-0.5*Q0AC;DISPLAY DRAGEX,DRAGEX*PSIATM,DRAGEX = -0.5*Q0*AC*
0001200 QUALIFY CONVTA
0001300 AT 0;SET MY(65)=MY(53),MY(66)=MY(53);DISPLAY MY(55),MY(65),MY(66)
0001400 SETPS 123,0.690
  CO88
   CO88
   8300
   C088
                                 0001400 SETPS 123,0.690
0000000 PROCDEF CO89
   CO88
  C089
C089
                                 0000100 KD0SEL 54, 55, 60, 62, 64, 67, 74, 95,124,137,139,157,158,160,165,166,169
0000200 KD0SEL 172,175,176,179,181,182,183,187,190,195,197,199
0000300 KD0SEL 210,223,224,226,227,230,235,248,249,250,252,289,29C,292,294
   C089
   C089
   C089
                                 0000700 AT 3(2);SET VAL(11, INITRO)=.75148, VAL(11, IOXY)=.24852;DISPLAY VAL(11, INITRO), VAL(11, IOXY)
   C089
                                 0000800 QUALIFY CONVTA
0000900 AT 0;SET MV(65)=MV(53),MV(66)=MV(53);DISPLAY MV(53),MV(65),MV(66)
0001000 SETPS 123,0,690
0000000 PROCDEF CO90
   C089
                                 UUUUUUU PROCDEF CO90
0000100 KDOSEL 54, 55, 60, 62, 64, 67, 74,124,137,139,157,158,160,165,172,175,176
0000200 KDOSEL 179,181,182,183,187,190,195,197,199,202,203,206,207
0000303 KDOSEL 208,210,215,224,226,227,230,235,248,249,250,252,273,289,290
CO00400 KDOSEL 292,294,305,313,314,315,320,321,329
0000500 KDOSEL 399
   C089
   C090
   C090
   C090
                                COOGGO KDOSEL 292, 294, 305, 313, 314, 315, 320, 321, 329

OCCOSOR KDOSEL 399, 305, 313, 314, 315, 320, 321, 329

OCCOSOR QUALIFY AINLETT

OCCOTOC AT 3(2); SET VAL(11, INITRO)=.7389, VAL(11, IOXY)=.2611; DISPLAY VAL(11, INITRO), VAL(11, IOXY)

OCCOSOR QUALIFY CONVTA

OCCOSOR AT 0; SET MY(65)=MY(53), MY(66)=MY(53); DISPLAY MY(53), MY(65), MY(66)

OCCOSOR AT 0; SET MY(65)=MY(53), MY(66)=MY(53); DISPLAY MY(53), MY(65), MY(66)

OCCOSOR AT 0; SET MY(65)=MY(53), MY(66)=MY(53); DISPLAY MY(53), MY(65), MY(66)

OCCOSOR KOOSEL 54, 55, 60, 62, 64, 67, 74, 98, 124, 137, 139, 118, 157, 158, 160, 165, 172

OCCOSOR KOOSEL 175, 176, 179, 181, 182, 183, 187, 190, 195, 197, 199, 206, 208

OCCOSOR CHOSEL 226, 227, 230, 235, 224, 249, 250, 252, 289, 290, 292, 294, 305, 313

OCCOSOR CHOSEL 314, 315, 320, 321, 329, 399

OCCOSOR QUALIFY AINLETT

OCCOSOR CHOSEL 314, 315, 320, 321, 329, 399

OCCOSOR QUALIFY CONVTA

OCCOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR KDOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

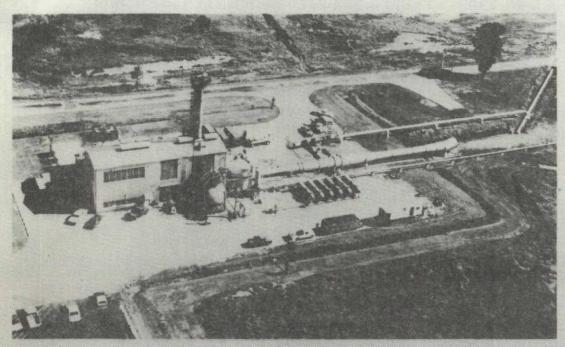
CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 266

CCOOSOR CHOSEL 197, 199, 206, 208, 226, 227, 230, 232, 248, 252, 265, 265, 266

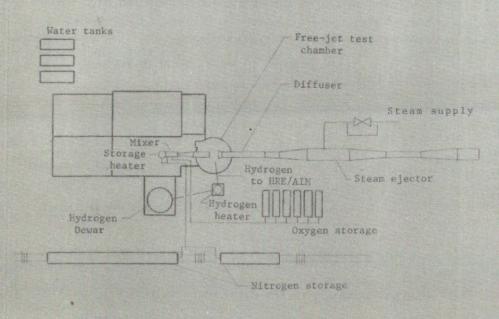
CCOOSOR CHOS
   C090
    C090
     C090
     C090
     C090
     C091
     C091
     C091
      C091
     C091
      C091
      C091
      C091
      C091
      C091
      CO91
      CO92
      C092
      C092
      C092
       C092
       CO92
        C093
        C093
                                       0000200 KDOSEL 96
        CO93
                                      0000000 AT 3(2);SET VAL(11, INITRO)=.655704, VAL(11, IOXY)=.344296;DISPLAY VAL(11, INITRO), VAL(11, IOXY)
0000700 TUNNOPT 3
0000000 PROCEEE CO94
0000100 COMACH5
        C093
        C093
C093
C094
         C094
                                        0000600 QUALIFY AINLETT

0000700 AT 3(2);SET VAL(11, INITRO)=.76284, VAL(11, IOXY)=.23716;DISPLAY VAL(11, INITRO), VAL(11, IOXY)

0000800 TUNNOPT 3
         C094
         C094
         C094
                                        0000000 PROCDEF C095
         C095
          C095
                                        0000100 QUALIFY AINLETT
0000700 AT 3(2);SET VAL(11, INITRO)=.7486, VAL(11, IOXY)=.25138;DISPLAY VAL(11, IMITRO), VAL(11, IOXY)
0000800 TUNNOPT 3
00000100 PROCDEF C096
0000100 COMACH5
          C095
          C095
          C095
          C096
         CO96 0000100 COMACHS
CO96 0000100 COMACHS
CO96 0000100 QUALIFY AINLETT
CO96 0000800 QUALIFY AINLETT
CO96 0000800 TUNNOPT 3
CO97 0000800 TUNNOPT 3
CO97 0000800 PROCEEF CO97
CO97 0000100 KDOSEL 54, 55, 60, 62, 64, 65, 66, 67, 74,124,137,139,181,182,183,187,190,195,197
CO97 0000200 KDOSEL 199,226,230,248,252,280,289,290,292,294,305,313,314,315,320,321,329,399
CO97 0000500 QUALIFY AINLETT
CO97 0000500 QUALIFY AINLETT
CO97 0000700 QUALIFY ANDZ
CO97 0000700 QUALIFY ANDZ
CO97 0000700 QUALIFY ANDZ
CO97 0000700 QUALIFY ANDZ
CO97 0000800 AT 360(3);SET DRAGEX=-0.5*QOAC;DISPLAY DRAGEX,DRAGEX*PSIATM, DRAGEX = -0.5*QO*AC*
CO97 0000800 AT 360(3);SET DRAGEX=-0.5*QOAC;DISPLAY DRAGEX,DRAGEX*PSIATM, DRAGEX = -0.5*QO*AC*
CO97 0000900 TUNNOPT 3
CO97 0001000 QUALIFY ACMBSTR
CO97 0001000 QUALIFY ACMBSTR
CO97 0001000 PROCEEF COMACHS
COMACHS 0000000 PROCEEF COMACHS
COMACHS 0000000 PROCEEF COMACHS
COMACHS 0000000 RDOSEL 54, 55, 60, 62, 64, 65, 66, 67, 74,124,137,139,157,158,160,162,165,172,176,179
COMACHS 0000000 KDOSEL 54, 55, 60, 62, 64, 65, 66, 67, 74,124,137,139,157,158,160,162,165,172,176,179
COMACHS 0000000 KDOSEL 313,182,183,187,190,195,197,199,206,226,230,248,249,252,280,289,290,292,294,305
          C096
```

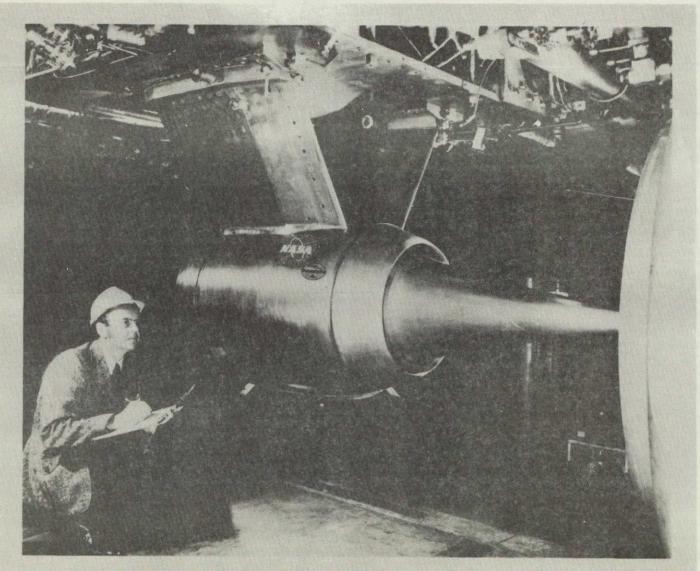


(a) Hypersonic Tunnel Facility (HTF).



(b) Schematic layout of the NASA - Lewis - Plum Brook Hypersonic Tunnel Facility (HTF).

Figure 1. - NASA - Lewis Research Center's Plum Brook Station Hypersonic Tunnel Facility (HTF) and the Hypersonic Research Engine/Aerothermodynamic Integration Model (HRE/AIM) installation.

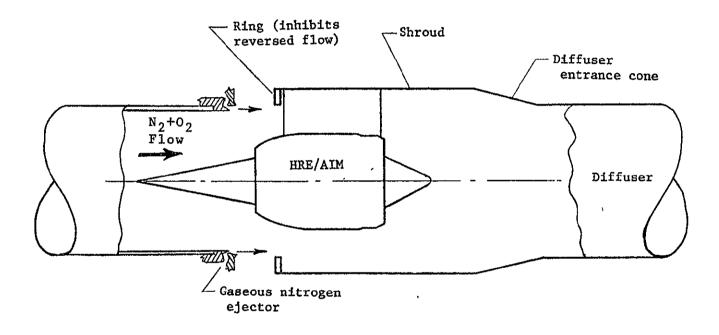


(c) HRE/AIM partically installed; pretest.

Figure 1. - Continued.

(d) HRE/AIM partically installed; Mach 5, 6, and 7 post test.

OF POOR QUALITY



(e) Schematic of HRE/AIM test section located in the free-jet test chamber of the HTF.

Figure 1. - Concluded.

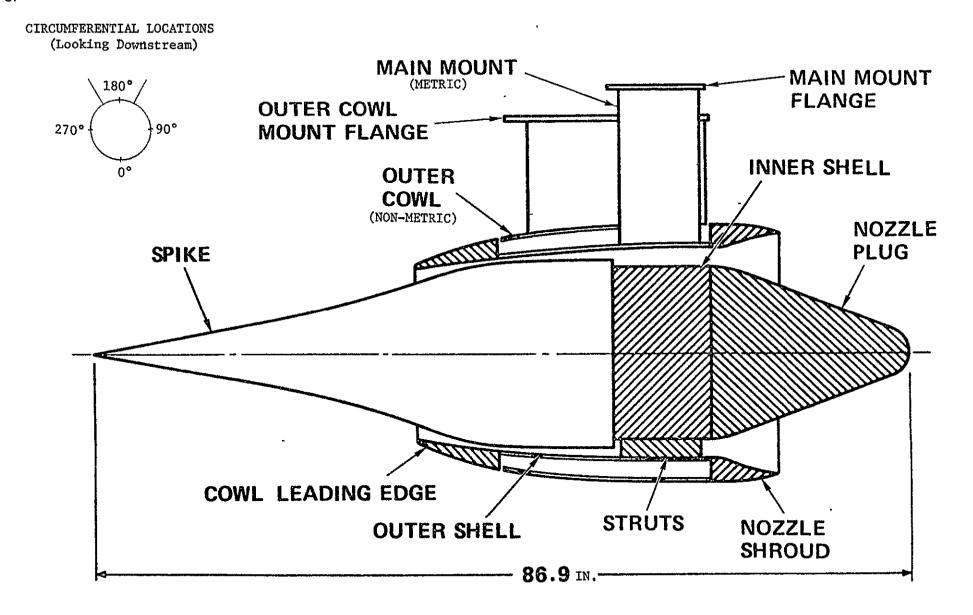
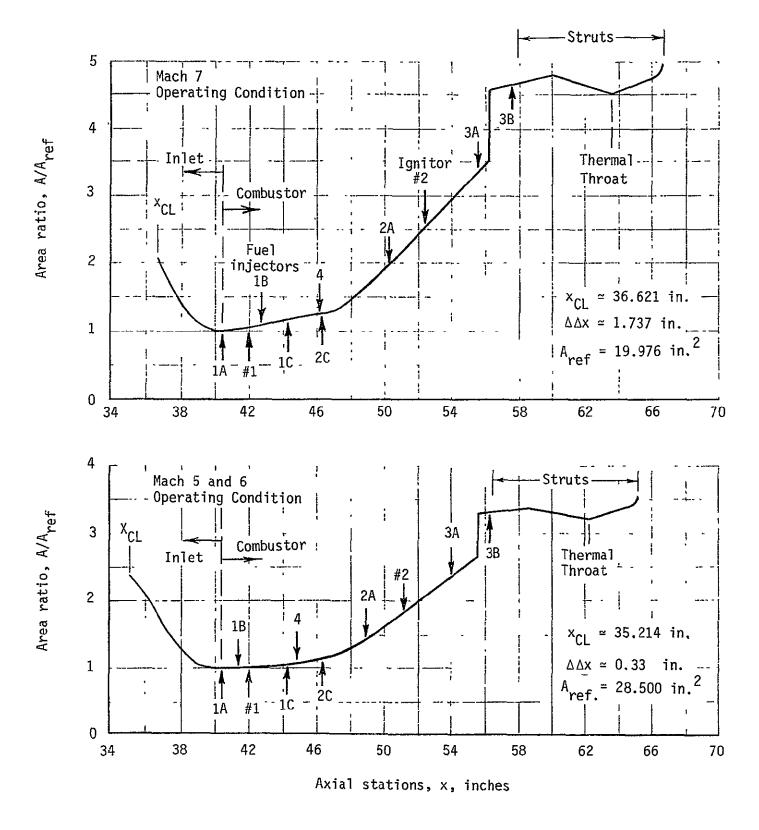


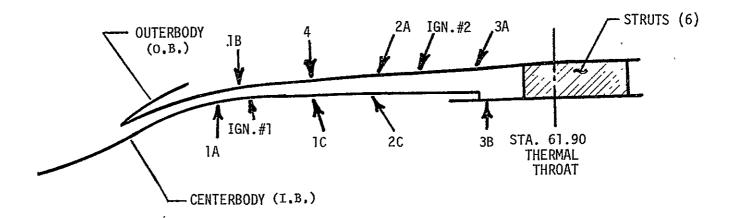
Figure 2. - General Configuration of the AIM



(a) Combustor area ratio distributions

Figure 3. - HRE/AIM combustor information.

COMBUSTOR CONFIGURATION



(Mach 6 position, $x_{CL} = 34.884$ in.)

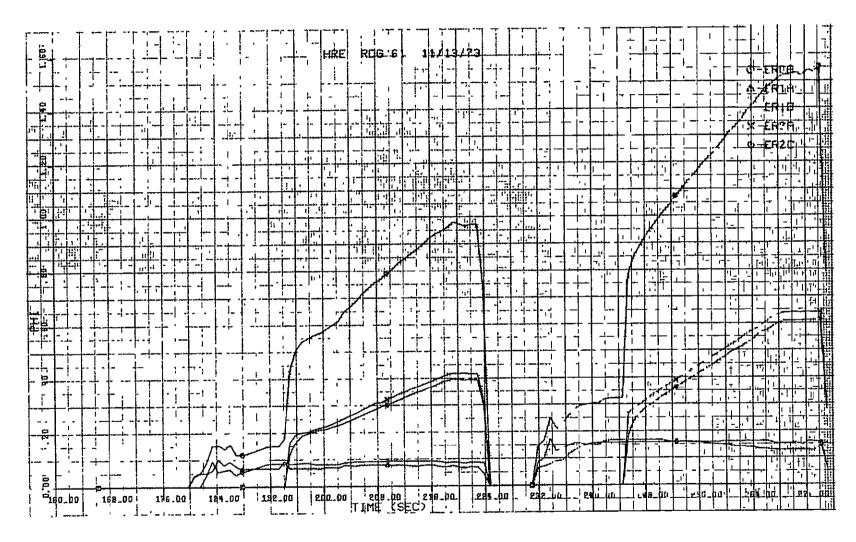
Injector	Number of Injectors	Diameter, in.	Injection Angle ^a , dec	<u>s/d</u>	x, in.	Location
1A	37	0.119	90	13.1	40.5	I.B.
18	37	0.119	90	13.9	41.25	0.B.
10	37	0.119	106	13.5	44.5	I.B.
4	37	0.119	90	14.2	44.5	0.B.
2A	60	0.095	67	11.4	48.5	0.B.
20	60	0.095	119	10.6	46.5	I.B.
3A	114	0.090	65	7.0	53.75	0.B.
3B	102	0.095	90	6.3	55.9	I.B.

IGNITOR PARAMETERS

Ignitor	x, in.	<u>(</u>			ial lo		<u>s</u>	Injection Angle ^a , deg.	Location
1°	42.00	55	110	165	230	290	350	94.5	I.B.
2	50.98	40	100	-	220	240	280	60.0 ^b	0.B.

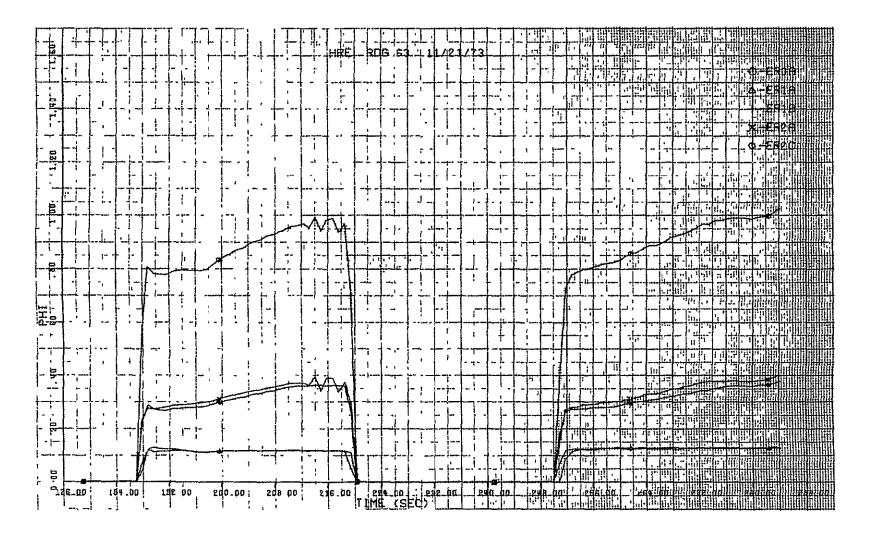
- a. With respect to AIM centerline.b. Also looking upstream, ignitors #2 are inclined 30° clockwise.
- c. Plug welded prior to reading 57.
 - (b) Combustor configuration and parameters.

Figure 3. - Concluded.



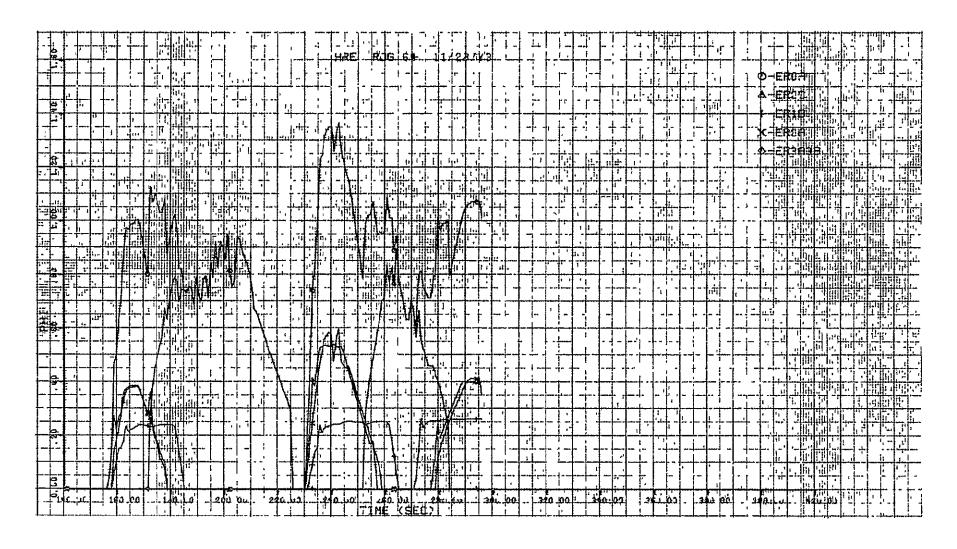
(a) Reading 61 - Measured Equivalence Ratio, ϕ

Figure 4. - HRE/AIM fuel equivalence ratio; Mach 6 engine performance results.



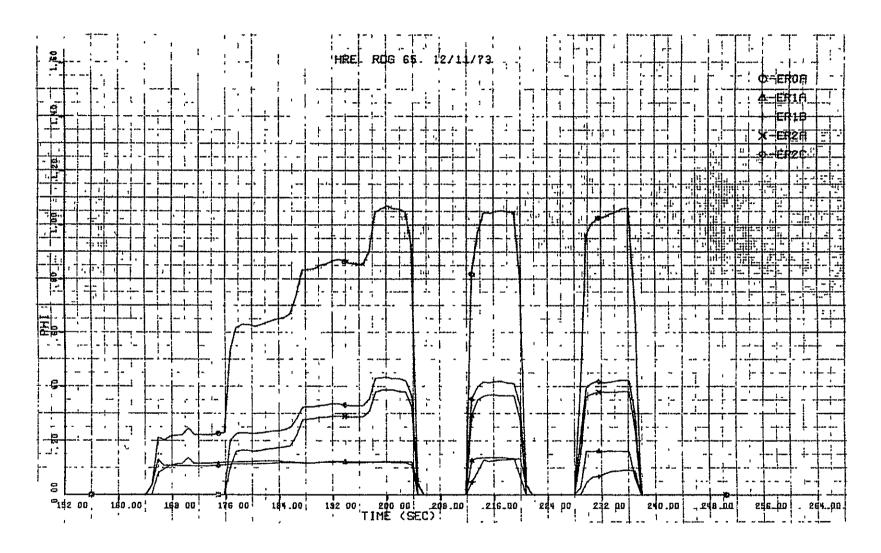
(b) Reading 63 - Measured Equivalence Ratio, ∅

Figure 4. - Continued.



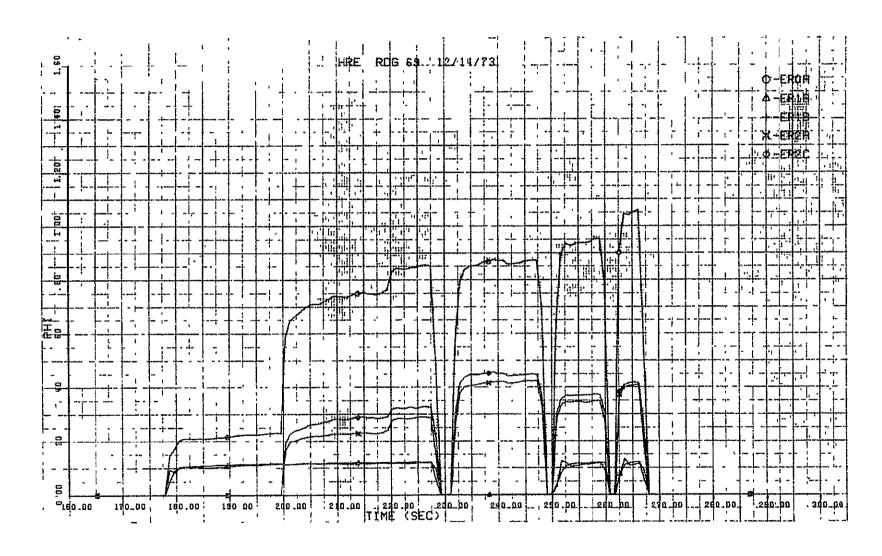
(c) Reading 64 - Measured Equivalence Ratio, ∅

Figure 4. - Continued.



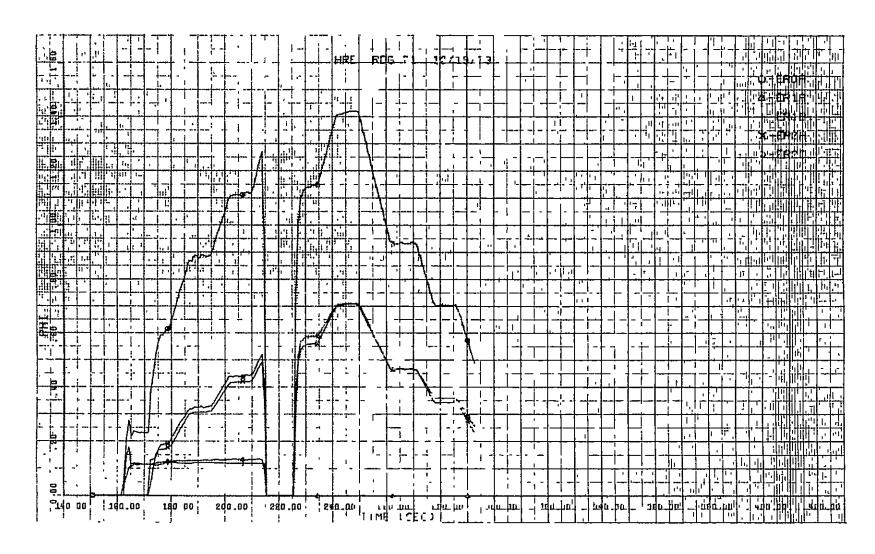
(d) Reading 65 - Measured Equivalence Ratio, ∅

Figure 4. - Continued.



(e) Reading 69 - Measured Equivalence Ratio, ϕ

Figure 4. - Continued.



(f) Reading 71 - Measured Equivalence Ratio, Φ

Figure 4. - Concluded.

Reading 61

t = 178.86 sec.

SUMMARY REPORT

			5 1	н н д	F Y	REI	20 8 1							
on p j	н	01464 40	MT CONS	N.A.C.W	u.C.	e	ul d k	W	4 4 4 5	MUMTH	Q	IVAC	But	ETAC
WIND TUNNEL 1	0 5	GAMMA MO	יאוטק וא.	мды	AET	S	W/A	ч	A/AC	j. On J.o.	4	1 440	r 0 1	E1#6
0.000 745.249 2998	668,9(794)	1_2020 28.1	155 25A0	1										
0.000 0.389 407	+31.3(98)				5919	1.827	0-10600	21.230	0.7820	3984	9.750	187.6		
SPIKE TIP NS 2	0 6	*****								• /				
0.600 15.675 2998	668,9(794)	1.2928 28.	54 2580)										
0.600 17.008 2935	649.8(775)				976	2.080	0.10600	21.230	0.7820	4051	1,608	190.8		
WIND TUNNEL 3	9 0													
0.000 745.249 2998	668,9(794)	1.2929 28.	755 2580	ļ.										
0.000 0.400 410	#30,5(98)	1.3989 28.	754 993	5,900	5916	1.827	0.10818	21.668	0.7620	4064	9.946	167.6		
SPIKE TIP NS 4	0 0				r									
0.600 18.675 2998	668,9(794)													
0.600 16.930 2931	648,9(774)	1.2949 28.	154 2553	0,392	1000	2,080	0,10815	21,668	0.7820	4064	1.681	187.6		
INLET THROAT 5	0 3													
40.400 307.275 2961 40.400 19.271 1512	657.9(783)				nen.	4 050	4 60513	21 270	0 07/4	7775	94 433	186.0		
INLET UPNASK 6	245.4(374)	1.3413 80*	and Tole	467	4544	1,004	1.00012	41.KJV	0.0764	2317	76,622	12410		
40.400 307.275 2961	657,9(783)	1 2040 28.	150 256E											
40.400 16.527 1453	229.7(359)				4629	1.884	0.98647	21.230	0.0840	3410	70.963	160.6		
INLET DNNRSK 7	0 4	***** ***	,		-0	••••	411-0-1		*****	W V				
40,400 140,460 2961	657.9(783)	1.2940 28.	954 2569	i										
40.400 120.028 2857	626,5(753)				1253	1.938	0.98647	21,230	0.0840	3410	19.212	160.6		
COMBUSTOR 0 8	1 3													
40,410 507.172 2961	657,9(783)													
40.410 19.270 1512	245.4(374)	1.5473 25.	754 1870	2,429	4543	1.884	1.08497	21,250	0.0764	3375	76.608	159.0		
COMBUSTOR 0 9	£ 3	4 30/2 00	184 1844											
40.841 301.878 2958	656,8(782)				/IEDD			24 220	A	774	74 407	455 5		
40.841 19.562 1522 COMBUSTOR 0 10	248.2(377)	1.3400 50	754 10/0	2 5 9 4 5 0	4366	14003	1.40000	21,230	040/01	2302	76.497	120.2		
41,331 277,602 2953	655,4(781)	1.2943 28.	954 2562	,			•							
41.331 20.243 1567														
• • • • • • • • • • • • • • • • • • • •					4448	1.890	1.07705	21.230	0.0770	3334	74.456	157-1		
COMBUSTUR 0 11	4 4			• -						•				
41.500 264.352 2951	654,9(780)	1.2944 28.	754 256	}										
41.500 20.658 1594	267.2(396)				4405	1.894	1.06990	21.230	0.0775	3316	73.235	150.2		
COMBUSTOR 0 12	5 4													
41.831 - 237.019 2948	653.9(779)													
41.831 21.571 1655	283.7(413)	1.3399 28.	954 195	2.200	4304	1.901	1.05147	21,230	0.0788	3276	70.338	154.3		
COMBUSTOR 0 13 42.460 183.440 2941	6 3	4 5047 50	16											
42,460 183,440 2941 42,460 23,945 1807	651.7(777)				4045	4 040	1 00777	14 770	0 5034	2470	47 550	1.45 E		
COMBUSTOR 0 14	325,2(454)	1,3332 60.	154 EV31	1 1 400	4042	1.410	1.003/2	<1.630	0.0828	51/4	63.054	144.5		
42.826 160.732 2936	650,3(776)	1.2948.28.	95# 25F											
42.826 25.778 1899	350.5(479)				2873	1.926	0.98531	21.230	0.0841	3111	59.305	144.5		
COMBUSTOR 0 15	8 4				30,5		*******	220	0 4 4 5 4 2		21,002			
42.891 157.326 2935	650,0(776)	1.2949 28.	954 2559	3										
42.891 26.060 1913	354.5(483)				3845	1.928	0.98134	21.250	0.0845	3101	58.639	146.1		
COMBUSTOR 0 16	9 5		- · ·	• •	-	-	· •			•				
44.310 119.142 2912	642.9(769)													
44,310 29,445 2093		1.3226 28.	954 218	1,584	3453	1,944	0.91035	21.230	0.0911	2965	48,851	139.7		
COMBUSTOR 0 17														
44,800 115,332 2903	640,2(766)	1,2959 28,	754 254	ļ 				. .						
44.800 29.501 2103 COMBUSTOR 0 18	407.6(536)	1,3222 28,	954 218	1.561	3411	1.946	0.89658	51.530	0,0924	2950	47.532	138.9		
		1 204// 30	95/ 95 ti	=										
	403.2(532)	1 2224 204	161 2 191 191 2 191) 1 (En4	7014	(0// 0	0 48777	71 274	0.007	3000	#7 A99	(7)) = 4		
		143660 501	794 E1/1	11200	3410	10202	A * a a l 3 i	C1 4 C 3 A	0 * 0 X 3 4	E7#4	47.027	1,000		

	READING #	0061	BLOCK	≅ 58	TIME =	178,86	S MACH	1 6.0	(Pl s	745	249 .	11 = 2997	7,0						,
		p	T	н		GAMPA	MOLWT	SONV	масн	VEL	s	4/A	٨	AZAC	нтион	Q	JVAC	PHI	ETAC
	COMBUSTOR			12 5		,													
				632.10					4 4 0 7			n (/ nor	24 272		\01 F	A. 706			
	46.260 COMBUSTOR				(255)	1.5241	28,424	2159	1,602	3400	1.444	0.66285	21.230	0.40401	4433	46,395	134.5		
				13 5 631,8(7581	1.2968	28.954	2530											
	46.326								1,606	3465	1.944	0.86053	21.230	0.0963	2956	46.335	139.2		
	COMBUSTOR	0	51	14 5						-	•								
				626.7(1 476	74.50	4 076	0 40070	21 240	0 1476	3070	44.275	4 /1 rs - 2		
	47.310 COMBUSTOR		55		(20%)	1+3500	60,434	5153	1.070	3004	1.944	0.80039	21.531	0.11720	27/7	44.513	14043		
				622,7(749)	1.2977	28,954	2518											
	48.110	20.730	1925	357.7((486)	1.3287	28.954	2095	1.758	3642	1.945	0.73492	21,230	0.1128	3002	41.590	141.4		
	COMBUSTOR			16 5			nu neu	25.4											
	48.851 3			619.1(338.9(
			•,	20-17	0-7	110010	101,124		1.818	3744	1.947	0,65632	21.230	0.1263	3033	38,190	142.8		
	COMBUSTOR	0	24								•	-							
	50.301			612.70					4 057	7010		A 53770	21 210	A 450 //	1046	*** ***	4 /1 E #		
	50.301 COMBUSTOR		25		(430)	1.3324	E0.424	1999	1.427	3910	1.731	0.53338	21.230	0.1004	2005	32.414	143.3		
	50.831			610.90	737)	1.2990	28,954	2501											
	50.831	11.505	1709	298.46	427)	1.3374	28.954	1981	1,996	3954	1.953	0,49883	21,230	0.1662	3099	30,656	146.0		
	COMBUSTOR		26			. 2005	35 05"	2005											
	52.241 52.241	9-080	1627	606,50	(/33) (465)	1,2777	20.424 20.424	1014	2.100	4066	1.054	0.42514	21.230	0.1950	3136	26,861	147.7		
	COMBUSTOR	7,000	27	20 5	0-,	113413	201754	. /	~	-000		0442314	# x # m m v	0 1 1 1 2 3	2120	*****	**(*)		
\dashv	54.341	77.419	2772	601,10	(728)	1.3000	28,954	2488											
	54.341				(379)	1.3463	28,454	1881	5,558	4190	1.959	0.34846	21.230	0.2379	3179	22,691	149.7		
\triangleright	COMBUSTOR 54.841		28 2768	500.00	7271	1.3002	28.954	2486											
	54.841								2.248	4208	1.960	0.33421	21.230	0.2480	3185	21.857	150.0		
	COMBUSTOR	٥	29	22 5															
\triangleright	55.59 ₁ 55.59 ₄			598.5(11 3 3 3		n 21EAE	31 370	0 5471	2 (0 %	20.724	150 //		
置	COMBUSTOR		30		367)	1.3404	C01724	1000	= 1 5 1 0	4623	1.70%	0.31505	E1 4E3A	0.5021	2173	200124	150.4		
	55.760			598.10	725)	1.3004	28,954	2483		•									
ᅜ	55.760 -	5,833	1489	239.20					5.585	4238	1.962	0.31104	21,230	0.2665	3194	20.485	150.5		
	COMBUSTOR 56,351			24 5	7 7 7 1 3		39 05/	2//42				`							
	56.351			597.0(220.20					2.393	4342	1.971	0.24373	21.230	0.3401	3235	16.445	152.4		
	COMBUSTOR	0	32	25 a	•			-				***	#	7 2 1 7 4			, = -,		
	57.776	62,502	2749	594.3	721)	1.3008	28,954	2478											
	57.776				(338)	1.3552	26,954	1789	2.054	4389	1.971	0.22531	51.530	0,3679	3251	15.369	153.2		
	COMBUSTOR 57.631		33 2749	26 4 594.2(7911	1.3008	28.954	247B											
	57.831								2.456	4391	1.971	0.22464	21.250	0.3690	3252	15.329	153.2		
	COMBUSTOR	. 0	34	27 4									•				• • • • •		
	57.971			594.00					3										
	57.971 COMBUSTOR			508.0((537)	1,1555	28.954	1/86	2.461	4595	1.971	0.62206	E1.530	0,3716	5253	15.235	153.2		
	58,051			593.8	(721)	1.3008	28,954	2477											
	58.051	3.746	1368	207.5						4397	1.970	0.22556	21,230	0.3675	3254	15.413	153.3		
	COMBUSTOR		36				50.55	 .											
	56,331 56,331	3.711	2746	593.3((720)	1,3009	28,954	2477	2.074	давл	1.070	0.22481	21.280	0 7497	1754	1 % 246	163 //		
ĊΠ.	COMBUSTOR		37		, 25-1	149990	LU1734	1101	L (~))	-404	19710	A # C C 4.0.7	E11530	V # 240 /	3630	15,585	1 3 3 4 M		
7	50.557			593.00	(720)	1,3009	28,954	2476											
	58.557	3.688	1357	204.6	(333)	1.3563	28.954	17/8				- مدن موجود							
									c.419	4468	1.969	0.22439	21.230	0.3694	3258	15.373	155.5		

2.4/9 4468 1.969 0.22439 21.230 0.3694 3258 15.373 154.5

GAMMA MOUNT SONV MACH VEL S W/A A/AC 4041H P IVAC PHI ETAC COMBUSTOR 0 38 31 CT 59.261 65,638 2741 591,8(719) 1,3011 28,954 2474 CO 59.281 3.590 1346 201.5(330) 1,3570 26.954 1771 2.496 4419 1.969 0.2208/ 21.230 0.3763 3261 15.169 153.6 COMBUSTOR 0 39 32 5 60.301 63.801 2736 590.4(717) 1.3012 28.954 2472 60.301 3.548 1339 199.8(329) 1.3574 28.954 1767 2.502 4421 1.969 0.21947 21.230 0.3777 3260 15.078 153.6 COMBUSTOR 0 40 33 62,311 64.618 2729 588.3(715) 1.3014 28.954 2469 62.311 3.711 1347 201.8(331) 1.3569 28.954 1771 2.483 4398 1.967 0.22710 21.230 0.3650 3249 15.522 153.0 COMBUSTOR 0 41 34 65.218 2725 587.1(714) 1.3016 28.954 2468 63,731 63.731 3.847 1354 203.6(333) .1.3565 28.954 1776 2.467 4380 1.966 0.23326 21.230 0.3553 3240 15.876 152.6 COMBUSTOR 0 42 35 66.195 60.092 2716 584.7(712) 1.3018 28.954 2464 66.195 3.702 1565 206.5(335) 1.3558 28,954 1782 2.441 4350 1.971 0.22110 21.230 0.3749 3226 14,947 152.0 COMBUSTOR 0 43 36 3 55.648 2715 584.3(711) 1.3019 28.954 2464 66,571 66.571 3,448 1366 206.8(336) 1,3558 28,954 1783 2,437 4346 1,976 0,20555 21,230 0,4032 3224 13,883 151.8 NOZZLE AL 44 37 88.807 55.648 2715 584.3(711) 1.3019 28.954 2464 88.807 0.309 705 40.6(170) 1.3939 28.954 1299 4.016 5216 1.976 0.04279 21.230 1.9371 3595 3.468 169.3 NOZZLE RO 45 38 88,807 55.648 2715 584.3(711) 1.3019 28.954 2464 88.807 0.389 752 52.2(181) 1.3919 28.953 1341 3.848 5160 1.976 0.04995 21.230 1.6593 3570 4.006 168.2 FICTIVE COMBUSTR 65 58 66.571 307.275 2715 584.3(711) 1.3018 28.954 2464 66.571 0.389 463 =17.8(111) 1.3991 28.954 1055 5.204 5489 1.858 0.08635 21.230 0.9599 3717 7.365 175.1 FICTIVE NOZZLE 66 59 88.807 74.045 2687 576.1(703) 1.3028 28.954 2452 88.807 0.266 616 19.0(148) 1.3969 28.954 1215 4.345 5280 1.953 0.04279 21.230 1.9371 3616 3.511 170.3

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KEADING	# VUE	i prof	K = 00	ATM	(E = 1/8 and) K	MACH I	5 • V	PI E /	45.	£44 #	241	11.0				PAGE 4
XABS		PNIB	P+0£	١	PDA		QUX		U#IB		0 ∞ 08		CAMALL	P=IB/PS0	P#IB/PTO	P=OB/PSo	P#OB/PTO
6.981E#	01 1	.040E 0		•	=4.547£=0	1 0	0.00		0.000		0.000		2.470E=02	2.675E 00	1.3966-03	0.000	0.000
1.836E		.040E U			-3.465E C		.000		0.000		0.000		1.634E 02	2.675E 00	1.3966-03	0.000	0.000
3.070E		.190E 0			■1.656E U		000		0.000		0.000		5.053E 02	5.634E 00	2.9391-03	0.000	0.000
3.508E		.893E 0			-3.627E C		0.00		0.000		0.000		6.804E U2	1.002E 01	5.224E-03	0.000	0.000
3.555E		960E U	0 0.000	}	-3.985E C		000		0.000		0.000		7.013E 02	1.019E 01	5.3146=03	0.000	0.000
3,606E		.870E 0			■4.382E C			0.2		02	0.000		7.246E 02	9.956E 00	5.1936-03	0.000	0.000
3.648E	01 4	.232E 0	0 0.000)	-4.729€ 0	2 -1	1.199E	02	-1-199E	0.2	0.000		7.443E 02	1.089E 01	5,678E=03	0.000	0.000
3.671E	01 4	.212E 0	0 5:694	F 00	#5,506f 0	2 -1	1.215E	02	•1.215E	0.2	0.000		7 551E 02	1.083E 01	5.6511-03	1.465E 01	7.640E=U3
3.671E	01 4	.211E 0	0 5.729	E 00	-5.507£ 0	2 -1	1.215E	02	-1.215E	0.2	0.000		7.554E 02	1.083E 01	5.651E-03	1.474E 01	7.688E=03
3.701E	01 4	.185E 0	0 7.490	E 00	-5.539L 0	2 -1	.236E	02	#1.236E	0.2	0.000		7.860E 02	1.077E 01	5.6164-03	1.927E 01	1.0036-02
3.73BE	01 4	.032E 0	0 9,700	E On	-5.512E 0	2 -1	1.264E	02	#1.264E	02	4.000		8.250E 02	1.037E 01	5.411E+03	2.495E 01	1.3026.02
3.803E	01 3	.745E 0	0 1.249	E 01	#5.30BE 0	5 -1	1.315E	02	#1.315€	02	0.000		6.950E 02	9.686E 00	5.052t=03	3.213E 01	1.6765=02
3.875E		.159E 0			-5,408E 0								9.751E 02	5.981E 01	1.555E=02	4.009E 01	2.091E=UZ
3.884E		.257E 0			-5.446E 0								9.854E 02	3.234E 01	1,687E=02	4.110E 01	5-144E-05
3.901E		#441E 0	1 1.684	E 01	-5,527E 0	2 -1	1.674E	0.2	#1 #449E	0.5	-2.251E	0 7	1.004E 03	3.707E 01	1,934E=02	4.333E 01	2.260E=02
3.950E		.861E 0			-5.770E 0								1.061E 03	4.788E 01	2,497E=02	4.981E 01	2.598£=02
3.986E		.677E 0			*5.815£ 0								1.102E 03	4.315E 01	2.2516-02	5.457E 01	2,8465=02
4.000E		.606E 0			-5.809E 0								1.118E 03	4.132E 01	2.155E=02	5.233E 01	2.7296=02
4.033E		.730E 0			-5,798E 0								1.157E 03	4.451E 01	5.351E=05	4.701E 01	2.4526=02
4.040E		.756E 0			-5.802E 0								1.16BE 03	4.517E 01	2.356E=02	4.719E 01	2.462E=U2
4.041E		760E 0			-5.801£ 0								1.166E 03	4.527E 01	2.361E=02	4.722E 01	2.463E=02
4.084E 4.133E		.921E 0			■5.809E 0								1.216E 03	4.9418 01	2.5778#02	4.833E 01	2.521Ep02
4.1502		.167E 0			-6.014E (1.274E 03	5.413E 01 5.576E 01	2.823E=02 2.908E=02	1.138E 01 1.080E 01	5,938E=03 5,631E=03
4.183E		.924E 0			-6.493E C								1.333E 03	7.523E 01	3.924E-02	9.647E 00	5.0326=03
4.246E		.365E 0			-7.386E 0								1.408E 03	1.123E 02	5.857E+02	8.950E 00	4.668E=03
4.283E		9528 0			-7.942E								1.452E 03	1.017E 02	5.303E=02	8.545E 00	4.457E-03
4.289E		.878E 0			-8.031E 0								1.460E 03	9.978E 01	5.204E-02	8.473E 00	4.420E=03
4.431E		275E 0			-9.134E 0							02	1 631E 03	5.852E 01	3.052E-02	3.130E 01	1.633E=U2
4.480E	01 1	.721E 0			-9.208E 0							02	1.690€ 03	4.428E 01	2.310E.02	3.918E 01	2.0446-02
4.561E	01 1	.569E 0	1 2.030	E 01	#9.131t 0	2 -7	.059E	02	=4.078E	02	#2.980E	0.2	1.789E 03	4.087E 01	2.132E=02	5.222E 01	2.7236-02
4.626E	01 1	.482E 0	1 1.841	E 01	-8.918£ 0	2 07	1.808E	02	-4.305E	02	-3.503E	02	1.869E 03	3.814E 01	1.9896-02	4.736E 01	2.470E=02
4.633E		472E 0			-8.897E 0								1.877E 03	3.7868 01	1.975E=02	4.687E 01	2.445E=02
4.731E		•311E 0			-8.504E 0								1.998E 03	3.372E 01	1.759E=02	3.950E 01	2,060E=02
4.811E		.444E 0			#8.[63£ 0								2.097E 03	3.714E 01	1.9376=02	3.352E 01	1.748E+U2
4.885E		.087E 0			-7.755E 0								2.189E 03	2.798E 01	1.459E#02	2.798E 01	1.459E=02
5.030E.		711E 0			-7.060E C								2.370E 03	1.984E 01	1.035E-02	1,984E 01	1.0358-02
5.083E 5.224E		-554E 0			+6.863E 0								2.437E 03	1.686E 01	8.795E=03	1.686E 01	8,795E=03
5.434E		.712E 0			-6.361E 0								2.6148 03	1.812E 01	9.452E=03	1.812E 01	9,452E+03
5.484E		.575E 0			-5.674E 0								2.681E 03	9.551E 00 9.197E 00	4.982E=03 4.797E=03	9.551E 00 9.197E 00	4.982E=03 4.797E=03
5.559E		-215E 0			-5.542E 0								3.040E 03	8,271E 00	4.3148.03	8.271E 00	4.3145=03
5.576€		134E 0			-5.515E 0								3.062E 03	8.061E 00	4.205E=03	8.061E DO	4.205E=03
5.635E		085E 0			=5.094E 0								3.102E 03	5 364E 00	2.798E=03	7.332E 00	3.8246=03
5.778E		958E 0			-4.887£ C								3.209E 03	7.610E 00	3,969E=03	7.610E 00	3,969E=03
5.783E		362E 0			-4.879E 0								3.216E 03	6.078E 00	3.170E=03	7.620E 00	3.975E=03
5.797E		.362E 0			=4.859E 0								3.234E 03	6.078E 00	3.170E-03	7.648E 00	3.9896=03
5.805E	01 2	.979E 0			#4.847E C								3 244E 03	7.663E 00	3.997E=03	7.663E 00	3.997E=03
5.833E		.000E 0			#4,808£ C								3,280£ U3	7.718E 00	4.025E=03	7.715E 00	4.0258=03
5.856E		.908E 0		E 90	-4,780E 0	2 -1	3516.1	03	-7.178E	02	■8.938E (02	3,309E 03	7,481E 00	3.902E=03	7.481E DO	3.902E=03
5.928E	01 5	*915E 0			-4.705E C								3.402E 03	6.721E 00	3.506£-03	6.721E 00	3.5066=03
6.030E		.875E 0			-4,653E (3.532t 03	4.824E 00	2.5162=03	4.824E 00	2.516E-03
6.231E		.250E 0			-4.649E 0								3.790E 03	3.216E 00	1.677E=03	3.216E 00	1.6778=03
6.373E		.462E 0			-4.649E 0								3.972E 03	6.335E 00	3.304E=03	6.335E 00	3.304Em03
6,619E	_	.69JE 0			. ₩4.649E 0								4.289E U3	9.499E 00	4.955E=03	9.499E 00	4.955E-03
6.657E	V1 2	.550E 0	n 7*880	F 00	*4.649£ 0	2 #1	L.797E	03	-7.784E	0.5	-1.018E	U 3	4.337E U3	6.560E 00	3.422E=03	9.982E 00	5.207E=03

	XABS	Pals	P⇔OB	PDA	QQX	Q≈IB	ଜ∞ମଞ	CAWALL	B=19/620	F=18/PT0	P=08/PS0	P#UB/PT0
	6,661E 01	2.550E 00	3.900E 00	=4.649E	02 -1.798E	03 #7.786L	02 #1.019E 03	4.342E U3	6.5608 00	3.4226=03	1.003E 01	5,233£#Ū3
ರಾ	6.681E 01	2.6516 00	4.000E 00	#4.649E	02 -1.8V2E	03 -7.799E	02 -1.022E 01	4.368E 03	6.820E 00	3,557£-03	1.029E 01	5.307E=03
	6.847E 01	5.490E 00	3.070E 00	~4.276E	02 -1.835E	03 -7.890E	02 -1.046E 03	4.583E 03	8.978E 00	4,683k≈03	7.898E 00	4.119E=03
	6.914E 01	2.487E 00	2.610E 00	-3.686k	02 -1.845E	03 -7.9196	02 w1.054E 03	4,665E U3	6.399E 00	3.338E=03	6.714E 00	3.502E+03
	6.991E 01	1.335E 00	2.031E 00	-3.105£	02 -1.857E	03 #7.949E	02 =1.062E 03	4.760E 03	3.434E 00	1.791E=03	5.225E 00	2.7266-03
	7.063E 01	1.219E 00	1.490E 00	-2.716E	02 -1.869E	03 =7.973E	02 -1,072E 03	4.848E 03	3,135E 00	1,6351-03	3.833E 00	1.999E=U3
	7.124E 01	1.120E 00	1.322E 00	-2.437E	02 -1.880E	03 -7.991E	02 -1.080E 03	4.9226 03	2.881E 00	1,503E=03	3.401E 00	1.774E=03
	7.219E 01	9.169E=01	1.060E 00	-2.085£	02 -1.897E	03 -8.016E	02 -1.095E 03	5.036£ Q3	2,359E 00	1.230E=03	2.727E 00	1.422E#03
	7.262E 01	0.250E=01	1.071E 00	-1,949E	02 -1.9U4E	03 -8.026E	02 -1.102E 03	5.088E 03	2.1226 00	1.107E=03	2.755E 00	1,437E=03
	7.415E 01	7.521E=01	1.110E 00	-1.508E	02 -1.926E	03 -8.057E	02 m1.120E 03	5.273E 03	1.935E 00	1,009E=03	2.856E 00	1.489E=03
	7.430E 01	7.450E=01	9.742E=01	=1,469£	02 -1.927E	03 #8.060E	02 -1-151E 03	5,290E 03	1.9176 00	9.997E=04	2.506E 00	1.307E=U3
	7.50SE 01	6.242E=01	2.950E-01	-1.247E	02 =1.937E	03 -8.0728	02 *1.130E 03	5.374E 03	1,606E 00	B.376E=04	7.589E=01	3.958E=04
	7.505E 01	6.236E-01	2.914E=01				02 *1.130E 03	5.375E 03	1.604E 00	8.367E=04	7.496E+01	3.910E=04
	7.638E 01	4.100E=01	0.000	-1.132E	02 -1.957E	03 ×8.091E	02 -1.148E 03	5.426E 03	1.0556 00	5.502E#04	0.000	0.000
	7.923E 01	8.000F=01	0.000	=8.905E	01 -1.961E	03 #8.123E	02 =1.148E 03	5.525E 03	2.058£ 00	1.073E=03	0.000	0.000
	8.313E 01	3.050E=01	0.000				02 -1.148E 03		7.846E=01	4.093E=04	0.000	0.000
	8.594E 01	3.650E=01	0.000				02 #1.148E 03		9.390E=01	4.898E=04	0.000	0.000
	8.880E 01	4,750E=01	0.000	=4.785E	01 -1.970E	3052.8- E0	02 =1.148E 03	5.707E 03	1.222E 00	6.374E=04	0.000	0,000
	8 8 8 6 1 E 0 1	4.752E=01	0.000	■4.785E	01 =1.9/0E	3052.8= £0	02 -1.148E 03	5,707E 03	1.223E 00	6.377E=04	0.000	0.000

×		DOKAL	CURAG		CF	HC
FEEEEEEEEEEEEEEEEEEE 014483584689101687118382385 000111222244506788002385		1.20E 02 2.1125E 01 9.105E 00 1.0575E 01 6.918E 00 1.2796E 00 1.2796E 00 1.2551E 00 1.2551E 01 1.356E 01 1.0569E 01 1.569E 01 1.569E 01 1.579	1.0317888888888888888888888888888888888888	00000000000000000000000000000000000000	20000000000000000000000000000000000000	2222222 00000 00000 000000 0000000 0000000
5.576E	01	1.095E 00	3.315E	05	2.451E=03	1.602E=02
5.635E	01	1.775E 00	3.333E	05	2.378&=03	1.208E=02
5.778E	01	4.043E 00	3.373E	05	2.343E=03	1.094E=02
5.783E 5.797E 5.805E 5.833E	01 01 01	2.533E=01 6.356E=01 3.663E=01 1.278E 00	3.376E 3.382E 3.386E 3.398E	20 20 20 20 20 20	2,342E=03 2,339E=03 2,332E=03 2,323E=03	1.091E=02 20=3100.1 20=3100.1
5.856E	01	1.029E 00	3.409E	05	2.316E+03	1.075E+02
5.928E	01	3.267E 00	3.441E	05	2.303E+03	1.051E+02
6.030E	01	4.545E 00	3.487E	05	2.295E+03	1.039E+02
6.231E 6.373E 6.619E 6.657F	01 01 01	9,055E 00 6,563E 00 1,126E 01 1,627E 00	3.577E 3.643E 3.756E 3.772E	20 20 20 20	2.2956=03 2.2946=03 2.3266=03 2.3546=03	1.0/6E=02 1.105E=02 1.004E=02 1.002E=02
6.661E	01	1.647E=01	3.773E	2005	2.342E=03	9.542E=03
6.681E	01	8.142E=01	3.782E		2.347E=03	9.755E=03
6.847E	01	6.873E 00	3.850E		2.348E=03	9.648E=03
6,914E 6,991E 7,063E	01 01	2.407E 00 2.286E 00 1.729E 00	3.874E 3.87E 3.915E	05 05 05	2.289E=03 2.209E=03 2.168E=03	7.9/9E=03 5.837E=03 4.943E=03
7.124E 7.219E 7.262E 7,415E	01 01 01	1.309E 00 1.824E 00 7.602E=01 2.636E 00	3.928E 3.946F 3.953E 3.980E	05 05 05	2.146E=03 2.105E=03 2.097E=03 2.090E=03	4.564Em03 3.879E=03 3.755E=03 5.696E=03
7,430E	01	2,385E=01	3.982E	20 20 20 20	2.075E=03	3.4/7E=03
7,505E	01	9,340E=01	3.992E		1.968E=03	2.154E=03
7,505E	01	1,415E=03	3.992E		1.967E=03	2.147E=03
7,638F	01	4.350E+01	3.996E	05	1.945E=03	1.969E=03
7,923E	01	1.014E 00	4.006E	05	2.045E=03	3.261E=03
8.313E	01	9.935E+01	4.016E	05	1.875E=03	1.552E=03
8.594E	01	3.751E=01	4.020E	20 20	1.894E=03	1.7/0E=03
6.680E	01	1.817E=01	4.022E		1.927E=03	2.153E=03
8.881E	01	0.000	4.022E		1.926E=03	2.154E=03

RAMJET PERFORMANCE

ក ស	ENGINE PERFORMANCE			INLET	
MEASURED THRUST CALCULATED SPECIFIC THEASURED SPECIFIC TO CALCULATED THRUST CO	IMPULSE	#462. (LBF) #689. (LBF=8EC/LBM) #462. (LBF=8EC/LBM) #689. (LBF=8EC/LBM) ,1848 ,2758	MASS FLOW RATIO ADDITIVE DRAG CO LIMITING PRESSUD DELTA PIZOCOCO TOTAL PRESSURE O TOTAL PRESSURE O	DEFFICIENT	0.0289 Y 0.1857 0.1390 (PSI) 0.4123
STREAM THRUST NET THRUST SPECIFIC IMPULSE	TIVE-COOLED ENGINE PERFOR	0. (LBF) 0. (LBF) 0. (LBF=SEC/LBM)	INLET PROCESS E KINETIC ENERGY : KINETIC ENERGY : ENTHALPY AT PO	FFICIENCY = SUBSONIC EFFICIENCY = SUPERSONI EFFICIENCY = SUBSONIC. = SUPERSONIC	0.9130 IC 0.9469
THRUST COEFFICIENT.		.0000			
	MOMENTUM AND FORCES			COMPRISION	
INLET MOMENTUM CHAN COMBUSTOR FRICTION COMBUSTOR STRUT DRA COMBUSTOR MOMENTUM NOZZLE FRICTION DRA NOZZLE STRUT DRAG.	GEAROORIA ARTESTERO W DRAG BERGERO BER	122,0 (LBF) 702,2 (LBF) 255,2 (LBF) 11,52 (LBF) =151, (LBF) 24,98 (LBF)	EQUIVALENCE RATE COMBUSTOR EFFICE TOTAL PRESSURE E COMBUSTOR EFFECE	IO444	0.000 0.000 0.1811
MUZZLE MOMENTUM CHA	NGEnevenanting	392. (LBF)		NOZZLE	
EXTERNAL FRICTION DE EXTERNAL PRESSURE 1 TOTAL EXTERNAL DRAG TOTAL STRUT DRAG OF CAVITY FORCE CALCULATED LOAD CEL	NTEGRALATARA PROPERTIES OF THE PROPERTY OF THE	1162, (LBF) 11.52 (LBF) 1020, (LBF) 2651, (LBF)	NOZZLE COEFFICIO PROCESS EFFICIES	HRUST COEFFICIENT = C8 ENT = CT	0.9588 1.0843
	STATIONS			FUEL INJECTORS	
SPIKE TRANSLATION INLET THROAT COWL LEADING EDGE NOZZLE SHROUD TRAIL NOZZLE PLUG TRAILINGTRUT LEADING EDGE SIRUT TRAILING EDGE	ING EDGE	34,884 (IN) 1,8307 (IN) 40,400 (IN) 36,715 (IN) 75,055 (IN) 88,807 (IN) 57,971 (IN) 66,571 (IN)	INJECTORS 18 10 2A 20 3A 3B 4	STATION 40,400 42,816 44,300 50,291 46,250 55,581 57,766 46,316	VALVE

Reading 61

t = 198.66 sec.

SUMMARY REPORT

								SU	и и А	RY	REF	ORT							
ð											•								
*	ſ	P	Ţ	н		GAMMA	MOLWT	SONV	MACH	VEL	5	W/A	lik	A/AC	MTMOM	Ġ	IVAC	PHI	ŁTAC
	MIND TUNNEL		1	0 5															
	0.000 744	999	2989	666.21	791)	1.2932	28.955	2576											
	0.000 0.	387	405	m31.7(97)	1.3989	28.954	986	5.993	5910	1.826	0.10592	21.279	0.7843	3986	9,728	187.3		
	SPIKE TIP NS		ے	0 6	· :						• •		_ , , , ,		•				
	0,600 18	700 2	2989	666,21	7911	1.2930	28.954	2576											
	0.600 17	045	2926	647.40	7731	1.2950	28.954	2551	0.380	971	2.079	0.10592	21.279	0.7843	4056	1.598	191.1		
	WIND TUNNEL	•	3	0 0						• • •					,				
		999	2989	666.21	7911	1.2932	28,955	2576											
	0.000 0.	401	409	-30 8	981	1.3989	28 954	991	5.959	5906	1.826	0.10852	21.800	0.7841	4082	9.959	187.2		
	SPIKE TIP NS	=	4	0 0					- • •	- 1 - 4	••••			.,					
	0,600 18	.700	2989	15.000	7911	1.2930	28.954	2576											
	0.600 16	951 2	2923	646.3(772)	1.2952	28.954	2550	0.392	999	2.079	0.10852	21.800	0.7843	4082	1,684	187.2		
	INLET THROAT		5	0 4						• •				*****		.,			
	40.400 376.	500 8	2920	645.4(771)	1.2953	28.954	2548											
	40.400 Zõ.	341	1550	255.6	384)	1.3453	28.954	1892	2.334	4416	1.887	1.08568	21.279	0.0765	3320	74.514	156.0		
	INLET UPNRSK		6	0 3							• • - • •	••••							
	40,400 276	.500 2	2920	645.4(7713	1.2953	28.954	2548											
	40.400 17	403	1489	239.3(368)	1.3486	28.954	1857	2.427	4508	1.887	0.98698	21.279	0.0842	3356	69.139	157.7		
	INLET DNNR8K		7	0 4	• •			• • •	- •	• • •	••••			.,					
	40,400 137	506 2	2920	645.4(7713	1.2954	28.954	2548											
	40,400 116	758	2812	613.20	700)	1,2988	28.954	2504	0.507	1269	1.935	0.98698	21.279	0.0842	3356	19.462	157.7		
	COMBUSTOR	Q	8	1 4								• • • • •				• • • • • • •	• • .		
		546		645.4(862)	1.2840	28,523	2663											
	40.410 28	455 2	2011	298.6(520)	1.3231	28.524	2154	1.934	4166	1.970	1.08778	21.323	0.0765	3319	70.420	155.6	0.06	0.85
	COMBUSTOR	0	9	2 202										-				•	•
	40.835 176	.361 .	3516	643.5(875)	1,2817	28.587	2677											
	40.835 41.	-644 8	5310	368.2(606)	1.3119	28.588	5596	1,617	3711	1.980	1.09145	21.323	0.0763	3273	62,954	153.5	0.06	1.00
	COMBUSTOR		10	3 21															
	41.325 153	.547	3209	641.21	873)	1.2819	28.586	2675											
		.780 2		350.6(588)	1,3139	28,587	8955	1.682	3813	1.989	1.08008	21.323	0.0771	3174	64.004	148.9	0.06	1.00
	COMBUSTOR		11	4 21															
		433		640.4	872)	1.2814	28,586	2673											
		•110 a			611)	1,3112	28.587	2305	1.584	3651	1.994	1.07268	21.323	0,0776	3117	60.856	146.2	0.06	1.00
	COMBUSTOR		12	5 21															
		.564		030.7[0713	1.2820	28,586	2671											
		834 8		371.50	624)	1.3091	28.587	2333	1.508	3517	5.004	1.05464	21.323	0.0789	3015	57.637	141.4	0.06	1.00
	COMBUSTOR		13	6 21	0.00														
		073					28.586												
	COMBUSTOR	538 2			95/1	1,5050	40.201	23/6	1.3/9	3278	5.051	1.00735	21.323	0.0859	2840	51.320	133.2	0.06	1.00
		.157 a	14	7 21	7.7.	4 300*	30 000												
		001		635,3((93)	1,6403	27.429	2276	4 404	****									
	COMBUSTOR		15	427,2(264)	1.3207	21,439	2201	1,404	3511	2.049	0.99180	21.572	0.0841	2758	49,494	129.0	0.13	0,11
		530 a		8 21	7-7.	4 7015	00 TB#	00/0											
		928			773)	1,3017	27 304	5200	4 423	*									
	COMBUSTOR		16	45783(2027	1.3540	\$1.030A	2633	1,463	3504	2.041	99092	21,3/2	0.0845	2756	49.423	159.4	0.13	0.02
		،753		9 21	7,0	1 3004	37 770	2844											
					5671	1 2042	27 172	2267	4 /1.54	7100	2 04.	0 00474	21 272		1345	40			
	COMBUSTOR	- 7 J F	17	10 21	2011	*****	611314	CC31	1 - 45 1	2124	4.041	0.98626	C1.3/2	0.0046	2/42	49.039	120.3	V . 1.5	V # Q Q
	44.310 69	. 162 :	2710	623.0(7671	1 707/	27.174	25/17											
	44.310 26	247	217#	450-87	「コーノ	1 7334	27.274	224/	(>##	2075	3 661	0 01604	34 273		3F / C				
	COMBUSTOR	1 1 Prior 6	18	11 21	2811	1.3221	E/#3/1	2203	1+503	とイコグ	E+V70	0.91581	c1,3/2	0.0411	2202	41.778	119.9	U.13	0,00
		. 80% :	2724	618.5(7-21	1 1070	27. 274	3500											
	44,800 25	487	2164	447.0	50//	1 2004	27.274	2240	1 351	2021	2 652	\$8009.0	24 775		35.01		445	4 =	
	70				2071	4	611310	2500	1,201	2756	E . U 3 /	V. TUUOK	61.3/6	0 4 0 A C 0	4546	40.906	11741	0.13	0.00

GAMMA MOLWE SONY MACH VEL S AZAC MOMTH Q IVAL PHI PTAC VI / A COMBUSTOR 0 19 12 21 45.605 68.043.2838 611.2(786) 1.2982 27.520 2580 45.605 31.348 2367 465.9(602) 1.3139 27.520 2370 1.148 2696 2.065 0.89268 21,372 0.0935 2542 37.40/ 118.9 0.13 0.19 COMBUSTOR 0 20 13 21 46.250 66,555 2666 611,3(783) 1.3072 25,631 2600 46.250 32.579 2247 475.61 6481 1.3213 25.631 2400 1.086 2607 2.163 0.87314 21.494 0.0961 2543 35.369 118.3 0.31 0.05 COMBUSTOR 0 21 14 21 46.260 67.960 2591 611.2(760) 1.3106 25.556 2570 46.260 32.596 2170 475.6(625) 1.3248 25.556 2365 1.102 2606 2.153 0.87275 21.494 0.0962 2544 35.342 118.3 0.31 0.01 COMBUSTOR 0 22 15 21 46.320 68.240 2578 610.7(756) 1.3112 25,545 2565 46.320 32.712 2159 475.50 621) 1.3254 25.545 2360 1.102 2601 2.151 0.86956 21.494 0.0965 2546 35.144 118.5 0.31 0.00 ROTAUBMOD 0 23 16 21 47.310 68,779 2548 601.4(746) 1.3122 25,544 2551 47.310 34.602 2158 475.9(621) 1.3254 25.543 2360 1.062 2506 2.147 0.80927 21.494 0.103/ 2593 31.519 120.7 0.31 0.00 COMBUSTOR 0 24 17 21 68.289 2525 593.9(738) 1.3130 25.543 2540 48 . 11n 48.110 34.526 2140 470.4(616) 1.3260 25.543 2350 1.058 2486 2.145 0.74329 21.494 0.1129 2659 28.719 125.7 0.31 0.00 COMBUSTOR 0 25 18 21 48.845 68,010 2506 587.0(732) 1,3136 25,546 2531 48.845 33.675 2113 461.0(607) 1.3270 25.546 2336 1.075 2511 2.142 0.66448 21.494 0.1263 2767 25.933 128.7 0.31 0.00 COMBUSTOR 0 26 19 50.285 63,276 2444 582,1(759) 1,3173 23,936 2586 50.285 20.633 1853 383.2(561) 1.3385 23.936 2270 1.390 3154 2.253 0.54397 21.623 0.1552 2940 26.665 136.0 0.49 0.03 COMBUSTOR 0 27 20 50.295 63.292 2443 582.0(758) 1.3174 23.935 2586 50.295 20.542 1850 382.5(540) 1.3386 23.935 2268 1.393 3160 2.253 0.54326 21.623 0.1554 2941 26.674 136.0 0.49 0.03 COMBUSTOR 0 28 21 21 50.825 65.343 2378 578.9(737) 1.3202 23.884 2557 50.825 15,742 1666 341,5(500) 1,3469 23,884 2161 1,595 3446 2,242 0,5080/ 21,623 0,1662 2986 27,212 138,1 0,49 0,00 COMBUSTOR 0 29 22 52.235 55.622 2618 571.4(815) 1.3090 24,126 2657 52.235 15,375 1915 333.0(578) 1,3339 24,126 2294 1,506 3454 2,282 0,43302 21,623 0,1950 3089 23,243 142,9 0,49 0.11 COMBUSTOR 0 30 23 4 54.335 51,259 2730 561,3(852) 1,3035 24,260 2700 54.335 11.437 1900 279.4(571) 1.3329 24.260 2278 1.649 3756 2.298 0.35491 21.623 0.2379 3221 20.715 149.0 0.49 0.17 COMBUSTOR 0 31 24 54.835 51.166 2725 559,2(850) 1.3036 24.261 2698 10.492 1857 264.8(557) 1.3346 24.261 2254 1.703 3838 2.298 0.34040 21.623 0.2480 3246 20.304 150.1 0.49 0.17 54.835 COMBUSTOR 0 32 25 3 55.585 50.623 2730 556.1(851) 1.3033 24.274 2699 55.585 9.434 1817 246.9(544) 1.3361 24.274 2230 1.764 3933 2.299 0.32088 21.623 0.2631 3279 19.615 151.7 0.49 0.17 COMBUSTOR 0 33 26 55.760 50.606 2728 555.5(851) 1.3034 24.274 2699 9.187 1803 242.6(540) 1.3366 24.274 2222 1.781 3957 2.299 0.31666 21.623 0.2666 3286 19.471 152.0 0.49 0.17 55.760 COMBUSTOR 0 34 27 56.345 42.177 2913 553.3(912) 1.2946 24.460 2769 56.345 7.282 1917 212.6(574) 1.3299 24.461 2276 1.814 4129 2.329 0.24824 21.623 0.3401 3409 15.928 157.7 0.49 0.25 COMBUSTOR 0 35 28 57.770 44.464 2847 548.6(890) 1.2976 24.408 2743 57.770 5.880 1747 176.1(520) 1.3375 24.408 2182 1.979 4317 2.319 0.22944 21.623 0.3679 3455 15.393 159.8 0.49 0.23 0 36 29 COMBUSTOR 57.825 39.901 2984 548.4(935) 1.2910 24.544 2793 57.825 6.717 1958 196.1(587) 1.3273 24.545 2294 1.830 4199 2.339 0.22880 21.623 0.3690 3457 14.930 159.9 0.49 0.29 COMBUSTOR 0 37 30 O 57,965 40.003 2977 548.00 933) 1.2914 24.538 2791 CT 57.465 6.595 1943 193.1(582) 1.3280 24.539 2286 1.843 4214 2.338 0.22715 21.623 0.3717 3460 14.875 160.0 0.49 0.29

GAMMA MOLHT SONV MACH VEL S A/AC PUPIM R IVAC PhI ETAC M/A COMBUSTOR 0 58 31 11 on 58,045 48.218 2775 547.8(866) 1.3009 24.341 2715 O 58.045 5.400 1627 161.8(482) 1.3437 24.341 2113 2.080 4395 2.306 0.22978 21.623 0.3674 3462 15.694 160.1 0.49 0.20 COMBUSTOR 0 39 32 58,325 52.583 2703 547.0(842) 1.3042 24.274 2687 58,325 4,912 1507 147,7(445) 1,3505 24,274 2041 2,190 4470 2,292 0,22894 21,623 0,3688 3468 15,903 160.4 0,49 0,17 COMBUSTOR 0 40 33 58,551 58.209 2628 546.4(817) 1.3076 24.204 2657 58.551 4.446 1383 134.3(407) 1.3578 24.204 1964 2.312 4541 2.277 0.22855 21.623 0.3694 3472 16,128 160.6 0.49 0.14 COMBUSTOR 0 41 34 59.275 92.768 2374 544.7(734) 1.3193 23.971 2549 59,275 2.950 968 92,2(282) 1.3826 23.971 1666 2.856 4759 2.210 0.22496 21.623 0.3753 3482 16.637 161.0 0.44 0.04 0 42 35 COYBUSTOR 60,295 32,956 3393 542.4(1072) 1,2698 24,982 2928 60,295 9.000 2543 237.5(776) 1,3007 24.988 2565 1,523 3905 2,382 0.22353 21,623 0,3777 3495 13,566 161.6 0.49 0.47 COMBUSTOR 0 43 36 62.305 33.470 3445 537.0(1090) 1.2667 25.054 2943 62.305 9.725 2625 240.8(803) 1.2969 25.061 2599 1.481 3850 2.383 0.23131 21.623 0.3650 3496 13.839 161.7 0.49 0.50 COMBUSTOR 0 44 37 63,725 32,033 3664 532.9(1163) 1.2535 25,304 3004 12.262 2993 282.5(926) 1.2805 25.319 2743 1.290 3540 2.397 0.23758 21.623 0.3553 3495 13.069 161.6 0.49 0.61 63,725 COMBUSTOR 0 45 38 66,189 29.381 3806 524.4(1211) 1.2436 25.490 3038 66,189 13,653 3268 317.3(1019) 1,2672 25.510 2841 1.133 3219 2.409 0.22520 21,623 0.3749 3493 11.264 161.6 0.49 0.68 COMBUSTOR 0 46 39 3 66,565 27,133 3843 522,9(1224) 1,2405 25,537 3047 66.565 13.948 3365 336.5(1053) 1.2623 25.559 2874 1.062 3054 2.417 0.20936 21.623 0.4032 3493 9.937 161.5 0.49 0.70 COMBUSTOR REGEN 47 40 21 66.565 27.133 4141 650,7(1333) 1,2228 25,499 3142 66,565 12.447 3574 416.8(1127) 1.2515 25.550 2950 1.160 3421 2.449 0.20936 21.623 0.4032 3585 11.131 165.8 0.49 0.70 NOZZLE ΑE 48 41 88.801 27.133 3843 522.9(1205) 1.2405 25.537 3047 86.801 0.739 1720 -220.5(497) 1.3265 25.568 2106 2.911 6132 2.417 0.04358 21.623 1.9371 4487 4.153 207.5 0.49 0.70 NOZZLE 49 42 4 88.801 27.133 3843 522.9(1205) 1.2405 25.537 3047 88,801 0.387 1463 #308.2(417) 1.3401 25.568 1953 3.302 6449 2.417 0.02824 21.623 2.9900 4631 2.830 214.2 0.49 0.70 NOZZLE AE REGEN 50 43 88.801 27.133 4141 650.7(1333) 1.2228 25,499 3142 86.601 0.803 1940 -158.0(567) 1.3167 25.568 2229 2.854 6362 2.449 0.04358 21.623 1.9372 4674 4.308 216.2 0.49 0.70 NOZZLE' PO REGEN 51 44 4 88.801 27.133 4141 650.7(1333) 1.2228 25.499 3142 88.801 0.387 1623 #258.9(467) 1.3313 25.568 2050 3.291 6746 2.449 0.02663 21.623 3.1698 4849 2.792 224.2 0.49 0.70 FICTIVE COMBUSTR 71 64 66.565 276,500 4473 522.9(1440) 1,2165 26,283 3208 66.565 0.387 1016 =688.5(279) 1.3610 26.360 1615 4.821 7786 2.257 0.05062 21.623 1.6679 5398 6.124 249.6 0.49 1.00 FICTIVE NOZZLE 72 65 88,801 17.805 3789 502,0(1204) 1.2412 25.537 3026 88,801 U.910 1970 -148.3(577) 1.3154 25.568 2245 2,541 5704 2.444 0.08358 21.623 1.9371 #285 3.864 198.2 0.49 0.70

XABS	P=IB	P=OB	POA	Q O x	UwIB		ខ⇔ព្ន	CAWALL	P=IH/PSO	P=IB/PTO	P=08/PS0	P=08/P10
6.981E+01		0.000	-4.553E-01	0.000	0.000		0.000	2.4706-02	2.712E 00	1.409E=03	0.000	0.000
1.836E 01	1.050£ 00	0.000	-3.498E UI	0.000	0.000		0.000	1.6346 02	2.712E 00	1.409E=03	0.000	0.000
					,			5.053E 02	5.733E 00	2.960E=03		
3.070E 01	S. 220E 00	0.000	■1.675E 02		0+000		0.000				0.000	0.000
3.508E 01	3.922E 00	0.000	-3.666E 02	0.000	0.000		0.000	6.804E 02	1.013E 01	5.265E=03	0,000	0.000
3.555E 01	4.015E 00	0.000	-4. 028€ 02	0.000	0.000		0.000	7.013E 02	1.037E 01	5.389E=03	0.000	0.000
3,606E 01	3,925E 00	0.000	-4.430E UZ	-2.5/3E	02 =2.573E	0.2	0.000	7.246E 02	1.0148 01	5.268E=03	0.000	0.000
3.648E 01	4.247E 00	0.000	■4.780E 02	-2.635E	02 -2.635 E	02	0.000	7.443E 02	1.097E 01	5,701E=03	0.000	0.000
3.670E 01	4.231E 00	5.672E 00	-5.551£ 0≥	-2.669E	02 -2.669E	0.5	0.000	7.548E 02	1.093E 01	5.680E-03	1.465E 01	7.614E=03
3.671E 01	4.231E 00	5.706E 00	-5.552E 02	-2.6/0E	02 -2.670E	0.2	0.000	7.551£ 02	1.093E 01	5.679t-03	1.474E 01	7.6625+03
3.701E 01	4.210E 00		₩5.586E 02				0.000	7.864E 02	1.087E 01	5.651E#03	1.935E 01	1.006E=02
3.737E 01	4.071E 00		-5.563E 02				0.000	8.247E 02	1.051E 01	5.464E-03	2.492E 01	1.2956-02
3.803E 01	3.820E 00		-5.362E 02				0.000	8 953E 02	9 865E 00	5.1286-03	3.231E 01	1.679E=02
3.875E 01												2.101E=02
	1.1516 01		=5.465E 02					9.754E 02	2.971E 01	1.5446.02	4.043E 01	
3.883E 01	1.241E 01		-5.506E 02					9.850E 02	3.204E 01	1,6666-02	4,138E 01	2,151E=02
3.901E 01	1.428E 01		=5,579E 02					1.005E 03	3.688E 01	1.917E=02	4.366E 01	2.269E=02
3.950E 01	1.854E 01		*5.816E 02					1.061E 03	4.787E 01	2.488£#02	5.002E 01	2.600E=02
3.985E 01	2.278E 01	2,115E 01	=5.943£ 02	#3.951E	02 #3.640E	02	-3.110E 01	1,102E 03	5.884E 01	3.058E=02	5.462E 01	2,839E=V2
4.000E 01	2.452E 01	2.021E 01	-6.008€ 02	₩4.075E	02 #3.743E	02	-3.316E 01	1.119E 03	6.333E 01	3.2926=02	5.218E 01	2.7126=02
4.032E 01	3.351E 01	1.810E 01	-6.270E 02	04.305E	02 #3.988E	0.2	-3.774E 01	1.156E 03	6.654E 01	4.498E=02	4.674E 01	2.430E=02
4.040E 01	3.559E 01	2.069E 01	+6.349E 02	-4.434E	02 #4.046E	02	-3.880E 01	1.105E 03	9.192E 01	4.778E=02	5.344E 01	2.778E=02
4.041E 01	3,587E 01		-6.357E 02					1.166E 03	9.264E 01	4.815E=02	5.433E 01	2.824E=02
4.083E 01	4.762E 01		-6.720E 02					1.216E 03	1.230E 02	6.3936+02	9.210E 01	4.7875-02
4.132E 01	6.119E 01		₽7.608E 02					1 274E 03	1.580E 02	8.213E-02	1.130E 01	5.872E-03
4,150E 01	6.604E 01		-8.140E 02					1.294E 03	1.705E 02	8.8648.02	1.080E 01	5.614E=03
4.182E 01	6.384E 01		-9.100E 02					1.333E 03	1.649E 02	8,570E=02	9.878E 00	5.134E+03
4.246E 01	5.955£ 01		=1.072E 03					1.408E 03	1.538E 02	7,9936+02	9-104E 00	4.732E-03
4.281E 01	5.464E 01		-1-147E 03					1.450E 03	1.411E 02	7.334E=02	8.678E 00	4.511E=03
4.282E 01	5.450£ 01		-1,149E 03					1.451E 03	1.407E 02	7.316E=02	8.666E 00	4.5048=03
4.288E 01	5.359E 01		-1.195E 03					1.459E 03	1.384E 02	7,193E=02	8-587E 00	4,463E=03
4.431E 01	3.358E 01		-1,318E 03					1.631E 03	8.672E 01	4.507E=02	4.885E 01	2,5396+02
4.480E 01	2.670E 01		-1.327E 03					1.640E 03	6,895E 01	3.5846-02	6.369E 01	3,258E-02
4,560E 01	2.962E 01	3.307E 01	#1.319E 03	-1,233€	03 ~8. 326E	0.5	-3.999E 02	1.789E 03	7.650E 01	3,976E+02	8,541E 01	4.4405-02
4.625E 01	3.196E Q1	5.319E 01	=1.292E 03	-1,358E	03 =8.736E	02	■4.848E 02	1.868£ 03	8.255E 01	4,291E=02	8.572E 01	4.456E=02
4.626E 01	3.200E 01	3.320F 01	-1.291E 03	#1.360E	03 #8.742E	0.2	-4.861E 02	1.869E 03	8.264E 01	4.295E=02	8.573E 01	4.486E=02
4.632E 01	3,222E 01		-1.288E 03					1.876E 03	8.320E 01	4.324E=02	8.576E 01	4.4576-02
4.731E 01	3.581E 01		#1.228E 03					1.998E 03	9.248E 01	4.807E-02	8.623E 01	4.482E=02
4.81 E- 01	3.551E 01		-1.153E 03					2 097E 03	9.171E 01	4.767E=02	6.661E 01	4.502E=02
4.884E 01	3.367E 01		-1.038E 03					2.189E 03	8.696E 01	4.520E=02	6,696E 01	4.520E=02
5.028E 01	2.063E 01		-8.360E 02					2.369E 03	5.328E 01	2.769E=02		
5.029E 01	2.054E 01										5.328E 01	2,769E=02
		4 5744 04	-8.349E 02	A241512	03 2141056	0.3	#1 0 1 E E D 3	2.370E 03	5.305E 01	2.757E=02	5.305E 01	2.757E-02
5,082E 01	1,5748 01		■7.848£ 02					2.437E 03	4.065E 01	2,1136-02	4.065E 01	2,113E-02
5.223E 01	1,5376 01		-6.697E 02					2,614E 03	3.971E 01	2.064E+02	3.971E 01	2.064E-02
5.433E 01	1.144E 01		-5.221£ V2					2,880E 03	2.954E 01	1,535t=02	2.954E 01	1.535E-V2
5.483E 01	1.049E 01		-4.936E 05					2.944E 03	2.709E 01	1.408E=02	2.709E 01	1.4085-02
5,558E 01	9,434E 00	9.434E 00	=4.551E U2	a5.000E	03 =1.330E	03	-1.356E 03	3.040E 03	2.436E 01	1.266E=02	2.436E 01	1.2665-02
5.576E 01	9,187E 00	9.187E 00	■4.467E 02	-2.700E	03 -1-336E	03	-1.365E 03	3.062E 03	2.372E 01	1.233E=02	2.372E 01	1.233E#02
5.634E 01	6.201E 00	8.362E 00	-3.221E 02	₩2.747E	03 -1.355E	03	-1.392E 03	3,1028 03	1.601E 01	8.324E+03	2.160E 01	1.122E=02
5.777E 01	5.880E 00		-2.714E 02					3.209E 03	1.518E 01	7.892E-03	1.518E 01	7.892E=03
5.782E 01	7.650E 00		-2.698E 02					3,2166 03	1.976E 01	1.027t=02	1.494E 01	7.763E=03
5.796E 01	7.650E 00		#2.661E 02					3.234E 03	1.976E 01	1.027E-02	1.431E 01	7.436E=03
5.804E 01	5.400E 00		-2.639E 02					3.244E 03	1.395E 01	7.249E=03		7.249E=03
5.832E 01	4.912E 00										1.395E 01	
5.855E 01	4.446E 00		#2.572E 02					3.280E 03	1.269E 01	6.594E=03	1.269E 01	6,594E=03
			-2.526E 02					3.309E 03	1.148E 01	5.9676-03	1.148E 01	5.967E+03
5.927E 01	2,950E 00		-2.426E 02					3.402E 03	7.618E 00	3,960E+03	7.618E 00	3.960E=03
6.029E 01	9.000E 00		45.581£ 05					3.532E 03	2.324E 01	1.2086=05	2.324F 01	1.208E=02
6.230E 01	9.7256 00	7.725F 00	-2.265E UZ	*7.100E	05 -1.489E	0.5	=1.611E 05	3.790E U3	2.511E 01	i.305E+02	2.511£ 01	1,305E=02

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XABS	P≈I8	Р≖ОВ	PDA	Q O X	Q≈1B	G=08	CAMALL	P-18/P80	P=18/P10	P=08/PS0	-P=08/P10
6.372E 01	1.226E U1	1.559E 01	-2.265t 02	-3.169E 0.	-1.516E 0	3 -1.673E 03	3,972E V3	3.167E 01	1.646E=02	3. '67E 01	1.646E=02
- 6.619E 01	1.385E 01	1.385E 01	*2.265F 0%	=3.373E 0.	=1.578E 0	3 #1.7958 03	4.289£ 03	3.577E 01	1.859£=02	3.577E 01	1.859£⊨02
6.656E 01	1.380E 01	1.4108 01	-2.265E 02	#3.405E 03	-1.589E 0	3 =1.816E 03	4.337E 03	3.564E 01	-1.852E=02	3.640E 01	1-8921-02
6.660E 01	1.380E 01	1.412E 01	-2,265E 02	-3.409E 03	-1.591E 0	3 -1.818E 03	4,342E 03	3.564E 01	1.852E=02	3.647E 01	1.895E=02
6.680E 01	1.311E 01	1-425E 01	-2.265E 02	-3,426E 0:	-1.597E 0	3 -1,829E 03	4.368E 03	3.384E 01	1.7596-02	3.680E 01	1.9136=02
6,846E 01	7.340E 00	6.370E 00	-1.122E 02	-3.542E 03	-1.637E 0	3 #1.905E 03	4.583E 03	1.896E 01	9.852E+03	1.645E 01	8,5506#43
6.913E 01	5.407E 00	0.337F 00	1,659E 01	=3.5/8E 0	-1.648E 0	3 +1.929E 03	4.665E 03	1.396E 01	7.2576-03	1.637E 01	8,507t=U3
6.990E 01	3,185E 00	4.910E 00	1.520E 02	-3.615E 03	•1•659£ 0	3 =1,956E 03	4.760E 03	8,225E 00	4.2756-03	1.268E 01	6.590E-03
7.062E 01	2.511E 00	3.575E 00	5.45SF 05	■3.649E 0:	1 =1.666E 0	3 -1.983E 03	4.84BE 03	6.485F 00	3.370E-03	9.232E 00	4,7996+03
7.123E 01	1.940E 00	2.969E 00	3.010E 02	#3.676E 0:	-1.671E 0	3 +2.005E 03	4.922E 03	5.010E 00	2.604E=03	7.667E 00	3.985E#03
7.218E 01	1.351E 00	2.025E 00				3 -2.034E 03	5,036E 03	3,490E 00	1.814E=03	5.229E 00	2.718E=03
7.261E 01	1.085E 00	1.867E 00	3,876£ 02	-3.726E 0	-1.680E D	3 -2.046E 03	5.088£ 03	2.802E 00	1.456E=03	4.822E 00	2,506E=03
7.414E 01	7.890E=01	1.305F 00				3 -2.079E 03	5.273E 03	2.038E 00	1.0596=03	3.370E 00	1.752E=03
7.429E 01	7.600E=01	1.151E 00				3 +2.0828 03	5,290E 03	1.963£ 00	1.0204=03	2.972E 00	1.545E=03
7.504E 01	6.3026=01	3.800E=01				3 -2.098F 03	5.374E 03	1.627£ 00	8.459£#04	9.813E-01	5.101E=04
7.505E 01	6.295E.01	3.7595=01	4.760E 02	-3.788E 0	=1.691E 0	3 =2.098E 03	5.375E 03	1.626E 00	8.450E=04	9.707E=01	5.045E-04
7.637E 01	4.000E=01	0.000	4,869E 02	-3.826E 0.	5 w1.695E 0	3 #2.131E 03	5.426E 03	1.033E 00	5.369E=04	0.000	0.000
7.922E 01	1.095E 00	0.000	5,168£ 02	#3.833E 0	5 =1.703E 0	3 m2.131E 03	5.525E 03	2.828E 00	1-4706=03	0.000	0.000
8.312E-01	8.500E=01	0.000				3 -2.131E 03	5.630£ 03	2.195E 00	1-1416-03	0.000	0.000
8.593E 01	6.950E=01	0.000				3 -2.131E 03	5.684E 03	1.795E 00	9.329E=04	0.000	0.000
8.879E 01	9,450E=01	0.000	5.953E 02	-3.857E 0	1.726E 0	3 -2.131E 03	5.707E 03	2.44DE 00	1,2688#03	0.000	0,000
8.880E 01	9.455E#01	0.000	5.953E 02	-3.857E 0	-1.726E 0	3 *2.131E 03	5.707E 03	2,442E 00	1.269E=03	0.000	0.000

x	DDRAG	CURAG	CF	нс
011 011 011 011 011 011 011 011 011 011	22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	E E E E E E E E E E E E E E E E E E E	00000000000000000000000000000000000000	03 5.484E=02 03 6.707E=02 03 6.707E=02 03 6.707E=02 03 6.707E=02 03 6.707E=02 03 5.809E=02 03 5.809E=02 03 5.408E=02 03 5.408E=02 03 5.408E=02 03 5.408E=02 03 5.408E=02 03 5.408E=02 03 5.308E=02 03 5.308E=02 03 5.308E=02 03 3.508E=02 03 3.508E=02 03 3.508E=02 03 3.508E=02 03 3.508E=02 03 3.508E=02 03 3.508E=02 03 3.508E=02 03 3.508E=02 03 3.508E=02 03 3.508E=02
		3.223E 3.226E 3.244E 3.256E 3.292E		1.674E=02 1.255E=02 1.255E=02 1.452E=02 1.350E=02 1.051E=02
6.230É 01 6.372E 01 6.619E 01 6.656E 01 6.660E 01 6.680E 01	9.364E 00 7.340E 00 1.192E 01 1.654E 00 1.694E=01 8.580E=01	3.432E 3.505E 3.641E 3.643E 3.651E	02 2.965Em 02 3.024Em 02 3.174Em 02 3.294Em 02 3.349Em 02 3.343Em	1.950E=02 2.170E=02 2.129E=02 1.994E=02 2.03 2.008E=02 1.998E=02
6.846E 01 6.913E 01 6.990E 01 7.062E 01 7.123E 01 7.218E 01 7.261E 01	7.389E 00 2.767E 00 2.974E 00 2.426E 00 1.819E 00 2.421E 00 9.551E-01	3.753E 3.783E 3.807E 3.825E 3.849E	3.175E= 02 3.145E= 02 3.078E= 02 3.027E= 02 2.991E= 02 2.927E=	1.349E=02 1.068E=02 03 8.817E=03 7.593E=03 03 5.807E=03
7.261E 01 7.414E 01 7.429E 01 7.505E 01 7.505F 01 7.922E 01 8.312E 01	2.951E 01 2.951E 01 9.540E=01 1.463E=03 1.340E=01 1.090E 00 1.422E 00	3.859F 3.889E 3.891E 3.900E 3.905E 3.905E 3.916E 3.930E	2.907E= 02 2.847E= 02 2.823E= 02 2.722E= 02 2.722E= 02 2.824E= 02 2.72E=	4.059E=03 3.798E=03 03 2.328E=03 2.319E=03 1.936E=05 4.157E=03

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7 8.593E 01 8.879E 01 8.880E 01	2.732E=01		2.723E=03 2.761E=03 2.761E=03	3.669E-03

RAMJET PERFURMANCE

ENGINE PERFORMANCE	INLET
CALCULATED THRUST	
REGENERATIVE=COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	INJET PROCESS EFFICIENCY = SUBSONIC
MOMENTUM AND FORCES	COMBUSTOR
INLET FRICTION DRAG	FUEL-AIR RATIO
STATIONS	FUEL INJECTORS
NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A 40.400 A 1B 42.810 B 1C 44.300 2A 50.285 U 2C 46.250 E 3A 55.575 3H 57.760 4 46.310

Reading 61

t = 205.86 sec.

SUPPARY REPORT

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WYSO -IIII	, p	٦.	, н "		GAMPA	ROLWT	SONV	MACH	VEL	s	*/4	*	DA\A	МІМЬМ	C	IVAC	PHI	ETAC
WIND TUNK		2004	0 5	* - • •	. 3071	10 055												
	744,999				1,2931													
0.000		405		97)	1.3989	58.423	987	5.944	5912	1.827	0.10593	21.166	0.7801 (3967	9.735	187.4		
SPIKE TIP		2	0 6															
0.000	18,712				1.2930													
V=600	17.057	5454	048 1 (774)	1,2950	28.954	2552	0.300	971	2.079	0.10593	21.166	0.7501	4047	1.596	191.2		
MIND TONV		3	0 0															
0.000	744,999	2991	600.9(792)	1,2931	28,955	2577											
0.000	0.401	409	-30.6(98)	1.3989	28,954	992	5,956	5908	1.827	0.10854	21.688	0.7601	4063	9.966	187.5		
SPIKE TIP	NS	4	0 0															
0,600	18,712	2991	666.9(792)	1,2930	28,954	2577											
0.600	16,463	2925	647.0(775)	1.2951	28,454	2550	0.392	999	2.079	0.10854	884.15	0.7601	4063	1,685	187.5		
INLET THR	TAD	5	0 4															
40.400	309,615	2906	642.0(768)	1.2957	28.954	2544											
40.400	18,843	1470	234.20	363)	1.3497	28,954	1846	2.447	4517	1.678	1.08509	21,166	0.0/62	5339	76.175	157.6		
INLET UPN	RSK	6	0 3			-	-	•	-			-		-				
40.400	309.615	2908	642.0(768)	1.2957	28.954	2544											
40.400	16,163		219.00	348)	1.3530	28.954	1811	2.540	4601	1.878	0.98645	21.166	0.0838	3373	70.526	159-4		
INLET DAN		7	0 4	., .		· ·		• •										
	139.419	2908	642.06	7481	1.2957	28.954	2544											
40.400	119,225								1239	1.933	0.98645	21.166	0.0838	3373	18,995	159.4		
COMBUSTOR			1 3										-,,,,,,					
	240.756	-		8>21	1,2909	28.249	2620											
40.410	23.673							2.160	4362	1.954	1-08757	21.217	0.0762	4339	73.732	157-4	0.07	0.42
COMBUSTOR		. 9	2 202						70-2	• • • • •			040,02				V	
	187.014			8001	1.2799	28.526	2694											
40.851	35.087							1.764	3975	1-984	1-09118	21-217	0.0759	3304	67-406	155.7	0.07	1.00
COMBUSTOR		10	3 21	-507	490.71	W-4-2-	W 14 14 14	• • • •	57.5		*******		040131	3304	011400		0.07	1,00
	161.868			8971	1,2800	28.528	2601											
41.341	28,985							1.795	4015	1.004	1.07020	21.217	0.0768	2518	67.349	121 7	0.07	1 60
COMBUSTOR		11	4 21	7/1/	110101	20,52,			-0.5	****	101727	611611	0.0700	3210	014347	13107	0.07	1.00
	151.248			8071	1.2801	28.828	2601											
41-500	31.063							1.707	1870		4 07306	31 217	0.0772	2177	A# 480	140 5		
COMBUSTOR		15	5 21	275)	119195	204321	5613	4 \$ 7 4 1	2017	11770	110/243	Ellefi	0.0112	5113	64,650	144.0	V # V /	1,00
	130.186			8051	1.2802	28 528	2688											
41.841	31.923			6493	1 3100	28.620	2114	1.692	7440	2 008	4 AE778	31 319	0.0786	1076	40 170	4.0.0.0	A A **	4 60
COMBUSTOR		13	6 21	01//	1.3100	201327	2310	1 1 2 7 1	3000	£ \$ 000	1.02330	ETTEL	0.0700	2012	60.370	144.4	0.07	1,00
	102.468			Rofs	1.2804	38.538	3447											
42.460	33.776							1.702	1120	3.824		21 217	0.0823	30.00	E 2 684	124 0	^ ^7	
COMBUSTOR		14	7 21	3607	1,000	501757	6301	11370	3364	E . VE "	1.00000	EISETI	0.0023	2704	52,001	170.4	V.V/	1,400
42.826	98,643			7051	1.2987	27. 26B	2504											•
42.826	30.894							1 //23	72/10	2 057	0.0000	21 271	0.0839	10.9	40 003	471 0		
COMBUSTOR		15	8 21	2017	Teneti	2/1200	EEOH	10463	3544	5 4 0 3 3	0.40440	CINCII	0.0034	5014	49.993	13446	0.12	0,11
42,836	101.656		-	7-21	4 5004	27 187	2640											
42.836	30.816				1.3024			1 005	9 9 6 4	2			4 4004					
COMBUSTOR				263)	1,3634	211103	6641	1 - 443	3600	C+044	0.90//0	21.6/1	0.0841	5910	49.829	134.1	0.15	0.02
42.901	99.874	16	9 21	7.8	4 7074	77 171												
42.901				150) 5113	142020	27 174	2204	4	7776	2 660							-	
COMBUSTOR	204302	20/3	46541	391)	1.1527	E/ • 1/0	2243	1 4 4 4 4	2529	C.044	0.98512	41.4/1	0.0843	2795	49.571	131.4	0.15	0,00
44.310		1/ 27:0	10 51	7-41	. 70.44	37 464	56.48											
44.310	27 277	31110	620.5(750)	1.3043	6/1107	Z247	4 TP 1. 2P	1015									
	F1 # 0 U 3	2143	44702	38c)	1.2634	c/+10A	2219	1,500	2402	∠.060	0.91327	21,271	0.0909	2606	45.044	124.5	0.15	0.00
COMBUSTOR 44.800			11 21	*. * .	1 204	37 1/0												
CO 44,800	76.3/9	2116	615.8((51)	1,5048	67,108	2540		***									
. 44*pA0	EG 4 3 4	2133	4434/(277)	1.3230	27.100	2273	1+279	2952	2,061	0.89943	21.2/1	0.0923	2589	41.262	121./	0.15	0.00

GAMMA MOUNT SONY MACH VEL S WIA AZAC MOMIM Q IVAC PHI FTAC COMBUSTOR (0 19 12 21 15.621 73.354 2800 608.0(779) 1.5000 27.501 2575 # 45.021 33.999 2336 464.5(638) 1.3154 27.501 2366 1.132 2679 2.068 0.88988 21.271 0.0933 2564 37.048 121.5 0.15 0.15 COMBUSTOR 0 20 13 21 46.250 69.243 2652 617.2(799) 1.3085 24.935 2631 46.250 35.405 2259 486.2(669) 1.3217 24.935 2440 1.050 2561 2.205 0.87323 21.432 0.0958 2575 34./47 120.1 0.38 0.05 COMBUSTOR 0 21 14 -21 46.260 70.892 2562 617.1(771) 1.3126 24.848 2594 46.260 35,427 2106 486,2(641) 1.3260 24,648 2397 1.068 2559 2.194 0.87254 21,432 0.0959 2575 34,703 120,1 0.38 0.01 0 22 15 21 COMBUSTOR 46.336 71.195 2547 616.3(766) 1.3133 24.835 2588 40.334 35.596 2153 486.3(636) 1.5267 24.635 2391 1.067 2551 2.191 0.86928 21.432 0.0963 2577 34.464 120.2 0.38 0.00 COMBUSTOR 0 23 16 21 -47+310 70.765 2515 606.5(755) 1.3144 24.833 2573 47.310 37.773 2160 489.3(639) 1.3204 24.833 2395 1.011 2422 2.188 0.80932 21.432 0.1034 2614 30.465 122.0 0.38 0.00 COMBUSTOR 0 24 17 21 45.110 68.994 2490 598.3(747) 1.3152 24.633 2561 48.110 35.172 2114 474.4(624) 1.3281 24.832 2371 1.050 2490 2.186 0.74339 21.432 0.1126 2673 28,763 124.7 0.38 0.00 COMBUSTOR 0 25 18 21 48.861 68.238 2472 590.6(741) 1.3158 24.837 2551 48.861 32.100 2056 454.3(605) 1.3301 24.637 2340 1.116 2611 2.165 0.66258 21.432 0.1263 27/8 26.886 129.6 0.38 0.00 COMBUSTOR 0 26 19 15 62.775 2344 588.0(760) 1.3230 22.751 2603 50.301 50.301 21.003 1783 391.7(564) 1.3435 22.751 2288 1.370 3134 2.326 0.54360 21.609 0.1552 2940 26.476 136.0 0.64 0.01 0 27 20 CUMBUSTOR 62.777 2344 587.9(760) 1.3230 22.751 2603 50.311 50.311 20.926 1781 391.0(563) 1.3436 22.751 2287 1.373 3138 2.326 0.54290 21.609 0.1554 2941 26.479 136.1 0.64 0.01 COMBUSTOR 0 58 51 50.841 63.778 2308 583.8(747) 1.3245 22.730 2586 50.841 16.842 1650 355.2(519) 1.3494 22.730 2207 1.532 3382 2.320 0.50774 21.609 0.1662 2988 26.684 138.3 0.64 0.00 COFBUSTOR 0 29 22 52.251 54.459 2536 573.9(825) 1.3137 22.953 2686 52.251 15.862 1868 338,5(590) 1.3376 22,953 2327 1.475 3432 2.360 0.43273 21.609 0.1950 3097 23,080 143.3 0.64 0.08 COMBUSTOR 0 30 23 54.351 46.163 2867 561.2(939) 1.2979 23.286 2819 54.351 14.662 2186 315.1(695) 1.3215 23.287 2485 1.413 3509 2.407 0.35468 21.609 0.2379 3250 19.341 150.4 0.64 0.21 COMBUSTOR 0 31 24 3 54,851 46.357 2851 558.4(933) 1.2986 25.278 2812 54.851 15.021 2108 291.3(668) 1.3244 25.278 2442 1.447 3656 2.405 0.34018 21.609 0.2480 3283 19.328 151.9 0.64 0.20 COMBUSTOR 0 32 25 4 55,601 44.954 2902 554.4(950) 1.2960 23.336 2831 55.601 12.067 2126 274.6(675) 1.3230 23.336 2448 1.528 3741 2.412 0.32067 21.609 0.2631 3326 18.644 153.9 0.64 0.23 COMBUSTOR 0 33 26 3 55.760 44.704 2911 553.5(953) 1.2956 23.346 2834 55,760 11.864 2127 271.0(674) 1.3229 23.547 2448 1.536 3760 2.415 0.31683 21.609 0.2663 3335 18,514 154.5 0.64 0.23 COMBUSTOR 0 34 27 56,361 38.340 3075 550.7(1011) 1.2875 23.510 2894 56,361 8.869 2187 227.5(692) 1.3186 23.512 2469 1.628 4021 2.439 V.24808 21.609 0.3401 3473 15.502 160.7 0.64 0.29 COMBUSTOR 0 35 28 57,786 42.422 2928 544.9(959) 1.2945 23.384 2839 6.539 1873 168.5(586) 1.3323 25.385 2303 1.884 4340 2.418 U.22929 21.609 0.3679 3531 15.466 165.4 Q.64 0.24 57.786 COMBUSTOR 0 36 29 57.841 35.578 3213 544.8(1059) 1.2804 23.660 2940 57.841 8.525 2317 215.2(735) 1.3120 25.662 2527 1.607 4061 2.455 0.22873 21.609 0.3689 3533 14.435 163.5 0.64 0.34 0 37 30 3 COMBUSTOR 57.981 35.724 3198 544.3(1053) 1.2811 23.646 2935 57.981 8.301 2288 210.2(725) 1.3132 25.648 2513 1.627 4088 2.453 0.22701 21.609 0.3717 3536 14.423 163.6 0.64 0.34

GAMMA MOLKT SONV MACH VEL S */A A/AC MONTH Q IVAC PHI ETAC 0 38 51 10 COMBUSTOR 58.061 48,141 2797 544.0(914) 1.3006 23.264 2788 58.061 5.659 1660 143.7(516) 1.3428 23.265 2183 2.050 4475 2.395 0.22963 21.609 0.3674 3538 15.971 163.7 0.64 0.20 COMBUSTOR 0 39 32 58.341 56.629 2659 543.1(866) 1.3070 23.140 2733 4.762 1436 118.7(443) 1.3554 23.140 2045 2.255 4609 2.368 0.22883 21.609 0.3687 3545 16.389 164.1 0.64 0.15 58.341 CUMBUSTOR 0 40 35 58,567 61,535 2603 542.5(846) 1,3095 23,091 2709 58,567 4.397 1342 107.5(413) 1.36.9 23.091 1983 2.352 4665 2.355 0.22836 21.609 0.3695 3549 10.556 164.3 0.64 0.14 COMBUSTOR 0 41 34 59.291 86.713 2414 540.5(782) 1.3181 22.428 2627 59,291 3.225 1030 72.6(315) 1.3792 22.928 1755 2.757 4839 2.304 0.22482 21.609 0.3753 3560 16.906 164.7 0.64 0.08 COMBUSTOR 0 42 35 32,425 3500 537,7(1160) 1,2645 23,967 3030 60,311 10.087 2712 238.1(870) 1.2940 25.975 2698 1.435 3871 2.480 0.22338 21.609 0.377/ 3576 13.440 165.5 0.64 0.45 60.311 COMBUSTOR 0 43 36 62.321 35.112 3392 531.6(1121) 1.2705 23.873 2996 156.50 9.425 2531 209.1(807) 1.3017 23.678 2619 1.534 4017 2.466 0.23116 21.609 0.3650 3579 14.431 165.6 0.64 0.42 COMBUSTOR 32,330 3735 527,0(1243) 1,2498 24,242 3094 63.741 63.741 13,381 3110 280.0(1010) 1.2758 24.258 2852 1.233 3515 2.492 0.23742 21.609 0.3553 3579 12.971 165.6 0.64 0.55 COMBUSTOR 0 45 38 66,205 29.921 3862 517.5(1288) 1.2407 24.405 3124 66,205 15.296 3377 320.0(1105) 1.2625 24.427 2946 1.067 3144 2.504 0.22505 21.609 0.3749 3580 10.995 165.7 0.64 0.60 COMBUSTOR 0 46 39 3 66.581 27,762 3876 515,9(1293) 1,2391 24,425 3127 15:163 3439 336:1(1128) 1:2594 24:447 2968 1:011 2999 2:510 0:20922 21:609 0:4032 3580 9:752 165:7 0:64 0:61 66.581 COMBUSTOR REGEN 47 40 21 66.581 27.762 4163 645.2(1402) 1.2219 24.389 3220 66.581 10.369 3448 340.4(1131) 1.2577 24.446 2970 1.315 3905 2.542 0.20922 21.609 0.4032 3694 12.696 170.9 0.64 0.61 NOZZLE 27.762 3876 515.9(1273) 1.2391 24.425 3127 88.817 88 817 0.761 1740 -276.2(527) 1.3260 24.458 2166 2.907 6296 2.510 0.04355 21.609 1.9371 4606 4.261 213.1 0.64 0.61 NOZZLF 49 42 88.817 27.762 3876 515.9(1273) 1.2391 24.425 3127 88.817 0.388 1471 -364.0(439) 1.3401 24.458 2002 3.315 6636 2.510 0.02768 21.609 3.0481 4759 2,854 220.2 0.64 0.61 NOZZLE, AE REGEN 50 43 27.762 4163 645.2(1402) 1.2219 24.389 3220 88,817 88,817 0.824 1954 -204.8(598) 1.3165 24.458 2287 2.852 6522 2.542 0.04355 21.609 1.9372 4789 4.414 221.6 0.64 0.61 NOZZLE PU REGEN 51 44 88,817 27,762 4163 645.2(1402) 1.2219 24.389 3220 88.817 0.388 1624 -314.3(489) 1.3317 24.458 2097 3.304 6929 2.542 0.02617 21.609 3.2243 4974 2.618 230.2 0.64 0.61 FICTIVE COMBUSTR 71 64 309.615 4838 515.9(1640) 1.1977 25.536 3359 66.581 0.388 1145 -881.9(326) 1.3469 25.697 1729 4.837 8363 2.346 0.04706 21.609 1.7928 5795 6.117 268.2 0.64 1.00 66,581 FICTIVE NOZZLE 72 65 21.395 3816 490.8(1269) 1.2410 24.428 3104 88,817 88.817 0.656 1872 -232.4(570) 1.3200 24.456 2241 2.684 6015 2.525 0.04355 21.609 1.9371 4465 4.071 206.6 0.64 0.61

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' XABS	P#18	P=08	PDA	QUA	6=18		6=08		CAmALL	8 T & 40 C /.	6-194016	B-00 4000	0.00.010
6.9818#01	1.045€ 00	0,000	#4.556E#01	0.000	0.000				CAMALL	P+16/PSU	P=18/P10	P∍UB/PS0	P=08/P10
1.836E 01	1.045E 00	0.000	-3.481E 01	0.000			0.460		2.470E-02	2.69nE 00	1.4036-03	0.000	0.000
3.070E 01	2.2356 00				0.000		0.000		1.6341 02	2.6966 00	1,403E-03	0.000	0.000
3.508E 01	3.910E 00	0.000	-1.678£ 02	0.000	0.000		0.000		5.053E 02	5.767E 00	3.000E=03	0.000	0,000
		0.000	-3.669£ 02	0.000	0.000		0.000		6.804E 02	1.009E 01	5.2486.03	0.000	0.000
3.555E 01	4.025E 00	0.000	-4.031E 02	0.000	0.000		0.000		7.013E 02	1.039E 01	5,403E=03	0.000	0,000
3.606E 01	3.945E 00	0.000	#4.435E 02				0.000		7.246E 02	1.0186 01	5.295E=03	0.000	0.000
3.648E 01	4.252E 00	0.000	#4.786E U2				0.000		7.443E UZ	1.097E 01	5,708E=03	0.000	0.000
3.672E 01	4.238E 00		0 -5.571E 02				0.000		7.5568 02	1.093E 01	5.6886=03	1.465E 01	7.620E=03
3.672E 01	4.237E 00	S.713E 0	00 =5.572E 02	-3,411E 0	2 =3.411E	02	0.000		7.5594 02	1.093E 01	5.608E+03	1.474E 01	7.6685=03
3.701E 01	4.220E 00		0 +5.606£ 02				0.000		7.855E 02	1.089E 01	5.6646.03	1.918E 01	9.976E=03
3.739E 01	4.082E 00	9.725E 0	0 35882€ 02	■3.546E 0	2 =3.546E	02	0.000		8.255E 02	1.053E 01	5.479E=03	2.509E 01	1.3056-02
3.803E 01	3.850E 00	1.248E 0	1 -5.386E 02	₩3.685E 0	2 -3.685E	02	0.000		8.944E 02	9.934E 00	5.168t=03	3.220E 01	1.6756=02
3.875E 01	1.145E 01	1.558E 0	1 -5.483E UZ	#4.055E 0	2 #3.901F	02		01	9.745E 02	2.955E 01	1.537E=02	4.0208 01	2.0918-02
3,885E 01	1.252E 01	1.601E 0	1 -5.5286 02	-4.120E 0	2 -3.940E	0.5	₩1.795E	0.1	9.857£ 02	3.230E 01	1.6506-02	4.131E 01	2.1491-02
3.901E 01	1.420E 01	1,680€ 0	-5.596E 02	-4.211E 0	2 -4.007E	02	#2.045E	01	1.004E 03	3.664£ 01	1.906E-02	4.335E 01	2.2556=02
3.950E 01	1.807E 01	1.922E 0	1 -5.824E 02	-4.552E 0	2 -4.252E	02	-2.806E	0.1	1.060E 03	4.664E 01	2.426E=02	4.959E 01	2.580E=02
3.987E 01	1.697E 01	2.105E 0	1 -5.871L 02	=4 817E 0	2 =4.479F	02	3.376F	01	1.103E 03	4.379E 01	2,278t+02		
4.000E 01	1.659E 01		-5 868E 02						1.118£ 03	4.280E 01		5.431E 01	2.8265=02
4.034E 01	2.595E 01		5 968E 02					01			2.227£=02	5.200E 01	2.705E=02
4.040E 01	2.758E 01	1.9245 0	-6.005E 02	#5.278F 0	2 = 4.8600	V 2	-4 1075		1.157E 03	6.696E 01	3.4848-02	4.593E 01	2.389E+02
4.041E 01	2.786E 01)1 =6.009£ 02						1.164E 03	7.117E 01	3,703E=02	4.965E 01	2.583€=02
4.085E 01	3.997E 01								1.165E 03	7.168E 01	3.739E=02	5.026E 01	2.616E=U2
4.134E 01	5.344E 01	7.535E 0	1 #6.267E 02	401070E U	E 42160AP	0.2	#4.000E	01	1,217E 03	1.031E 02	5.366E=02	7.792E 01	4.054E-02
4.150E 01	5.782E 01	413636 0	0 -7.020E 02	-0.1/DC U	2 42+0105	0.5	45,574E	01	1.275E 03	1,379E 02	7,174E=02	1.168E 01	6.074E=03
4.184E 01	6.002E 01	4 4 3 0 E E	0 -7 436E 02	*0+330E U	£ 45.758E	0.0	=5.808E	01	1.293E 03	1.492E 02	7.762E=02	1-110E 01	5.774E+03
4.246E 01		3 P C C C C	0 -8.340E 02	-0.0776 0	2 =5.064F	05	-6.294E	0.1	1,334E 03	1.549E 02	8.056E=02	9.869E 00	5.134E+U3
4.283E 01	5.401E 01	3 1340E 0	S0 45.953E 05	#/ 4/2E 0	2 #6.646E	02	-8.263E	01	1.407E 03	1.652E 02	8,5926-02	9.134E DO	4.752E=Q3
4.284E 01	5.842E 01	343/26 0	0 -1.077E 03	0.0146 0	2 -6.974E	02	#1.040E	0.2	1.451E 03	1.507E 02	7.8416+02	8.700E 00	4.526£=U3
4.290E 01	5.826E U1	3:30/6 0	0 =1.079E 03	=8.050E 0	2 -6.983E	02	#1.047E	02	1,452E 03	1.503E 02	7.821E=02	8.688E 00	4.520E-03
4.431E 01	5.727E 01	3+33/6 0	0 -1.093E 03	-8-112E 0	2 -7.040E	02	-1.092E	02	1,460E 03	1.478E 0≥	7,6876-02	8.61 IE 00	4.480€≠∪3
	3.570E 01	1 4416 0	1 -1.259E 03	-1.070E 0	3 #8,161E	05	-2.535E	02	1.630E 03	9.211E 01	4,792E=02	5.136E 01	2.6722-02
4,480E 01	2.820E 01	2.5075 0	1 -1.268£ 03	=1.170E 0	3 +8.502E	02	=3.198E	02	1,6896 03	7.276E 01	3.7856-02	6.623E 01	3.445E=02
4,562E 01	3.268E U1	3.532F 0	1 =1.261E 03	-1.357E 0	3 m9.042E	02	#4,325E	0.2	1.790E 03	8.432E 01	4.387E=02	9.1128 01	4.740E=02
4.625E 01	3.612E 01	3.469E 0	1 -1.237E 03	■1.407E 0	3 -9.444E	0.5	#5.223E	0.2	1.867E 03	9.319E 01	4 . 848E + 02	8,951E 01	4.657E=02
4.626E 01	3,6176 01	3,468E 0	1 =1.236E 03	=1.459E 0	3 m9:450E	0.5	-5.238E €	02	1.868£ Q3	9.333E 01	4.855E=02	8.948E 01	4.655E=02
4.634E 01	3.659E 01	3.461E 0	1 -1.233E 03	-1.465E 0	3 =9.497E	02	#5.350E	0.2	1.877E 03	9,440E 01	4.9111=02	8,929E 01	4.645E-02
4.731E 01	4.191E 01	3,364E 0	1 -1.184E 03	-1.696E 0	3 -1.010E	03	-6.862E	0.2	1.997E 03	1.081E 02	5,625E=02	8.679E 01	4.515E=02
4.811E 01	3.750E 01	3.284E 0	1 =1.117E 03	=1.872E 0	3 =1.057E	03	#8.155E	02	2.096E 03	9.676E 01	5.034E=02	8.475E 01	4.409E=UZ
4.886E 01	3.210E 01	5.210E 0	11 -1.004E 03	-2.057E 0	3 =1.099E	03	-9.371E	0.2	2,190E 03	8.282E 01	4.309E-02	8.282E 01	4.309E-02
5.030E-01	2.100E 01	5.100E 0	1 #8.064F 05	₩2.320E 0	3 -1.177E	03	-1.143E	03	2.370E 03	5.4198 01	2.819E=02	5.419E 01	2.819E=02
5.031E 01	2.093E 01	2.093E 0	1 =8.0535 02	-2.322E 0	3 -1.176E	03	■1.145E (03	2.371E 03	5.399E 01	2.809E=02	5.399E 01	2.809E=02
5.084E 01	1.684E 01	1.684E 0	1 #7.531E 02	-2.411E 0	3 =1.205E	03	-1.206E (03	2.437E 03	4.345E 01	2.261E=02	4.345E 01	2.201L=02
5.225E 01	1.586E 01	1.586E 0	1 =6.322E 02	-2.624E 0	3 -1.274E	03	-1.351E (03	2.615E 03	4.093E 01	2.129E-02	4.093E 01	2.129E=02
5.435E 01	1.466E 01	1.466E 0	1 =4.642E 02	-2.898E 0	3 =1.366E	03	#1.532E (0.3	2.881E 03	3.783E 01	1.9681=02	3.783E 01	1.9686=02
5,485E 01	1,302E 01	1.502E 0	1 -4.282E UZ	₩2.959E 0	3 -1.387E	0.3	#1.572E (0.3	2.745E U3	3.360E 01	1.748E+02	3.360E 01	1.7486+02
5.560E 01	1.207E 01	1.207E 0	1 =3.797E 02	-5.047E 0	3 -1.416E	0.3	=1.631E (0.3	3.041E 03	3.113E 01	1.6201-02	3.113E 01	1.6206=02
5.576E 01	1.186E 01	1.186E 0	1 =3.699E 02	-3.064E 0	3 -1.4225	03	-1.643E	03	3.061E 03	3.061E 01	1.5921-02	3.061E 01	
5.636E 01	6,637E 00	1.110E 0	1 #2.294E 02	-3.126E 0	3 -1.4438	0.3	-1.683F (กร	3,102E 03	1.713E 01	8,909E=03		1.592E=02
5.779E 01	6,539E 00	6,539E 0	0 =1.666E 02	-3.249E 0	3 -1 4885	0.1	-1.7A1F	0.3	3.209E 03	1.687E 01	8.777E=03	2.864E 01	1.490E=02
5,784E 01	1.069E 01	6.363E 0	0 -1.648E 02	-3.253E 0	3 -1 489F	03	-1.764F	กร	3.216E 03	2.758E 01		1.687E 01	8.777E=03
5.798E 01	1.069E 01	5.915E 0	0 -1.608E 02	-5.264F n	3 -1 DONE	n 7	1 77nF	0 K		•	1.435E=02	1.642E 01	8.541E=03
5.806E 01	5.659E 00	5.659F 0	0 =1.584E 02	#3.269F A	3 -1-4045	7.7	-11/1/VI V	עט	3.254E 03 5.244E U3	2.758E 01	1.435£=02	1.526E 01	7.939E-03
5,834E 01	4.762E 00	4.7625 0	0 =1.516E 02	- 1 DARE A	2 -1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	62		V 2	•	1.460E 01	7.596E=03	1.460E 01	7,596L=03
5.857E 01	4.397E 00	4.397F 0	0 -1.4726 02	-4. init o	2 mls=000E	03 01	-1 7076	ν.»	5,280E 03	1,2298 01	6.393E=03	1.229E 01	6.393t=03
5,929E 01	3.225E 00	3.225F A	0 =1.3685 02	-3-3-3- U	2 ml 6000	0 J	-1 0175 (V .D	3.309E 03	1.134E 01	5.9028-03	1.134E 01	5.902E=03
6,031E 01	1.009E 01	1.0095 0	1 =1.214E U2	-5-3-3-35 U	L. BOTE	0.7	#1.01/C (0.5	3.402E 03	8.321E 00	4.329E=03	8.321E 00	4.329E=03
6.232E 01	9.425E 00	9.4255 0	0 =1.192£ 02		3 411333E	0.7	4 000 C	0.3	3,532E 03	2.603E 01	1.354E=02	2.6035 01	1.354E=02
	AUMAR AA		U -1817CE VE	-3,3376 0	3 41.344E	Q A	-1.4446	0.5	3.790E 03	2.432£ 01	1.2656 = 02	2.432E 01	1.2056-02

XABS	P#IB	P∍Oe	PDA	X Q G	⊌ ≈]	F	ម្គោប់ម	CAMALL	P#18/250	P#18/P10	P+OR\\80	P=08/P[0
6.374E U1	1.338E 01		-1.192£ U		05 -1.62	5E 03	-2.012E 03	3.972£ 03	3.453E 01	1.796E=02	3.453E 01	1.796E#Ū2
6.620E 01	1.530E U1	1.530E 01					#2.148E 03	4.289E 03	3.947E 01	2.053E#02	3.947E 01	2.053E+02
0.658E U1	1.474E 01						-2.171E 03		3,603E 01	1.9786-02	4.022E 01	2.0925-02
6,662E 01	1 4746 01						-2.173E 03		3.803E 01	1.9786=02	4.030E 01	2.0976=02
6.682E 01	1 402E 01						-2,185E 03		3,6198 01	1.883E=02	4.070E 01	2.117E=V2
6.848E 01	8.110E 00	6 500E 0n					#2.270F 03		2.093E 01	1.089E#02	1.677E 01	8.725E=U3
6.915E 01	5.9536 00	6.877E 00					#2.298E 03		1.536E 01	7.9916-03	1.775E 01	9.232E=03
6,992E 01	5.475E 00	5.331E 00					-2.330E 05		8.966E 00	4.664E=03	1.375E 01	7.1565-03
7.064E 01	2.704E 00	3,885E 00					-2.363E 03		6.976E 00	3,6296-03	1.003E 01	5.2156=03
7.125E 01	2.050E 00	3.162E 00		2 -4.190E					5,2896 00	2.7528-03	8.157E 00	4.2446-03
7.2206 01	1 440 00	2.035E 00		3 mu. 241E				5.036E 03	3.726E 00	1.939E=03	5.251E 00	2.732E=03
7,263E 01	1.170E UO	1.889F 00					-2.441E 03	5.088E 03	3.019E 00	1.570E=03	4.874E 00	2.536E=03
7.416E 01	8 103E=U1	1.370F 00		2 -4.304E					2.0918 00	1.088E-03	3,535E 00	1.839E=03
7.431E 01	7.750E#01	1.212E 00	6 079E 0	2 -4.307E	03 =1.82	7E 03	#2.481E 03	5,290E 03	2.000E 00	1.040E+03	3.126E 00	1.626E=03
7,506E 01	7.353E=01	4.200E-01					-2,497E 03		1.697E 00	9.870E=04	1.084E 00	5.638E=04
7.506E 01	7.351E-01	4-158E-01					2.497E 03		1.697E 00-	9.8676#04	1.073F 00	5.581E+04
7.639E 01	6.650E-01	0.000		2 -4.367E					1.716E 00	8.926E=04	0.000	0.000
7.924E 01	1.505E 00	0.000	6 9396 0	2 -4.378E	03 #1.84	8E 03	. ≈2.530E 03	5.525E 03	3.883E 00	5.050E-03	0.000	0.000
8.314E 01	1.125E 00	0.000	7.501E 0	2 -4,390E	03 =1.86	1E 0	-2.530E 03	5.630E 03	2.403E 00	1.510E=03	0.000	0,000
8,595E 01	8.650E=01	0.000					-2.530E 03		5.535E 00	1.161E=03	0.000	0.000
8.881E 01	1.185E 00	0.000		2 #4.420E					3.057£ 00	1.591E=03	0.000	0.000
8.882E 01	1.186E 00	0 . 000	7.969E 0	2 -4.420E	03 -1.89	1E 03	=2.530E 03	5.707E 03	3.059E 00	1.592E-03	0.00	0.000

×	DDRAG	CURAG	CF	нc
**************************************	01 1.218E 02 01 2.18E 01 01 9.359E 01 01 3.517E 00 01 1.359E 00 01 1.347E 01 01 7.654E 00 01 1.847E 00 01 1.847E 00 01 1.847E 00 01 1.847E 00 01 1.847E 00 01 1.847E 00 01 1.847E 00 01 1.847E 00 01 1.847E 00 01 1.847E 00 01 1.847E 00 01 1.849E 00	22222222222222222222222222222222222222	33333333333333333333333333333333333333	22222222222222222222222222222222222222
6,68 <u>2</u> E	01 8,480E=01	3.630F 02	3.364E=03	2.133E=02
7.064E 7.125E 7.263E 7.263E 7.416E 7.416E 7.506E 7.506E 7.639E 7.924E 8.314E	01 2.545E 00 01 1.904E 00 01 2.509E 00 01 9.843E=01 01 3.052E 00 01 2.501E=01 01 1.015E 00 01 1.616E=03 01 5.412E=01 01 1.407E 00 01 1.722E 00	3.790E 02 3.809E 02 3.834E 02 3.874E 02 3.877E 02 3.887E 02 3.887E 02 3.892E 02 3.906E 02	3.038Ew03 3.001E=03 2.937E=03 2.916E=03 2.859E=03 2.859E=03 2.752E=03 2.751E=03 2.768E=03 2.883E=03 2.8817E=03	9.652E=03 6.155E=03 6.155E=03 5.602E=03 4.351E=03 4.051E=03 2.601E=03 2.673E=03 2.979E=03 5.471E=03 4.3/8E=03

READING = 0001 BLOCK = 118 TIME = 205.862 MACH 0.0 PT = 744.499 TT = 2991.1

Χ.		DDRAG	CURAG	£ F	nc
6.595E	ŪΊ	7.533E=01	3,931E 02	2.7634=03	5.575E=03
6.881E	0 1	3.1706-01	3.934E 02	2.800E=03	4.508E+03
3588.8	01	0,000	3.934E 02	2.800E=03	4,509E⊨03



RAMJET PERFORMANCE

80	ENGINE PERFORMANCE				INLET		
MEASURED THRUST CALCULATED SPECIFIC MEASURED SPECIFIC IM CALCULATED THRUST CO	IMPULSE	459. 911. 1036. 0.1618	(LBF) (LBF+SEC/LBM) (LBF+SEC/LBM)	MASS FLOW RATIO ADDITIVE DRAG COE LIMITING PRESSURE DELTA PTZ TOTAL PRESSURE RE- TOTAL PRESSURE RE-	FFIGIENT	0.7801 0.0293 (see 0.1844 0.1374 0.4156	(PSI)
STREAM THRUST NET THRUST SPECIFIC IMPULSE	IVEWCOOLED ENGINE PERF CALCULATED	4643. 561. 1312.		INLET PROCESS EFF KINETIC ENERGY EF- KINETIC ENERGY EF- ENTHALPY AT PO	ICIENCY - SUPERSONIC ICIENCY - SUBSONIC FICIENCY - SUPERSONIC FICIENCY - SUBSONIC SUPERSONIC SUBSONIC SUBSONIC	0.9155 C 0.9308	(8TU/L8M)
	MUMENTUM AND FORCES				COPBUSTOR		
INLET MOMENTUM CHANG COMBUSTOR FRICTION D COPBUSTOR STRUT DRAG COMBUSTOR MOMENTUM CRAME OF THE COMBUSTOR MOZZLE FRICTION DRAG NOZZLE HOMENTUM CHAN NOZZLE PRESSURE INTE EXTERNAL FRICTION DRESTERNAL PRESSURE IN TOTAL EXTERNAL DRAG TOTAL STRUT DRAG CAVITY FORCE CAVITY FORCE CALCULATED LOAD CELL	E D D D D D D D D D D D D D D D D D D D	31.49 -0.00 885. 916. 63.34 *1110. *1173. *45.00 *1014. *1785.	(LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF)	EQUIVALENCE RATIO COMBUSTOR EFFICIE TOTAL PRESSURE RA COMBUSTOR EFFECT: INJECTOR DISCHARGE VACUUM STREAM THE NOZZLE COEFFICIENT PROCESS EFFICIENC	NCY	0.637 0.612 0.0897 0.5782 60.0.4826.	0.7729, 0.7145
	STATIONS			FI	UEL INJECTORS		
SPIKE TRANSLATION INLET THROAT COWL LEADING EDGE NOZZLE SHROUD TRAILII NOZZLE PLUG TRAILII STRUT LEADING EDGE STRUT TRAILING EDGE	EDGE	34,884 1,840 40,40 36,72 75,68 88,81 57,98 66,58	O (ÎN) O (IN) O (IN) O (IN) O (IN) O (IN) O (IN) O (IN) O (IN)	INJECTORS 1A 1B 1C 2A 2C 3A 38	STATION 40.400 42.826 44.300 50.301 46.250 55.591 57.776 46.326	VALVE A B D E	

Reading 61

t = 212.16 sec.

7 4-75

SLMMARY REPORT

GAMMA MOLHT SONV HACH VEL S A/AC MUMTH IVAC PHI ETAC W/A WIND TUNNEL 1 0 5 745,499 2991 666,9(792) 1,2931 28,955 2577 0.000 0.388 405 *31.6(97) 1.3989 28.955 987 5.992 5912 1.827 0.10600 21.194 0.7806 5972 9.739 187.4 SPIKE TIP NS 0 6 0.600 18,700 2991 666,9(792) 1,2930 28,954 2577 17.040 2928 648.0(774) 1.2950 28.954 2552 0.381 972 2.079 0.10600 21.194 0.7806 4047 1.602 191.0 0.600 WIND TUNNEL 745.499 2991 666.9(792) 1.2931 28,955 2577 0.000 0.000 0.401 409 =30.7(98) 1.3989 28.954 991 5.960 5908-1.827 0.10847 21.686 0.7806 4062 9.959 18/.3 SPIKE TIP NS 0.600 18.700 2991 666.9(792) 1.2930 28.954 2577 0.600 16.951 2925 647.0(773) 1.2951 28.454 2550 0.392 999 2.079 0.10847 21.686 0.7806 4062 1.684 187.3 INLET THROAT 40.400 308,325 2906 641,3(767) 1,2958 28,954 2543 18.901 1471 234.6(363) 1.3496 28.954 1847 2.443 4511 1.878 1.08587 21.194 0.0762 3341 76.131 157.6 INLET UPNKSK 40.400 508.326 2906 641.3(767) 1.2958 28.954 2543 16.211 1414 219.4(348) 1.3529 28.954 1812 2.535 4595 1.878 0.98716 21.194 0.0838 3375 70.491 159.2 INLET DNNHSK 40,400 139.377 2906 641.3(767) 1.2958 28.954 2543 40,400 119.157 2804 610.6(737) 1.2990 28.954 2501 0.496 1240 1.935 0.98716 21.194 0.0838 5375 19.018 159.2 COMBUSTOR 40.410 233.551 5048 642.0(830) 1.2896 28.290 2628 40.410 24.420 1781 266,2(498) 1.3334 28.290 2043 2.125 4336 1.957 1.08832 21.245 0.0762 3340 73.343 157.2 0.07 0.49 COMBUSTOR 2 202 40.849 185.611 3248 640.1(888) 1.2801 28.532 2692 40.849 334.5(588) 1.3137 28.534 2267 1.725 3910 1.984 1.09200 21.245 0.0760 3303 66.360 155.5 0.07 1.00 37.046 2245 COMBUSTOR 0 10 41.539 160.738 3241 637.8(886) 1.2802 28.532 2689 41.539 30.801 2218 326.6(580) 1.3146 28.533 2254 1.751 3946 1.993 1.08016 21.245 0.0766 3211 60.239 151.2 0.07 1.00 COMBUSTOR 0 11 4 21 41.500 149.421 3239 637.0(885) 1.2803 28,532 2688 41.500 33.114 2294 348.9(603) 1.3119 28.533 2290 1.658 3797 1.998 1.07319 21.245 0.0773 3163 63.324 148.9 0.07 1.00 COMBUSTOR 0 12 5 21 41.839 127.999 3233 635.3(883) 1.2804 28.532 2686 41.639 -33.133 2376 372.9(626) 1.3091 28.533 2328 1.556 3623 2.008 1.05418 21.245 0.0787 3060 59.360 144.0 0.07 1.00 COMBUSTOR 0 13 6 21 42.460 100,168 3221 631,5(879) 1,2807 28,532 2681 42.460 33,487 2513 413,6(667) 1,3045 28,533 2390 1,382 3302 2,024 1,00792 21,245 0,0823 2886 51,726 135,9 0,07 1,00 COMBUSTOR 0 14 42.824 96.138 2848 632.9(795) 1.2988 27.249 2598 42.824 30.583 2171 424.3(589) 1.3214 27.249 2288 1.412 3230 2.056 0.99076 21.300 0.0839 2796 49.739 131.3 0.15 0.11 COMBUSTOR 0 15 42.834 99.018 2769 632,8(772) 1.3025 27.164 2569 42,834 30.503 2090 424.6(566) 1.3252 27.164 2251 1.433 3227 2.047 0.98873 21.300 0.0841 2794 49.586 131.2 0.15 0.02 COMBUSTOR 0 16 42.899 97.289 2756 632.3(768) 1.3031 27.152 2564 42.899 29,984 2079 425,2(563) 1.3258 27,151 2247 1.433 3219 2.047 0.98619 21.300 0.0843 2779 49.336 130.5 0.15 0.00 0 17 10 21 COMBUSTOR 44,310 73,663 2714 619,8(795) 1,3045 27,150 2546 44.310 27.569 2146 445.6(583) 1.3234 27.150 2280 1.294 2952 2.062 0.91452 21.300 0.0909 2596 41.952 121.9 0.15 0.00 COMBUSTOR 0 18 11 21 44.800 71.652 2698 614.8(750) 1.3050 27.149 2539 44.800 20.730 2131 441.2(578) 1.3239 27.149 2273 1.297 2947 2.062 0.90124 21.300 0.0923 2583 41.278 121.5 0.15 0.00

	READING =	0061	BLOCK	≈ 125	TIME :	= 515.1	62 MACI	н 6.	O PT:	745	.499	11 = 299	l e i						
		ρ	т	h		GAMMA	MOLHT	SONV	MACH	VEL	ક	WA	W	A/AC	HOFIM	Q	IVAC	PH1	ETAC
	COMBUSTOR	. (12 21		•		•			-		••		•				
	45.619			606.7	£ 7865	1.2989	27.511	2583											
	45.619	35.166	2376	466.5	(650)	1.3137	27.511	2384	1,105	2629	2.071	0.89147	21.300	0.0933	2581	36.420	121.2	0.15	0.18
	COMBUSTOR	(20	13 21		•••••					••	• •	•	•		-		• •	_
	46.250			621.1	(815)	1.3091	24.413	2658											
	46.250	37.869	2298	501.7	(696)	1.3209	24.413	2486	0.983	2445	2.243	0.87575	21.503	0.0959	2564	33.273	119.2	0.44	0.00
	COMBUSTOR			14 21	, . ,				•	-			• -	• • • • • • • • • • • • • • • • • • • •					•
	46.260	70.364	2540	621.0	(779)	1.3141	24.309	2613											
	46.260									2443	2.229	0.87525	21.503	0.0959	2564	33.226	119.2	0.44	0.01
	COMBUSTOR			15 21										•					
	46.334	70.717	1 2521	620.2	(773)	1,3150	24,294	2605				•			•				
	46.334	38,227	2171	502.4	(656)	1.3268	24.294	2428	1,000	2428	2.226	0.87157	21.503	0.0963	2566	32.891	119.3	0.44	0.00
	COMBUSTOR	(23	16 21															
	47.310	70.603	2486	609.3	(761)	1,3161	24.292	2588								•			
	47.310				(665)	1,3260	24,291	2442	0.905	2210	2.221	0.81175	21,503	0.1034	2600	27,877	120.9	0.44	0.00
	COMBUSTOR			17 21															
	48.110	68,726					24.291												
	48.110				(654)	1.3271	24,291	2424	0,919	8888	5.550	0.74546	21,503	0.1126	2662	25.612	153.8	0 - 44	0,00
	COMBUSTOR			18 21															
	48.859			591.7									.						_
	48,859	36,600			(635)	1,3294	24,296	2389	1.000	5784	2.218	0.66476	21,503	0.1263	2781	24,685	129.3	0.44	0.00
	COMEUSTOR			19 10															
	50.299			590.3															
	50.299	24.806			(024)	1.3340	21.959	2398	1,225	2438	2.401	0.54641	21.720	0.1225	2404	24,947	130.7	0.76	0.03
	COMBUSTOR		27		. 7.7.		D. D.												
	50,309			590.2					1 439	2047	2 404	A E 1670	11 750	0	2021	34 054	1 T L D	A 41 6	4 47
	50.309 Combustor				(024)	1.3340	K1.400	2341	1.220	5443	2.401	0.54570	21./20	0.3554	24/1	24.954	130.0	0.76	0.03
	50.639		28			1 7219	24 002	2440											
	50.839	20.387	1 1 5 1 5	585.1	5071	1 2251	21 082	2364	1.362	7204	2 // 0.3	0.51035	21 720	0 4445	20.28	25,384		0 76	0.00
	COMBUSTOR		59		(341)	1.3454	211102	2300	11305	3501	E . 403	0.51035	E14160	4.1005	3020	20,304	19484	0.70	0.04
	52.249			573.4	. 9481	1 3007	22 117	reac											
	52.249	21.72	2231	182.1	7799	1 3221	22.317	2541	1.206	CPAF	2.457	0.43496	21.720	0 1950	2172	20.902	186.1	0.26	A 15
	COMBUSTOR		30		(/3//		22777	2000	***	20 12	£ # 4 2)	0,43470	411160	0 1 1 7 3 0	3715	E O S YOR	14011	0 # 7 5	0 4 1 3
	54,349			559.2	(1043)	1.2892	22.638	2944											
	54.349								1.294	3432	2.495	0.35650	21.720	0.2379	3373	19.014	155.3	0.76	0.26
	COMBUSTOR			24 3					****			******			52.5	,,,,,,			0,20
	54.849			550.1		1.2879	22.668	2953											
	54.849									3568	2.498	0.34193	21.720	0.2480	3412	18,959	157.1	0.76	0.27
	COMBUSTOR	(32	25 4	, ,-,													., .	
	55,599			551.7	(1079)	1.2840	22.750	2979											
	55,599								1,384	3669	2.506	0.32232	21.720	0.2631	3466	18.378	159.6	0.76	0.29
	COMBUSTOR		33		• •	• • •	, -		- • -						•			• • • •	- •
	55.760	43.819	3177	550.8	(1084)	1.2833	22.765	2984											
	55.700									3691	2.507	0.31842	21.720	0.2665	3477	18.266	160.1	0.76	0.30
	COMBUSTOR	(34	27 4	•														• • •
	56,359	37,897	/ 3351	547,7	(1247)	1.2741	22.939	3042											
	56,359									4036	2.532	0.24935	21.720	0.3401	3634	15.639	167.3	0.76	0.36
	COMBUSTOR	(35	28 4										-					·
	57.784	42.786	3 3140	541,5	(1070)	1.2848	22.753	2969											
	57.784	7.270	2077	142.2	(676)	1.3224	22.755	2450	1.824	4470	2.506	0.23055	21.720	0.3678	3703	16,015	170.5	0.76	0.30
	COMBUSTOR		3 5 6															-	•
	57.839	36.686	3425	541.3	(1174)	1.2698	53.056	3064											
	57.839	9+298	2522	190.9	(833)	1.3025	25,032	5992	1.572	4187	2.539	0.22991	21.720	0.3689	3705	14.960	170.6	0.76	0.38
α	COMBUSTOR	. (37	30 3															
Ċ	57,979			540.6															
	51.979	0.989	2478	163.9	(817)	1.3044	23.009	c643	1,599	4226	2.537	0.22817	21.720	0.3717	3708	14,985	170.7	0.75	0.38

GAMMA MOLMT SONV MACH VEL S A/AC MIMUM IVAC PHI ETAC MIA COMBUSTOR 0 36 51 10 58,059 49.769 2960 540.5(1005) 1.2935 22.589 2903 58.059 6,068 1788 108,2(570) 1,3361 22,590 2293 2,028 4651 2,477 0,23077 21,720 0,3675 3711 16,679 170.8 0.76 0.24 COMBUSTOR 0 39 32 58,339 61.829 2765 539,5(935) 1.3026 22.415 2826 58,339 4.837 1474 73.2(471) 1.3530 22.416 2103 2.297 4830 2.440 0.23001 21.720 0.3687 3718 17.266 171.2 0.76 0.18 COMBUSTOR 0 40 53 3 61.408 2777 538.8(939) 1.3020 22.428 2831 58.569 58,565 4.864 1486 72.1(475) 1,3522 22.429 2111 2,289 4832 2.442 0.22953 21.720 0,3695 3723 17.237 171.4 0.76 0.19 COMBUSTOR 0 41 34 4 58,927 2824 536,5(956) 1,2998 22,475 2849 59.289 59.289 4.950 1539 70.4(492) 1.3490 22.475 2143 2.254 4830 2.450 0.22597 21.720 0.3755 3756 16.961 172.0 0.76 0.20 0 42 35 COMBUSTOR 33,399 3770 535,2(1301) 1,2487 23,393 3163 60.309 60.309 11.287 3006 221.9(1006) 1.2801 23.412 2859 1.381 3947 2.567 0.22453 21.720 0.3777 3756 13.771 172.9 0.76 0.50 COMBUSTOR 0 43 36 62.319 37,590 3545 526,0(1217) 1,2626 23,182 3098 62,319 9.600 2629 166.7(870) 1.2967 23.191 2704 1.568 4240 2.543 0.23235 21.720 0.3650 5760 15.310 173.1 0.76 0.43 COMBUSTOR U 44 37 63,739 35,974 3962 520,7(1372) 1,2354 23,627 3209 63.739 14.231 3334 254.2(1127) 1.2638 23.657 2976 1.227 3651 2.574 0.23664 21.720 0.3555 3760 13.542 173.1 0.76 0.58 COMBUSTOR 0 45 38 66,203 31,451 4105 509,5(1424) 1,2240 23,809 3239 66.203 10.726 3645 305.5(1243) 1.2466 23.847 3078 1.038 3195 2.985 0.22621 21.720 0.3749 3763 11.231 173.2 0.76 0.64 COMBUSTOR 0 46 39 66.579 29,226 4111 507,6(1426) 1,2228 23,620 3239 00,579 10-353 3689 318.9(1260) 1.2439 25.859 3092 0.994 3073 2.591 0.21030 21.720 0.4032 3763 10.041 173.3 0.76 0.64 COMBUSTOR REGEN 47 40 21 66,579 29.226 4374 640.8(1531) 1,2055 23,764 3321 66.579 10.474 3637 297.9(1240) 1.2446 23.859 3071 1.349 4142 2.622 0.21030 21.720 0.4032 3878 13.537 178.5 0.76 0.64 NOZZLE 88,815 29.226 4111 507.6(1398) 1.2228 23.820 3239 0.819 1906 =361.4(599) 1.3159 23.882 2285 2.886 6594 2.591 0.04378 21.720 1.9372 4858 4.486 223.7 0.76 0.64 68.815 NOZZLE. 49 42 29,226 4111 507,6(1398) 1,2228 23,820 3239 88.815/ 88,815 0.388 1588 -469.8(490) 1.3312 23.882 2098 3.334 6993 2.591 0.02640 21.720 3.2128 5040 2.869 232.1 0.76 0.64 NOZZLF AE REGEN 50 43 29,226 4374 640,8(1531) 1,2055 23,764 3321 88.815 88.815. 0.883 2123 -285.6(674) 1.3068 23.882 2403 2.833 6808 2.622 0.04377 21.720 1.9373 5034 4.632 231.8 0.76 0.64 NOZZLE PO REGEN 51 44 88.815 29,226 4374 640.8(1531) 1.2055 23.764 3321 0,388 1743 #417.5(543) 1.3234 23.882 2191 3.321 7277 2.622 0.02503 21.720 3.3884 5249 2,830 241.7 0.76 0.64 88.819 FICTIVE COMBUSTR 71 64 66,579 308,326 5074 507,6(1789) 1,1834 24,915 3462 60,579 0.588 1274-1029.9(375) 1.3375 25.182 1834 4.783 8771 2.422 0.04352 21.720 1.9484 6115 5.935 281.5 0.76 1.00 FICTIVE NOZZLE 72 65 88.815 22,058 4044 478,3(1400) 1,2244 23,825 3215 88,615 0.930 2058 -305.2(652) 1.3094 25.882 2369 2.648 6273 2.607 0.04378 21.720 1.9371 4696 4.268 216.2 0.76 0.64

XABS	P=IB	P=05	PDA .	Oox		d≠1B		Q=OB		CAWALL	P=18/PS0	P=18/P10	P#08/P80	P=0B/P10
6.981E#01	1.650E 00	0.000	-4.553E=01	0.000		0.000		0.000		2.470E=02	2.707E 00	1.408E=03	0.000	0.000
1.836E 01	1.0508 00	0.000	+3.498E U1	0.000		0.000		0.000		1.634E 02	2.707E 00	1.408E+03	0.000	0.000
3.070E 01	2.240E 00	0.000	=1.683£ 02	0.000		0.000		0.000		5.053E 02	5.776E 00	3.005E-03	0.000	0.000
3,508E 01	3.930E 00	0.000	#3.683E 02	0.000		0.000		0.000		6.804E 02	1.013E 01	5.2726=03	0.000	0.000
3,555E 01	4.040E 00	0.000	04.046E UZ	0.000		0.000		0.000		7.013E 02	1.0428 01	5.419E-03	0,000	0.000
3.606E 01	3.960E 00	0.000	-4.452£ 02	-3.372E	02	-3.372E	02	0.000		7.246E 02	1.021E 01	5.312E=03	0.000	0.000
3,648E 01	4.244E 00	0.000	=4.803E 02	-3.454E	02	-3.454E	02	0.000		7.443E 02	1.094E 01	5.693E=03	0.000	0.000
3.672E 01	4.238E 00	5.680E 90	9 .5.587£ 02	-5.5V1E	02	-3.501E	02	0,000		7.555E 02	1.0938 01	5.685E=03	1.465E 01	7.619E=U3
3.672E 01	4.238E 00	5./17E 0	5.588£ 02	-3.502E	05	=3.502E	02	0.000		7.558E 02	1.093E 01	5.684E-03	1,474E 01	7.668E=03
3.701E 01	4.230E 00		9-622E U2					0.000		7.856E 02	1.091E 01	5.674E=03	1.923E 01	1.0005-02
3.739E 01	4.089E 00		=5.597£ 02					0.000		8.254E 02	1.054E 01	5.4856+03	2.514E 01	1.3086=02
3.803E 01	3.850£ 00		-3.399£ 02					0.000		8.943E 02	9.927E 00	5.1646#03	3.222E 01	1.676E#02
3.8755 01	1.145E 01		-5,498E 02							9.746E 02	2.953E 01	1.5366.02	4.017E 01	2.090E=02
3.885E 01 3.901E 01	1.250E 01		#5,540E 02							9.856E 02	3.222E 01	1.6766-02	4.126E 01	2.146E=02
3.950E 01	1.8098 01		-5.611£ 02							1.004E 03	3.661E 01 4.664E 01	1.905E=02 2.426E=02	4,335E 0; 4,969E 01	2.255E=02 2.585E=02
3.987E 01	1.709E 01		=5,839E 02 =5,886E 02							1.105E 03	4.406E 01	2.2926=02	5.447E 01	2.834E=02
4.000E 01	1.673E 01		#5.883E 02							1.1185 03	4.314E 01	2.244E-02	5.207E 01	2.709E=U2
4.034E 01	2.693E 01		-5.992E 02							1.157E 03	6.944E 01	3.613E-02	4.590E 01	2.388E-U2
4.040E 01	2.878E 01		-6.038E 02							1.164E 03	7.421E 01	3.660E-02	5.024E 01	2.614E=02
4.041E 01	2,908E 01		-6.043E 02							1.166E 03	7 498E 01	3.9016-02	5.095E 01	2.650E=U2
4.085E 01	4.229E 01		-6.323E 02							1.217E 03	1.090E 02	5 673E=02	8,199E 01	4.2666.02
4.134E 01	5.705E 01		-7.133E 02							1.275E 03	1.4718 02	7.653E-02	1.173E 01	6.103E=03
4.150E 01	6,191E 01		=7.585€ 02							1.294E 03	1.596E 02	8.305E=02	1.113E 01	5.789E=03
4.184E 01	6.2446 01	3.825E 0	-8.537E 02	-6.872E	02 4	-6.212E	50	≈6.599E	01	1.334E 03	1.610E 02	8.376E-02	9.863E 00	5.131E=03
4.246E 01	6.341E '01		-1.015E 03						01	1.408E 03	1.635E 02	8.506E=02	9.182E 00	4.777E=03
4.282E 01	5.776E 01		=1.098E 03						02	1.451E 03	1.489E 02	7.748E=02	8.784E 00	4.570E+03
4,283E 01	5.760E 01		=1.101E 03							1.452E 03	1.485E 02	7.7276-02	8.773E 00	4.564E=03
4+290E 01	5.659E 01) *1.114E 03							1.460E 03	1.459E 02	7.591E-02	8.702E 00	4,527E=03
4.431E 01	3.465E 01		=1.274E 03							1,630E 03	8.935E 01	4.648E=02	5.282E 01	2.748E=02
4-480E 01	2.704E 01		+1.279E 03							1.690E 03	6.971E 01	3.6276-02	6.813E 01	3.544E+02
4.562E 01	3.398E 01		01.270£ 03							1.789E 03 1.867E 03	8.763E 01	4.559t=02 5.277E=02	9.372E 01	4.8766=02
4.626E 01	3.943E 01		-1.245E 03							1.868E 03	1.014E 02	5.289E+02	9,385E 01 9,385E 01	4.882E=U2 4.882E=U2
4.633E 01	4.005E 01		-1.242E 03							1.877E 03	1.033E 02	5.373E+02	9.386E 01	4.8836-02
4.731E 01	4 834E 01		-1.197E 03							1.997E 03	1.246E 02	6.484E-02	9.406E 01	4.893E=02
4.811E- 01	4.477E 01		-1 127E 03							2.097E 03	1.1546 02	50#3000.0	9.42ŽE 01	4.902E=02
4.886E 01	3.660E 01		-1.001E 03							2.190E 03	9.437E 01	4.909E-02	9.437E 01	4.909E=02
5.03oF 01	2.481E 01		€7.727E 02							2.370E 03	6.396£ 01	3.327E-02	6.396E 01	3.327E-02
5.031E 01	2.472E 01		#7.714E 02							2,371E 03	6.375E 01	3.316E=02	6.375E 01	3.316E=02
5.084E 01	2.038E 01	2.038E 0	■7,091E 02	#2.54SE	03	-1.233E	03	=1.362E	03	2,437E 03	5.256E 01	2.734E+02	5.256E 01	2.734E=02
5.225E 01	2.172E 01	2.172E 0	. •5.534E 02	≈2.850E	03	-1.305E	03	#1,544E	03	2,615E 03	5,602E 01	2.914E=02	5.602E 01	2.914E=02
5.435E 01	1.732E 01		-3.385£ 02							2.881E 03	4.467E 01	2.324E=02	4.467E 01	2.324E-V2
5.485E 01	1.580E 01		-2.954E 02							2.945E 03	4.073E 01	2.119E=02	4.073E 01	2.119E=U2
5.560E 01	1.467E 01		₩2.365E 02							3.041E 03	3.784E 01	1.9686=02	3.784E 01	1.968E=02
5.576E 01	1.443E 01		-2.244E 02							3.061E 03	3.721E 01	1.9366-02	3.721E 01	1.936E=02
5.636E 01 5.778E 01	7.342E 00		#6,519E 01							3.102E 03	1.893E 01	9.848L+03	3.491E 01	1.8166=02
5.784E 01	7.276£ 00	7.276F 0(3.209E 03	1.876E 01	9.760E#03	1.876E 01	9.760E=03
5.798E 01	1.155E 01 1.155E 01	7.034E 0(3.216E 03	2.978E 01	1.549E-02	1.814E 01	9.4366#03
5.806E 01	6.068E 00	6.068E 0								5.254E 03	2.978E 01	1.549E=02	1.655E 01	8.6115#03
5.834E 01	4.837E 00	4.837F 0								3.244E 03 3.280E 03	1.565E 01 1.247E 01	8.139E=03 6.489E=03	1.565E 01	8.1392#03
5.856E 01	4.864E 00	4.864E 0								3.309E 03	1.254E 01	6.5256#03	1.247E 01 1.254E 01	6.489E=03 6.525E=03
5 929E 01	4.950E 00	4.950E 0								3.402E 03	1.2768 01	6.6406.03	1.276E 01	6.640E#03
6.031E 01	1 129E 01	1.129E 0								3.532E 03	2.910E 01	1.5146-02	2.910E 01	1.5146-02
6.232E 01	9 600E 00	9.600F 0								5.790E U3	2.475L 01	1.2886-02	2.475E 01	1.2886=02
-		- '							•	- · ·				* # # # # # # # # # # # # # # # # # # #

	XABS	P•18	P=08	PDA	QOX	G-IB	Q=08	CAMALL	P#18/P80	P=18/PT0	P=08/P80	P=08/P10
	6.374E 01	1.4238 01	1.423E 01	6.418E 01	=3.995E	03 #1.687E 0	3 -2.50eE 03	3.972E U3	3.669E 01	1.909E=02	3.459E 01	1.9091-02
<u> </u>	0.650E 01	1.673E 01	1.673E 01	6,418E 01	#4.258E (25 -1.761E 0	3 -2.476E 03	4,289E 03	4.313E 01	2.244E+02	4.313E 01	2.2446-02
	6.658E 01	1.560E 01	1.711E 01	6.418E 01	-4.279E (03 -1.774E 0	3 +2.505E 03	4,337E 03	4.022E 01	2.093E+02	4.411E 01	2.2956-02
	6.665E 01	1.560E 01	1.715E 01			03 -1. 776£ 0		4.342E 03	4.022E 01	2.093E=02	4.421E 01	2.3000=02
	6.682E 01	1.483E 01	1.735E 01			03 *1. 783£ 0:		4.368E 03	3.825E 01	1.9906.02	4.474E 01	2.327E=02
	6.808E 01	8,470E 00	6 990E 00	1.974E 02	•4.457E (03 =1.831E 0	5 =2.626E 03	4.583E 03	2.184E 01	1.136E=02	1.8022 01	9.3766=43
	6.915E 01	6.199E 00	7.065E 00	3.427E 42	=4.507£ (3 -1.846E 0	3 #2.661E 03	4,665E 03	1.598E 01	8.316E=03	1.822E 01	9.4/7E=03
	6.992E 01	3.590E 00	5.484E 00)3 =1.860E 0:		4.760E 03	9.257E 00	4.816E=03	1.414E 01	7.356E=03
	7.064E 01	2.786E 00	4.005E 00			03 -1.871E 0:		4.848£ 03	7.184E 00	3.737E=03	1.035E 01	5.372E-03
	7.125E 01	2.105E 00	3.248E 00			03 #1.879E 0:		4.922E 03	5.428E 00	2.824E-03	8.376E 00	4.357E-03
	7.220E 01	1.496E 00	2.070E 00			33 =1.887E 0		5.0366 03	3.857E DO	2.006E=03	5.337E 00	2.777€≈∪3
	7.263E 01	1.2205 00	1.931E 00	7.544E 02	-4.727E	03 -1.890E 0	3 -2.837E 03	5.088E 03	3.146E 00	1,6366=03	4.978E 00	2,5908=03
	7.416E 01	8.147E=01	1.435E 00	8.170E 02	=4.780E (3 -1.900E 0	3 =2.880E 03	5.273£ 03	2.101E 00	1.093E=03	3.700E 00	1.9258-03
	7,431E 01	7.7508=01	1.271E 00	8.2156 02	#4.785E (3 -1-901E 0	3 =2.884E 03	5.290E 03	1.998E 00	1.040E=03	3.277E 00	1.705E=03
	7.506E 01	8.183E=01	4.500E=01	8 444F 05	#4,808E (03 =1.905E 0	5 -2.9 03E 03	5.374E 03	2.110E 00	1.0985=03	1.160E 00	6.036E#U4
	7.506E 01	0.165E=01	4.456E=01	8,5085 02	-4.808E	73 +1.905E 0:	\$ -2.903E 03	5.375E 03	2.110E 00	1.098E=03	1.149E 00	5.977E=0A
	7.639E 01	8.950E=01	0.000	8.689E 02	r4.854E (03 w1.912E 0	1 -2,942E 03	5.426E 03	2.308E 00	1.2016=03	0.000	0.000
	7.924E 01	1.665E 00	0.000			03 =1.924E 01		5,525E 03	4.293E 00	2.233E-03	0.000	0.000
	8-314E 01	1.185E 00	0.000	9.810E 02	=4.861E (03 -1.938 E 0:	3 -2.942E 03	5,630E 03	3.055E 00	1,590E=03	0.000	0.000
	8.595E 01	9.200E=01	0.000	1.004E 03	₩4.893E (3 -1.951E 0	-2,942E 03	5.684E 03	2.372E 00	1.234E=03	0.000 -	0.000
	8.8815 01	1.250E 00	0,000	1.031E 03	-4.915E	3 =1.973E 0	5 -2.942E 03	5.707E 03	3.223E 00	1.677E=03	0.000	0.000
	8.881E 01	1,251E 00	0.000	1.031E 03	#4.915E (3 -1.973E 0	5 -2.942E 05	5.707£ 03	3.225E 00	1.678E=03	0.000	0.000

x	DORAG	CORAG	CF	нс
4.040E 01	1.220E 02	1.220E 02	2.313E=03	5.285E=02
4.041E 01	2.123E*01	1.223E 02	2.535E=03	6.184E=02
4.085E 01	9.286E 00	1.315E 02	2.643E=03	7.901E802
4.134E 01	1.044E 01	1.420E 02	2.819E=03	6.554E=02
4.150E 01	3.510E 00	1.455E 02	2.870E=03	6.706E=02
4.184E 01	7.164E 00	1.526E 02	2.956E=03	6.406E=02
4.246E 01	1.242E 01	1.651E 02	3.092E+03	5.809E=02
4.282E 01	7.004E 00	1.721E 02	3.2676=03	5.205E=02
4.283E 01	1.631E=01	1.723E 02	2.994E=03	5.706E=02
4.290E 01	1.147E 00	1.734E 02	2.957E=03	5.705E=02
4.431E 01	2.340E 01	1.968E 02	3.0756*03	4.906E=02
4.480E 01	7.612E 00	2.044E 02	3.0756*03	4.844E=02
4.562E 01	1.197E 01	2.164E 02	3.090E*03	5.503E=02
4.625E 01	8.928E 00	2.253E 02	3.5376*03	4.999E=02
4.626E 01	1.393E=01	2.254E 02	3.2006*05	5.674E=02
4.633E 01	9.475E=01	2.264E 02	3.1396*03	5.821E=02
4.731E 01	1.146E 01	2.379E 02	3.126E=03	5.813E=02
4.811E 01	8.257E 00	2.461E 02	3.083E=03	5.612E=02
4.886E 01	7.140E 00	2.533E 02	2.990E=03	5.399E=02
5.030E 01	1.383E 01	2.671E 02	3.207E=03	4.211E=02
5.031E 01	9.480E=02	2.672E 02	2.867E=03	4.748E=02
5.084E 01	4.735E 00	2.719E 02	2:792c=03	4.345E=02
5.225E 01	1.141E 01	2.833E 02	2:760E=03	4.340E=02
5.435E 01	1.488E 01	2.982E 02	2:840E=03	5.559E=02
5.485E 01	3.528E 00	3.017E 02	2:992E=03	3.173E=02
5.560E 01	5.332E 00	3.071E 02	2:969E=03	3.045E=02
5.576E 01	1.130E 00	3.062E 02	3:006E=03	2.950E=02
5.736E 01	2,014E 00	3.102E 02	2.893E=03	2.343E=02
5.778E 01	4,921E 00	3.151E 02	2.893E=03	1.835E=02
5.784E 01	3,115E=01	3.154E 02	2.816E=03	2.191E=02
5.798E 01	7,692E=01	3.162E 02	2.965E=03	2.041E=02
5.806E 01	5,092E=01	3.167E 02	3.319E=03	1.438E=02
5.834E 01 5.856E 01 5.929E 01 6.031E 01 6.232E 01 6.374E 01	1.786E 00 1.240E 00 3.803E 00 5.056E 00 1.068E 01 7.991E 00	3.185E 02 3.197E 02 3.235E 02 3.286E 02 3.393E 02 3.473E 02	2.5618=03 2.404E=03 2.399E=03 2.636E=03 3.060E=03 3.021E=03	1.514E=02 1.590E=02 1.603E=02 2.566E=02 2.030E=02
6.620E 01 6.658E 01 6.662E 01 6.682E 01	1.230E 01 1.700E 00 1.746E=01 8.848E=01 7.873E 00	3.596E 02 3.613E 02 5.614E 02 3.623E 02 3.702E 02	3.2596-03 3.3696-03 3.4166-03 3.4106-03 3.2296-03	2.434E=02 2.257E=02 2.254E=02 2.279E=02 1.697E=02
6.915E 01	3.059E 00	3.733E 02	3.200E=03	1.554E=02
6.992E 01	3.274E 00	3.765E 02	3.133E=03	1.227E=02
7.064E 01	2.676E 00	3.792E 02	3.085E=03	1.011E=02
7.125E 01	1.999E 00	3.812E 02	3.049E=03	8.5/9E=03
7.220E 01	2.627E 00	3.838E 02	2.988E=03	6.413E=03
7.263E 01 7.416E 01 7.431E 01 7.506E 01 7.506E 01 7.639E 01	1.031E 00 3.200E 00 2.621E=01 1.082E 00 1.763E=03 6.325E=01	3.849E 02 3.881E 02 3.883E 02 3.894E 02 3.894E 02	2.9696+03 2.9146+03 2.8986+03 2.8216+03 2.8206+03 2.8666+03	5.856E=03 4.550E=03 4.235E=03 2.937E=03 2.949E=03 3.811E=03
7.924E 01	1,619E UO	3.917E 02	2.945t+03	6.026E=03
8.314E 01	1,856E 00	3.935E 02	2.874E+03	4.650E=03

READING = 0061 BLOCK = 125 TIME = 212.102 MACH 6.0 Pl = 145.499 TT = 2991.1

X		DDRAG	CURAG		CF	HC
 8.8812	01	8.021E=01 3.377E=01 0.000	3.943E 3.947E 3.947E	ΟŽ	2.856E=03	4.745E-05

RAMJET PERFORMANCE

11.11.001	1 Mill will install
ENGINE PERFURMANCE	Inte7
MEASURED THRUST	ANGLE OF ATTACK
REGENERA) I VE*COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	INLET PROCESS EFFICIENCY = SUPSONIC 0.9156 KINETIC ENERGY EFFICIENCY = SUPERSONIC 0.9298 KINETIC ENERGY EFFICIENCY = SUESUNIC 0.8857 ENTHALPY AT PO = SUPERSONIC
MUMENTUM AND FORCES	CUMBUSTOR
INLET FRICTION DRAG	FUEL-AIR RATIO
STATIONS	
· · · · · · ·	FUEL INJECTORS
NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A 40.400 A 18 42.824 B 1C 44.300 2A 50.299 D 2C 46.250 E 3A 55.589 3B 57.774 4 46.324

Reading 61

t = 222.06 sec.

SUMMARY REPORT

				ŞUI	M M A	RY	REP	U H I							
	PT	Н	GAMMA MOLWT	SONV	HACH	γEL	\$	W/A	*	A/AC	MURTP	ଭ	IVAC	PHI	ETAC
	WIND TUNNEL 1 0.000 745.749 299: 0.000 0.388 40	0 5 667.0(792) 31.6(97)	1.2931 28.955	2577 987 9	5,992	5912	1,827	0.10604	21,296	0.7841	3991	9.743	187.4		
	SPIKE TIP NS 2 0,600 18,700 299	0 6 67-06 7021	1.2930 28.954	2577											
	0.600 17.038 292 WIND TUNNEL 3	0 0	1,2950 28 954	2552	0.381	973	2.080	0.10604	21.296	0.7841	4066	1.603	190.9		
	0.000 745.749 299 0.000 0.401 40	30.7(98)	1.2931 28.955	2577 991	5.960	5909	1.827	0.10846	21.781	0.7841	4081	9.959	187.3		
	SPIKE TIP NS 4 0,600 18,700 299 0,600 16,951 292	0 0 667.0(792) 5 647.0(773)	1.2930 28.954	2577 2551	0.392	999	2.080	0.10846	21.781	0.7841	4081	1.084	187.3		
	INLET THROAT 5 40,400 305,483 290 40,400 19,042 147	0 # 3 541-91 7481	1.2957 28.954 1.3492 28.954	2544							3354	76.047	157.5		
	INLET UPNRBK 6 40,400 305,483 290	0 3 3 641-01 7481	1 2957 28.95#	2544											
	40.400 16.328 142 INLET DNNR8K 7	1 221.3(350) 0 4	1,1525 28,954	1817	2,526	4588	1.879	0.98776	21.296	0.0842	3389	70.426	154*1		
	40;400 139;319 890; 40;400 119;039 860; COMBUSTOR 0 8	5 611.1(738)	1.2957 28.954 1.2990 28.954	2501	0.497	1242	1.933	0.98776	21.296	5480.0	3389	19.071	159+1		
	40.410 230.328 306 40.410 24.775 180	6 642.7(833) 6 269.2(464)	1.2888 28,369	2631 2633	2.105	4323	1.956	1.08878	21.343	0.0765	3354	75.151	157.1	0.07	0,56
	COMBUSTOR 0 9 40,835 188,894 322 40.835 35.915 220	6 641 01 8791	1.2812 28,564	2682 2245	1.756	3941	1.978	1.09245	21.343	0.0763	3316	66.914	155.4	0.07	1.00
	COMBUSTOR 0 10 41.325 163.067 321	3 21 9 638-77 8771	1.2813 28.566	2679			١					66.601	151.1	0 - 0.7	1 - 00
	41,325 30.143 218 COMBUSTOR 0 11 41,500 150,720 321	4 21	1.3162 28.565		14//3	3704	1,700	1,00101	411040	V , U , 7 .	*****			••••	.,
	41,900 32,940 226 COMBUSTOR 0 12	2 348 1{ 592; 5 21	1,3133 28,565	2274	1.675	3808	1.993	1.07366	21,343	0.0776	3173	63,536	148.7	0.07	1.00
) 1	41.825 130.008 321 41.825 32.579 234	0 370.8(615	1.2815 28,564	2676	1.578	3645	2.003	1.05561	21,343	0.0789	3076	59,792	144.1	0.07	1.00
4	COMBUSTOR 0 13 42,460 101,174 319 42,460 32,952 247	9 632-61 8711	1,2818 28,564	2672	1.400	3323	2.019	1.00828	21.343	0.0826	2902	52,065	136.0	0.07	1.00
9	COMBUSTOR 0 14 42,810 97,324 285	7 21	1.2985 27.37	2594								60 1E8		0.18	0 11
i	42.810 30.352 216 COMBUSTOR 0 15	8 21	1,3215 27,37		1.460	3251	2.048	0.44504	C1+244	0.0041	2010	50,158	13110	0,14	0.11
3	42.820 100.176 278 42.820 30.277 208 COMBUSTOR 0 16	9 422.9(563	1.3019 27.29 1.3251 27.29	3 2246	1.447	3249	2.040	0.99197	21.394	0.0842	2813	50.084	131,5	0.14	20.0
	42.885 98.247 276 42.885 29.794 208	8 633,4(768 1 423,9(561	1.3025 27.28	2563	1.444	3238	2.040	0.98730	21.394	0.0846	2799	49,684	130.6	0.14	0,00
	44.310 78.500 272	10 21 8 621,50 756 3 457,60 594) 1.3038 27.27°) 1.3216 27.27°	9 2546	1.246	2863	2,051	0.91678	21.394	0.0911	2636	40.795	123.2	0.14	0.00
	COMBUSTOR 0 18 CO 44.800 78.327 271	11 21 · 3 616.91 752	1.3043 2/.27	9 2540								30 674	127.7	0.17	0 - 00
	44.800 31.914 219	0 457.16 593	1.3217 27.27	4 4447	1.551	2028	£ 1000	0.701//	C1 + 344	U + U7E0	2020	39,636	12343	V # 1 H	J # V U

ORIGINAL PAGE IS OF POOR QUALITY

1 1 GAMMA MOLWT SONV MACH VEL S W/A AJAC HOMIN G IVAC PHI ETAC COMBUSTOR 0 19 12 21 φ 45.605 82.799 2732 609.5(757) 1.3031 27.325 2545 ₩ 45,605 42.461 2333 486.7(635) 1.3163 27.325 2364 1.049 2479 2.047 0.09362 21.394 0.0935 2665 34.421 124.6 0.14 0.05 COMBUSTOR 0 20 13 21 75,398 2652 630,2(829) 1,3096 23,983 2683 46.250 46.250 44.503 2337 521.3(722) 1.3202 23.983 2529 0.923 2334 2.266 0.87915 21.642 0.0961 2665 31.885 123.2 0.49 0.06 COMBUSTOR 0 21 14 21 46.260 77.206 2536 630.1(791) 1.3149 23,876 2635 46.260 44.535 2219 521.3(683) 1.3256 23.676 2475 0.942 2333 2.251 0.87876 21.642 0.0962 2666 31.855 121.2 0.49 0.01 COMBUSTOR 0 22 15 21 46,320 77,585 2517 629,5(785) 1,3157 23,860 2627 46.320 44.724 2202 521.4(678) 1.3264 23.860 2467 0.943 2326 2.249 0.87554 21.642 0.0965 2670 31.646 123.4 0.49 0.00 COMBUSTOR 0 25 16 21 47.310 77.583 2484 618.8(774) 1.3169 23.857 2611 47.310 47,658 2208 524,5(680) 1,3262 23,657 2470 0,879 2173 2,244 0,81484 21,642 0,1037 2733 27,515 126,3 0,49 0,00 0 24 17 21 COMBUSTOR 75.795 2457 609.8(765) 1.3178 23.857 2998 48-110 48.110 44.848 2162 509.0(664) 1.3278 23.857 2446 0.918 2246 2.242 0.74841 21.642 0.1129 2808 26.125 129.7 0.49 0.00 COMBUSTOR 0 25 18 48.845 72.123 2609 601.6(814) 1.3105 24.019 2660 48.845 38.025 2236 473.5(687) 1.3232 24.019 2475 1.023 2832 2.263 0.66905 21.642 0.1263 2933 26.322 135.5 0.49 0.07 COMBUSTOR 0 26 19 50.285 63,509 2544 604.1(887) 1,3184 21,360 2791 50.285 27.964 2082 428.1(712) 1.3316 21.360 2540 1.168 2968 2.485 0.55102 21.904 0.1552 3132 25.413 143.0 0.87 0.08 COMBUSTOR 27 63,472 2546 604,0(888) 1,3153 21,361 2792 50.295 50.295 27.895 2082 427.5(712) 1.3316 21.361 2540 1.170 2972 2.485 0.55030 21.904 0.1554 3133 25.414 143.1 0.87 0.08 COMBUSTOR 0 28 21 61.797.2611 599.0(911) 1.3122 21.426 2820 50,825 50.825 24.192 2078 395.7(709) 1.3309 21.426 2533 1.259 3189 2.495 0.51466 21.904 0.1662 3200 25.504 146.1 0.87 0.10 COMBUSTOR 25 62 0 52.235 54.115 3024 586.7(1064) 1.2925 21.806 2985 52.235 26.100 2555 401.7(882) 1.3086 21.807 2761 1.102 3042 2.547 0.43863 21.904 0.1950 33/5 20.739 154.1 0.87 0.22 COMBUSTOR 0 30 23 54,335 49.382 3339 571.2(1182) 1.2764 22.126 3095 54.335 18.487 2680 306.4(924) 1.2997 22.130 2798 1.301 3640 2.579 0.35951 21.904 0.2379 3604 20.336 164.6 0.87 0.31 COMBUSTOR 0 31 24 54.835 49,308 3335 567.8(1180) 1.2765 22.129 3092 54.835 . 16.379 2603 275,1(894) 1.3023 22,133 2760 1,387 3827 2.579 0.34482 21.904 0,2480 3646 20.508 166.4 0.67 0.31 COMBUSTOR 0 32 25 55.585 47.839 3408 563.0(1207) 1.2725 22.208 3116 55,585 15.154 2638 253.3(906) 1,3000 22.213 2771 1.421 3936 2.586 0.32504 21.904 0.2631 3701 19.884 169.0 0.87 0.34 COMBUSTOR 0 33 26 % 55.760 47.549 3421 562.0(1213) 1.2717 22.224 3120 55.760 14.868 2642 248.1(907) 1.2996 22.229 2771 1.430 3963 2.587 0.32077 21.904 0.2666 3713 19.755 169.5 0.87 0.34 COMBUSTOR 0 34 27 56.345 41.178 3604 558.6(1282) 1.2611 22.406 3176 10.846 2695 187.8(924) 1.2952 22.416 2782 1.545 4308 2.612 0.25146 21.904 0.3401 3877 16.834 177.0 0.87 0.40 56.345 COMBUSTOR 0 35 28 57.770 46.450 3382 551.8(1197) 1.2734 22.210 3105 57.770 7.651 2244 102.6(757) 1.3140 22.215 2569 1.846 4741 2.585 0.23242 21.904 0.3679 3949 17.125 180.3 0.07 0.34 COMBUSTOR 0 36 29 57.825 38,972 3736 551,6(1332) 1,2528 22,551 3212 57.825 10.098 2800 164,5(961) 1.2894 22,567 2821 1.560 4401 2.624 0.23176 21.904 0.3690 3951 15.852 180.4 0.87 0.44 COMBUSTOR 0 37 30 57.965 39.224 3712 551.0(1323) 1.2543 22.528 3205 57.965 9.791 2756 157.1(945) 1.2913 22.543 2802 1.585 4440 2.622 0.23010 21.904 0.3717 3954 15.875 180.5 0.87 0.43

GAMMA MOLWY SONV MACH VEL S M/A AZAC MUNTH Q IVAL PHI ETAC COMBUSTOR 0 38 31 11 58.045 53.818 3196 550.7(1127) 1.2831 22.041 3041 58.045 6.443 1943 66.6(649) 1.3279 22.043 2413 2.040 4922 2.558 0.23276 21.904 0.3674 3957 17.803 180.6 0.87 U.29 COMBUSTOR 0 39 32 5 65,963 2996 549,6(1052) 1,2928 21,663 2968 58.324 58.329 5.212 1622 30.0(936) 1.3442 21.864 2226 2.290 5099 2.522 0.23191 21.904 0.3688 3904 18.378 181.0 0.87 0.23 COMBUSTOR 0 40 33 58.551 54.730 3195 548.8(1126) 1.2831 22.044 3041 56.21 602) 1.3287 22.046 2401 2.064 4955 2.556 0.23151 21.904 0.3694 3969 17.826 181.2 0.87 0.29 58.551 6.301 1924 COMBUSTOR 0 41 34 59.275 39.273 3782 546.2(1349) 1.2498 22.609 3224 59.275 9.787 2817 145.2(9.7) 1.2860 22.628 2824 1.586 4479 2.625 0.22788 21.904 0.3753 3990 15.863 182.2 0.87 0.46 COPBUSTOR 0 42 35 60.295 36.268 4069 542.4(1459) 1.2296 22.909 3295 60.295 11.737 3255 185.1(1131) 1.2668 22.951 2989 1.415 4229 2.647 0.22643 21.904 0.3777 4014 14.880 183.3 0.87 0.55 COMBURTOR 0 43 56 62,305 40.832 3822 533.9(1364) 1.2470 22.678 3233 62.305 10.050 2845 126.40 976) 1.2860 22.699 2831 1.595 4516 2.622 0.23431 21.904 0.3650 4014 16.444 183.5 0.87 0.48 CUMBUSTOR 0 44 37 63.725 36.355 4313 527.6(1553) 1.2104 23.203 3344 63.725 15.350 3690 232.7(1298) 1.2420 23.273 3129 1.288 3841 2.655 0.24066 21.904 0.3653 4012 14.565 183.2 0.87 0.64 COMBUSTOR 0 45 38 33.711 4439 514.3(1601) 1.1986 23.372 3364 66.189 66.189 17.110 3959 272.7(1403) 1.2237 23.458 3204 1.005 3477 2.665 0.22812 21.904 0.3749 4010 12.326 183.1 0.87 0.70 COMBUSTOR 0 46 39 3 66,565 31.249 4460 512.1(1609) 1.1956 23.401 3366 66.565 16.956 4031 292.1(1432) 1.2162 23.487 3224 1.029 3317 2.672 0.21207 21.904 0.4032 4010 10.933 183.1 0.87 0.71 COMBUSTOR REGEN 47 40 21 66.565 31.249 4660 636.0(1693) 1.1821 23.314 3428 66.565 8.173 3740 187.9(1313) 1.2319 23.516 3121 1.567 4891 2.699 0.21207 21.904 0.4032 4174 16.120 190.6 0.87 0.71 NOZZLE 48 41 88,501 31.249 4460 512.1(1569) 1.1956 23.401 3366 88.801 0.909 2194 #463.7(716) 1.2993 23.551 2453 2.848 6988 2.672 0.04414 21.904 1.9373 9208 4.794 237.8 0.87 0.71 NOZŽLE 49 42 88.801 31.249 4460 512.1(1569) 1.1956 23.401 3366 88,801 0.388 1795 0606.7(573) 1.3165 23.551 2234 3.349 7482 2.672 0.02464 21.904 3.4702 5439 2.866 248.5 0.87 0.71 NOZZLE - AE REGEN 50 43 88,801 31.249 4660 636.0(1693) 1.1821 23.314 3428 88.801 0-969 2395 -389.2(790) 1.2915 23.551 2556 2.803 7162 2.699 0.04415 21.904 1.9371 5357 4.914 244.6 0.87 0.71 NOZZLE PO REGEN SI 44 88.801 31.249 4660 636.0(1693) 1.1821 23.314 3428 0.388 1939 -556.0(624) 1.3099 23.551 2315 3.330 7723 2.699 0.02356 21.904 3.6302 5619 2.827 256.5 0.87 0.71 88,801 FICTIVE COMBUSTR 71 64 66.565 305.483 5263 512.1(1924) 1.1702 24.291 3550 0.388 1406-1163.3(427) 1.3263 24.714 1937 4.727 9156 2.494 0.00000 21.904 2.1167 6444 5.749 294.2 0.87 1.00 66.565 FICTIVE NOZZLE 72 65 88,801 21.052 4367 479.6(1579) 1.1951 23.404 3337 88,801 1.093 2455 =366.9(812) 1.2893 23.551 2585 2.518 6508 2.698 0.04415 21.904 1.9371 4973 4.465 227.0 0.87 0.71

XABS	₽=18	P=08	PDA	Q O X	U≕IB	(4乗り台	CAMALL	P=18/P50	₽#18/P10	P⇔UB/180	P=OB/PIO
6.372E 01	1.535E 01	1.535E 01		#4.085E 0:	#1.692E	03 =2.3958 03	3.972E 03	3.956E 01	2.0586-02	5.956E 01	2.0586-02
6.619E 01	1.711E 01	1.711E 01		-4.375E 0.			4.289E 03	4.410E 01	2.2946-02	4.410E 01	5.2946*05
6,656E 01	1.654E 01	1.738E 01				03 -2.640t 03	4.337E 03	4.2628 01	2.218E=02	4,479E 01	2.330t=02
6,660E 01	1.654E 01	1.741E 01				03 -2,643E 03	4.342E 03	4.262£ 01	2.218E=02	4.486E 01	2.334E+02
6.680E 01	1.570E 01	1.755E 01				03 =2.661E 03	4.508E 03	4.046E 01	2,105E=02	4.523E 01	2.3536=02
6.846E 01	8.720E 00	7.360E 00				03 -2.784E 03	4,583E 03	2.247E 01	1,169E=02	1.897E 01	9.8692-03
6.913E 01	6.312E 00	7-147E 00				03 -2.823E 03	4.665E 03	1,6278 01	8.4646-03	1.842E 01	9.5846#03
6.990E 01	3.545E 00	5.516E 0n				03 -2.869E 05	4.76DE 03	9.137E 00	4,754E=03	1.422E 01	7.396E=03
7,062E 01	2.779E 00	3.9900 00				03 -2.915t 05	4.848E 03	7.162E 00	3.726E=03	1.028E 01	5.350E=03
7.123E 01	2.130E 00	3.278E 00				03 -2.9536 03	4.922E 03	5.490£ 00	2.856t-03	8,449E 00	4.396E=03
7.2188 01	1.5175 00	2.170E 00				03 =3.002E 03	5.036E 03	3.911E 00	2.035E=03	5.593E 00	2.910E=03
7.261E 01	1.240£ 00	2.027E 00				03 -3.021E 03	5.088E 03	3.196E 00	1,663E=03	5,225E 00	2.719E=03
7.414E 01	8.666E#01	1.520E 00				03 =3.072E 03	5,273E 03	2.2336 00	1.162E=03	5.917E 00	2,038E=03
7.429E 01	8.300E=01	1.354E 00				03 =3.076E 03	5.290E 03	2.139E 00	1.113E-03	3.490E 00	1.816E=03
7.504E 01	9.274E-01	5.250E=01	1.128E 03	#5.018E 0	-1.918E	03 -3.100E 03	5.374E 03	2,390E 00	1,244E=03	1.353E 00	7,040E=04
7.505E 01	9.279E=01	5.2066-01				03 a3.100E 03	5.375E 03	2.391E 00	1.2446.03	1.342E 00	6,980E=04
7.637E 01	1.100E 00	0.000				03 #3.149E 03	5.4266 03	2.835E 00	1.4756-03	0.000	0.000
7.7922E 01	1.765E 00	0.000				03 -3.149E 03	5.525E 03	4.549E 00	2.3671-03	0,000	0.000
8.312E 01	1.215E 00	0.000				03 #3.149E 03	5.630E U3	3.131E 00	1.629E=03	0.000	0.000
8.593E 01	9.500E=01	0.000				03 =3.149E 03	5.684E 03	2.448E 00	1.274E-03	0.000	0.000
8.879E 01	1.390E 00	0.000				03 =3.149E 03	5,707E 03	3,582E 00	1.864E=03	0.000	0.000
8,880E 01	1.391E 00	0.000				03 -3,149E 03	5.707E 03	3.585E 00	1.865E=03	0.000	0.000

×	DDRAG	CDRAG	CF	нс
11112111111111111111111111111111111111	21001001001010100012001100000010111000000	2020000000000000000000000000000000000	33333333333333333333333333333333333333	22222222222222222222222222222222222222
8,312E 01	1.978E 00	4.025E.02	2.961E=03	4.815E=03

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DDRAG

CORAG

8.593E 01 8.469E=01 4.034E 02 2.912E=03 3.976E=03 8.879E 01 3.661E=01 4.037E 02 2.953E=03 5.275E=03 6.080E 01 0.000 4.037E 02 2.953E=03 5.278E=03

КÇ

OF POOR	ORIGINAL	
QUALILLA		

RAMJET PERFORMANCE

8		INLET .
æ	CALCULATED THRUST	ANGLE OF ATTACK
	REGENERATIVE-COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	INLET PROCESS EFFICIENCY = SUBSONIC 0.9154 KINETIC ENERGY EFFICIENCY = SUPERSONIC 0.9299 KINETIC ENERGY EFFICIENCY = SUBSONIC 0.8863 ENTHALPY AT PO = SUPERSONIC = 7.70 (BTU/LBM) ENTHALPY AT PO = SUBSONIC 22.78 (BTU/LBM)
	AND TARREST AND TARREST	COMBUSTOR
	INLET FRIGTION DRAG	FUEL#AIR RATIO
	STATIONS	FUEL INJECTORS
	NOMINAL COWL LEADING EDGE	INJECTORS BTATION VALVE 1A 40,400 A 1B 42,810 B 1C 44,300 2A 50,285 D 2C 46,250 E 3A 55,575 3B 57,760 4 46,310

Reading 61

t = 231.06 sec.

100

SUMMARY REPORT

7 GAMMA MOLWT SONV MACH VEL S W/A AZAC ሥርጽነት ፅ IVAC PHI ETAC WIND TUNNEL 745.999 2985 665.0(790) 1.2933 28.955 2575 0.000 0.387 404 =32.0(97) 1.3988 28.954 985 5.995 5905 1.826 0.10605 13.500 0.4970 2527 9.733 187.2 SPIKE TIP NS 19.100 2985 665.0(700) 1.2932 28.954 2574 0.600 17.486 2925 647.1(773) 1.2951 28.954 2551 0.371 947 2.077 0.10605 13.500 0.4970 2623 1.561 194.3 0.600 WIND TUNNEL 745.999 2985 665.0(790) 1.2933 28.955 2575 0.000 0.413 412 #30.1(99) 1.3989 28.954 994 5.932 5898 1.826 0.11098 14.127 0.4970 2642 10.172 187.0 0.000 SPIKE TIP NS 0.600 19.100 2985 665.0(790) 1.2932 26.954 2574 17,312 2919 645,1(771) 1,2953 28,954 2548 0,392 999 2,077 0,11098 14,127 0,4970 2642 1,722 187,0 0.600 INLET THROAT 215,919 2903 640,2(766) 1,2959 28,954 2541 40.40n 17.478 1978 263.1(392) 1.3438 28.954 1908 2.276 4344 1.903 0.90143 13.500 0.0585 2085 60.856 154.4 40.400 INLET UPNESK 215,919 2903 640,2(766) 1,2959 28,954 2541 40.400 40.400 14,934 1516 246,4(375) 1.3471 28,954 1872 2.371 4439 1.903 0.81949 13,500 0.0643 2109 56.535 156.2 INLET DNNRSK 40.400 112,800 2903 640,2(766) 1,2959 28,954 2541 95.384 2793 607.4(734) 1.2994 28.954 2496 0.513 1281 1.947 0.81949 13.500 0.0643 2109 16.310 156.2 40.400 COMBUSTOR 40.410 215.899 2902 640.1(766) 1.2959 28.954 2541 40.410 17.474 1578 263.0(392) 1.3438 28.954 1908 2.276 4344 1.903 0.90131 13.500 0.0565 2085 60.847 154.4 COMBUSTOR 40.646 215.749 2899 639.0(765) 1.2900 28.954 2540 17.625 1579 263.4(392) 1.3437 28,954 1909 2.271 4335 1.902 0.90640 13.500 0.0582 2082 61.067 154.2 40.646 COMBUSTOR 0 10 41.117 216.256 2891 636.7(763) 1.2963 28.954 2537 17.415 1569 260.6(389) 1.3443 28.954 1903 2.279 4338 1.901 0.90217 13.500 0.0584 2081 60.823 154.1 41.117 COMBUSTOR 0 11 41.500 218,439 2885 634,8(761) 1.2965 28,954 2534 41,500 254.8(384) 1.3454 28,954 1891 2.306 4361 1.900 0.88806 13,500 0.0594 2085 60,183 154.5 16.817 1547 COMBUSTOR 0 12 41,626 219,674 2882 634,2(760) 1,2965 28,954 2533 41.626 . 16.535 1537 252.0(381) 1.3460 26.954 1885 2.320 4373 1.899 0.88139 13.500 0.0598 2088 59.895 154.7 COPBUSTOR 0 13 42,117 205,879 2874 631,6(758) 1,2968 28,954 2530 42,117 16,164 1549 255,1(384) 1,3453 28,954 1891 2,295 4340 1,903 0,84885 13,500 0,0621 2078 97,255 153,9 COMBUSTOR 185,308 2868 629,8(756) 1,2970 28,954 2527 42.460 42.460 16.359 1592 266.8(396) 1.3431 28,954 1916 2.224 4262 1.909 0.82055 13.500 0.0642 2058 54.349 152.4 COMMUNTOR 0 15 176,843 2865 629,0(755) 1,2971 28,954 2526 42.617 16.394 1610 271.7(401) 1.3421 28.954 1926 2.195 4228 1.912 0.80632 13.500 0.0654 2049 52.997 151.7 42.617 COMBUSTOR 0 16 43.611 135,255 2845 623.0(749) 1,2977 28,954 2518 43.011 16,424 1711 299.0(428) 1.3373 26,454 1982 2.031 4027 1.929 0.72414 13,500 0.0728 1996 45,314 147.8 COMBUSTOR 0 17 10 133,496 2844 622,6(749) 1.2978 28,954 2517 43.676 43.676 16,475 1717 300.6(429) 1.3370 28,954 1986 2.021 4014 1.929 0./2152 13.500 0.0731 1992 45.005 147.6 COMBUSTOR 0 18 11 44,310 118,171 2828 617,9(744) 1,2983 28,954 2511 44.310 10.947 1772 315.76 445) 1.3346 28.954 2015 1.929 3888 1.936 0.69657 13.500 0.0757 1960 42.093 145.2

GAMMA MOLNT SONV MACH VEL S 41A 4 / A C MOMIN Q IVAC PHI ETAC COMBUSTOR 19 12 5 Λ 44-800 109.287 2816 614.1(741) 1.2967 28.954 2506 17.163 1804 324.5(453) 1.3333 26.954 2033 44.600 1.873 3807 1.940 0.67846 13.500 0.0777 1939 40.139 143.6 COMBUSTOR 0 20 13 95.818 2780 603.5(730) 1.2998 28,954 2491 46.260 46.266 16,604 1824 329,9(459) 1.3325 28,954 2043 1.811 3700 1.945 0.63112 13.500 0.0835 1908 36.290 141.3 COMBUSTOR 0 21 14 46.396 95.427 2777 602.6(729) 1.2999 28.954 2490 46.396 16.511 1821 329.1(458) 1.3326 28.954 2041 1.812 3699 1.945 0.62843 13.500 0.6839 1907 36.127 141.2 COMBUSTOR 0 22 15 47.111 92.074 2761 597.8(725) 1.3004 28,954 2483 15.451 1796 322.2(451) 1.3336 28.954 2028 1.831 3714 1.946 0.59866 13.500 0.0880 47.111 1907 34.551 141.2 COMBUSTOR 0 23 16 47.310 91.132 2757 596.6(723) 1.3005 28.954 2481 47.310 15.194 1790 320.66 449) 1.3338 28.954 2025 1.835 3716 1.946 0.59096 13.500 0.0892 1906 34.129 141.2 COMBUSTOR 0 24 17 48.110 85,948 2740 591,7(719) 1,3011 28,954 2474 48.110 13.417 1749 309.46 438) 1.3356 28.954 2003 1.876 3758 1.949 0.54009 13.500 0.0976 1912 31.545 141.7 COMBUSTOR 0 25 18 49.636 76.744 2711 582.9(710) 1,3020 28.954 2462 49.636 9.118 1613 272.5(401) 1.3420 26.954 1928 2.044 3941 1.953 0.41735 13.500 0.1263 1949 25.562 144.3 COMBUSTOR 0 26 19 51.086 71.743 2686 575.7(703) 1.3028 28,954 2451 51,086 6.629 1497 241.5(370) 1.3481 28.954 1862 2.196 4089 1.955 0.33917 13.500 0.1554 1980 21.553 146.6 COMBUSTOR 0 27 20 3 70.659 2679 573.5(701) 1.3030 28.954 2448 51.617 5.965 1458 231.1(360) 1.3503 28.954 1839 2.251 4139 1.955 0.31721 13.500 0.1662 51.617 1991 20.403 147.4 COMBUSTOR 0 28 21 53.026 67,495 2662 568,5(696) 1,3036 28,954 2441 53.026 4.683 1376 209.4(338) 1.3552 28.954 1789 2.369 4239 1.957 0.27035 13.500 0.1950 2012 17.809 149.1 COMBUSTOR 55 25 0 55.126 62.644 2641 562.5(690) 1.3042 28.954 2432 55.126 3.521 1290 187.2(316) 1.3604 28,954 1736 2.496 4334 1.959 0.22158 13.500 0.2379 2033 14.924 150.6 COMBUSTOR 0 30 23 55.626 61.836 2637 561.3(689) 1.3044 28,954 2430 55.626 -3.313 1272 182.4(311) 1.3615 28.954 1724 2.525 4355 1.960 0.21253 13.500 0.2480 2038 14.383 150.9 COMBUSTOR 0 31 24 55.760 61.656 2636 561.0(6AB) 1.3044 28.954 2430 55.760 3.260 1267 18111 310) 1.3618 28,954 1721 2.533 4360 1.960 0.21024 13.500 0.2507 2039 14.246 151.0 COMBUSTOR 0 32 25 56,376 59.353 2631 559,6(687) 1,3046 28,954 2428 56.376 2.201 1150 151.0(280) 1.3692 28.954 1644 2.750 4522 1.962 0.16220 13.500 0.3250 2080 11.397 154.1 COMBUSTOR 0 33 26 57.136 59,739 2626 557,9(685) 1,3048 28,954 2425 57-136 2.037 1121 143.7(273) 1.3710 28.954 1624 2.802 4552 1.961 0.15498 13.500 0.3401 2088 10.965 154.6 COMBUSTOR 0 34 27 58.561 60.178 2616 555.1(682) 1.3051 28,954 2421 58,561 1.787 1075 132.1(261) 1.3739 28.954 1593 2.889 4600 1.959 0.14325 13.500 0.3679 2099 10.241 155.5 COMBUSTOR 0 35 28 3 58.617 60.190 2616 555.0(682) 1.3051 28.954 2421 58.617 1.779 1074 131.8(261) 1.3740 28.954 1592 2.892 #602 1.959 0.14287 13.500 0.3689 2099 10.218 155.5 COMBUSTOR 0 36 29 58.757 60.145 2615 554.7(682) 1.3051 28.954 2421 □58.757 1.759 1070 130.9(260) 1.3742 25.954 1589 2.898 4605 1.959 0.14184 13.500 0.3716 2100 10.152 155.5 COMBUSTOR 0 3/ 30 58.836 61.047 2614 554.6(682) 1.5051 28.954 2421 58.836 1.775 1068 130.4(259) 1.3744 28.954 1588 2.902 4607 1.958 0.14546 13.500 0.3674 2100 10.271 155.6

MIMIM Q IVAC PHI ETAC GAMPA MOLWI SONV MACH VEL S A/AC W/A COMBUSTOR . 0 35 31 3 O 59.117 61.547 2613 554.1(682) 1.3052 28.954 2420 N 59,117 1.758 1062 128.9(258) 1.3747 28.954 1584 2.915 4613 1.957 0.14304 13.500 0.3685 2101 10.253 155.7 COMBUSTOR 0 39 32 59.342 61.875 2612 553.7(681) 1.3052 28.954 2419 59.342 1.745 1058 127.8(257) 1.3750 28.954 1581 2.921 4616 1.957 0.14269 13.500 0.3694 2102 10.237 155.7 COMBUSTOR 0 40 33 60.066 61.981 2608 552.6(680) 1.3053 28.954 2418 60.06A 1.699 1048 125.3(254) 1.3756 28,954 1573 2.939 4624 1.956 0.14046 13,500 0.3753 2104 10.693 155.8 COMBUSTOR 0 41 34 61.086 62.047 2603 551,3(679) 1,3055 28,954 2416 1.678 1042 123.8(253) 1.3760 28.954 1569 2.947 4625 1.956 0.13956 13.500 0.3777 2103 10.030 155.8 61.086 COMBUSTOR 0 42 35 3 63.096 62.725 2595 549.0(676) 1.3057 28.954 2412 63.096 1.754 1048 125.5(254) 1.3756 26.954 1573 2.927 4605 1.954 0.14441 13.500 0.3650 2096 10.334 155.3 COMBUSTOR 0 43 36 64.516 63.232 2590 547.4(675) 1.3059 28.954 2410 64.516 1.817 1053 126.6(255) 1.3753 28.954 1577 2.910 4589 1.953 0.14833 13.500 0.3553 2091 10.578 154.9 COMBUSTOR 0 44 37 66,980 58,146 2580 544,5(672) 1,3062 28,954 2406 66.980 1.745 1061 128,6(257) 1.3748 28,954 1583 2.882 4562 1.958 0.14060 13,500 0.3749 2082 9.968 154.2 COMBUSTOR 0 45 38 5 67.356 53,834 2579 544.1(672) 1,3063 28,954 2405 67.356 1.625 1062 128.8(258) 1.3747 28.954 1583 2.679 4558 1.963 0.13071 13.500 0.4032 2081 9.259 154.1 NOZZLE AE 46 39 5 89,592 53.634 2579 544.1(672) 1.3063 28.954 2405 89,592 0.153 547 2.5(131) 1.3984 28,953 1146 4.542 5206 1.963 0.02721 13.500 1.9372 2260 2.201 167.4 NOZZLE PO 47 40 89.592 53.834 2579 544.1(672) 1.3063 28.954 2405 89.592 0.387 713 42.5(171) 1.3936 28.954 1306 3.837 5010 1.963 0.05100 13.500 1.0335 2205 3.971 163.3 FICTIVE COMBUSTR 67 60 0 215.919 2579 544.1(672) 1.3063 28.954 2405 67.356 67.356 0,387 480 +13.6(115) 1,3991 28.954 1074 4,919 5283 1.867 0.07982 13.500 0.6604 2282 6.553 169.0 FICTIVE NOZZLE 68 61 0 89,592 1842,284 2565 540,1(668) 1,3066 28,955 2399 89,592 - 0.033 130 =98.3(31) 1.3874 28.954 55710.148 5652 1.719 0.02721 13.500 1.9371 2388 2.390 176.9

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XABS	1	P=IB	P=08	1	PDA	90x		Q=IB		9-08		CAWALL	P-IB/PSU	P=18/PTO	P#08/P80	P=08/P10
6.981E		055E 00			-4.648E=(1 0.000	}	0.000		0.000		2.470E-02	2.725E 00	1.414E+03	0.000	0.000
1.836E		055E 00			-3.515k (,	0.000		0.000		1.634E 02	2.725E 00	1.414E=03	0.000	0.000
3.070E		240E 00			#1.687E (0.000		0.000		5.053E 02	5.786E 00	3.003E=03	0.000	0.000
3.50ag		955E 00			#3.695E			0.000		0.000		6.804E 02	1.055E 01	5.302E=03	0.000	0.000
3.555E		040E 00			#4.059E			0.000		0.000		7.013E 02	1.044E 01	5.4166=03	0.000	0.000
3.606E		965E 00			#4.465£ (0.5	0.000		7.246E 02	1.024E 01	5.315E=03	0.000	0.000
3.648E		284E 00			#4.818£ (0.000		7.443E V2	1.107E 01	5.743L=u3	0.000	0.000
3.7016	01 4	240E 00			#5,290E (0.000		7,6966 02	1.095E 01	5.684E-03	0.000	0.000
3.749E	01 4	.071E 00	5,659	E 00	=6.295£ (2 -2.350	E 02	=2,350E	0.2	0.000		7.934E 02	1.052E 01	5.458t=03	1.462E 01	7.586E=03
3.750E	01 4	069E Q	5.707	E 00	₩6,296£ (2 =2.351	€ 02	-2.351E	50	0.000		7.937E 02	1.051E 01	5.455E=03	1.474E 01	7.650E-03
3.803E	01 3	885E 00	9.935	E 00	#6.252E (2 =2.427	E 02	#2.427E	0.2	0.000		8,502E 02	1.004E 01	5.208E=03	2.566E 01	1.3326-02
3.8175	01 5	.029E 00	1.102	E 01	-6.203E (2 -2.448	E 02	-2.448E	02	0.000		8,650E 02	1.299E 01	6.742E=03	2.848E 01	1.478E=02
3.875E		.921E 00	1.378	E 0	-6.123F (2 -2.292	E 02	-2.546E	02	2.544E	01	9.294E 02	2.563E 01	1.330E=02	3.559E 01	1.847E=02
3.901E		210E 01			-6.118E (9.586E 02	3,125E 01	1.622F=05	3.876E 01	2.011E=U2
3.95eE		6158 01			-6.204E							1.01#E 03	4.172E 01	2.165E=02	4.473E 01	2.321E+02
3.963E		620E 01			-6.553E (1.029E 03	4,185E 01	2,1726-02	4.627E 01	2.401E=U2
4.000E		636E 01			-6.254E (1.072E 03	4.2258 01	2,1936=02	4.630E 01	2.403E#Q2
4.040		401E 01			*6.266E (1,118E 03	4.137E 01	2.147E-02	4,634E 01	2.405E=02
4.041E		601E 01			#6,265E (1.119E 03	4.134E 01	2.1466-02	4,634E 01	2.405E+02
4,0658		580E 01			-6.250E							1.147E 03	4.082E 01	2.119E=02	4.637E 01	2.406E=02
4.112E		540E 01			-6.169E							1.202E 03	3.9798 01	2.0656-02	4.727E 01	2.453E=02
4.150E 4.163E		507E 01			₩6.053E (1.247E 03	3.894E 01	2.0216-02	4 9628 01	2.5756+02
4.212E		507E 01			=6.004E (1.262E 03	3.894E 01	2.0216+02	5.040E 01	2.616E=02
4.2465		507E 01			-6.0148 (1.320E 03	3.694E 01	2.0215=02	9.880E 00	5.1276=03
4.262E		500E 01			₩6.162E 0							1.360E 03	3.894E 01 3.874E 01	2.021E=02	9.703E 00	5.035E=03 4.993E=03
4.3616		450E 01			-6.594E C							1.498E 03	3.746£ 01	1.944E=02	7.576E 00	3.932E=03
4.368E		447E 05			=6.618E 0							1.506E U3	3.738E 01	1.9408-02	7.442E 00	3.8626=03
4.431E		416E 01			#6 849E C							1.582E 03.		1.898E-02	1.222E 01	6.340E=03
4.480E		391E 01			#6.991E (1.641E 03	3.594E 01	1.865E-02	1.591E 01	8.257E=U3
4.626E		205E 01			-7.107E							1.819E 03	3.112E 01	1.615E-02	2.692E 01	1.397E=02
4.640E	01 1	187E 01	1.082	E O	#7.097E	2 =8.432	E 02	#4.834E	0.2	43.598£	02	1.8366 03	3.0678 01	1.5926+02	2.795E 01	1.450E=02
4.7116	01 1	096E 01	9.755	E 00	#7.009E 0	2 -9.073	E 02	#5.026E	02	#4.046E	02	1.924E 03	2.831E 01	1.4698-02	2.520E 01	1 3086-02
4.731E	01 1	071E 01			₩6.988E (1.949E 03	2.765E 01	1.4356+02	2.444E 01	1.268E=02
4.8115		,166E 01	8.270	E 00	₩6,835E (2 -9.893	E 05	-5.282E	02	#4.612E	02	2.047E 03	3.012E 01	1.563E=02	2.136E 01	1.1098#02
4.964E		.000E 00			+6,320E (2,237E 03	1.550E 01	8.0436-03	1.550E 01	8.043E=03
5.109E		384E 00			*5.895E (2.418E 03	1.391F 01	7.2176=03	1.391E 01	7.2175-03
5.1628		158E 00			-5.749E (2.485E 03	1.332E 01	6,915E=03	1.332E 01	6.9156-03
5.303E		144E 00			-5,442E C							2.662E 03	8,120E 00	4.214E=03	6*150E 00	4.214E=03
5.513E		587E 00			#5.127E (2.9281 03	6.684E 00	3.469E=03	6.684E 00	3.469E=03
5.563E		717E 00			#5.058E (2.992E 03	7.017E 00	3.642E-03	7.017E 00	3.642E+03
5.576E		659E 00			-5.039E							5.009E 03	6.868E 00	3.564E=03	6.868E 00	3.564E=03
5.638E		392E 00			₩4.612E (3.051E 03	6.178E 00	3.206E-03	6 178E 00	3.206E-03
5.714E		.316E ((.793E ((-4.525E (3.109E 03	3.400E 00	1.764E=03	5.328E 00	2.765E=03
5.856E 5.862E		687E 00			#4.388E (3.217E 03	4.630E 00	2.4036-03	4.630E 00	2.403E#03
5.8768		687E 00			₩4.383E 0							3.2248 03	4.359£ 00	2.2621-03	4.603E 00	2.3896 = 03
5.884E	-	741E 00			=4,365E (3.241E 03 3.252E 03	4.359E 00	2.262E=03	4.535E 00	2.3536=03
5,912E		687E 00			-4.3428 (3.287E 03	4.496E 00 4.359E 00	2.333E+03	4.496E 00	2.333E=03
5.934E		601E 00			-4.326£ (3.316£ 03	4.136E 00	2.1465=03	4,359E 00 4,136E 00	2.262E=03 2.146E=03
6.007E		325E 00			₩4.286E (3.409E 03	3,423E 00	1.776E=03	3.423E 00	1.776E=03
6.109E		275E 0			=4,256£ (3.539E 03	3.293E 00	1.709E=03	3.293E 00	1.709E=03
6.310E		525E 00		FOA	-4.253E (12 -1.566	Enz	, 7 . 307F	02	#H. 7435	0.2	3.7978 03	3.939E 00	2.0446=03	3.939E 00	2.044E=03
6.4525		781E 00		E On	-4.253E (2 -1 567	E 03	97.4575	0.2	-8-414F	در٥	3.980E 03	4.601E 00	2.388E=03	4.601E 00	2 388E=03
6.698E		536L 00		E 00	-4.253E (2 -1.620	F 03	-7.574F	0.2	-8.689F	02	4.296E 03	6.551E 00	3.400E+03	6.551E Q0	3.400E=03
6.736E		137E 0	2.651	E 00	=4.253£ (2 -1.652	E 03	-7.592E	0.2	-8.732E	0.2	4.344E 03	5.521E 00	2.8656-03	6.649E 00	3.554E=03
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XABS	P⇔IA	P=0E	PDA	QOX	0=18	Q = 0 B	CAHALL	P#IB/FS0	F#18/P]0	P≖U8/PS0	P#0B/P1.0
6.740E 01	2.137E 00	5.064E 00	#4,253E 0	2 -1.655F	03 -7.594E	02 -8.736E 02	4.349E 03	5.521E 00	2.8656-03	6.F80E 00	3.571t=03
6.760E 01	2.166E 00	2.725E 00	-4.253E 0	2 -1.636E	03 -7.604E	02 -8.758E 02	4.375E 03	5.594E 00	2.9036=03	7.0398 00	3,653E=V3
6.926E 01	2.400E Q0	1.500F 00	=4.011E 0	2 -1.6594	03 =7.675E	02 #8.915F 02	4.591E 03	6.199E 00	3.217E+03	5.875E 00	2.011E=03
6.993E 01	1.914E 00	1.200E 00	-3.655E 0	2 =1.666E	93 07,698E	02 #8.4676 02	4.672E 03	4.9438 00	2,565£#03	3.100E 00	1.6096-03
7.070E 01	1.355E 00	1.004E 00	⇒3.262£ 0	2 =1.675E	03 -7.722E	S0 31E0.0= S0	4.767E 03	3.500E 00	1.816E=03	2.592E 00	1.345E#03
7.142E 01	1.073E 00	8.200E.01	=2.978E 0	2 -1.665E	03 =7.741E	02 -9.106E 02	4.855E 03	2.773E 00	1.439E-03	2.118E 00	1.099€≈03
7.203E 01	8.350E+01					02 +9.185E 02	4.929E 03	2.157E 00	1.119E-03	2.310E 00	1.1996+03
7.29BE 01	7.455E=01					02 #9.345E 02	5.043E 03	1.926E 0v	9.993E=04	5.60AE 00	1.350E=03
7.341E 01	7.050E=01					S0 3554.0+ 50	5.096E 03	1,821E 00	9.450E=U4	2.394E 00	1.2426=03
7.494E 01	7.596E=01	6.300E=01	#2.021E 0	2 -1.742E	03 -7.805E	20 3024.6# 20	5,280E 03	1.962E 00	1.018E=03	1.627£ 00	8.445E-04
7.509E 01	7.650E=01					02 -9.634E 02	5.297E 03	1.976E 00	1.025E=03	1.481E 00	7.685E=04
7.584E 01	6.947E#01	2.9006=01	-1.806E 0	2 -1.754E	03 -7.819E	02 49.716E 02	5,382E 03	1.79#E 00	9.312E=04	7.491E-01	3.887E-04
7.584E 01	6.943E=01	2.8856-01	=1.800E 0	2 -1.754E	03 -7.819E	02 -4.717E 02	5,382E 03	1.793E 00	9.307E=04	7.452E=01	3.867E=04
7.717E 01	5.700E=01	0.000	-1.666E 0	2 -1.775E	03 -7.839E	02 -9.889E 02	5.434E 03	1.472E 00	7.641£=04	0.000	0.000
8.002E 01	6.250E#01	0.000	-1.427E 0	2 -1.740E	03 -7.880E	02 #9.523E 02	5.532E 03	1.614E 00	8,378£=04	0.000	0.000
8.392E 01	4.750E=01	0.000	-1.192E 0	2 =1,745E	03 -7.932E	02 -9,5216 02	5.637E 03	1.227E 00	6.367E=04	0.000	0.000
8.673E 01	4.650E=01	0.000	-1.088E 0	2 -1.6762	03 -7.985E	02 -8.772E 02	5,691E 03	1.201E 00	6.233E-04	0.000	0.000
8.959E 01	5,100E=01	0,000	-9.703€ 0	1 -1.685E	03 +8.083E	02 =8.772E 02	5.714E 03	1.317E 00	6.836E-04	V . 000	0.000
8.959E 01	5.101E-01	0.000	-9.703₺ 0	1 =1.685E	03 =8,083E	02 -8.772E 02	5.714E 03	1.318E 00	6.838E=04	0.000	0.000

x	DDRAG	CDRAG	CF	нс
4.041E 01 4.041E 01 4.041E 01 4.15E 01 4.153E 01 4.153E 01 4.246E 01 4.266E 01 4.361E 01 4.361E 01 4.361E 01	1.083E 00 1.0853E 00 8.739E 00 7.083E 00 2.314E 00 2.314E 00 5.961E 00 1.587E 01 9.803E 00 9.803E 00	1.083E 022 1.085E 022 1.1287E 022 1.216E 022 1.310E 022 1.378E 022 1.457F 022 1.4643E 022 1.652E 022	2.609E=03 2.609E=03 2.613E=03 2.613E=03 2.591E=03 2.591E=03 2.644E=03 2.644E=03 2.765E=03 2.771E=03 2.862E=03	5.015E=02 5.015E=02 5.015E=02 4.052E=02 4.0534E=02 4.0534E=02 4.0535E=02 4.5338E=02 4.5338E=02 4.5358E=02 4.3258E=02
4.640E 01 4.711E 01 4.731E 01 4.731E 01 4.731E 01 4.731E 01 5.103E 01 5.576E 01 5.576E 01	1.760E 00 8.964E 00 2.434E 00 1.154E 00 1.154E 00 1.154E 00 1.154E 00 1.154E 00 1.154E 00 1.154E 00 1.154E 00 1.154E 00 1.154E 00 1.154E 00 1.154E 00	02220222222222222222222222222222222222	2.901E=03 2.890E=03 2.887E=03 2.887E=03 2.857E=03 2.652E=03 2.652E=03 2.459E=03 2.449E=03 2.446E=03 2.446E=03	4.032E=02 3.711E=02 3.711E=02 3.711E=02 3.7155E=02 1.9156=02 1.9756=02 1.1276=02 1.1276=02 1.011E=02 1.012E=02
5.714E 01 5.856E 01 5.8676E 01 5.8676E 01 5.876E 01 5.871ZE 01 5.91ZE 01 6.109E 01 6.469E 01 6.4736E 01	1.494E 00 00 1.604E=01 4.024E=01 4.024E=01 4.024E=01 5.499E=00 2.664E=00 2.664E=00 4.135E=00 4.135E=00 1.026E=00	2.793E 0 0 2 2 2 2 2 3 2 2 2 2 2 2 2 2 2 2 2 2	2.275E+03 2.226E+03 2.221E=03 2.221E=03 2.204E+03 2.196E+03 2.173E+03 2.171E+03 2.171E+03 2.171E+03 2.171E+03 2.171E+03 2.171E+03 2.171E+03 2.171E+03	7:120E>03 6:405E*03 6:384E*03 6:326E*03 6:321E*03 6:321E*03 6:280E*03 6:280E*03 6:280E*03 6:280E*03 6:280E*03 6:280E*03 6:280E*03 6:440E*03 6:440E*03
6.740E 01 6.760E 01 6.993E 01 7.142E 01 7.203E 01 7.203E 01 7.203E 01 7.298E 01 7.341E 01 7.509E 01 7.584E 01 7.584E 01 7.5747E 01	1.192E=01 6.650E=01 5.2728E 00 1.706E 00 1.341E 00 1.527E 00 1.527E 00 1.527E 00 1.527E 00 1.527E 00 1.943E=01 2.443E=01 1.496E=01	3.072E 022 3.078E 022 3.1318E 022 3.148E 022 3.148E 022 3.149E 022 3.2418E 022 3.2418E 022 3.2448E 022 3.2448E 022	2.260E=03 2.263E=03 2.173E=03 2.173E=03 2.078E=03 2.078E=03 2.043E=03 2.043E=03 2.006E=03 1.953E=03 1.953E=03	7.666Em03 7.769Em03 6.545Em03 4.472Em03 3.762Em03 3.556Em03 3.556Em03 2.972Em03 2.885Em03 2.285Em03 2.285Em03
8.002F 01 8.392E 01 07 8.673E 01	1:003E 00 1:003E 00 4:665E=01	3.259E 02 3.269E 02 3.273E 02	1.975E=03 1.917E=03 1.904E=03	2.714E=03 2.187E=03 2.141E=03

READING = 0061 BLOCK = 146 TIME = 231.062 MACH 6.0 PT = 745.999 TT = 2964.6

HC

X DDRAG CDRAG CF

8,959E 01 1,979E=01 3.275E 02 1.910E=03 2.285E=03 6.959E 01 0.000 3.275E 02 1.910E=03 2.285E=03

RAMJET PERFORMANCE

ENGINE PERFORMANCE	INLET
CALCULATED THRUST	ANGLE OF ATTACK ASSOCIATION OF OUR OFFICIENT OF OUR OFFICIENT OF OUR OUR OUR OUR OUR OUR OUR OUR OUR OUR
REGENERATIVE COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	INLET PROCESS EFFICIENCY * SUBSONIC 0.9004 KINETIC ENERGY EFFICIENCY * SUPERSONIC 0.9121 KINETIC ENERGY EFFICIENCY * SUBSONIC 0.8731 ENTHALPY AT PO * SUPERSONIC 4.52 (BTU/LBM) ENTHALPY AT PO * SUBSONIC 31.70 (BTU/LBM)
MANUAL TIME AND MANAGE	COMBUSTOR
INLET FRICTION DRAG	FUEL-AIR RATIO
STATIONS	FUEL INJECTORS
NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A 40.400 1B 43.601 1C 44.300 2A 51.076 2C 46.250 3A 56.367 3B 58.551 4 47.101

t = 243.66 sec.

Fuel equivalence ratios, ϕ , were higher than planned because the change in captured mass flow with inlet spike position change was not accounted for in the pre-test selection of the fuel regulating pressures.

READING = 0061 BLOCK = 160 TIME = 243,667 MACH 6.0 PT = 745,249 TI = 2493.5 RAMJET PERFORMANCE

SUMMARY REPORT

	towarmrrackers	P	T.	, H		GAMMA	FOLWT	SONV	MACH	VEL	\$	#/A	¥	A/AC	HUHTM	G.	IVAC	PHI	ETAC
	WIND TUNNEL 0.000 745	.249	1 2993	0 5 667.3(792)	1.2930	28.955	2578											
	0.000	388	406	-31.5(97)	1,3989	28,954	987	5.991	5914	1.827	0.10598	13,437	0.4950	2519	9.739	187.5		
	SPIKE TIP NE 0.600 19	3 9.087	2025	0 6 667.3(7021	ם מפע	28.95/	2578											
		7.469		649.3(775)	1,2948	28.954	2554	0.372	950	2.078	0.10598	13,457	0.4950	2612	1,564	194.4		
	WIND TUNNEL	5 240	3	0 (J															
) 413	2993 413						5.930	5906	1.827	0.11074	14.041	0.4950	2630	10.164	187.3		
	SPIKE TIP NS	3	4	0 0		•	·					,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	• •						
		7.087 7.301		667.3(0 792	1000	2.078	0.11074	10.001	0-//950	2630	1.720	187.4		
	INLET THROAT		5	0 6	1121	146734	608724	¢.,,	11 4 3 7 14	1000	E . V / U	V##*V14	1-1041	V 5 44 7 3 11	F 0 \$ 0	*****	10111		
		124	2873	631.4(757)	1,2968	28,954	2529	2 479	4454	4 000	0.0044	47 077	* ****	7400	42 554	156 (
	40.400 15 INLET UPNRSK	5.582	1433	230.3	35Y)	1.3505	50.434	1037	2,430	4400	1.004	0.89861	13,43/	0.0384	6104	62,557	130,0		
	40.400 258	124	2873	631.4(757)	1.2968	28.954	2529											
	40.400 13 Inlet Dnnrsk	361	1398	215.3(344)	1,3538	28,954	1803	2,531	4563	1.889	0.81692	13,437	0.0642	2125	57,927	158.2		
			2873	631.40	757)	1.2968	28,954	2529											
	40,400 97	870	2771	600.9(728)	1.3001	28.954	2467	0.496	1235	1.943	0.81692	13.437	0.0642	2125	15,673	158.2		
	COMBUSTOR 40.410 146	572	8 3256	4 4 6 5 4 4 6 6	9163	1.2798	27.740	2733											
	40.410 27	.804	5554						1.757	4022	2.052	0.90287	13.503	0,0584	2104	56.434	155.8	0.15	0.61
	COMBUSTOR 40,650 133	0 893,	441E	2 4 632.3(9431	1.2710	27.931	2781											
	40.650 38	-518	2489						1.600	3844	2.067	\$1809.0	13.503	0.0581	2097	54.251	155.3	0.15	58.0
	COMBUSTOR		10	3 202	0 - 7 -	4 2454	38 445	2017											
		2.675 2.279		528.6(1 389.9(1.364	3456	2.077	0.90361	13.503	0.0583	2082	46,527	154.2	0.15	1.00
	COMBUSTOR	0	11	4 200			·		- • -					• • • • • • • • • • • • • • • • • • • •			•		
		7.751).889	3536 2050	625.5(999)	1,2653	28,102	2813	1.197	1000	2-070	0.88960	17.503	A. A&Q E	2077	42.850	157.6	0.15	1.00
	COMBUSTOR		12	5 200	0121	118030	504100	VACA	20111	3074	£ 1017	Q & CO TO U	131703	0 1 0 2 7 3	2013	46.000	12367	0 1 2 3	
			3533						4 461	2000		A 46 176				"			
	41,630 53 COMBUSTOR	3.205 0	13	6 21	950)	1.2046	20,108	2004	14121	2944	2.000	0.88278	15.503	0.0547	2012	41.137	123.5	0.15	1.00
	42.120 101	.580	3520	620.40		1.2656													
	42.120 33 COMBUSTOR	5.944	2772 14	377.3(7 21	760)	1.2919	28.108	2517	1,386	3487	880.5	0.84996	13.503	0.0650	2003	46.059	148.3	0,15	1.00
		710			991)	1.2657	28.102	2804											
		493			802)	1.2868	28.107	2578	1,208	3113	2.100	0.82189	13.503	0.0641	1906	39.767	141.2	0.15	1.00
	`COMBUSIOR 42.620 78	0 3.953	15 3507	5 21 616.2(9001	1.2657	28.102	2803											
	42.620 35	124	2944	431.7(1.174	3038	2.105	0.80740	13,503	0.0653	1862	38.115	137.9	0.15	1,00
	COMBUSTOR 43.605 57	. •	16 2770	9 21	B. 2.	1 3025	26 82v	3474											
		7.107 5.441				1.3025			1.132	2741	2.178	0.73014	13,568	0.0726	1647	31.097	121.4	0.30	0.11
	COMBUSTOR	0	17	10 21						•					- '	,	J. J.		
		3.382		614.50					1.164	274A	2.161	0.72894	IX.SAR	በ. በንጋን	1645	31.011	121.2	ሰ. ጀለ	n . 62
1	COMBUSTOR			11 21			~ D # O , O		4 8 4 4 4	-120	~ T . W .	A E I PO M	121200	A B ICT E F	* 0 47	~*****	45.45	V # 3 V	~ , v E
)				613.70					1 4 0	777.	3 150	A 19677		A 474.	4 4 4 0	71. 650		,	
•	43,680 25	789	<131	H D 4 € # (010)	1.3505	€2.048	< 341	1.100	2/33	5.124	0.72573	13.508	0.0730	1634	30.820	120.5	0 4 3 0	0 . 00

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IVAC PHI ETAC HUMIH G A/AC GAMPA MOLAT SONV MACH VEL S A/A - CUMBUSTOR 0 19 12 21 H44,310 48.201 2568 605.7(750) 1.3114 25.644 2555 23.269 2154 472.7(618) 1.3254 25.644 2353 1.096 2579 2.171 0.70005 13.568 0.0757 1539 28.061 113.4 0.30 0.00 C 44.310 COMBUSTOR 0 20 13 21 43.278 2547 598.9(743) 1.3121 25.644 2545 44,800 21.315 2146 470.4(615) 1.3257 25.644 2349 1.000 2536 2.176 0.68342 13.568 0.0775 1493 26.933 110.0 0.30 0.00 44.800 0 21 14 21 COMBUSTOR 40.045 2974 578.5(874) 1.2914 26.147 2703 46,260 26.452 2706 489.0(787) 1.3006 26.148 2587 0.818 2116 2.218 0.63566 13.568 0.0833 1457 20.904 107.4 0.50 0.31 46.260 0 22 15 21 COMBUSTOR 46.400 42.943 2552 576.5(743) 1.3110 25.717 2543 26.946 2282 489.6(657) 1.3201 25.717 2413 0.864 2086 2.176 0.63115 13.568 0.0839 1459 20.466 107.5 0.30 0.05 46.400 COMBUSTOR 0 23 16 21 47.115 42.101 2461 567.4(715) 1.3148 25.655 2504 24.887 2166 473.3(621) 1.3248 25.055 2358 0.920 2171 2.167 0.00439 13.568 0.0876 1474 20.388 108.6 0.30 0.01 47.115 COMBUSTOR 0 24 17 21 47.310 41,809 2444 565,1(710) 1,3155 25,645 2497 24.326 2143 469.0(614) 1.3258 25.645 2347 0.934 2193 2.166 0.59441 13.568 0.0891 1480 20.260 109.1 0.30 0.00 47.310 COMBUSTOR 0 25 18 21 48.110 39.165 2416 556.4(701) 1.3165 25.644 2483 19.834 2046 439.0(584) 1.3292 25.644 2296 1.055 2424 2.167 0.54327 15.568 0.0975 1517 20.463 111.8 0.30 0.00 48.110 COMBUSTOR 0 26 19 21 36.049 2368 540.9(685) 1.3181 25.644 2460 49.640 1629 18.316 120.1 0.50 0.00 13.725 1866 383.1(528) 1.3359 25.643 2199 1.278 2810 2.167 0.41946 13.568 0.1263 49.640 COMBUSTOR 0 27 20 21 31.090 32.531 2418 528.5(700) 1.3153 25.732 2479 1706 16,620 125,8 0,30 0,06 ' 9.627 1792 331.7(\$64) 1.3379 25.732 2152 1.458 3137 2.180 0.34088 13.568 0.1554 51.090 0 28 21 21 COMBUSTOR 91,620 33.163 2331 624,9(674) 1.3191 25,057 2441 8.129 1642 310.4(460) 1.3453 25.657 2069 1.584 3276 2.168 0.31880 13.568 0.1662 1727 16.230 127.3 0.30 0.01 51,620 0 29 22 21 COMBUSTOR 32,623 2294 516,7(662) 1,3206 25,646 2423 53,030 6.631 1538 282.8(428) 1.3505 25.646 2006 1.705 3421 2.164 0.27171 13.568 0.1950 1774 14.445 130.7 0.30 0.00 53.030 15 23 02 0 COMBUSTOR 55.130 31.845 2261 506.6(651) 1.3217 25.644 2407 4.725 1394 240.7(386) 1.3582 25.644 1916 1.904 3647 2.162 0.22270 13.568 0.2379 1826 12.623 134.6 0.30 0.00 55,130 COMBUSTOR 0 31 24 21 55.630 31.852 2254 504.6(649) 1.3219 25.644 2403 4.696 1387 238,8(384) 1.3586 25,643 1911 1.908 3647 2.161 0.21360 13.568 0.2480 1836 12.105 135.3 0.30 0.60 55,630, COMBUSTOR 0 32 25 21 31.135 2273 504.0(655) 1.3210 25.664 2412 55.760 4.608 1402 236.5(388) 1.3576 25.664 1920 1.905 3658 2.165 0.21137 13.568 0.2506 1839 12.017 135.5 0.30 0.01 55.76n COMBUSTOR 0 33 26 56,380 24.659 2460 501.6(712) 1.3123 25.857 2492 4,189 1586 229.5(441) 1.3460 25.857 2026 1.821 3690 2.203 0.16301 13.568 0.3250 1905 9.347 140.4 0.30 0.13 56.380 COMBUSTOR 0 34 27 21 57.140 30.419 2268 498.7(653) 1.3211 25.675 2409 2.754 1227 182.1(337) 1.3675 25.675 1802 2.208 3980 2.166 0.15577 13.568 0.3401 1918 9.635 141.4 0.30 0.02 57.140 COMBUSTOR 0 35 28 21 58.565 32.313 2225 494.0(640) 1.5229 25.648 2389 2.245 1118 159.5(306) 1.3740 25.648 1726 2.371 4091 2.155 0.14402 13.568 0.3676 1937 4.157 142.7 0.30 0.00 58.565 COMBUSTOR 0 36 29 58.620 28.087 2322 493.9(670) 1.3184 25.744 2432 2.820 1296 180.2(356) 1.3628 25.744 1847 2.145 3962 2.178 0.14359 15.568 0.3689 1937 0.841 142.8 0.30 0.06 58.620 COMBUSTOR 0 37 50 58,760 28,389 2312 493,5(666) 1,3189 25,735 2427 2.749 1277 177.66 351) 1.3640 25.734 1934 2.107 3975 2.176 0.14253 13.568 0.3717 1938 8.606 142.9 0.30 0.06 58.760

P T h GAPHA HOLKT SONV MACH VEL S M/A W A/AC HOMIK O IYAC PHI ET	TAC
COMBUSTOR 0 38 31 21	1 ~ 6
58.840 26.716 2537 493.2(674) 1.3177 25.761 2438	
58.840 1.969 1202 147.7(329) 1.3682 25.761 1782 2.334 4156 2.183 0.14413 13.568 0.3675 1939 9.314 142.9 0.30 0.0	0.7
COMBUSTOR 0 39 32 21	,,
59.120 31,160 2234 492.5(643) 1,3224 25.661 2392	
59.120 1.687 1049 135.9(286) 1.3778 25.061 1673 2.524 4224 2.159 0.14368 13.566 0.3687 1941 9.432 143.0 0.30 0.0	n ı
COMBUSTOR 0 40 33 21	·•
59.346 52.715 2217 491.9(637) 1.3232 25.646 2385	
59.346 1.783 1042 138.5(284) 1.3783 25.646 1668 2.521 4205 2.153 0.14341 13.568 0.3694 ~ 1942 9.372 143.1 0.30 0.0	5 0
COMBUSTOR 0 41 34 21	, ,
60.070 34.003 2209 490,3(635) 1.3235 25.644 2381	
60.070 2.087 1072 147.9(293) 1.3766 25.644 1691 2.447 4139 2.149 0.14116 13.568 0.3753 1946 9.080 143.4 0.30 0.0	าก
COMBUSTOR 0 42 35 21	. •
61.090 34.642 2202 488.0(633) 1.3237 25.644 2377	
61.090 1.912 1037 138.2(283) 1.3785 25.643 1665 2.513 4184 2.147 0.14026 13.568 0.3777 1950 9.120 143.7 0.30 0.0	3.0
COMBUSTOR 0 43 36 5	, •
63.100 26.238 2420 483.7(699) 1.3135 25.873 2472	
63.100 3.150 1424 176.6(393) 1.3544 25.873 1925 2.036 3920 2.192 0.14514 13.568 0.3650 1948 8.841 143.5 0.30 0.1	Δ
COMBUSTOR 0 44 37 4	. 7
64.520 29.064 2352 480.96 678) 1.3166 25.815 2442	
64.520 2.969 1321 165.6(363) 1,3608 25.813 1861 2,154 3972 2,177 0.14907 15.566 0.3555 1945 9,203 143.4 0.30 0.1	1.1
COMBUSTOR 0 45 38 5	, •
66.984 17.758 2905 475.5(848) 1.2905 26.402 2657	
66,984 5,394 2202 247.6(623) 1.3150 26,403 2335 1.446 3377 2.261 0.14131 13.568 0.3749 1942 7.415 143.1 0.30 0.4	17
COMBUSTOR 0 46 39 3	•
6/.360 16.207 2948 474.6(861) 1.2883 26.451 2672	
67.360 5.263 2273 255.0(645) 1.3120 26.452 2368 1.400 3315 2.271 0.13137 13.568 0.4032 1941 6.767 143.1 0.30 0.5	50
COMBUSTOR REGEN 47 40 5	
67,360 16,207 3515 671,9(1049) 1,2649 26,442 2891	
67,360 7,263 2955 477,1(863) 1,2876 26,451 2674 1,168 3122 2,332 0,13137 13,568 0,4032 2067 6,374 152,3 0,30 0,5	i ()
NOZZLE AE 48 41 2	
89.596 16.207 2948 474.6(852) 1.2883 26.451 2672	
89.596 0.345 1141 -63.66 3.66 1.3660 26.492 1712 3.088 5285 2.271 0.02734 13.568 1.9373 2400 2.246 176.9 0.30 0.5	0
NOZZLE PO 49 42 2	
89.596 16.207 2948 474.6(852) 1.2883 26.451 2672	
89.596 0.588 1178 -73.4(317) 1.3638 26.452 1737 3.014 5236 2.271 0.02952 13.568 1.7942 2387 2.403 175.9 0.30 0.5	Q
NOZZLE - AE REGEN 50 43 3	
89-596 16-207 3515 671-9(1049) 1.2649 26-442 2891	
89.596 0.412 1481 13.6(404) 1.3459 26.452 1935 2.965 5739 2.332 0.02735 13.568 1.9371 2625 2.439 193.5 0.30 0.5	0
NOZZLE PO REGEN 51 44 3	
89.596 16.207 3515 671.9(1049) 1,2649 26,442 2891	
89.596 9.388 1458 6.9(397) 1,3472 26,452 1921 3,002 5768 2,332 9.02627 13,568 2,0163 2633 2,355 194.1 9.30 0,5	i O
FICTIVE CUMBUSTR 71 64 0	
67.360 252.124 3699 474.6(1098) 1,2539 27.312 2906	
67.360 0.388 767 *438.2(199) 1,3807 27,322 1388 4.870 6758 2,106 0.06046 13,568 0.8762 2937 6,350 216.5 0.30 1.0	10
FICTIVE NOZZLE 72 65 0	
89.596 14.005 2868 447.9(835) 1.2911 26.451 2638	
89.596 0.363 1164 477.2(313) 1.3646 26.452 1728 2.966 5126 2.273 0.02735 13.568 1.9371 2342 2.178 172.6 0.30 0.5	0

X≱Bs	P≈18	P≖08	PDA	u o x	ü≠IR	G⇔OB	CAWALL	P-18/+S0	P=18/PT0	P=06/F50	P=CB/PTO
₩ 6.981E=01	1.0556 00	0.000	-4.645E=01		0.000	0.000	2.470E=02	2.720E 00	1.416E=03	0.100	0.000
1.836E 01	1.055E 00	0.000	#3.515E 01		0.000	0.000	1.634E 02	2.720E 00	1.416E-03	0.000	0.000
NO 3,070E 01	2.260E 00	0.000	₩1.695E 02	0.000	0.000	0.000	5.0536 62	5.826E 00	3.033E=U3	0.000	0.000
3,508E 01	3.959£ 00	0.000	-3.711E 02	0.000	0.000	0.000	6.804£ 02	1.021E 01	5.313E=03	0.000	0.000
3.555E 01	4.075E 00	0.000	#4.077E 02	0.000	0.000	0.000	7.0138 02	1.050E 01	5.468E=03	0.000	0.000
3.606E 01	3.975E 00	0.000	-#.485€ Q2	+2,369£ (2.369E		7.246E 02	1,025E 01	5.334E=03	0.000	0.000
3.648E 01	4.277E 00	0.000	*4.838E 02	-2.426E (3424.5 × S	02 0.000	7.443£ Q2	1.102E 01	5.739E-03	0.000	0.000
3.701E 01	4.240E 00	0.000	-5.309E 02			02 0.000	7.696E 02	1.093E 01	5.689E=03	0.000	0.000
3.750E 01	4.060£ 00		-6.319E 02				7.936E 02	1.047E 01	5.448E=03	1.462E 01	7.609E#03
3.750E 01	4.058E 00		#6.320E 02				7.939E 02	1,046E 01	5.445E=03	1.474E 01	7.673E=03
3,803E 01	3.865E 00		96.276E 02				8.499E 02	9.963E 00	5.186E-03	2.554E 01	1.3296=02
3.817E 01 3.875E 01	5.007E 00		-6.223E 02				8,651E 02	1 291E 01	6.718E=03	2.842E 01	1.4794-02
3.901E 01	9,717E 00 1.183E 01					02 =4.393E 01	9,291E 02	2.505E 01	1.304E=02	3,517E 01	1.831E=02
3.950E 01	1.1348 01	1.7045 01	#0.131E UZ	-1 00EE (15 05.401F	02 =4.749E 01	9.583E 02	3.050E 01	1.5876-02	3.820E 01	1.989E=02
3,963E 01	1.274E 01	1.7628 0		-/ ADDE (A 4310435	02 #8.921E 01 02 #9.454E 01	1.0146 03	2,9238 01	1.5211-02	4.391E 01	2.286E=02
4.000E 01	1.672E 01	2.281F 01	#6-021F 02	-44077E C)	02 =1.0956 02	1.029E 03	3.285E 01	1.710E+02	4.543E 01	2.3656=02
4.040E 01	2,679E 01	2.8425 0	-6.003E 02	-4,435F (12 -3.570F	02 =1.256E 02	1.1186 03	4.311E 01 6.907E 01	2.244E=02 3.595E=02	5.880E 01 7.327E 01	3.061E=02
4.041E 01	2 704E 01					05 =1.590E 05	1.119E 03	6,971E 01	3.6296=02	7.363E 01	3.814E=02 3.833E=02
4.065E 01	3.310E 01					02 -1.357E 02	1.147E 03	8.532E 01	4.441E=02	8.233E 01	4.2858-02
4.112F 01	4.493E 01	3.9628 0	-6.085E 02	-5.581E	12 =4.036E	02 -1.5456 02	1.202E 03	1.158E 02	6,0296+02	1.021E 02	5.3176-02
4.150E 01	5.449E 01	4.729E 01	-6.107E 02	-5.994E	2 =4.2988	02 -1.696E 02	1.247E 03	1.405E 02	7.311E-02	1.2198 02	6.345E+ù2
4.163E 01	5,649E 01	4.992E 01	=6.095g 02	#6.140E (2 =4.392E	02 #1.747E 02	1.262E 03	1.456E 02	7.579E-02	1.287E 02	6.699E=02
4.212E 01	6,399E 01	3.900E 00	₩6.707E 02	#6.697E (2 -4.798E	02 -1.9398 02	1.320E 03	1 650E 02	8.586E-02	1.005E 01	5.233E-03
4.246E 01	6.919E 01	3.798E 00	•7.614E 02	∞7.083E ()2 -5.015E	02 =2.068E 02	1.360E 03	1.784E 02	9.284E=02	9.791E 00	5.096E+03
4.262E 01	6.650E 01	3.750E 00	-8.027E 02	=7.262E (2 -5.133E	02 -2.1295 02	1.379E 03	1.714E 02	8,923E#02	9.667E 00	5.0326-03
4.361E 01	4,999E 01	2.896E 00	=1.003E 03	-8.585E (2 -5.815E	02 =2.769E 02	1.497E 03	1.589E 05	6.707E=02	7.466E 00	3.886E=03
4.362E 01 4.368E 01	4.982E 01	\$. 000E U	1.0058 03	eb.bult (2 *5.822E	02 -2.779E 02	1.498E 03	1.284E 02	6.685E=02	7.444E 00	3.875E=03
4.431E 01	4.873E 01 3.818E 01	2 4 4 3 E U C	1.0158 05	-0.7048 (2 -5,8646	02 -2.840E 02	1.506E 03	1.256E 02	6,539E=02	7.298E 00	3.799E=03
4.480E 01	2.996E 01	1.3675 0	-1 403E 03	-1 071E (2 =0.2605	02 -3.531E 02	1.582E 03	9.841E 01	5.123E=02	2.156E 01	1.125E-05
4.626E 01	2.741E 01	2 5/100 0	-1 1414 02	-1 7/16	73 -0 37446	02 #4,166E 02 02 #6,125E 02	1.641E 03	7.724E 01	4.020E+05	3.265E 01	1,7006=02
4 640E 01	2 716E 01	2.6738 0	-1-160F 03	#1.374F	7. 47.43UE	02 =6.3125 02	1.819E 03 1.836E 03	7.066E 01	3.678E=02	6.572E 01	3.421E-02
4.712E 01	2.592E 01	2.386F 0	-1.139E 03	#1-498F	7.7875	02 47.1948 02	1.924E 03	7.003E 01	3.645E=02 3.477E+02	6.89DE 01	3.586E=02
4.731E 01	2.557E 01	2.308E 0	-1.131E 03	#1.529E	3 -7.883F	02 -7.409E 02	1.948E 03	6.593E 01	3.432E-02	6.150E 01 5.949E 01	3.201E=02 3.097E=02
4.811E 01	1.980E 01	1.987E 01	-1.087E 03	#1.648E (3 #8-2665	02 =8.213F 02	2.047E 03	5.104E 01	2.6576-02	5.121E 01	2.666E=02
4.964E 01	1.372E 01	1.3728 01	●9.632E 02	-1.858E (3 -8.942E	02 49.638E 02	2.237E 03	3.538E 01	1.8426-02	3.538E 01	1.842E=02
5.109E 01	9.627E 00	9.627E 00	#8.759E 02	-2.027E (3 -9.515E	02 -1.075E 03	2.418E 03	2 482E 01	1 2925-02	2.482E 01	1.292E-02
5.162E-01	8.129E 00	8.129E 00	.8.514E 02	#2.075E ()3 ⇔9,708E	02 -1.104E 03	2,485E 03	2.096E 01	1.091E=02	2.096E 01	1.091E=02
5.303E.01	6.631E 00	6.631E 00	•7.969E 02	-2.187E (3 =1.018E	03 m1.169E 03	2.662E 03	1.709E 01	8.898E=03	1.709E 01	8.8986-03
5.513E 01	4.725E 00	4.725E 00	-7.343E 02	#2.323E (3 -1.077E	03 -1.246E 03	2,929E 03	1.218E 01	6.340E=03	1.218E 01	6.340E=03
5.563E 01	4.696E 00	4.696E 00	1 =7.221E 02	=2.351E	3 -1.089E	03 -1.262E 03	2,992E 03	1.210E 01	6.301E=03	1.210E 01	6.301E=03
5.576E 01	4.608E 00	4.5085 00	=7.190E UZ	-2.358E (3 =1.092E	03 =1.266E 03	3,009E 03	1.188E 01	6.184E=03	1.188E 01	6.184E=03
5.638E 01 5.714E 01	4,189E 00 1.832E 00	4.189E 00	#0.518E 02	*2.392E (3 =1.107E	03 -1.285E 03	3.051E U3	1.080E 01	5.621L=03	1.080F 01	5.621E=03
5.857E 01	2.245E 00	3 9 0 1 3 5 0 0	-4 1851 02	#6.4312 (3 -1-152E	03 -1.306E 03	3,109E 03	4,724E 00	2.459E=03	9.473E 00	4.931E=03
5.862£ 01	3.450E 00	2.1805 0	-4 1486 VS	#5 # 4 A 4 5 (13 H1-154E	03 =1.340E 03	3.217E 03	5.786E 00	3.012E-03	5.786E 00	3.0126=03
5.876E 01	3.450E 00	2.0495 00	-6-146E 02	-2.5025	/2 -1 100c	03 =1.341E 03 03 =1.344E 03	3.224E 03	8.893E 00	4.629E-03	5.644E 00	2.938E=03
5.884E 01	1.969E 00	1.969F 00	-4-1375 VE		13 mi_150t	03 =1.345E 03	3.2416 03	8,893E 00	4.6291+03	5.2822 00	2.749€=03
5.912E 01	1.687E 00	1.687F 0n	6.103F 02	#2.515F	13 -1-164F	03 =1.351E 03	3.252E 03 3.287E 03	5,075E 00 4,350E 00	2.6416=03	5.075E 00	2,6418#03
5.935E 01	1.783E 00	1.783E 00	*6.086E 02	™2.522E (3 =1.168F	03 ×1.355E 03	3.316E 03	4.595E 00	2.264E=03 2.392L=03	4.350E 00 4.595E 00	2.264E=03
6.007E 01	2.087E 00	2.087E 00	-6.033E 02	+2.545E	3 +1.178F	03 -1.367E 03	3.409E 03	5.381E 00	2.8018-03	5.381E 00	2.3922=03
6,109E 01	1.912E 00	1,9120 00	.5.987E 02	-2.5/SE	3 *1.190F	03 +1.385E 03	3.539E 03	4.930E 00	2.566E=03	4.930E 00	2.801E=03 2.566E=03
6.310E 01	3,150E 00	3,150E 00) #5.981E 02	-2.654E ()3 ×1.207E	03 -1.427E 03	3.797E 03	8 150E 00	4.227E=03	8.120E 00	4.227E=03
6,452E 01	2.969E UO	2.969E 00) ∍5.98 1€ 02	20.612E (3 -1.2165	03 -1-455E 05	3.980E 03	7.6538 00	3.9846-03	7.653E 00	3.984E=03
6,698E 01	5.394£ 00	5.3948 00	-5.981E 02	-2.745E (3 -1.235E		4.296E 03	1.390E 01	7.2386-03	1.390E 01	7.2386.03
									. 4 W - 4 B		

		•									
XABS	P=18	P=DB	PDA	QOX	0=18	90*0	CARALL	P-IH/PS0	P#IB/PT0	P+08/P50	P=QB/FIQ
6.7360 01	4.7626 00	5-7646 00	-5-981F ua			03 -1.520E 03	4.344E 03	1.228E 01	6.390£#03	1.486E 01	7.734L-U3
		E BATA A.	-5 0816 03	-2.760E	03 -1.239F	03 -1.521E 03	4.349E 03	1.228E 01	6.3908+03	1.496E 01	7.787E=03
6.740E 01	4.7628 00	3.0036.00	#3 401C VC	7666	73 -1 7437L	0% #1 526F 03	4.375L U3	1 162E 01	6.0516-03	1.547E 01	8.051E=03
6.760E 01	4.510E 00	9 000E 00	-2.401# 05	-K. 100E	na mitenie	03 *1.526E 03		6.213F 00	3.4346=03	8.578E 00	4.361E=03
6.926E 01	2.410E 00	3.250E 00	*5.517£ 02	2.816E	03 -1-4528	03 =1.564E 03	4.5916 03				4.025E=03
6.993E 01	1.961E 00	3.000F 00	#4,980E 0	2.833E	03 -1.255E	03 #1.578E 03	4.672E 03	5.0556 00	2.631E=03	7.733E 00	
7.070E 01	1.445E 00	2.623F 00	#4.374E 08	≥ -2.853E	03 -1.258E	03 =1.595E 03	4.767E 03	3.72SE 00	1.9396=03	6.761E 00	3.519b+03
7.142E 01	1.399E 00	2.270F DO	-3.887E 02	#2.872E	03 m1.260E	03 -1.612E 03	4.855E 03	3,606E 00	1.877E=03	5.852E 00	3.046E-03
7.203E 01	1.360E 00	1.86.0	-1.519F 0	2.888F	03 -1.2626	03 =1.626E 03	4,929£ 03	3.5066 00	1.825E-03	4.798E 00	2.498E=03
		1 3354 V	-7 AGIE 01	-2.000F	A3 -1.265E	03 -1.644E 03	5.043E 03	2.548E 00	1.326E=03	3.158E 00	1.6446=03
7.298E 01	9.83E+01	1.6256 00	# 3 8 0 3 1 E 9 C	E # 7 V 7 E	07 - 1 7446	03 m4 4b1E 03	5.096E 03	2.114E 00	1.100E=03	2.920E 00	1.520E=03
7.341E 01	8.200E#01	1.133E 00	-2.943E V	45.4115	U3 W1 4 C 0 0 E	03 -1.651E 03	-	1.691E 00	8.803E-04	2.075E 00	1.080E=03
7.494E 01	6.561E#01	8 = 050F=01	#2.542E 07	5 65.9416	03 wl*K64F	03 m1.672F 03	5.200E 03		-		9.672E=04
7.500E 01	6.400E=01	7.208E-01	2.512E 0	5 =5.044E	03 mt.270E	03 -1.674F 03	5.2976 03	1.650E 00	8.588E=04	1.858E 00	
7.584E 01	5.462E=01	3.000E=01	-2.328E 07	3956E	03 -1.271E	03 -1. 685E 03	5.382£ 03	1.40BE 00	7.330E#04	7.733E=01	4.025E=04
7.564E 01	5.457E=01	2.977E-01	-2.322E 0	+2.956E	13 -1.271E	03 -1.685E 03	5.382E 03	1.407E 00	7.323E-04	7.675E#01	3.995E+U4
7.717E 01	3.800E=01	0.000				03 -1.707E 03	5.434E 03	9.796E+01	5.0996-04	0.000	0.000
			-3 ABSE AT	OHAE	03 -1-2765	03 -1.708E 03	5.532E 03	7.605F-01	3.958E+04	0.000	0.000
8,002E 01	2.950E=01	0.000	*** VOTE VI	2 4466	03 -1 -2700	03 -1 987E 03	5.637E 03	8 120E-01	4.227E-04	0.000	0.000
8,3926 01	3,150E=01	0.000	*1.954F 0	5 63 1135	03 01 06/05	03 -1.837E 03		8.378E-01	4.361E=04	0.000	0.000
8.6736 01	3.250E=01	0.000	■1.888E 0	2 -3-117E	03 =1.2808	03 -1.837E 03	5.691E 03				
8,959E 01	3,700E=01	0.000	=1.804£ 07	2 -5.1198	03 =1.2826	03 -1.837E 03	5.714E 03	9.538E=01	4.965E=04	0.000	0.000
8.960E 01	3.701E-01	0.000	-1.804E 0	2 m3.119E	03 -1.282E	03 -1.837E 03	5.714E 03	9.540E=01	4.9666.04	0.000	0.000
- 0-		· ·		· ·							

×		DDRAG	CORAG		CF	HC.
4.040E 4.041E 4.065E	01 01 01	1.090E 02 1.880E=01 4.611E 00	1.0918	02 02 02	2,483E=03 2,931E=05 3,019E=03	4.707E=02 6.501E=02 7.050E=02
4.112E 4.150E	01	8.756E 00 6.619E 00	1.225g	20 20	3.184E=03 3.317E=03	7.715E-02 7.955E-02
4.163E 4.212E	01	2.146E 00 8.390E 00	1.3136	02 02	3.335t = 03 3.313E = 03	6.300E=02
4.2465	01 01	5.837E 00 2.576E 00	1.4812	02 02	3.442E = 03 3.490E = 03	6.013E=02 5.666E=02
4.361E	01	1.504E 01 1.394E=01	1.633E	02 02	3.892E=03 3.424E=03	3.995E=02
4.368E 4.431E 4.480E	01 01 01	8.127E-01 7.577E 00 5.652E 00	1.717E	02 02 02	3.345E=03 3.442E=03 3.489E=03	4.742E=02 4.161E=02 3.820E=02
4.626E	01	1.492E 01 1.306E 00	1.9225	05 05	3.525E=03 3.787E=03	3.900E=02 3.550E=02
4.712E 4.731E	01	6,580E 00 1,700E 00	2.001E	02 02	3.5338+03 3.484E=03	3.733E=02 5.745E=02
4.811E 4.964E	01	6,928E 00 1.219E 01	2.087E 2.209E	0 2 0 2	3.405E=03 3.210E=03	3.438E=02 2.809E=02
5,109E 5,162E 5,303E	01 01	9.923E 00 3.358E 00 8.191E 00	2.5428	02 02	3.062E=03 3.089E=03	2.270E=02 1.946E=02
5.513E 5.563E	01	8.191E 00 1.029E 01 2.186E 00	2.527E	02 02 02	2.9276+03 2.7856+03 2.7636+03	1.758E=02 1.368E=02 1.374E=02
5.576E 5.638E	01	5.501E=01 1.203E 00	2.5548	02 02	2.756E=03 2.661E=03	1.356E-02
5.714E 5.857E	01	1.506E 00 2.674E 00	2,581E 2,608E	05 05	2.778E=03 2.508E=03	8.647E=03 7.881E=03
5.862E 5.876E 5.884E	01 01 01	1,589E=01 4.009E=01	2.614E	02 02	2.503E=03 2.610E=03	9.257E=03 8.822E=03
5.912E 5.935E	01 01	2,726E=01 9,796E=01 6,821E=01	2.6265	02 02	3.271E=03 2.589E=03 2.443E=03	5.930E=03 6.267E=03 6.745E=03
6.007E 6.109E	01	2.075E 00 2.850E 00		02 02	2.413E=03 2.379E=03	7.559E=03 7.124E=03
6.310E		5.569E 00	2.738E 2.780E	02 02	2.429E=03 2.650E=03	1.002E-02 9.045E-03
6.698E 6.736E 6.740E	01 01	7.110E 00 1.020E 00 1.114E=01	2.851E 2.861E	02	2.764E=03 3.200E=03	1.289E.02
0.760E	01	5.578E=01	2.868g 2.911E	02 02 20	3.213E=03 3.211E=03 3.068E=03	1.075E=02 1.072E=02 7.531E=03
6.993E 7.070E	01	1.497E 00 1.623E 00	2.926E 2.943E	20	3.039E=03 2.998E=03	6.919E=03
7.142E 7.203E	01	1.408E 00	2.957E 2.968E	05 05	2.973E=03 2.946E=03	5.654E=03 5.168E=03
7.298E 7.341E 7.494E	01 01 01	1.528£ 00 6.062E=01 1.910£ 00	2,983g 2,989g 3,008g	02 02 50	2.873E=03 2.849E=03 2.789E=03	3.963E=03 3.619E=03 2.921E=03
7.509E 7.584E	01 01	1.603E=01 6.698E=01	3.010E 3.417E	05 05	2.776E=03 2.686E=03	2.771E=03 1.944E=03
7.584E 7.717E	01 01	1.097E=03 3.393E=01	3.017F 3.020E	02	2.685E=03 2.660E=03	1.939E=03 1.789E=03
8,002F 8,392E	01 01	5.714E=01 5.699E=01	3.026E 3.031E	20 20	2.601E=03 2.594E=03	1.4/0E=03 1.553F=03

x	DDRAG	CDRAG	CF	HC
8,673E 01 8,959E 01 8,960E 01	3.040E=01 1.326E=01 0.000	3.036E	1 -	1.561E=03 1.713E=03 1.713E=03

RAMJET PERFORMANCE

-		RAMJET PERFO	RMANCE			
9	LNCTUE BEDEROUTHEE			INLET		
	CALCULATED THRUST	(LBF) (LBF=8ec/LBM)	ANGLE OF ATTACK MASS FLOW RATIO ADDITIVE DRAG COEFFI	CIENT	0.4950 0.0978	EES)
	CALCULATED THRUST COEFFICIENT		DELTA PTZ TOTAL PRESSURE RECOV TOTAL PRESSURE RECOV INLET PROCESS EFFICE	ERY = SUPERSONIC ERY = SUBSONIC ENCY = SUPERSONIC.	0.1134 (P81) 0.3383 0.1537)
	REGENERATIVE=COOLED ENGINE PERFORMANCE CALCULATED .		INLET PROCESS EFFICE	IENCY - SUPERSONIC	0.9074	
	STREAM THRUST	(1.87)	KINETIC ENERGY EFFIC ENTHALPY AT PO - SUF ENTHALPY AT PO - SUE	ERSONIC	#2.81 (BTU/	(LBM)
	MOMENTUM AND PORCES			COMBUSTOR'		
	INLET FRICTION DRAG	(LBF) (LBF) (LBF) (LBF) (LBF) (LBF)	FUEL-AIR RATIO EQUIVALENCE RATIO COMBUSTOR EFFICIENCY TOTAL PRESSURE RATIC COMBUSTOR EFFECTIVEN INJECTOR DISCHARGE	ESS	0.297 0.497 0.0643	
	NOZZLE PRESSURE INTEGRAL EXTERNAL FRICTION DRAG EXTERNAL PRESSURE INTEGRAL TOTAL EXTERNAL DRAG CAVITY FORCE CAVITY FORCE MEASURED LOAD CELL FORCE MEASURED LOAD CELL FORCE FUEL VACUUM SPECIFIC IMPULSE 0.00 418 59.02 1152 1	(LBF) (LBF) (LBF) (LBF) (LBF)	VACUUM STREAM THRUST NOZZLE COEFFICIENT = PROCESS EFFICIENCY., KINETIC ENERGY EFFIC	CT	0.9006 0.9937	
	STATIONS		FUEL	INJECTORS		
	NOMINAL COWL LEADING EDGE	5 (IN) 0 (IN) 4 (IN) 4 (IN) 5 (IN) 5 (IN) 6 (IN)	INJECTORS S 18 16 26 26 36 4	TATION 40.400 43.605 44.300 51.080 46.250 56.370 58.555 47.105	VALVE A B	

t = 246.36 sec.

 $\boldsymbol{\varphi}^{\boldsymbol{\dagger}}\boldsymbol{s}$ were higher than planned.

3-4-75

 α н GAMMA MOLHT SONY MACH VEL S W/A AZAC MIMOM IVAC PHI ETAC WIND TUNNEL 745.499 2994 667.6(793) 1.2930 28.955 2578 0.000 0.388 406 -31.56 97) 1.3989 28.953 987 5.991 5915 1.827 0.10602 15.460 0.4957 2524 9.745 187.5 SPIKE TIP NS 2 0 6 0.600 19.100 2993 667.6(793) 1.2929 28.954 2578 0.600 17.482 2934 649.6(775) 1.2948 28.954 2554 0.372 950 2.078 0.10602 13.460 0.4957 2617 1.565 194.4 WING TUNNEL 745.499 2994 667.66 7931 1.2930 28.955 2578 0.414 413 =29.7(99) 1.3989 28.954 996 5.929 5907 1.827 0.11079 14.067 0.4957 2635 10.171 187.3 SPIKE TIP NS 19.100 2993 667.6(793) 1.2929 28.954 2578 0.600 17,312 2927 647,7(773) 1.2950 26.954 2551 0.392 1000 2.078 0.11079 14.067 0.4957 2635 1.722 187,3 INLET THROAT 245.310 2909 642.2(768) 1.2957 28.954 2544 40.400 16.153 [504 243.1(372) 1.3478 28.954 1865 2.395 4468 1.895 0.89948 13.460 0.0584 2111 62.462 156.8 INLET UPNER 243,310 2909 642,2(768) 1,2957 28,954 2544 40.400 13.842 1445 227.5(356) 1.3511 28.954 1831 2.488 4555 1.895 0.81771 13.460 0.0643 2134 57.884 158.5 INLET DNNRSK 114,730 2909 642,2(768) 1,2957 28,954 2544 40.400 40.400 97.803 2805 610.9(737) 1.2990 28.954 2501 0.500 1251 1.947 0.81771 13.460 0.0643 2134 15.904 158.5 COMBUSTOR 40.410 145.693 3278 644.9(923) 1.2792 27.713 2743 40.410 28,246 2251 322,6(607) 1,3139 27,715 2303 1,744 4016 2,056 0,90378 13,527 0,0584 2111 56,406 156,1 0,18 0,59 COMBUSTOR 0 0 40.648 133.629 3441 643.3(972) 1.2710 27.910 2791 40.64R 32.986 2519 348.2(685) 1.3025 27,914 2417 1.590 3842 2.071 0.90899 13.527 0.0581 2106 54.273 155.7 0.15 0.80 COMBUSTOR 0 10 3 202 122,868 3584 639,9(1014) 1,2635 28,094 2831 41.118 41-118 42.025 2840 396.9(781) 1.2895 28.101 2546 1.370 3487 2.081 0.90458 13.527 0.0584 2094 49.014 154.8 0.15 1.00 COMBUSTOR 0 11 4 200 41.500 118,331 3575 637.0(1012) 1,2637 28,094 2828 41.500 50.581 2978 440.5(824) 1.2848 28.100 2602 1.205 3136 2.083 0.89050 13.527 0.0593 2087 43.401 154.3 0.15 1.00 COMBUSTOR 0 12 5 200 41.628 116,891 3572 636,1(1011) 1,2638 28,094 2827 52,915 3013 451.8(835) 1.2836 28.100 2616 1.161 3036 2.084 0.88379 13.527 0.0598 2086 41.703 154.2 0.15 1.00 41.628 0 13 COMBUSTOR 102,152 3561 632,3(1007) 1,2640 28,094 2822 42.118 42-118 33.821 2801 384.4(769) 1.2908 28.101 2529 1.392 3521 2.092 0.85100 13.527 0.0621 2018 46,571 149.2 0.15 1.00 COMBUSTOR 0 14 42.460 86,225 3553 629,6(1005) 1,2640 28,094 2819 42.460 30.500 2952 432.2(816) 1.2855 28.100 2591 1.213 3142 2.104 0.82275 13.527 0.0642 1921 40.178 142.0 0.15 1.00 COMBUSTOR 0 15 42.618 79.508 3549 628.4(1003) 1.2640 28.094 2818 42.618 35.148 2977 440.3(824) 1.2846 28.100 2601 1.179 3057 2.109 0.80849 13.527 0.0653 1878 38.541 138.8 0.15 1.00 COMBUSTOR 0 16 9 21 43.603 57.523 2809 627.7(826) 1.3012 25.808 2654 26.527 2340 474.6(674) 1.3169 25.808 2436 1.136 2768 2.183 0.72970 13.592 0.0727 1663 31.386 122.4 0.30 0.11 43.603 COMBUSTOR 0 17 10 21 43,613 59.799 2660 627.6(779) 1.3081 25.650 2597 43.613 26,440 2106 474.8(628) 1,3240 25,656 2368 1,167 2765 2,166 0,72966 13,592 0,0727 1661 31,350 122,2 0,30 0,02 COMBUSTOR 0 10 11 21 43.678 58,737 2635 626,96 772) 1,3092 25,634 2587 43.678 25.871 2163 474.8(621) 1,3251 25.634 2358 1.170 2759 2.165 0.72586 13.592 0.0731 1650 31.119 121.4 0.30 0.00

SUMMARY REPORT

A/AC MUMIM G IVAL PHI ETAC GAMMA HOLMT SONV MACH VEL S W/A COMBUSTUR 0 19 12 21 44.310 50.199 2610 619.5(763) 1.3161 25.631 2575 25,218 2211 491,1(636) 1,3234 25,631 2383 1,004 2535 2,174 0,70240 13,592 0,0756 1559 27,671 114,7 0,30 0,00 44.310 COMBUSTOR 0 20 13 21 44.800 47.025 2590 613.4(757) 1.3107 25.630 2566 24.711 2219 493.6(638) 1.3252 25.650 2386 1.026 2448 2.176 0.68360 15.592 0.076 1525 26.005 112.2 0.30 0.00 44.800 COMBUSTUR 0 21 14 21 46.250 49.413 2530 610.9(792) 1.3145 23.816 2635 35,556 2337 544,1(726) 1.3210 23,016 2539 0.720 1828 2.295 0.64071 13,685 0.0834 1537 10.206 112,3 0.51 0.03 46.250 COMBUSTOR 0 22 15 21 46.260 49,924 2464 610.8(770) 1.3176 23.756 2607 35.631 2270 544.1(704) 1.3241 23.756 2508 0.729 1828 2.286 0.64114 13.665 0.0833 1538 16.212 112.4 0.51 0.00 46.260 COMBUSTOR 0 23 16 21 46.398 50.046 2449 609.1(765) 1.3182 23.747 2600 36.666 2264 545.4(702) 1.3244 23.747 2566 0.712 1785 2.283 0.63660 13.685 0.6839 1548 17.661 113.1 0.51 0.00 46.398 COMBUSTOR 0 24 17 21 47.113 50.661 2424 600.8(756) 1.3191 23.745 2587 34,079 2200 524,1 (680) 1,3267 23,745 2472 0,792 1959 2,279 0,61036 13,685 0,0875 1597 18,581 116,7 0,51 0,00 47.113 COMBUSTOR 0 25 18 21 47.310 47.064 2953 598.7(932) 1.2945 24.250 2800 47.310 33.368 2729 518.7(854) 1.3021 24.250 2699 0.741 2001 2.338 0.59922 13.685 0.0892 1613 18.638 117.9 0.51 0.22 COMBUSTOR 0 26 19 21 49,198 2475 590,6(773) 1,3163 23,819 2608 48.110 48.110 30.986 2212 500.3(683) 1.3253 23.819 2474 0.859 2126 2.287 0.54779 13.685 0.0975 1679 18.100 122.7 0.51 0.03 COMBUSTOR 0 27 20 3 49.638 46,909 2455 576.1(766) 1.3168 23,838 2596 17.962 1939 401.1(591) 1.3350 23.838 2323 1.274 2960 2.288 0.42307 15.685 0.1263 1840 19.461 134.5 0.51 0.04 49.638 0 28 21 COMBUSTOR 51.078 42,550 2331 571.9(784) 1.3237 21.907 2646 51.078 12.644 1719 350.4(563) 1.3466 21.907 2292 1.452 3329 2.433 0.34713 13.799 0.1552 1930 17.958 139.9 0.77 0.03 COMBUSTOR 0 59 51.088 42.541 2331 571.8(784) 1.3237 21.907 2646 51.088 12.607 1718 349.97 563) 1.3467 21.907 2291 1.454 3332 2.435 0.34668 13.799 0.1554 1931 17.952 139.9 0.77 0.03 COMBUSTOR 0 30 23 51.61A 42.588 2320 568.3(780) 1.3241 21.905 2640 51.018 10.650 1635 321.8(534) 1.3503 21.905 2239 1.569 3512 2.431 0.32422 13.799 0.1662 1960 17.696 142.0 0.77 0.03 COMBUSTOR 0 31 24 53.028 37,457 2492 559,8(841) 1,3159 22,069 2718 53.028 9.481 1773 298.0(580) 1.3424 22.069 2316 1.563 3619 2.465 0.27633 13.799 0.1950 2025 15.540 146.8 0.77 0.09 COMBUSTOR 0 32 25 55.128 35.126 2557 548.4(863) 1.3125 22.150 2745 55.128 6.862 1708 239.5(556) 1,3441 22,150 2270 1.752 3932 2,475 0,22648 13,799 0,2379 2104 13,839 152,5 0,77 0,12 COMBUSTOR 0 33 26 55.628 33,674 2608 546,2(881) 1,3101 22,199 2766 55.628 0.725 1755 234.9(571) 1.3415 22.199 2296 1.719 3946 2.484 0.21723 13.799 0.2480 2120 13.322 153.6 0.77 0.13 COMBUSTOR 0 34 27 33,687 2605 545,5(880) 1,3102 22,198 2765 55.760 55.760 6.570 1742 230.9(567) 1,3421 22,198 2288 1,734 3968 2,484 0,21493 13,799 0,2507 2123 13,252 153.9 0,77 0.13 COMBUSTOR 0 35 28 25.859 2956 542.7(1007) 1.2935 22.516 2906 56.378 5.843 2080 214.8(682) 1.3245 22.517 2467 1.642 4050 2.541 0.16579 13.799 0.3250 2224 10.436 161.1 0.77 0.24 56.378 COMBUSTOR 0 36 29 57.13A 33,356 2634 539,3(891) 1.3086 22,238 2776 3.792 1536 142.0(495) 1.3512 22.238 2154 2.070 4459 2.487 0.15841 13.799 0.3401 2243 10.977 162.5 0.77 0.15 57.138 → COMBUSTOR 0 37 30 ₩ 58.563 24.301 3037 533.5(1035) 1.2892 22.612 2934 ₩ 58.563 4.977 2094 179.2(685) 1.3228 22.013 2466 1.706 4211 2.552 0.14647 13.799 0.3678 2275 9.585 164.9 0.77 0.27

GAMMA MOLAT SONV MACH VEL S IVAC PHI ETAC W/A AZAC MUMIM LONBUSTOR 0 38 31 3 58.618 24,360 3032 533,3(1034) 1,2894 22,408 2932 58.018 4.927 2004 177,2(682) 1.3232 22.010 2062 1.714 4221 2.551 0.14603 13.799 (.3684 2276 9.580 164.9 0.77 0.27 COMBUSTOR 0 39 52 3 24,125 3047 532,8(1039) 1,2887 22,622 2937 58.758 58.758 4.928 2100 176.9(687) 1.3224 22.624 2470 1.708 4220 2.553 0.14498 13.799 0.3716 2279 9.507 165.1 0.77 0.27 0 40 33 6 COMBUSTOR 58.83a 24.424 3051 532,5(10#0) 1,2885 22,627 2939 58.838 4.982 2102 175.9(688) 1.3222 22.629 2471 1.709 4224 2.552 0.14656 13.799 0.3675 2281 4.622 165.3 0.77 0.2/ **COMBUSTOR** 0 41 34 3 24.391 3069 531.5(1047) 1.2876 22.646 2945 59.11a 59,118 4.987 2118 173.5(693) 1.5214 22.648 2478 1.798 4233 2.554 0.14610 13.799 0.3688 2266 9.610 165.7 0.77 0.28 CUMBUSTOR 0 42 35 20,259 2906 530,7(1009) 1,2927 22,553 2907 59.344 59.344 4.470 1948 151.8(634) 1.3292 22.554 2389 1.823 4354 2.539 0.14585 13.799 0.3694 2290 9.869 166.0 0.77 0.25 COMBUSTOR 0 43 36 6 60.068 39.001 2582 528.5(871) 1.3107 22.217 2752 60.068 2.812 1332 81.6(426) 1.3619 22.217 2015 2.347 4729 2.447 0.14356 13.799 0.3753 2299 10.550 166.6 0.77 0.14 COMMUSTOR 0 44 37 23.611 3156 525.5(1078) 1.2829 22./42 2975 01.08A 61.088 5-062 2211 167.3(725) 1.3167 22.744 2523 1.678 4234 2.563 0.14265 13.799 0.3/77 2306 9.385 16/.1 0.77 0.31 0 45 38 5 COMBUSTOR 28.402 2919 519.8(992) 1.2946 22.536 2887 63.098 4.200 1848 123.6(599) 1.3335 22.537 2331 1.910 4453 2.526 0.14761 13.799 0.3650 2302 10.214 166.9 0.77 0.24 63.098 COMBUSTOR 0 46 39 5 20.800 3622 515.6(1249) 1.2557 23.220 3121 64.518 64.518 8.487 2996 202.3(1008) 1.2817 23.233 2867 1.242 3560 2.603 0.15161 13.799 0.3553 2299 6.388 166.6 0.77 0.46 COMBUSTOR 0 47 40 4 19.259 3707 507.2(1280) 1.2495 23.327 3142 66.982 589.00 9.198 3182 290.6(1076) 1.2728 23.343 2937 1.121 3292 2.613 0.14371 13.799 0.3749 2295 7.351 166.3 0.77 0.50 COMBUSTOR 0 48 41 3 67.358 17.794 3738 505.8(1291) 1.2468 23.363 3149 9.284 5273 312.0(1111) 1.2683 23.580 2971 1.048 3114 2.621 0.13360 13.799 0.4032 2294 6.464 166.3 0.77 0.51. 67.358 COPBUSTOR REGEN 49 42 21 17.794 4019 634.0(1402) 1,2298 23,335 3245 67.358 67.358 9.380 3553 427.8(1219) 1.2541 23.370 3079 1.043 3212 2.654 0.13360 13.799 0.4032 2346 6.669 170.0 0.77 0.51 NOZZLE AE 50 43 89,594 17.794 3738 505.8(1274) 1.2468 23.363 3149 0.480 1646 -289,6(517) 1.3328 23.386 2160 2.921 6309 2.621 0.02781 13.799 1.9370 2944 2.727 213.3 0.77 0.51 89,594 -NOZZLE PU 51 44 3 17.794 5738 505.8(1274) 1.2468 23.363 3149 89,594 0.388 1561 +318.2(488) 1.3372 23.386 2107 3.048 6421 2.621 0.02416 13.799 2.2299 2976 2.411 215.6 0.77 0.51 89.594 NUZZLE AE REGEN 52 45 17.794 4019 634.0(1402) 1.2295 23.535 3245 89.594 0.520 1848 #220.0(587) 1,3234 23.386 2280 2.866 6537 2.654 0.02781 13.799 1,9371 3061 2,825 221.9 0.77 0.51 89.594 NOZZLE PO REGEN 53 46 17.794 4019 634.0(1402) 1.2295 23.335 3245 89,594 0.386 1720 -264.2(542) 1.3292 23.386 2205 3.040 6704 2.654 0.02289 13.799 2.3534 3109 2.385 225.3 0.77 0.51 59.594 FICTIVE CUMBUSTR 73 66 67.358 243.310 5072 505.8(1793) 1.1799 24.846 3461 0.388 1362-1010.8(464) 1.5316 25.142 1894 4.608 8729 2.446 0.04046 13.799 1.3514 3876 5.489 280.9 0.77 1.00 67.358 FICTIVE NOZZLE 74 67 89.594 11.888 3663 483.3(1270) 1.2478 23.563 3127 89.594 0.586 1877 -210.0(596) 1.3221 23.586 2297 2.504 5890 2.649 0.02781 13.799 1.9371 2817 2.546 204.1 0.77 0.51

READING =	doet afock	= 163	TIVE = 246.362	MACH 6.	D PI = 745	*444 II = 5.	143.5				PAGE 4
XABS	P=18	P=08	PDA	QUX	e=1B	Q+08	CAWALL	P-IB/PS0	P#18/PT0	P=0B/PS0	P=08/P10
6.981F=01		0.000	-4.648E=01		9.000	0.000	2.470E+02	2.718E 00	1.415E=03	0.000	0.000
1.836E 01	1.055E 00	0.000	-3.515E 01		0.000	0.000	1 634E 02	2.718E 00	1.4156-03	0.000	0.000
3.070E U1		0.000	-1.697E 02	•	0.000	V.000	5.0538 02	5.834E 00	3.038E=03	0.000	0.000
3.508E 01	3.963E 00	0.000	-3.715t 02		0.000	0.000	6 804E 02	1.0218 01	5.3162=03	0.000	0,000
3.555E V1	4.080E 00	0.000	#4.082E 02		0.000	0.000	7.013E 02	1.051E 01	5.473L=03	0.000	0.000
3.606E 01	3.980E 00	0.000			2 -2.297E Q		7.2466 02	1.0256 01	5.339€+03	0.000	0.000
3.648E 01		0.000			2 -2.352E 0		7.443E 02	1.101E 01	5.7358-03	0.000	0.000
3.701E 01	4.240E 00	0.000	·		2 -2.426E 0		7.6966 02	1.092E 01	5.687E=03	0.000	0.000
3.750E 01	4.064E 00		00 -6.324E 02		· · · · · · · · · · · · · · · · · · ·		7.9358 02	1.047E 01	5.451E=03	1.462E 01	7.612E=03
3.750E 01			50 00 00.325E 02				7.938E 02	1.046E 01	5.448E=03	1.474E 01	7.676E=03
3.803E 01	3.870E 00		00 #6.279E 02				8,500E 02	9.969E 00	5,191E+03	2.551E 01	1.3286#02
3.817E 01			F 01 -6.230E 02				8,6508 02	1.285E 01	6.693E=03	2.834E 01	1.476E=02
3.875E 01	9.689E 00		01 -6.1426 02				9.293E UZ	2.496€ 01	1.300E=02	3.525E 01	1.835E+02
4.901E 01	1.179E 01		0 +6,130E 02				9,585E 02	3.037E 01	1.581E=02	3,834E 01	1.996E=U2
3,950E 01	1.119E 01		50 40.100E 02				1.014E 03	2.882E 01	1,5014=02	4.416E 01	2.3006-02
3.963E 01	1.264E 01		0 -6.0808 02				1 029E 03	3.255E 01	1.6956-02	4.569E 01	2.379E=02
4.000E 01			01 =6.007E 02				1.072E 03	4.335E 01	2.2576-02	6.019E 01	3.134E=02
4.040E 01	2.667E 01		01 45.971E 02				1.118E 03	6,8708 01	3.578E+02	7.579E 01	3.9476#02
4.041E 01	2,692E 01	2.958	01 -5.969E 02	#3.458E 0	2 +3 467E 0	2 2.964E 00	1,119E 03	6.934E 01	3.611E=02	7.616E 01	3.967E=02
4.065E 01	3.278E 01	3.319	01 -5.973E 02	-3.661E 0	2 -3.007E 0	2 *5.325E 00	1.147E 03	8,445E 01	4.3986-02	8.549E 01	4.452E=02
4.112E 01	4.435E 01	3.9708	E. 01 -6.003E 02	#4.114E 02	2 43.898E 0	2 #2.159E 01	1.202E 03	1.142E 02	5.949E=02	1.023E 02	5.325E=02
4.150E 01	5.374E 01	4.7428	E 01 -6.010E 02	#4.448E 0	2 =4.151E 0	2 =3.473E 01	1.2476 03	1.384E 02	7,2086=02	1.255E 05	6.361E=02
4.163E 01	5.581E 01	5.0029	2 01 +5.993E 02	#4.631E 0	2 #4,239E 0	2 #3,913E 01	1,262£ 03	1.4388 02	7.486t-02	1.289E 02	6.710E#02
4.212E 01	6.369E 01		50 3 592€ 00 3				1.320E 03	1.041E 02	8,5436#02	1.017E 01	5.298E-03
4.2466 01			₹ 00 - 7.501E 02				1.360E 03	1.782E 02	9.281E=02	9.623E 00	5.115E=03
4.262E 01	6.655E 01	3.750	I 00 ₩7.910E 02	=5.6/1E 0	2 =4.949E 0	2 -7.214E 01	1.3798 03	1.714E 02	8.926F=05	9,660E 00	5.030E=03
4.360E 01			20 3100.04 00 E				1.497E 03	1,2916 02	6.724E=02	7.535E 00	3.924E-03
4.361E 01			E 00 -9.929E 02				1.498E 03	1.287E 02	6.7026-02	7.514E 00	3.913E=03
4.368E 01	4.888E 01		E 00 -1.003E 03				1.506E 03	1.259E 02	6.5575-02	7.374E 00	3.840E=03
4.431E 01	3,835E 01		01 -1.086E 03				1.582E 03	9.680E 01	5.1456-02	3.11dE 01	1.621E-02
4.480E 01	3.019E 01		01 =1.114E 03				1.641E 03	7.776E 01	4.0445-05	4.955E 01	2.580E=02
4.625E 01	3.071E 01		01 =1.074E 03				1.818£ 03	7.910E 01	4.119E-02	1.041E 02	5.420E=02
4.626E 01	3.071E 01		01 =1.073E U3				1.819E 03	7.911E 01	4.150F-05	1.045E 02	5.439E-02
4.640E 01			01 -1.063E 03				1.836E 03	7,924E 01	4.126E-02	1.097E 02	5.711E=02
4.711E 01	3.102E 01		01 =1.007E 03				1.924E 03	7.990E 01	4.1618-02	9.567E 01	4.9826-02
4.731E 01			2 01 *9 ,898£ 02				1.9488 03	8.008E 01	4.170E=02	9.1838 01	4.7826-02
4.811E-01			E 01 =9.182E 02				2.0476 03	8.346E 01	4.3466=02	7.618E 01	3.967E=02
4,964E 01 5.108E 01			E 01 =7.447E 02				2,237E 03	4.627E 01	2,409E=02	4.627E 01	2,409E=02
5.109E 01			E 01 =6.311E 02				2,417E 03	3.257E 01	1.6961-02	3,257E 01	1.696E+02
5,162E 01	1.065E 01		2 01 =6.304E 02				2,4186 03	3.248E 01 2.743E 01	1.691E=02 1.429E=02	3.248E 01	1.691E=02 1.429E=02
5.303E 01			2 01 -5.983E 02 2 00 -5.239 E 02				2.485E 03 2.662E 03	2.442E 01	1.2726-02	2.743E 01 2.442E 01	
5.5138 01			E 00 =4.339E 02				2.929E 03		9.2056-03		1.272E=02 9.205E=03
5.563E 01			E 00 =4.163t 02				2.9926 03	1.768E 01	9.021E=03	1.768E 01	9.021E+03
5.576E 01			F 00 = 4.117E 02				3.009E 03	1.692E 01	8.8135-03	1.6925 01	8.813E-03
5.638E 01			E 00 =3.103E 02				3.051E U3	1.5058 01	7.8386=03	1.505E 01	7.838E-03
5.714E 01			E 00 #2.894E 02				3.109E 03	6.788E 00	3.535t=03	1.2755 01	6.640E=03
5.856E 01			00 =2.541E 02				3.217E 03	1.282E 01	6.676E=03	1.2825 01	6.676E=03
5.862E 01			E 00 =2.526£ 02				3.224E 03	1.2568 01	6.5396+03	1.282E 01	6.677E=03
5.876E 01			E 00 =2.494E U2				3.241E 03	1.256E 01	6.5398-03	1.283E 01	6.681E=03
5.884F 01			00 =2.4746 02				3.252E 03	1.283E 01	6,683E=03	1.283E 01	6.683E=03
5.912E 01			00 -2 409E 02				3.287E 03	1.285E 01	6.690E=03	1.285E 01	6.690E=03
5.934E 01			E 00 =2.363E 02				3.316E 03	1.1516 01	5.9961-03	1.1518 01	5.996E=03
6.007E 01			50 -2.264E 02				3.409E 03	7.245E 00	3.7736-03	7.245F 00	3.773E=03
6.109F 01			F. 00 -2.173E 02				3.539E 03	1.304E 01	6.791E=03	1.304E 01	6.791E=U3
0.310E 01			E 00 =2.162E 02				3.797E 03	1.0821 01		1.082E 01	5.634E=03
				· · · · · · · · · · · · · · · · · ·						4	

XABS	PelB	P=08	PDA	x o o	Ģ≂IB	90 - 0	CANALL	P=18/PS0	r=18/P10	P=08/PS0	P=GB/PT0
6.452E 01	8.487E UO	8.487E 00	#7.162£ 02	#2.545E 03	4115.1 m	03 -1.337E 03	3.980E 03	2.186E 01	1.138E=02	2.186E 01	1.138E=02
6.698E U1	9.198E 00	9.198F 00	-2.162k 02	-2.664E 03	-1.240E	03 -1.424F 05	4.296£ 03	2,369E 01	1.230E=02	2.369E 01	1.234E=V2
6.736E 01	9.262E 00	9.306E 00	#2.162E UA	-2.684E 03	-1.246E	03 -1.438E 03	4.3446 03	2,3868 01	1,242E=02	2.397E 01	1.2486=02
6.740E 01	9.262E 00	9.3178 00	-2.162£ 02	#2.686E 03	-1.246E	03 -1.440E 03	4.349E 03	2.3866 01	1.2425-02	2.400E 01	1,2505=02
6.76gE 01	8,842E 00	9.375E 00	-2.162t 02	#2.696E 03	-1.249E	03 =1.447E 03	4.3758 03	2.278E 01	1.1868-02	2.415E 01	1.2588.02
6.9268 01	5.350E 00	4.360E 00	-1.388. 02	#2.769E 03	-1.268E	03 #1.501E 03	4.591E 03	1.378E 01	7.176E#03	1.123E 01	5.848E=03
6,993E 01	3.831E 00	4.410E 00	-4.797E 01	*2.793E 03	#1.273E	03 -1.520E 03	4.6/2E 03	9.868E 00	5.139E=03	1.136E 01	5.915Em03
7.070E 01	2.085E UD	3.431E 00	4.585E VI	#2,819E 03	#1.279L	03 -1.540E 03	4.707E 03	5.371E 00	2.797E=03	8.837E 00	4.602E+03
7.142E 01	1.706E 00	2,515g 0n	1.076E Ud	. ■2.804E 03	3585.1- E	03 w1.561F 03	4.855E 03	4.395E OU	2.288E-03	6.475E 00	3.374E+03
7,263E 01	1.385E 00	1.987F 00	1.482E 02	#2.864E 03	#1.285E	03 =1.578E 03	4.929E 03	3.568E 00	1.658E=03	5.119E 00	2.605E=03
7.298F 01	9,789E=01	1.165E 00	1.916L 02	#2.889E 03	#1.289E	03 #1.601E 03	5.043E 03	2.521E 00	1.313E=03	3.001E 00	1.563E=03
7.341E 01	7.950E#01	1.097E 00	2.058E 02	*2.849E 03	-1.290E	03 -1.609E 03	5.096E 03	2.048E 00	1.066£=03	2.826E 00	1.471E=03
7.4948 01	6.402E=01	8.550E=01	2.457E 02	-2.929E 03	-1.294E	03 #1.635F 05	5.280E 03	1.649E 00	8.587£=04	2.202E 00	1.1476-03
7.509E 01	6.250E=01	7.675E=01	2,488£ 02	#2.951E 03	-1.294E	03 *1.637E 03	5.297E 03	1.61UE 00	8,384E=04	1.9/7E 00	1.0296-03
7,584E 01	5,367E#01	3.300E-01	2,678E 02	-2.946E N3	1.296E	03 -1.650E 03	5.382£ 03	1.3826 00	7.199E=04	8.501E=01	4.4275-04
7.584E 01	5.362E=01	3.2775-01	2.685E 02	-2.947E 03	1 m1 . 296E	03 =1,651E 03	5.382E 03	1.381E 00	7.192E=04	8.440E=01	4.395E=04
7.717E 01	3.800E=01	0.000	2.781E 02	-2.977E 03	-1.298E	03 =1.678E 03	5.434E 03 `	9.789E=01	5.0976-04	0.000	0.000
8.002E 01	3.550E=01	0.000	2.928E 02	-2.981E 03	-1.303E	03 =1.678E 03	5.532E 03	9.145E=01	4.7628=04	0.000	0.000
8.392E 01	3.800E=u1	0.000	3.0856 02	#2.905E 03	-1.306E	03 -1.678E 03	5.637E U3	9.789E#01	5.097E=04	0.000	0.000
8.673E 01	3.650E=01	0.000	3.1688 02	•2.988E 03	#1.310E	03 =1.678E 03	5.691E 03	9.402E=01	4.896E#04	0.000	0.000
8,959E 01	4.600E=01	0.000	3,268E 02	*2.994E 07	-1.315E	03 -1.678E 03	5.714E 03	1.185E 00	6.170E=04	0.000	0.000
8.959E 01	4.6026=01	0.000	3.268E 02	#2.994E 01	=1.315E	03 -1.678E 03	5.714E 03	1.185E 00	6.1736-04	0.000	0.000

X	DDR4G	CORAG	CF	нс
X 4.0405E 01 4.045E 01 4.1508E 01 4.1508E 01 4.1508E 01 4.1628E 01 4.2662E 01 4.3668E 01 4.3668E 01 4.368E 01 4.480E 01	DDFAG 1.092E 02 1.894E*01 4.595E 00 8.814E 00 6.735E 00 2.143E 00 8.504E 00 2.575E 00 1.521E 01 1.382E*01 8.306E*01 7.600E 00 5.503E 00 5.503E 00	1.094E 022 1.140E 022 1.228E 022 1.228E 022 1.317E 022 1.402E 022 1.4039E 022 1.649E 022 1.7280E 022 1.7280E 022 1.7280E 022 1.7280E 022	CF 2.95116=03 3.0266=03 3.1866=03 3.1866=03 3.3386=03 3.3396=03 3.44966=03 3.4996=03 3.4956=03 3.4956=03 3.4956=03 3.4956=03 3.4956=03 3.4956=03 3.4956=03	### ##################################
4.626E 01	8.074E=02	1.933E 02	3.582E=03	4.448E#02
4.640E 01	1.089E 00	1.934E 02	3.545E=03	4.523E#02
4.711E 01	5.583E 00	1.990E 02	3.460E=03	4.618E#02
4.731E 01	1.549E 00	2.005E 02	3.437E=03	4.618E#02
4.811E 01	6.419E 00	2.069E 02	3.438E=03	4:0/76=02
4.964E 01	1.201E 01	2.169E 02	3.100E=03	3,692E=02
5.108F 01	1.067E 01	2.298E 02	3.361E=03	2,763E=02
5.109E 01	7.140E=02	2.299E 02	2,987E=03	3:117E=02
5.162E 01	3.504E 00	2.334E 02	2.926E=03	2.830E=02
5.303E 01	8.482E 00	2.419E 02	2.823E=03	2.595E=02
5.513E 01	1.105E 01	2.529E 02	2.829E=03	2.003E=02
5.563E 01	2.473E 00	2.554E 02	2.886E=03	1.921E=02
5.576E 01 5.638E 01 5.714E 01 5.856E 01 5.662E 01	6.476E=01 1.402E 00 1.802E 00 3.160E 00 1.944E=01	2.560E 02 2.574E 02 2.592E 02 2.624E 02	2,922E=03 2,788E=03 2,982E=03 2,727E=03 3,032E=03	1,866E002 1,651E002 1,166E02 1,467E02 1,330E002
5.876E 01	9.139E=01	2.631E 02	3.027E=03	1,330E=02
5.884E 01	3.168E=01	2.634E 02	3.446E=03	1,181E=02
5.912E 01	1.109E 00	2.645E 02	3.019E=03	1,339E=02
5.934E 01	8.463E=01	2.654E 02	3.008E=03	1,251E=02
6.007E 01 6.109E 01 6.310E 01 6.452E 01 6.698E 01	2.789E 00 3.602E 00 7.140E 00 5.103E 00 7.990E 00	2.682E 02 2.718E 02 2.789E 02 2.840E 02 2.920E 02	2.639E=03 3.011E=03 3.013E=03 3.411E=03	9:423E=03 1:494E=02 1:187E=02 1:803E=02
6.736E 01	1.155E 00	2.932E 02	3.518E=03	1.504E=02
6.740E 01	1.171E=01	2.933E 02	3.541E=03	1.500E=02
6.760E 01	5.902E=01	2.939E 02	3.533E=03	1.494E=02
6.926E 01	5.145E 00	2.990E 02	3.366E=03	1.146E=02
6.993E 01 7.070E 01 7.142E 01 /.203E 01 7.298E 01	1.966E 00 2.099E 00 1.720E 00 1.296E 00 1.693E 00	3.010E 02 3.031E 02 3.048E 02 3.061E 02 3.078E 02	3.331E=03 3.254E=03 3.205E=03 3.166E=03	1:046E=02 8:168E=03 6:839E=03 5:862E=03
7.278E 01 7.341E 01 7.494E 01 7.509E 01 7.584E 01	6.553E+01 2.092E 00 1.783E+01 7.447E+01	3.078E 02 3.084E 02 3.105E 02 3.107E 02 3.115E 02	3.090£*03 3.068E*03 3.023E*03 3.011£*03 2.928E*03	4.248E.03 3.877E.03 3.253E.03 3.085E.03 2.158E.03
7.584E 01	1.219E=03	3.115E 02	2.928E=03	2.153E=03
7.717F 01	3.740t=01	3.118E 02	2.899E=03	1.947E=03

	x ^		DDRAG	CURAG		CF	HG
 							
3	3,002E	01	5.617E=01	3.125E	02	2.872E=03	1.838E=05
45.4	8.392E	01	7.0296-01	3.132E	02	2.864E=03	1.9228=03
	8.67 E	01	3.665E=01	3.136E	0 2	2.843E=03	1.854E=03
	8.959E	01	1.616E#01	3.137E	02	2.8686.03	2,199E=03
	8,950E	01	0.000	3.137E	02	2.868E=03	2.200E=03

RAMJET PERFORMANCE

ENGINE PERFORMANCE	1 NL E T
CALCULATED THRUST	
REGENERATIVE COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	INLET PROCESS EFFICIENCY = SUBSONIC 0.9019 KINETIC ENERGY EFFICIENCY = SUPERSONIC 0.9178 KINETIC ENERGY EFFICIENCY = SUBSONIC 0.8735 ENIMALPY AT PO = SUPERSONIC 0.51 (BTU/LBM) ENTHALPY AT PO = SUBSONIC 31.50 (BTU/LBM)
WARENTIN AND BODFES	COMBUSTOR
INLET FRICTION DRAG	FUEL-AIR RATIO
STATIONS	FUEL INJECTORS
NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A 40.400 A 1B 43.603 B 1C 44.300 2A 51.078 D 2C 46.250 E 3A 56.368 3B 58.553 4 47.103

t = 251.76 sec.

 $\boldsymbol{\varphi}^{\boldsymbol{\cdot}} \boldsymbol{s}$ were higher than planned.

SUMMARY REPORT

								0 0	-, ., -										
		p	т	н		GAMMA	MOLNT	SONV	масн	VEL	5	W/A	i v	A/AC	MIYUM	ø	IVAC	PHI	ETAC
	WIND TUNN	ŁL	1	0 5															
		745,749	2993	667.50	793)	1.2930	28,955	2578											
	0.000	0.388	406	-31.5(97)	1.3989	28.954	987	5,991	5914	1.827	0.10605	13,526	0.4980	2536	9.747	187.5		
	SPIKE TIP		ž	0 6															
	0.600	19,112	2993	667.5(793)	1.2929	28,954	2578											
	V.600	17.495		649.5(775)	1.2948	28.954	2554	0.372	949	2.078	0.10605	13.526	0.4980	2630	1,564	194.5		
	WIND TUNN	EL	3	0 0		-									•				
		745.749	2993	667.50	793)	1,2930	28,955	2578											
	0.000	-	413	-29.70	993	1.3989	28.954	996	5.929	5907	1.827	0.11088	14.141	0.4980	2649	10.178	187.3		
	SPIKE TIP		4	0 0		- •													
	0.600	19,112	2993	667.50	793)	1.2929	28,954	2578											
	0.600	17.324		647.51	773)	1.2950	28.954	2551	0.392	1000	2.078	0.11088	14.141	0.4980	2649	1.723	187.3		
	INLET THR		5	0 6															
			2865	629.00	755)	1.2971	28,954	2526											
	40.400	15.189		222.10	351)	1.3523	28.954	1618	2,481	4512	1.885	0.90174	13.526	0.0586	2125	63.233	157.1		
	INLET UPN	HSK	6	0 3															
		263.977	2865	629.00	755)	1.2971	28,954	2526											
	40.400	13.035		207.40	336)	1.3556	28.954	1785	2,573	4593	1.885	0.81977	13,526	0.0644	2146	58,510	158.6		
	INLET DAN		7	0 4	• •		-	-											
		115.441	2865	629.00	755)	1.2971	28.954	2526											
	40.400	98.885		599 1	726)	1.3003	28.954	2485	0.492	1223	1.942	0.81977	13,526	0.0644	2146	15.585	156.6		
	COMBUSTOR			1 4	•		•												
		145.461	3308	631.80	931)	1.2772	27.821	2748											
	40.410	28.652		310.00	616)	1.3118	27.823	2314	1.734	4012	2.054	0.90599	13,591	0.0586	2125	56.493	156.3	0.15	0.69
	COMBUSTOR	0		2 4	• •														
		134.004	3471	630.3(979)	1,2690	28,019	2796											
	40.643	33.306	2549	334.8(693)	1.3006	28.024	2425	1,586	3845	880.5	0.91112	13.591	0,0582	2121	54.440	156.1	0.15	0.90
	COMBUSTOR	0	10	3 202															
		126,796	3536	627.00	998)	1.2655	28,109	2813											
	41-113	41.892	2777	380.76	761)	1,2918	26.115	2519	1.394	3510	2.074	0.90703	13,591	0.0585	2111	49.480	155.3	0.15	1.00
	COMBUSTOR	0	11	4 200															
	41.500	121,519	3527	624,2(996)	1,2657	28,109	5810											
4	41.500	50.532	2917	424.8(805)	1,2870	28.114	2577	1.226	3159	2.076	0.89268	13.591	0.0594	2104	43.824	154.8	0.15	1.00
E	COMBUSTOR	0	12	5 200															
ü	41.622	119,980	3525	623.3(995)	1.2658	28,109	2809											
Ç	41.622	52.775	2951	435.7(815)	1.2858	28-114	2591	1.183	3064	2.076	0.88632	13,591	0.0599	2104	42.205	154.8	0.15	1.00
킺	COMBUSTOR	0	13	6 21															
>	42,113	105,913	3513	619,6(991)	1,2660	28,109	2805											
4	42.113	33,863	2738	366.6(750)	1.2931	28.114	2502	1.416	3544	2.084	0.85348	13.591	0.0622	2036	47.008	149.8	0.15	1.00
-	COMBUSTOR	0	14	7 21															
7	42.460	88,044	3505	616,9(989)	1.2661	28.108	2802											
•	42.460	30.526	2892	416.90	797)	1.2878	28.114	2566	1.233	3164	2.096	0.82490	13,591	0.0643	1938	40.556	142.6	0.15	1,00
	COMBUSTOR	Q	15	8 21															
	42,613	82,091	3501	615,7(988)	1,2661	28,108	2800											
	42.613	35.843	2927	427.8(807)	1.2865	28,114	2580	1,186	3066	2.101	0.81131	13.591	0.0654	1896	38.662	139.5	0.15	1.00
	COMBUSTOR		16	9 21															
	43.597	60.167	2770	614.0(810)	1.3024	25.885	2632											
	43.597	31.482	2377							2528	2.170	0.73306	13,655	0.0727	1659	28,803	121.5	0.29	0.11
	COMBUSTOR			10 21															
	43.607	62.164	2623	613.9	765)	1.3092	25.736	2576											
	43.607	31.437	2227	486.4(639)	1.3225	25.736	2385	1.059	2525	2.153	0.73129	13.655	0.0729	1659	28,696	121.5	0.29	0.02
	COMBUSTOR			11 21															
	NO 43,673	61.038	2599	613.0(758)	1.3103	25.714	2566											
	43,673	31.149	5510	488.3(634)	1.3233	25.714	2378	1.051	5444	2.152	0.72979	13,655	0.0731	1643	28,338	120.3	0.29	0,00

ORIGINAL PAGE IS OF POOR QUALITY

GAPPA MOLHI SONV MACH VEL S PUPTH Q IVAC PHI ETAC ×/A A/AC COMBUSTUR 15 51 91 0 N44.310 53.035 2567 604.0(748) 1.3113 25.711 2552 CO 44.310 34.455 2315 522.6(667) 1.3197 25.710 2431 0.830 2018 2.159 0.70398 13.455 0.0757 1525 22.073 111.7 0.29 0.00 COMBUSTOR 0 20 13 21 44.800 46,071 3735 596.1(1112) 1.2515 27,010 2933 44.800 36.996 3573 537.1(1058) 1.2582 27.016 2876 0.597 1718 2.248 0.68624 13.655 0.0777 1465 18.320 107.3 0.29 0.81 COMBUSTOR 0 21 14 21 46.250 51.292 2622 590.4(845) 1.3101 23.271 2709 46,250 46,660 2564 569.4(824) 1.3120 25.271 2681 0.382 1024 2.354 0.64570 13,792 0.0834 1436 10.276 104.1 0.60 0.10 COMBUSTOR 0 22 15 21 46.260 51.740 2385 590.2(765) 1.3209 23.060 2606 46.200 46.727 2327 569.5(744) 1.3229 23.060 2576 0.395 1018 2.326 0.64518 13,792 0.0835 1435 10.202 104.0 0.60 0.01 COMBUSTUR 0 23 16 21 46.393 52,454 2344 588,0(751) 1,3228 23,029 2587 46.393 47.010 2289 568.7(731) 1.3247 23.029 2558 0.365 984 2.319 0.64067 13.792 0.0840 1447 9.601 104.9 0.60 0.00 COMBUSTOR 0 24 17 21 50.139 2308 577.2(738) 1,3241 23,024 2569 47.107 47.107 42.086 2210 543.0(704) 1.3274 23.024 2517 0.519 1307 2.317 0.61143 13.792 0.0881 1510 12.419 109.5 0.60 0.00 COMBUSTOR 0 25 18 21 49.567 2299 574.4(735) 1.3244 23.024 2564 47.310 47.310 40.521 2188 535.4(696) 1.3282 23.023 2505 0.558 1397 2.317 0.60321 13.792 0.0895 1525 13.096 110.6 0.60 0.00 COMBUSTOR 0 26 19 21 45,106 2056 564,6(924) 1.2983 23,553 2798 48.110 48 110 35.441 2701 506.1(868) 1.3036 23.553 2726 0.617 1682 2.385 0.55134 13.792 0.0977 1607 14.410 116.6 0.60 0.20 0 27 20 13 COMBUSTOR 49.632 44.887 2259 547.6(721) 1.3253 23.055 2541 49.032 18.825 1818 395.5(569) 1.3416 23.055 2293 1.203 2759 2.319 0.4263/ 15.792 0.1263 1792 18.283 129.9 0.60 0.01 COMBUSTOR 0 28 21 21 51.072 38.091 2196 551.4(773) 1.3303 20.772 2645 51.072 12.807 1665 351.2(573) 1.3508 20.771 2320 1.364 3165 2.522 0.35076 13.943 0.1552 1801 17.255 134.9 0.94 0.03 COMBUSTOR 0 29 22 10 51.082 40.671 2083 551.3(731) 1.3356 20.684 2586 51.082 12,765 1546 350.6(531) 1.3573 20,684 2246 1.411 3169 2.498 0.35030 13.943 0.1554 1881 17.252 134.9 0.94 0.00 COMBUSTOR 0 30 23 21 51.613 40.920 2066 545.9(725) 1.3363 20.682 2576 51,013 10.550 1455 318.6(498) 1.3617 20.682 2182 1.545 3372 2.494 0.32761 13.943 0.1662 1910 17.168 137.0 0.94 0.00 COMBUSTOR 0 31 24 5 53.022 34.728 2291 532.2(807) 1.3253 20.884 2688 53.022. 10.512 1667 303.9(579) 1.5484 20.884 2327 1.452 3380 2.543 0.27922 13.943 0.1950 1980 14.665 142.0 0.94 0.06 COMEUSTOR 0 32 25 5 55,122 29.880 2534 514.6(897) 1.3134 21.115 2799 55.122 8.925 1883 265.0(648) 1.3372 21,115 2435 1,451 3534 2.586 0.22885 13.943 0.2379 2075 12.570 148.9 0.94 0.13 COMBUSTOR 0 33 26 3 55.622 29.727 2537 510.7(898) 1.3132 21.126 2800 55,622 0.125 1844 245.3(633) 1.3387 21.126 2410 1.512 3644 2.586 0.21950 13.943 0.2480 2095 12.430 150.3 0.94 0.14 0 34 27 COMBUSTOR 55.760 29.471 2550 509.7(903) 1.3125 21.139 2806 8.058 1855 243.0(637) 1.3381 21.139 2416 1.512 3652 2.589 0.21707 13.943 0.2508 2100 12.321 150.6 0.94 0.14 55.740 COMBUSTOR 0 35 28 5 56.372 22.652 3005 505.0(1074) 1.2908 21.534 2992 56.372 7.759 2343 241.7(814) 1.3141 21.535 2666 1.362 3630 2.658 0.16752 13.943 0.3250 2219 9.449 159.1 0.94 0.26 COMBUSTOR 0 36 29 57.132 25.850 2757 499.7(980) 1.3025 21.332 2893 57.132 5.286 1879 160.3(443) 1.3345 21.332 2417 1.705 4121 2.622 0.16067 13.943 0.3401 2246 10.251 161.1 0.94 0.20 COMBUSTOR 0 37 30 22.889 2980 491.8(106#) 1.2916 21.5#0 2980 58 557 58,557 5.579 2139 160.96 736) 1.3215 21.541 2554 1.593 4069 2.653 0.14795 13.943 0.3679 2269 9.356 164.2 0.94 0.26

READING # 0061	BĽOČK	= 169	TIME	251.7	62 MAGI	6.0) PI:	745.	749	TT = 299.	5 . 1						
p	Ţ	н		CAMMA	HOLWT	SONV	MAT.H	VFI	5	W/A	₩	A/AC	M0 P 1 P	Ģ	IVAC	PHT	ETAC
COMBUSTOR	0 38		ı	חווהט	(10 L-1-1	0-111		126	•			,, no		•			.
				1.2874	21,615	3012											
	6 2271						1.515	3970	2.664	0.14758	13,943	0.3689	1852	9.106	164.3	0.94	0.28
COMBUSTOR	0 39			*****	- •	-											•
58,753 21,93	2 3064	490,9	(1096)	1.2874	21,616	3012											
58,753 5.94	7 2264	173.2	(782)	1.3158	21.616	2617	1.523	3487	2.664	0.14652	13.943	0.3715	2294	9.079	164.5	0.94	0.28
COMBUSTOR	0 40																
					21.498												
			(701)	1.3257	21,499	2503	1.602	4195	2.604	0-14817	13,943	0.3674	\$546	9.582	164.0	0,94	0,25
COMBUSTOR	0 41																
59,113 24,91	2 2075	489.2	(1024)	1,2966	21.455	2439	4 - 4 7 6	0506			47 507	0 - 1 0 7	1763	0 940			
59.113 4.67				1.5501	21.450	2450	1,734	4249	2,035	0.14765	13,445	0.3007	2302	9.749	10201	0.94	0.23
COMBUSTOR 59.339 24.72	0 42	_	•	. 2052	21 477	2011											
	4 1976	128 2	1 4763	1 2227	21.477	2740	4 722	113/17	2 LTA	0.14735	17 0/7	0 7405	23/16	9.717	145.0	0.0/	0.24
COMBUSTOR	0 43	36 0	i oroj	103501	211410	Ç M U J	18166	-6-3	61030	481-132	131743	0.000	£300	7111	10314	V 1 74	0,64
			110431	1.2914	21.555	2979				_							
	5 2076	130.3	7121	1.3237	21.556	2516	1.673	4212	2.648	0.14505	13.943	0.3753	2318	9.494	166.2	0.94	0.26
COMBUSTOR	0 44										***	- 45, - 2					
	4 5207		(1150)	1.2797	21.768	3062											
61.082 6.18	7 2415	161.5	(837)	1.3082	21.771	2686	1.487	3993	2.675	0.14414	13,943	0.3777	2329	8.944	167.0	0.94	0.33
COMBUSTOR	0 45	38 5	i				_										
					21.445												
_ · · · · -	0 1808		(615)	1.3360	21.446	2347	1.856	4417	2.618	0.14915	13,943	0.3650	2326	10,238	166,8	0,94	0,23
COMBUSTOR	0 46	-	4 . 5 = 4 .		~~												
		405 . 1	(1291)	1.2582	22.143	3177	4 43"	704.	. 762		47 047						
64,512 10,91 COMBUSTOR	9 3133		(1114)	7.44.00	56.125	5440	1.024	3000	2./03	0.15319	13.943	0.3553	2323	7.300	100.0	0.74	0,45
	0 3561	`_	1.506	. DE9/	22,159	2171											
	4 3107						1.043	3115	2.706	0.14521	13.043	0.8749	2310	7.023	166.3	0.04	6.44
COMBUSTOR	0 48				001100	2.05			40104	091-261	424142	0 1 2 1 4 1	C 3 * '	7 4 7 1 2	.0413	0,14	V #
	6 3564			1.2579	22.166	3171											
67.352 9.58	3 3123						1.025	3066	2.712	0.13500	13,943	0.4032	2318	6.431	166.3	U.94	0.44
	N 49												•				•
	6 3950	629.6	(1446)	1.2358	22.139	3311											
		540.1	(1367)	1.2459	22.153	3242	0.652	2115	2.760	0,13500	13,943	0,4032	2348	4.438	168.4	0.94	0.44
NOZZLE, AL	50	43 3															
89.589 17.94	6 3564	450.6	(1267)	1.2579	22.166	3171											
89,589 0.47			(200)	1,3401	22.176	2150	2,933	6306	2.712	0.02810	13,943	1.9370	2970	2.754	213.0	0.94	0,44
NOZZLE PO	51	44 3	4.5.5.	. 25-0	22 444	****							•				
					22.166		1 ACO	4010	7 717	0.03440	17 047	7 5574	7561	5 005	316 8		A 11.11
NOZZLE AE REGE			1 470)	1.3443	EC+110	204/	3 4 0 3 7	0413	E+115	0.02449	13,443	2.2660	2001	2.442	613.6	0.74	0,44
			teBaba	4 2788	22.139	2711											
							2.858	6626	2.760	0.02810	13.043	1.0371	2136	2.894	224.0	0.0/	0 48
NOZZLE PU REGE			i qûrj	110010		2210	.,000	0040	-	4.05010	131742	4 4 7 2 7 1	2130	Egora	65787	V . 7 4	0,44
			(1446)	1.2358	22,139	3311											
							3.049	6811	2.760	0.02274	13,943	2.3942	3190	2,407	228.8	0.94	0.44
FICTIVE COMBUST	'R 73	66 0)				•	•									- F
67,352 263,97	7 5248	450.6	(1953)	1.1654	23,937	3564											
67.352 0.38	8 1488	#1244.6	(460)	1.3196	24.433	1999	4.608	9210	2.537	0.03801	15.943	1.4323	4134	5.440	296.5	0.94	1.00
PICTIVE NOZZLE		67 0														•	-
89,589 16,11					22,168												
89.589 0.49	לכבן כי	≈337 . 4	(215)	1,3391	22.178	5165	2.848	6157	2.713	0.02810	13.943	1.9371	2914	2,689	209.0	0.94	0,44

XABS Palb	P#OB PDA	90X 9	.=18 G=0#	CAHALL	P=187P30	P=18/810	P=UE/PSO	P=08/PI0
— 6.981E=01 1.055E (00 υ,υ00 =4,651E=01	O ± 0 0 U 0 ■	000 0.000	2.4/0E=02	2.717E 00	1.415E=U3	0.000	0.000
ω 1.636E 01 1.055E (00 0.000 -3.515E 01	V.000 0.	000 0.000	1.634E 02	2.717E 00	1.415t=03	0.000	0.000
□ 3.070E 01 2.275E			000 0.000	5.053E 02	5.859E 00	3.0516-03	0.600	0.000
3.50RE 01 3.979E			000 0.000	6.804E 02	1.025E 01	5.3366.03		•
3.555E 01 4.100E			000 0.000	7.013E 02	1.056E 01		0.000	0.000
3.606E 01 3.930E		-2.317E 02 -2.				5,098E=03	0.000	0.000
3.648E 01 4.279E				7.246E U2	1.012E 01	5.270E=03	0.000	0.000
3.701E 01 4.240E		-2.373E 02 -2.		7.443E 02	1.102E 01	5.738E+03	0.000	0.000
		-2.447E 02 -2.		7.696E U2	1.092E 01	5.686E=03	0.000	0.000
		-4.51/E UE -2.	5176 02 0.000	7.932E 02	1.048E 01	5.458L-03	1.462E 01	7.611E=03
		#5.218F 05 #5.	5186 02 0.000	7.935E 02	1.048E 01	5,455E-03	1.474E 01	7.674E=U3
3.803F 01 3.880E		#5*000£ 05 #5*	900E 05 0*000	8.504E 02	9.993E 00	5.2036-03	2.568E 01	1,337E=02
3.816E 01 4.935E				8.6478 02	1.271E 01	6.617E=03	2.839E 01	1.478E=02
3.875E 01 9.611E				9,297E UZ	2.475E 01	1.2896=02	3.555E 01	1.851E#02
3.901E 01 1.168E		-3.906E 02 -2.	830E 02 -1.076E 02	9.587E 02	3.008E 01	1.5666#02	3,871E 01	2.015E=02
3,950E 01 1,105E	01 1.735E 01 -6.082£ 02	-4.449E 02 -3.	008E 02 -1.441E 02	1.015E 03	2.846E 01	1.462E=02	4.467E 01	2.3266-02
3.962E 01 1.251E	01	+4.544E 02 -3.	060E 02 =1.48SE 02	1.029E 03	3.223E 01	1.678:=02	4.617E 01	2.404E=02
4.000£ 01 1.702E	01 2.367g 01 -5.980E 02	-4.857E 02 #3.	239E 02 =1.618E 02	1 072E 03	4.385E 01	2.283E=02	6.147E 01	3.200E+02
4.040E 01 2.674E	01 3.016E 01 -5.933E 02			1.119E 03	6.888E 01	3.586E=02	7.768E 01	4.044E=02
4.041E 01 2.699E	01 3.032E 01 -5.930E 02	-5-220E 02 -3.	4586 02 P1-762E 02	1.120E U3	6.951E 01	3.619==02	7.608E 01	4.065E=U2
4.064E 01 3.264E	01 3.397E 01'-5.924E 02	#5-431E 02 #3-1	588F 02 =1-844F 02	1.147E 03	8 406E 01	4.376E=02	6.750E 01	4.5566=02
4.111E 01 4.406E	01 3.972E 01 -5.939E 02	#5.8/2F 02 #3.	845E 02 =2-007E 02	1.202E 03	1.135E 02	5.9086-02	1.0235 02	
4.150E 01 5.347E	1 4.759E 01 -5.938E 02	m6.251F 02 m/l	100E 02 02 1/12E 02	1.247E 03	1.377E 02	7.171E=02		5.3276.02
4.162E 01 5.548E	01 5.007E 01 -5,919E 02	- n6 - 1215 02 - n.	1805 A2 -2 184E A2				1.2265 05	6.3812#02
4.211E 01 6.348E		-6 677E 03 -0	Entr of -1 sect of	1.262E 03	1.429E 02	7.439E=02	1.290E 02	6.715E=02
4.246E 01 6.915E	1 3.902E 00 =7.428E 02	-7.343E 02 -4	7745 42 42 3305 02	1.320E 03	1.635E 02	8.512E=02	1.095E 01	5.699E=03
4.261E 01 6.794E		-7 442E V6 044	7/06 02 42,400E 02	1.361E 03	1.781E 02	9.273E-02	1.00SE 01	5.2336+03
4.360E 01 6.009E		-9 7645 02 ###	400 PZ PZ 510E UZ	1.379E 03	1.750E 02	9.110E=02	9.658E 00	5.028E=03
4.361E 01 6.001E		WOSTOOK UK MOST	052F 05 -7-145E 05	1.497E 03	1.54BE 02	8.058E=U2	7.399E 00	3.853E=03
4.367E 01 5.949E		90,7842 02 85+	927E 05 -2'12IF 05	1.498E 03	1.546E 02	8.047E=02	7.3778 00	3.841E=03
		#0*8APE 05 #2*	083E 02 =3.214E 02	1.506E 03	1.532E 02	7.978E=02	7.2282 00	3.763E=03
		-1.013E 03 m6.	181E 02 =3.947E 02	1.582E 03	1.401E 02	7.297E=02	3.733E 01	1.944E=02
4-480E 01 5-051E		P1+121E 03 =6+	574E 02 =4,634E 02	1.642E 03	1,301E 02	6,773E=02	6.047E 01	3.1486-02
4.625E 01 4.326E		-1.451E 03 -7.	706E 02 -6.808E 02	1.818E 03	1.114E 02	5.800E=02	1.289E 02	6.713E=02
4.626E 01 4.321E		#1.454E 03 #7.	713E 02 -6.823E 02	1.850E 03	1.113E 02	5.794L=02	1.294E 02	6.738E=Q2
4.639E 01 4.254E		1.484E 03 -7.	812E 02 -7.024E 02	1.836E 03	1.096E 02	5.705E-02	1.357E 02	7.064E=02
4.711E 01 3.896E				1.924E 03	1.004E 02	5,225E-02	1.164E 02	6.062E=U2
4.731E 01 3.795E (@1.671E 03 =8.	478E 02 #8.235E 02	1.949E 03	9.774E 01	5.089E-02	1.1108 02	5.778E-02
4.811E 01 3.615E		-1.807E 03 -9.	032E 02 #9.038£ 02	2.048E 03	9.310E 01	4.847E=02	8,945E 01	4.657E+UZ
4.963E 01 1.88ZE ()1	=2.041E 03 =1.	002E 03 -1.039E 03	2.237E 03	4 848E 01	2.524E=02	4 848E 01	2.5246-02
5.107E- 01 1.261E ()1 1,281E 01 =6,908E 02	-1- EO 3ddS.5-	087E 03 -1.168E 03	2.417E 03	3.298E 01	1.7176-02	3.298E 01	1.7176=02
5.108E 01 1.277E	1.277E 01 06.90ZE 02	#2.256E 03 #1.	087E 03 =1.169E 03	2.418E 03	3.288E 01	1.7126-02	3.288E 01	1.7126-02
5.161E 01 1.055E	1 1.0558 01 =6.5808 02	■2.333E 03 ■1.	116E 03 W1.216E 03	2.484E 03	2.717E 01	1.4156=02	2.717E 01	1.415E=02
5.302E 01 1.031E	01 1.031E 01 =5.808E 02	#2.524E 03 #1.	189E 03 01.335E 03	2.662E 03	2.656E 01	1.3836-02	2.656E 01	1.383E+02
5.512£ 01 8.925g (10 8.925E 00 -4.749E 02	#2.768F 03 -1.	2836 03 m1.4856 03	2.928£ 03	2.2996 01	1.1976-02	2.2998 01	
5.562E 01 8.125E	0 8.125E 00 -4.528E 02	#2.822F 03 =1.	3030 03 -1.5100 03	2.992E 03	2.093E 01			1,1976=02
5,576E 01 8,058E	00 8.058E 00 -4,470E 02	=2.84AE 03 -1.	100E 01 -1 E70E 01	3.009E 03		1.090E=02	2.093E 01	1.090E=02
5.637E 01 7.759E	0 7.759E 00 -3.274E 02	=2.902E A3 =4.	3235 V2 -1 EPOE V2	3.051E 03	2.075E 01	1.0816-02	2.075E 01	1.081E=UZ
5.713E 01 3.185E	0 7.387E 00 -2.980E 02	-2-97AF A3 -4 1	3436 03 -1 4448 03		1.998E 01	1.040E-02	1.998E 01	1.040E=02
5.856E 01 5.579E	0 5.579E 00 =2.519E 02	MINAL OF STATE	#436 A2 =4 /#28 A2	3.109E 03	8.203E 00	4.271E=03	1.903E 01	9.906E=03
5.861E 01 6.562E	ABSILE OF THE EVER VO	TOURS OF AT HE	7132 03 91:073E 03	3.217E 03	1.437E 01	7.481E-03	1.437E 01	7.481E=03
5,875E 01 6,562E		-3 AUDE 03 41+	415t 05 #1.675t 03	3.224E 03	1.690E 01	8.800E-03	1.419E 01	7.388E-03
5.883E 01 5.230E (-3.077E 05 -1.	46UE 03 #1.679E 03	3.241E 03	1.690E 01	8.800E=03	1.373E 01	7.150E=03
		=3:104E 05 =1:	422E 03 -1.682E 03	3.252E 03	1.347E 01	7.013E=03	1,347E 01	7.013E=03
		ab 155E 03 at 4	431E 03 -1.691E 03	3.287E 03	1.256E 01	6.537E=03	1.256E 01	6.537E=03
5.934E 01 4.934E		●3.157E 03 #1.	438E 03 -1,699E 03	3.316E 03	1.271E 01	6.617E=03	1,271E 01	6.617E+03
6.006E 01 5.125E		*3.183E 03 -1.	458E 03 -1.725E 03	3.409E 03	1.320E 01	6.872t#03	1.320E 01	6.872E=03
6.108E 01 6.187E		=3.249E 03 =1.	483E 03 =1.766E 03	3.539E 03	1.594E 01	8.297L=03	1.594E 01	8,297E=03
6,309E 01 4,400E	00 4.400E 00 -2.053£ 02	=3.3/2E 03 =1.		3.797E 03			1.133E 01	5.900E=03
			•		• • •			

XABS	P≈IB	P∞OB	PDA	GUX	na I B	Q=75	CAMALL	P#16/P80	P=18/PT0	P#U8/P90	P#08/PT0
0.451E 01	1.092E 01	1.045E 01	#2.053E 02	-3.45BE 0	3 -1.549E	03 -1.910E 03	3,980£ 03	2.812F 01	1.464E.02	2.812E 01	1,4545#02
6,698F 01	1.010E 01	1.010E 01	-2.053t UZ	-3.652E 0	3 01.5988	03 -2.034E 03	4,2961 03	2,602E 01	1.355E=02	6.60SE 01	1.355E=02
6.735E 01	9.187E 00	9,979E 00	-2.053E 02	₩3.660E 0	3 -1.606E	03 -2.054E 03	4.344E 03	2.366E 01	1.232E=02	2.570E 01	1.338£=02
6.739E 01	9.187E 00	9,966E 00	-2.053E U≥	-3.663E 0	3 -1.607E	03 -2.0566 03	4.349E 05	2.366E 01	1.232t=02	2.567E 01	1.336E=U2
6.759E 01	8.816E 00	9.900E 00	#2.053E 02	-5.678E 0	3 =1.611E	03 #2.067E 03	4.375E 03	2.2708 01	1.162t=02	2.550E UI	1.3286-02
6.925F 01	5.730E 00	4.620E 00	-1.245E 02	-3.784E 0	3 =1.640E	03 =2.143E 03	4.591E 03	1.4768 01	7.684t=03	1.190E 01	6,195E=03
6.992E 01	4.1906 00	4.792E 00	-2.662E 01	=3,819E 0	3 =1.649E	03 -2.170E 03	4.672E 03	1.0798 01	5.6186=03	1.254E 01	6.426£=03
7.069E 01	2,420E 00	3.654E 00	7.636E 01	-3.857E 0	3 -1.657E	03 =Z.200E 03	4.767E U3	6.233E 00	3.2451-03	9.412E 00	4.900E=03
7 . 14 E 01	1.8898 00	2.590E 00	1.436E 02	-3.891E 0	3 -1.663E	03 =2:228E 03	4.855E U3	4,866E 00	2.534t=03	6.671E 00	3.4736#03
7.202E 01	1.440E 00	2.062E 00	1.864E 02	-3.918E 0	3 =1.667E	03 -2.2528 03	4.929E 03	3.709E 00	1.931E=03	5.311E 00	2.7658#03
7.297E 01	1.010E 00	1.240E 00	2.317E 02	=3.953E 0	3 =1.671E	03 #2°585E 03	5.043E 03	2.601E 00	1.3546-03	5.194E 00	1.6638=03
7.340E 01	8.150E-01	1.172E 00	2.466E 02	₩\$.966E 0	3 -1 -673E	03 =2.293E 03	5.096E 03	2,0998 00	1.093E#03	3.018E 00	1.572E+03
7.493E 01	6.283E=01	9.300E=01	2,881E 02	-4.0U3E 0	3 =1.678E	03 =2.325E 03	5,280E 03	1.618E 00	8.425E=04	2.395E 00	1.247E=03
7.508E 01	6.100E=01	8.400E-01	2,913E 02	=4.006€ 0	3 =1.678E	03 #2.328E 03	5,2978 03	1.5718 00	8.180E=04	2.163E 00	1,1264-03
7.583E 01	5.649E=01	5.900E=01	3,118E 02	94.023E 0	3 -1.681E	03 =2.342E 03	5,382E 03	1.455E 00	7.5756+04	1.004E 00	5.230E=04
7.584E 01	5,647E=01	3.876E-01	3,126E 02	-4.023E 0	3 -1.681E	03 #2.342E 03	5,382E 03	1.454E 00	7.572E=04	9.98ZE#01	5.197E-04
7.716E 01	4.850E=01	0.000	3,236E 02	#4,057E 0	3 m1.684E	03 =2.373E 03	5,434E Q3	1.2498 00	6.504E=04	0.000	0.000
8.001E 01	8,650E=01	0.000	3.506E 02	#4.063E 0	3090cm E	03 =2.373E 03	5.532E 03	2.2288 00	1.160E=03	0.000	0.000
8.391E 01	6.800E#01	0.000	3.837E 02	'=4.059E 0	3 -1.697E	03 -2.373E 03	5.657E 03	1.751E 00	9.118E=04	0.000	0.000
6.672E 01	5,300E=01	0.000				03 -2.373E 03	5.691E 03	1.365E 00	7.107E=04	0,000	0.000
8.958E 01	6.950E=01	0.000	4.119E 02	₩4.085E 0	3 -1.712E	03 -2.373E 03	5.714E 03	1.790E 00	9.3196-04	0,000	0.000
8.950E 01	6.953E+01	0.000	4_119F 02	-4-085E 0	3 -1.7126	03 m2.373E 03	5.714F 03	1-791F 00	9.3246-04	0.000	0.000

щ ×	DUBAC	CURAG	CF	HC
4.040F 01 4.040F 01 4.040E 01 4.111E 01 4.150E 01 4.150E 01 4.211E 01 4.261E 01 4.261E 01 4.361E 01 4.361E 01 4.361E 01 4.361E 01 4.462E 01 4.462E 01	1.095E 02 1.874E 01 4.467E 00 8.879E 00 2.044E 00 8.498E 00 6.033E 00 2.465E 00 1.4207E 01 1.207E 01 6.623E 00 4.230E 00	1.095E 02 1.097E 02 1.142E 02 1.230E 02 1.320E 02 1.320E 02 1.405E 02 1.405E 02 1.405E 02 1.405E 02 1.405E 02 1.405E 02 1.405E 02 1.405E 02 1.405E 02 1.405E 02 1.405E 02	2.4526=03 2.9136=03 3.0356=03 3.1876=03 3.2786=03 3.3036=03 3.4086=03 3.4566=03 3.4566=03 3.4176=03 3.4176=03 3.4916=03 3.4916=03 3.5796=03	4.640E=02 6.717E=02 7.115E=02 7.055E=02 8.116E=02 6.384E=02 6.384E=02 6.384E=02 6.30E=02 4.602E=02 4.602E=02 4.602E=02
4.626E 01 4.639E 01 4.711E 01 4.731E 01 4.811E 01 4.812E 01 5.107E 01 5.108E 01	1.031E 01 5.356E=02 6.343E=01 3.639E 00 1.152E 00 1.059E 01 1.096E 01 6.957E=02	1.855E 02 1.856E 02 1.862E 02 1.899E 02 1.910E 02 1.910E 02 2.173E 02 2.173E 02	4.579E=03 3.960E=03 3.835E=03 3.628E=03 3.582E=03 3.438E=03 3.417E=03 3.442E=03 2.995E=03	2.716E002 3.374E002 4.015E002 4.015E002 4.017E002 4.0276E002 3.347E002 2.716E002 3.126E002
5.161E 01 5.302E 01 5.512E 01 5.562E 01 5.576E 01 5.6713E 01 5.866E 01 5.866E 01	3.331E 00 7.854E 00 1.006E 01 2.314E 00 6.507E=01 1.726E 00 3.176E 00 1.949E=01	207E 02 2286g 02 2.286g 02 2.386g 02 2.410E 02 2.4169E 02 2.4476E 02 2.478E 02 2.480E 02	2.827E=03 2.732E=03 2.815E=03 2.995E=03 2.998E=03 2.997E=03 3.109E=03 2.909E=03	2.905E=02 2.813E=02 2.380E=02 2.103E=02 1.911E=02 1.421E=02 1.528E=02 1.516E=02
5.875E 01 5.883E 01 5.934E 01 5.934E 01 6.108E 01 6.309E 01 6.453E 01 6.73E 01	5,023E=01 1.128E=01 1.1334E=01 2.623E 00 3.597E 00 7.566E 00 4.944E 00 7.389E 00 1.124E 00	2485E 022 2488E 022 2498E 022 2534E 022 25576E 022 2695E 022 2780	3.132E=03 3.419E=03 2.992E=03 2.998E=03 3.019E=03 3.090E=03 3.437E=03 3.439E=03	1.44/9E=02 1.260E=02 1.369E=02 1.389E=02 1.412E=02 1.540E=02 1.540E=02 1.977E=02 1.674E=02
6.739E 01 6.759E 01 6.975E 01 7.925E 01 7.049E 01 7.14E 01 7.297E 01 7.340E 01 7.493E 01 7.588E 01 7.584E 01	1.152E=01 5.794E=01 5.111E 00 1.982E 00 2.143E 00 1.762E 00 1.317E 00 6.691E=01 2.134E 00 1.817E=01 1.817E=01 1.289E=03	22.02222222222222222222222222222222222	3.485E.03 3.477E.03 3.288E.03 3.288E.03 3.214E.03 3.117E.03 3.117E.03 3.044E.03 3.023E.03 2.978E.03 2.966E.03 2.892E.03	1.578E=02 1.574E=02 1.5676E=02 1.6254E=02 1.144E=03 7.414E=03 4.548E=03 4.548E=03 5.521E=03 5.521E=03 2.4424E=03

x	DORAG	CDRAG	· CF	нс
8.001E 01 8.391E 01 8.672E 01 8.958E 01 8.959E 01	9.464E=U1 1.106E 00 4.934E=01 2.056E=01	2.979E 02 2.990E 02 2.995E 02 2.997E 02	2.907E=03 2.852E=03 2.883E=03	3.745E+03 3.113E+03 2.572E+03 3.151E+03 3.153E+03

RAMJET PERFURMANCE

-		RAPULET PERF	JAP HNUE			
34	ENGINF PERFORMANCE			INLET		
	MEASURED THRUST. 120	(LBF) (LBF=SEC/LBM) (LBF=SEC/LBM)	MASS FLOW RATIO ADDITIVE DRAG COEFF LIMITING PRESSURE DELTA PTZ	FICIENT	0.4980 0.0968 0.1526 0.1127	
	REGENERATIVE COOLED FRGIRE PERFORMANCE CALCULATED 3077.	(Lar)	TOTAL PRESSURE RECINATE PROCESS EFFIINLET PROCESS EFFIIKINETIC ENERGY EFFENTALPY AT PO = SI	OVERY # SUBSONIC	0.1548 0.8948 0.9053 0.9067 0.8594	(BTU/LBM) (BTU/LBM)
	. HOMENTUM AND FURCES			COMBUSTER		
	INLET FRICTION DRAG	(L8F) (L8F) (L8F) (L8F) (L8F) (L8F) (L8F) (L8F) (L8F) (L8F) (L8F) (L8F)	EQUIVALENCE RATIO. COMBUSTOR EFFICIENT TOTAL PRESSURE RAT COMBUSTOR EFFECTIVE INJECTOR DISCHARGE VACUUM STREAM THRU: NOZZLE CCEFFICIENT PROCESS EFFICIENCY	NOZZLE ST COEFFICIENT * CS CIENCY	0.939 0.440 0.0680 0.4361 0.5782. 0.9812 0.9982	0.7760, 0.7035
	STATIONS		FUI	EL INJECTORS		
	NOMINAL CUML LEADING EDGE	CIN) CIN) CIN) CIN)	INJECTORS 1A 1B 1C 2A 2C 3A 30	40,400 43,597 44,300 51,072	LVE. A B D E	

t = 262.56 sec.

 $\boldsymbol{\varphi}^{\intercal}\boldsymbol{s}$ were higher than planned.

SUNMARY REPORT

1 GAMMA MOLAT SONV MACH VEL S A/AC MINUM IVAL PHI ETAC */A WIND TUNNEL 1 0 5 745.249 2993 667.6(793) 1.2930 28.955 2578 0.000 0.388 406 =31.5(97) 1.3989 28.954 987 5.991 5915 1.827 0.10598 13.644 0.5026 2558 9.741 187.5 SPIKE TIP NS 2 0 6 0.600 19.087 2993 667.6(793) 1.2929 28.954 2578 0.600 17.469 2934 649.6(775) 1.2948 28.954 2554 0.372 950 2.078 0.10598 13.644 0.5076 2652 1.565 194.4 WIND TUNNEL 0.000 745.249 2993 667.6(793) 1.2930 28.955 2578 0.000 0.413 413 +29.7(99) 1.3989 28.954 996 5.930 5907 1.827 0.11072 14.254 0.5026 2670 10.164 18/.3 SPIKE TIP NS 0.600 19,087 2993 66/.6(793) 1,2929 28,954 2578 17.301 2927 647.6(773) 1.2950 28.954 2551 0.392 1000 2.078 0.11072 14.254 0.5026 2670 1.720 187.3 243,627 2931 648,7(774) 1,2950 28,954 2553 16.435 1523 248.2(377) 1.3468 28.954 1876 2.386 4477 1.897 0.90542 13.644 0.0588 2146 62.991 157.3 INLET UPNRSK 243,627 2931 648,7(774) 1,2950 28,954 2553 40.400 14,081 1463 232,4(361) 1,3501 28,954 1842 2,478 4564 1,897 0,82311 13,644 0,0647 2169 56,386 159,0 INLET DNNRSK 40.400 115,802 2931 648,7(774) 1,2950 28,954 2553 40.400 98.671 2825 617.1(743) 1.2983 28.954 2510 0.501 1258 1.948 0.82311 13.644 0.0647 2169 16.091 159.0 COMBUSTOR 40.410 144.418 3332 651.7(939) 1.2768 27.769 2760 40.410 29.364 2319 332.3(627) 1.3111 27.772 2333 1.714 3948 2.059 0.90970 13.710 0.0588 2146 56.518 156.5 0.15 0.64 COMBUSTOR 40.631 133.569 3489 650.4(986) 1.2689 27.959 2806 40.631 33.981 2575 357.1(702) 1.3002 27.964 2440 1.570 3831 2.073 0.91470 13.710 0.0585 2142 54.456 156.2 0.15 0.84 COMBUSTOR 0 10 3 202 41,101 124,171 3599 647.5(1019) 1.2630 28,103 2836 41.101 42.738 2857 404.8(786) 1.2890 28.110 2552 1.365 3485 2.081 0.91095 13.710 0.0588 2128 49.332 155.2 0.15 1.00 COMBUSTOR 0 11 4 200 41,500 118,706 3591 644,9(1016) 1,2632 28,103 2833 52.034 3009 452.8(833) 1.2838 28.110 2614 1.186 3100 2.084 0.89636 13.710 0.0597 2117 43.184 154.4 0.15 1.00 41.500 COMBUSTOR 0 12 41.611 117.348 3589 644.2(1016) 1.2633 28.103 2832 41.611 - 53.946 3038 462.4(802) 1.2828 26.109 2626 1.149 3016 2.084 0.89053 13.710 0.0601 2116 41.739 154.3 0.15 1.00 COMBUSTOR 0 13 6 21 42.101 102.823 3579 640.8(1012) 1.2634 28.103 2828 42.101 35.087 2835 397.8(779) 1,2897 28.110 2543 1.371 3487 2.093 0.85827 13.710 0.0624 2046 46.511 149.3 0.15 1.00 COMBUSTOR 0 14 7 21 42,460 86.317 3571 638.3(1010) 1.2634 28.103 2825 42.460 36,902 2975 442,0(823) 1,2848 28,109 2600 1,205 3134 2,105 0.82855 13,710 0.0646 1946 40,350 141,9 0.15 1.00 COMBUSTOR 0 15 8 71 42.601 80.615 3568 637,2(1009) 1,2634 28,103 2824 42.601 36.314 5007 452.2(832) 1.2837 28.109 2613 1.165 3043 2.109 0.81589 13.710 0.0656 1907 38.581 139.1 0.15 1.00 COMBUSTOR 0 16 9 21 43.586 59,794 2840 635.0(828) 1.2999 26.066 2654 33.675 2483 518.6(713) 1.5118 26.066 2492 0.968 2413 2.167 0.73672 13.765 0.0730 1662 27.624 120.7 0.27 0.11 43,586 COMBUSTOR 0 17 10 21 43.596 61,239 2699 634,9(784) 1,3064 25,922 2601 43.596 33.649 2341 519.3(670) 1.3183 25.922 2433 0.988 2404 2.152 0.73608 13.765 0.0730 1658 27.501 120.4 0.27 0.02 COMBUSTOR 0 18 11 21 43.661 60.267 2676 634.1(777) 1.3075 25.900 2591 43.661 33.475 2326 521.4(666) 1.3191 25.900 2427 0.978 2374 2.150 0.73229 13.765 0.0734 1645 27.020 119.5 0.27 0.00

REACING =	0061	RFOCK	E 181 7	[hE =	262.5	62 MACI	н 6.	0 P1 1	= 745	249	TT = 299.	3.4						
	P	7	h		GAMMA	MOLWT	80NV	MACH	VEL	8	W/A	jų.	A/AC	MOMTM	©	IVAC	PHI	ETAC
CUMBUSTUK		19	12 21															
44,310	53.493	2646	025.31	768)	1.3085	25.897	2578											
44.310	38,930	2453	563.2(7n6)	1.3148	25.897	2489	0.709	1764	2.156	0.70695	13,765	c.n760	1513	19.377	109.9	0.27	0.00
COMBUSTOR	(20	13 21															
44.800	44.837	3539	617.7(1	044)	1.2640	26,889	2876											
44.800			579,9(1						1374	2.224	0.59021	13,765	0.0779	1446	14.739	105.1	0.27	0.66
COMBUSTOR			14 21	• .				•					• • •			•		
46.250	55.692	2652	626.3(892)	1.3105	22.275	2785											
46.250			620.10						558	2.432	0.65182	13,972	0.0837	1405	5,649	100.6	0.73	0.08
COMBUSTUR			15 21			-		•		-	-		•	-	-			•
46.260	55.893	2415	626,2(8(8)	1.3214	22.073	2681											
46.260			620.01					0.208	556	2.403	0.65177	13.972	0.0837	1406	5.634	100.6	0.73	0.01
COMBUSTOR			16 21	• - •				-			-		*	·				•
46.381	56.672	2374	624.2(794)	1.3233	22.043	2662											
46.381			618.8						520	2.396	0.64772	13,972	0.0842	1418	5.239	101.5	0.73	0.00
COMBUSTOR			17 21		• • • • • • • • • • • • • • • • • • • •		-	-				-	-	_				•
47.096	52.636	2338	10.516	781)	1.3246	22.039	2643											
47.096			596.5(900	2,397	0.62077	13.972	0.0879	1467	6.685	106.4	0.73	0.00
COMBUSTOR	0	25	16 21	•	-		-	-					•				-	•
47.310	49,635	4082	609.3(1	411)	1.2323	23.695	3249				,							
47.310	46.745	4036	588,9(1)	393)	1.2344	23,699	3233	0.313	1011	2.545	0.60971	13.972	0.0895	1510	9.577	108.1	0.73	0,56
COMBUSTOR			19 21															
48.110	47.116	2576	597.5(864)	1.3131	22.275	2748											
48 - 110			556.8(824)	1.3168	22.275	5943	0,530	1427	2.436	0.55727	13.972	0.0979	1606	12.362	114.9	0.73	0.08
COMBUSTOR			20 21															
49.621	43.244	2280	576.3(759)	1.3261	22.073	2610											
49.621			437.2(6	620)	1.3401	22.073	2391	1.103	2638	2.405	0.43195	13.972	0.1263	1812	17.710	129.7	0.73	0.01
COMBUSTOR			21 21			_												
51.061			584.0(8															
51.061			416.9(672)	1.3476	19,185	2505	1.161	5000	2.695	0.35707	14.194	0.1552	1909	16,140	134.5	1.23	0,03
COMBUSTOR			55 51															
51.071			585.9						.									
51-071	15.721			6(9)	1,3545	19.091	2420	1.203	5415	2+667	0.35661	14,194	0.1554	1910	16.135	134,6	1,23	0.00
COMBUSTOR		30																
51.601			578.6(
51,601			390.10	39V)	1.3578	14,000	2308	1.24/	3071	54001	0.33351	14-144	0.1002	1948	15.914	137.2	1.23	0.00
COMBUSTOR		31		n D .														
53.011	33.310							4 225	7400	3 74 4	0 10 11 21	4 4 4 0 4	0.4050	104.1	. 7 605			
53.011 COMBUSTOR		32	367.9((08/1	1.2445	17.277	6254	1.257	2100	6+/14	V.20424	14,174	0.47.420	2042	13.695	143.4	1.63	0.00
				0.00	. 7124	40 557	2002											
55,111 55,111			536.0(S					1 378	7744	2 743	0 27207	4 / 4 / 5 //	0 2770	7148	(5 (47	4 E O D	. 27	A 17
COMBUSTOR		33	309.5(,60)	1.3321	17,000	2033	1.2/0	2200	E . 100	V. 23271	14,174	V . & 3 1 7	\$100	12.187	13500	1 * 5 2	0.4.2.3
55,611			530.8(16	A . Z .	1 3100	10 403	2045											
55,611			294.5						3/130	3 770	0.33146	1// 10/	0 5040	25 61 //	11.941	1 E // 4	4 22	A 15
COMBUSTOR		34		, , , ,	1 4 3 2 4 1	171003	2050	11510	2474	21110	V 9 E E J 4 J	14117-	0.2400	6174	119741	12410	1,63	0413
55.760			529.3(1	0.63	1 3004	10.411	2048											
55.760			287.8						3476	2.772	0-22076	14.194	0.2510	2202	11,926	155.1	1.22	A 15
COMBUSTOR		35		, , , ,	10200	,,,,,,	5041		2410		4122010	448444	015210	FEVE	11112		1 5 6 7	0115
56,361			523.5(1	2471	1.2856	20.012	3170											
56.361			263.9						360#	2.800	0-17054	14-194	0.3250	J345	9.551	166-6	1.23	0.26
COMBUSTOR		36		- U 1	.,	~~~		- 42		~V	2001024		447674	2242		*****		3,50
57.121			516.9(1	1491	1,2937	19.89n	3105											
57.121			182,0(4094	2.818	0.16295	14.194	0.3401	2397	10.367	168.9	1.23	0.22
TOPALLETOR		37		. 1 - 7	.,											,		» J
			507.6(1	173)	1.2905	19,955	3127											
758.546 58.546			145.70						4255	2.825	0.15066	14.194	0.3678	2443	9.963	172.1	1.23	0.24
•			• •			-	-	• -				• •						

GAMMA MOLHT SONV MACH VEL S AZAC HUMTH H/A IVAC PHI ETAC H COMBUSTOR 0 38 31 4 56.601 23,017 3160 507.4(1222) 1,2844 20,053 3172 58.601 6.716 2361 170.9(891) 1.3122 20.056 2783 1.474 4103 2.841 0.15021 14.194 0.3689 2445 4.578 172.2 1.23 0.27 COMBUSTUR 0 39 32 58.741 22,970 3161 506,6(1222) 1,2844 20,055 3172 58.741 0.620 2374 167.3(888) 1.3124 20.057 2779 1.403 4121 2.841 0.14915 14.194 0.3716 2448 9.550 172.5 1.23 0.27 COMBUSTOR 0 40 33 6 58.82: 25,363 2989 506,1(1152) 1,2930 19,916 3106 58.821 5.632 2095 127.6(777) 1,3250 19.917 2632 1.654 4352 2.816 0.15083 14.194 0.3674 2450 10.202 172.6 1.23 0.23 COMBUSTOR 0 41 34 4 59,101 26.460 2934 504.4(1129) 1.2956 19.875 3084 59.101 5.250 1996 109.7(738) 1.3295 19.876 2576 1.725 4445 2.806 0.15039 14.194 0.3685 2456 10.387 173.1 1.23 0.22 COMBUSTOR 0 42 35 4 59.327 25.760 2990 502.9(1152) 1.2929 19.922 3106 59.327 5.479 2073 115.5(768) 1.3257 19.923 2619 1.681 4403 2,814 0.15002 14.194 0.3694 2061 10.266 173.4 1.23 0.23 0 43 36 4 COMBUSTOR 23.716 3168 497.6(1225) 1.2838 20.078 3173 60,051 60.051 6.212 2327 136.5(868) 1.3138 20.080 2751 1.547 4256 2.838 0.14767 14.194 0.3753 2475 9.768 174.4 1.23 0.27 COMBUSTOR 0 44 37 22.577 3322 490.3(1288) 1.2754 20.220 3228 61.071 61.071 6.937 2548 151.4(957) 1.3037 20.224 2858 1.441 4118 2.854 0.14673 14.194 0.3777 2468 9.590 175.3 1.23 0.31 COMBUSTOR 0 45 38 6 63.081 30.147 2853 478,6(1095) 1.2988 19.858 3046 63,081 4,600 1812 45,6(665) 1.3374 19.659 2463 1.890 4655 2.782 0.15184 14.194 0.3650 2463 10.983 175.0 1.23 0.22 COMBUSTOR 0 46 39 64,501 21.785 3645 470.7(1423) 1.2558 20.539 3329 64.501 12.094 3224 275,3(1237) 1.2738 20.549 3152 0.992 3127 2.878 0.15595 14.194 0.3553 2480 7.578 174,7 1.23 0.39 COMBUSTOR 0 47 40 66,965 20,630 3630 454,9(1415) 1,2561 20,556 3321 66.965 10.779 3169 241.8(1213) 1.2757 20.567 3126 1.045 3265 2.880 0.14782 14.194 0.3749 2475 7.501 174.4 1.23 0.40 COMBUSTOR 0 48 41 3 67.341 19.164 3632 452.4(1416) 1.2556 20.562 3320 67.341 10.183 3182 244.4(1219) 1.2749 20.573 3131 1.030 3226 2.887 0.13743 14.194 0.4032 2478 6.889 174.4 1.23 0.40 COMBUSTOR REGEN 49 42 21 67.341 19.164 3951 611,9(1559) 1.2372 20.541 3439 67.34 13-127 3671 472-5(1433) 1-2517 20-559 3333 0.792 2641 2-929 0.13743 14-194 0.4032 2521 5-641 177-6 1-23 0.40 NOZZLE 50 43 89.577 19.164 3632 452.4(1399) 1.2556 20.562 3320 89,577 0.511 1573 -421.6(559) 1.3391 20.577 2256 2.931 6613 2.887 0.02861 14.194 1.9370 3171 2.940 223.4 1.23 0.40 NOZZLE PO 51 44 19,164 3632 452,4(1399) 1,2556 20,562 3320 89.577 89.577 0.388 1466 -462.0(518) 1.3447 20.577 2183 3.099 6764 2.887 0.02383 14.194 2.3250 3215 2.505 226.5 1.23 0.40 MOZZLE AE REGEN 52 45 89.577 19.164 3951 611.9(1559) 1.2372 20.541 3439 89.577 0.560 1795 #336.0(644) 1.3285 20.577 2400 2.869 6887 2.929 0.02861 14.194 1.9371 3316 3.062 233.6 1.23 0.40 NOZZLE PU REGEN 53 46 4 89.577 19.164 3951 611,9(1559) 1,2372 20,541 3439 0.388 1638 #396.7(583) 1.3358 20.577 2299 3.090 7104 2.929 0.02241 14.194 2.4726 3380 2.474 238.1 1.23 0.40 89.577 FICTIVE COMBUSTR 73 66 243,627 5276 452,4(2123) 1,1733 22,126 3729 67.34 67.341 0.388 1426-1326.6(477) 1.3266 22.426 2048 4.607 9435 2./10 0.03726 14.194 1.4874 4310 5.463 303.7 1.23 1.00 FICTIVE NOZZLE 74 67 0 89.577 17.257 3562 419.4(1385) 1.2588 20.565 3293 89.577 0.529 1591 *414.8(565) 1.3382 20.577 2268 2.849 6461 2.888 0.02861 14.194 1.9371 3113 2.872 219.3 1.43 0.40

					•						
XABS	Pe18	P⇔oβ	PD#	X O O	⊌≠IB	Q=()B	CAMPLL	PwIH/FS0	P=18/PT0	P=08/P80	P=OB/PIO
6.981E=01	1.060E 00	0.000	-4.645L=01		0.000	0.000	2.470E-02		1.422E-C3	0.000	0.000
1.836E 01	1.060E 00	0.000	-3.531E 01		0.000	0.000	1.634E 02	2.732E 00	1.422E-03	0.000	0.000
3.070E 01	2.275E 00	0.000	-1.705t 02		0.000	0.000	5.053E U2	5.863E 00	3.053£=03	0.000	0.000
3.508E 01	4.009E 00	0.000	-3.741E 02		0.000	0.000	6.804E 02	1.033E 01	5.379E=03	0.000	0.000
3.555E 01	4.115E 00	0.000	-4.112E 02		0.000	0.000	7.013£ 02	1.060E 01	5.522E=03	0.000	0.000
3.606E 01	3.905E 00	0.000	-4.522E 02				7.2466 02	1.0256 01	5.320t=03	0.000	0.000
3.648E 01	4.289E 00	0.000	-4.875E 02				7.443E 02	1.105E 01	5.756E=U3	0.000	0.000
3.701t 01	4.250E 00	0.000	=5.347t 02				1.696E 02	1.095E 01	5.703E-03	0.000	0.000
3.7488 01	4.0802.00		#6.340E 02				7.926E 02	1.051E 01	5.475t=03	1.4628 01	7,611E=03
3.748E 01	4.078£ 00		-6.341£ 0≥				7.929£ 02	1.051E 01	5.472E+03	1.474E 01	7.675E=03
3.8038 01				-			8.510E 02	9.9998 00	5.2066-03	2.599E 01	1.3536>02
	00 3088.E		-6.293E 02					1.240E 01	6.457£#03	2.848E 01	
3.815E 01	4.812€ 00		06.245£ 02				8,641E 02				1.4836+02
3.875E 01	9,449E 00		□6.128E 02				9,304E 02	2.4358 01	1.2686#02	5,595E 01	1.8726+02
3.901E 01	1.146E 01		50 3801.6				9,595L 02	2,9538 01	1.5366+02	3.919E 01	2,041E=02
3.950E 01	1.085E 01		-6.054E 02				1.015E 03	2.796E 01	1.456E=02	4.530E 01	2.3596 = 02
3.961E 01	1.226E 01		#6.030E 02				1.028E 03	3.160E 01	1.645E=02	4.667E 01	2.430E=02
4.0002 01	1.724E 01		m5,943E 02				1.073E 03	4.442E 01	2.3136-02	6.269E 01	3.264E+02
4,040E 01	2.760E 01		-5.898E 02				1.119E 03	7.113E 01	3.704E-02	7.914E 01	4.121E=02
4.041E 01	2.786E 01		*5.896E 02				1.120E 03	7.179E 01	3.738E=02	7.955E 01	4.142E = 02
4.063E 01	3.357E 01		-5,897E 02				1.146E 03	8.652E 01	4.505E-02	8.861E 01	4.6146-02
4.110E 01	4.575E 01		-5.944E 02				1.201E 03	1.179E 02	6.139E=02	1.024E 02	5.330E+02
4-150E 01	5.610E 01		-5.985E 02				1.248E 03	1.446E 02	7.528E-02	1.236E 02	6.437E=02
4.161E 01	5.764E 01		-5.979E 02				1.261E 03	1.485E 02	7.735E-02	1.295E 02	6.743E=02
4-210E 01	6.447E 01		-6.587€ 02				1.319E 03	1.661E 02	8.651E=02	1.469E 01	7,648E=03
4.246E 01	6.949E 01		-7.529E 02				1.361E 03	1.791E 02	9.324E=02	1.112E 01	5.792E+03
4.260E 01	6.885E 01		=7.897£ 02				1.378E 03	1.774E 02	9.239E-02	9.728E 00	5.065E=U3
4.359E 01	6.440E 01					02 =3.371E 01	1.496E 03	1.060E 05	8.641E-02	7.603E 00	3.959E=03
4.360E 01	6.436E 01					02 #3.451E D1	1.497E 03	1.028E 05	8.635E=02	7.581E 00	3.948E+03
4.366E 01	6.406E 01					02 -3,986E 01	1,505E 03	1.651E 02	8.596E=02	7.441E 00	3,875E+03
4.431E 01	6.113E 01					02 m1.041E 02	1.583£ 03	1.575E 02	8.2026+05	4.312E 01	2.2456.02
4,480E 01	5.891E 01					02 41.649E 02	1.642E 03	1.518E 02	7.905E=02	7.004E 01	3.647E=02
4.625E 01	5.040E 01					02 93,683E 02	1,819E 03	1.299F 02	6.763E=02	1.497E 02	7.795E=02
4.626F 01	5.034E 01					02 -3.697E 02	1.820E 03	1.297E 02	6.755E=02	1.502E 02	7.823E+02
4.638E 01	4.963E 01					02 #3.874E 02	1.835E 03	1.279E 02	50=3099°9	1.569E 02	8.168E=02
4.710E 01	4.543E 01					S0 3088.44 50	1.923E 03	1.171E 02	6.0966=02	1.340E 02	6.975E=02
4.731E 01	4.417E 01					02 #5.164E 02	1.950E 03	1.138E 02	5.9286-02	1.271E 02	6,617E=02
4.811E-01	3.926E 01					50 3571.8m	2.04BE 03	1.012E 02	5.268E=02	1.015E 02	5.2836=02
4.962E 01	2.059E 01					03 @8.013E 02	2.236E 03	5.305E 01	2.762£=02	5.305E 01	2,762E=02
5.106E 01	1.575E 01					03 =9.841E 02	2.416E 03	4.060E 01	2.114E=02	4.060E 01	2.114E+U2
5.107E 01	1.572E 01					03 =9.854E 02	2.417E 03	4.051E 01	2.109E-02	4.051E 01	2.1095-02
5.160E 01	1.394E 01					03 =1.056E D3	2.484E 03	3.593E 01	1.871E=02	3,593E 01	1,871E+02
5.301E 01	1.350E 01					03 =1.238E 03	2,661E 03	3.479E 01	1.8116=02	3.479E 01	1.811E=02
5.511E 01	1.121E 01					03 -1.473E 03	2.927E 03	2,889E 01	1.505E=02	2.889E 01	1.505E=02
5,561E 01	1.066E 01					03 -1.524E 03	2,991E 03	2.748E 01	1.431E=02	2./48E 01	1.431E=02
5.576E 01	1.039E 01					03 #1.539E 03	3.010E 03	2.678E 01	1.3956-02	2.678E 01	1.395E=02
5.636E 01	9.315E 00					03 =1.595E 03	3.051E 03	2.400E 01	1,250E-02	2,400E 01	1,250E=02
5.712E 01	5.616E 00					03 =1,654E 03	3,109E 03	1.447E 01	7,535E#03	2.049E 01	1.067E-02
5.855E 01	6.007E 00					03 -1.730E 03	3.217E 03	1.548E Q1	8.060E=03	1.548E 01	B.060E=U3
5.860E 01	7.500E 00					03 =1.732E 03	3.224£ 03	1.933E 01	1.0064-02	1.529E 01	7,959E+U3
5.874E 01	7.500E 00					03 =1, 738E 03	3.241E 03	1.933E 01	1.006E=02	1.479E 01	7.703E=03
5.882E 01	5.632E 00					03 -1.741E 03	3.252E 03	1.451E 01	7.557E=03	1.451E 01	7,557L=03
5.910E 01	5.250E 00					03 -1.755E 03	3,287E 03	1.353E 01	7.045E-03	1.353E 01	7.045E=U3
5.933E 01	5.479E 00					03 -1.770E 03	3.316E 03	1.412E 01	7.352E=03	1.412E 01	7.352E=03
6.005E 01	6.515E 00					03 ₽1,823E 03	3.409E 03	1.601E 01	8,336E+03	1.601E 01	8,336E+03
6.107E 01	6.937E 00					03 -1.899E 05	3.539E 03	1.78BE 01	9.309E=03	1.788E 01	9,309E=03
6.30BE 01	4.600E 00	4.600F 00	=4.87#L 01	=3.662E 0	3 =1.639E :	03 #2.023E 03	3.797E U3	1.185E 01	6,172E=03	1.185E 01	6,172E=03
,			_								

L XABS	P=18	P=08	PDA	OOx	ធ=18	ធ≕ក្ន	CAMALL	P=18/PS0	F#18/PT0	P=0b/F80	P=08/PT0
5.450E 01	1.2098 01	1.209E 01	-4.874E 01	+3.7/4E 03	3 +1+665E 03	-2.109E 03	3.980E U3	3.116E 01	1.6236=02	3.116b 01	1.6231=02
6.696E 01	1.0766 01	1.078F 01	-4.874E 01	03.998E 03	3 ×1.714E 03	uŽ 204E 03	4.296E U3	2.7786 01	1.4461-02	2.778E 01	1.4466-02
6.734E 01	9.787E 00				\$ -1.722E 03		4 344E 03	2 5228 01	1.313E-02	2.726E 01	1.419E=02
6.738E 01	9.787E UO	1.056F 01	=4.874E 01	=4.058F 03	3 -1-723E 03	-2.419F 03	4 349E 03	2.522E 01	1.313E-02	2./20E 01	1.417E=02
6.758F 01	9.381E 00				3 =1.727E 03		4.375E 03	2.4186 01	1.259E=02	2.693E 01	1,402E=02
6,924E 01	6,010E 00	4.980E 00			3 =1.756E 03		4.591E 03	1.549E 01	8.0648-03	1.283E 01	6.682E=03
6.991E 01	4.354E 00	4.845E 20	1.3925 02	-4.2175 AT	3 -1 - 764E 03	-2 4675 67	4.672E 03	1.122E 01	5.8424-03	1.249E 01	
7.068F 01	2.450E 00	3.721E 00			3 =1.772E 03		4.767E 03				6.501E#03
7.140E 01	1.938E 00	2.670E 00			3 =1.777E 03		4.855£ 03	6.514F 00	3.287E-03	9.589E UU	4.9936=U3
7.201E 01	1.505E 00	2.181E 00						4.995E 00	2.601E-03	5.880E 00	3.583E=03
7.296E 01	1.058E 00	1.420E 00	•		3 =1.781E 03		4.929E 03	3.878E 00	2.019E-03	5.621E 00	2.927E=03
7.339E 01	8.550E=01	•			3 =1.786E 03		5.043E 03	2.725E 00	1.4198-03	3.659E 00	1.905E=03
7.49>E 01	6.319E+01	1.329E 00			-1.788E 03		5,096£ 03	2.203E 00	1.147E=03	3.425E 00	1.7836=03
7.507E 01		1.005E 00		#4.411E 03	3 -1.793E 03	-2.618E 03	5.280E 03	1.6288 00	6.479E=04	2,590E 00	1.3496-03
7.587E 01	6.100E=01	9-1175-01	4.700E 02	=4.414E 03	3 +1.793E 03	=2.620F 03	5.297E 03	1.572E 00	8 . 185E = 04	2,349E 00	1.2236.03
	6.569E=01	4.450E=01	4.925E 02	#4.431E 03	3 -1.796E 03	≥2.635E 03	5.382E 03	1,6938 00	8,814E=04	1.147E 00	5.971E=U4
7.582E 01	6.371E=01	4.425E-01	4.933E 02	m4-431E 03	3 =1.796E 03	#2,635E 03	5,382E 03	1.693E 00	8.818E-04	1.140E 00	5.938E-04
7.719E 01	7.400E=01	0.000	5.081E 02	#4.465E 03	3 a1.799E 03	□2.666E 03	5.434E 03	1.907E 00	9.930t=04	0.000	0.000
8.000E 01	9.850E=V1	0.000	5.426£ 02	●4.472E 03	3 -1.806E 03	-2.656E 03	5.532E 03	2.538E 00	1.322E-03	0.000	0.000
8.390E 01	7.700E=01	0.000	5.801E 02	-4.401E 03	3 =1.815E 03	-2.666E 03	5,6376 03	1.984E 00	1.033E=03	0.000	0.000
8,671E 01	6.150E=01	0.000	5,9558 02	=4.488E 03	3 -1 -823E 03	=2.666E 03	5.691E 03	1.585E 00	8.252E=04	0.000	0.000
8.957E 01	8.000E=01	0.000	6.126E 02	-4.50ZE 03	3 =1.836E 03	-2.666E 03	5.714E 03	2.062E 00	1.0736-03	0.000	0.000
8.958E 01	8.004E=01	0.000	6.126E 02	#4.502E 03	3 +1.836E 03	#2.666E 03	5.714E 03	2.063E 00	1.074E-03	0.000	0.000

X	DDRAG	CORAG	CF	нс
44444444444444444444444444444444444444	DDR AG	######################################	2.03 2.03	22222222222222222222222222222222222222
6,308E	01 3.796E 00 01 8.154E 00	2.513E 02	3.088E=03	1.708E#02 1.332E#02
6.696E 6.734E 6.738E	01 5.243E 00 01 7.752E 00 01 1.197E 00 01 1.228E-01	2.647E 02 2.725E 02 2.737E 02 2.738E 02	3.423E > 03 3.474E = 03 3.466E = 03	2.229E=02 1.858E=02 1.751E=02 1.743E=02
6,924E	01 6.178E=01 01 5.446E 00 01 2.101E 00	2.744E 02 2.799E 02 2.820E 02	3.310E=03 3.276E=03	1.754E=02 1.368E=02 1.241E=02
7.140E	01 2,253E 00 01 1,847E 00 01 1,368E 00 01 1.841E 00	2.842E 02 2.861E 02 2.874E 02 2.893E 02	3.151E+03 3.115E+03	9.738E=03 8.038E=03 6.903E=03 5.216E=03
7.339E 7.492E	01 7.260E=01 01 2.288E 00 01 1.920E=01	2.900E 02 2.923E 02 2.925E 02	3,030Em03 2,979E=03	4.762E=03 3.851E=03 3.649E=03
7.58ŽE	01 8,372E=01 01 1,446E=03 01 S,079E=01	2.933E 02 2.933E 02 2.938E 02	2.910E=03 2.909E=03	2.867E=03 2.863E=03 3.559E=03

READING = 0061 BLOCK = 181 TIME = 262.562 MACH 6.0 PT = 745.249 TT = 2993.4

[emi	×		DORAG	CDRAG		CF	н¢
42	8.000E 8.390E 8.671F 8.957E 8.958E	01 01 01	1.140E 00 1.225E 00 5.498E=01 2.302E=01 0.000	2.950E 2.962E 2.968E 2.970E 2.970E	20 20 20	2.979E=03 2.919E=03 2.869E=03 2.898E=03 2.898E=03	4.303E=03 3.615E=03 3.645E=03 3.601E=03 3.602E=03

RAMJET PERFORMANCE

ENGINE PERFORMANCE	INLET
CALCULATED THRUST, 3000000000000000000000000000000000000	ANGLE OF ATTACK ************************************
REGENERATIVE COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	INLET PROCESS EFFICIENCY - SUBSUNIC 0.9012 KINETIC ENERGY EFFICIENCY - SUBSUNIC 0.9256 KINETIC ENERGY EFFICIENCY - SUBSUNIC 0.9256 KINETIC ENERGY EFFICIENCY - SUBSUNIC 0.8814 ENTHALPY AT PO - SUPERSUNIC 1.66 (BTU/LBM) ENTHALPY AT PO - SURSUNIC 32,56 (BTU/LBM)
MOMENTUM AND FORCES	COMBUSTOR
INLET FRICTION ORAG	FUELWAIR RATIO
SHOITATE	FUEL INJECTORS
NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A 40.400 A 1B 43.586 E 1C 44.300 2A 51.061 D 2C 46.250 E 3A 56,351 3B 58,536 4 47,066

t = 273.36 sec.

 ϕ 's were higher than planned.

Test cell pressure was high which resulted in slightly increased AIM nozzle pressures.

SUHMARY REPORT

								SU	н м д	RY	н Е з	, 0 4 1							
		P	7	н		GAMMA	MOLHT	SONV	MACH	۷۴L	8	W/A	4	A/AC	MIMOM	Q	IVAC	PHI	ETAC
	WIND TUNN 0:000	EL 745.749	1 3001	0 5 670.00	7951	1.2928	28.455	2581											
	0.000	0.390		=31.10 0 b	98)	1.3989	28,954	989	5,987	5923	1.828	0.10609	13,415	0.4937	2519	9.765	187.8		
	SPIKE TIP	19.062	3001	670-01	795)	1.2926	28.954	2581						6 4077	2447		4 EL /2 A		
	0.600 WIND TUNN	17.433 EL	2941 3	651.8(777)	1.2946	28,954	2557	0,374	955	2.079	0.10609	15,415	0.4437	2003	1.575	17440		
		745.749		670.00	795)	1.2928	28.955	2581 998	5.931	5916	1.828	0.11040	13,961	0.4937	2619	10.151	187.6		
	SPIKE TIP	N8	4	0 Q					.,,.,	.,	*,		•••	•					
	0,600 0.600	19.062 17.279		670.0(650.0(776)	1,2948	28,954	2555	0,392	1001	2.079	0.11040	13,961	0.4937	2619	1.717	187.6		
	INLET THR	740 252.216	5 2862	0 6 628.0(754)	1.2972	28,954	2525											
	40.400 INLET UPN	15,498	1447	228.10	357)	1.3510	28,954	1832	2,442	4474	1,888	0.89786	13,415	0.0583	2097	62.421	156.3		
	40,400	252,216	2862	628.01	754)	1,2972	28,954	2525	2 630	11554		0,81624	17.815	0 06/12	2118	57.798	157.9		
	40.400 INLET DNN		7	0 4						4220	14000	4441014	121412	PERCE	2110	3, , , , ,			
	40.400	97.640		628.0(597.7(754) 724)	1.2972	28.954 28.954	2525	0.495	1232	1.942	0.81624	13.415	0.0642	2118	15,623	157.9		
	COMBUSTOR		8	1 4	9291	1.2758	27.827	2757											
	40,410 COMBUSTOR	29.986		381.80	637)	1.3090	27.630	2347	1,677	3935	2.061	0.90216	13,482	0.0583	2097	55.167	155.5	0.15	0.71
	40.652	127,726	3510	629.81	992)	1.2669	28,041	8085		***	3 495	5 5577/I	12 // 22	0 0500	2000	52.596		0.15	A 9/1
	40.652 COMBUSTOR		10	3 202						2130	E + U 1 3	0.90734	134405	0 2 0 2 0 0	2070	25 \$ 2 7 0	10081	V 1 1 2	V 4 7 77
	41.122	45.330		626.91: 404.91	1002) 789)	1.2649	28.094 28.100	2817 2556	1.304	3332	2.079	0.90289	13,482	0.0583	2073	46.756	153.8	0.15	1.00
	COMBUSTOR 41.500	115,007	11 3538	4 200			28.094												
	41.500	54.134	3009	450.20	834)	1,2837	28,100	2614	1,129	2952	2.082	0.88890	13,482	0.0592	2058	40.781	152,7	0.15	1.00
		113.234		5 200 623.5(999)	1.2652	28.095	2814		5050	2 407				2051	70 . 77	163 4	^ 1E	
	41.632 COMBUSTOR	56,058 0	3040 13	460.3(6 21	843)	1,2020	\$6.100	2021	1-000	2626	2.003	0.88201	13,402	1,650.0	2074	39,177	13614	0.13	1444
	42,122	99,322		620.2(399.1(996) 784)	1.2653	28.094 28.100	2810 2549	1.305	3326	2.091	0.84896	13,482	0.0620	1983	43,880	147.1	0.15	1,00
	COMBUSTOR		14	7 21			28,094												
	42.460	38.498	2968	437.2(8211	1.2850	28,100	2598	1.157	3006	2.102	0.82119	13.482	0.0641	1892	36.560	140.3	0.15	1.00
	COMBUSTOR	78,653		8 21 610,5(992)	1.2654	28,094	2805								=			
	42.622 COMBUSTOR	37•972 0 ≀	3004 16	448.9(9 21	832)	1.2837	28.099	2612	1,109	2896	2,107	0.80674	13.482	0.0652	1846	36,308	137-1	0,15	1.00
	43,607 43,607	60,254 36.589	2780 2413	613.4(805) 707)	1.3018	26,192	2621	0.898	2230	2.151	0.72803	13.529	0.0726	1618	25.227	119.6	0.26	0,12
	COMBUSTOR	₹ ģ	17	10 21 613.4(* *		•				•	Ţ
فيسار	43.617	36.579	2332	514.4(664)	1.3184	26,050	2455	0.918	2225	2.136	0,72625	13,529	0.0727	1617	25,111	119.5	85,0	0.02
113	45.002	60.645	2618	11 21.5	755)	1,3092	26.029	2559			_								
451	43.682	36,483	2319	516.9(660)	1,3191	26.029	2417	0.905	2189	2.135	0.72364	13,529	0.0730	1605	24.613	118.4	0.26	0.00

OF POOR QUALITY

	₽	T	н		GAMMA	MOLWT	SONV	MACH	VEI.	8	W/A	W	A/ÅC	MOMEN	Q	IVAC	PHT	ETAC
TCOMBUSTOR	0	19	12 21							•	, -,	•	7-7-11-0	• ,	-	. ,		
ም 744 - 31 ስ	54.611	2589	504.11	746)	1.3102	20.020	2546											
¥4.310	41.667	2428	552.3(695)	1.3155	26,026	2470	0.652	1510	2.139	0.69917	15.529	0.0755	1483	17,494	109.0	0.26	0.00
COMBUSTOR	0	20	13 21										•					-
44.800	51.700	3287	596.5(960)	1,2766	26,796	2790											
44.800	45,715	3200	566.9(935)	1,2797	26,797	2756	0.441	1217	2.197	0.6B197	13.529	0.0775	1419	12.896	104.9	0.26	0.53
COMBUSTOR		21	14 21															
46.250	70.000	2503	616.5(089)	1,3138	21,672	2790											
46.250 Combustor	220100	2013	612.70	080)	1.3141	21.6/2	2785	0.157	437	2.473	0.64547	13.777	0.0833	1376	4,381	99.9	0.82	0.08
46.260			15 21	0 - 11 5	4 7347	2. 42.	2/02											
46.260	55.740	2775	616.3(004)	1.324/	21.470	2002	A 44.3	4.7.4	2 442	A 4.0.04		A 4090					
COMBUSTOR	0	23	612.60	2001	113631	E11410	2011	0.100	424	C • 446	0.04440	13.///	0.0034	12//	4.348	100.0	0.02	0,01
46.402	57.583	2304	614.0¢	7 p Q 1	1.3266	21.888	2662						*					
46,402	50.750	2296	610.90	7851	1.3269	21.448	2657	0.148	794	2.414	0.64040	13.777	0-0846	1700	3.923	100.0	6.85	0.00
COMBUSTOR	0	€4	17 21					0	2,-	4 T T T	V,0-0-0	*****	0,000	1370	24762	100,7	0,02	0,00
47.117	52.950	2267	602.11	775)	1.3279	21.443	2642											
47.117	49.795	2233	589.3(762)	1.3291	21.443	2623	0.305	801	2.436	0.61452	13.777	0.0875	1459	7.645	105.9	0.82	0.00
COMBUSTOR	0	≥ 5	18 21					• •	• • •							• • • • •	- ,	.,
47.310	50.393	3767	598.8(1	328)	1.2531	22,795	3209											
47.310	47.922	3729	582,4(1,	312)	1,2547	22.796	3195	0.284	907	2.579	0.60364	13,777	0.0891	1482	8,505	107.6	0.82	0.43
COMBUSTOR	0	25	19 21														-	-
48.110	47.375	2457	585.00	842)	1,3186	21.636	2729											
46.110 COMBUSTOR	40.277	5705	549.1(607)	1,3218	21,636	2679	0,500	1341	2.471	0.55181	13.777	0.0975	1580	11.498	114.7	0.82	0.06
49,642	// // U	2144	50 51	7 . 0 .		2. 07.												
49.642	20.125	180/	558.9([44]	1,3504	21,4/1	2595		2442									
COMBUSTOR	0.353	28	418.8()	004)	1.5441	21.4/1	23/0	14111	2647	C+440	0.42590	13.777	0.1263	1791	17.522	130.0	0.82	0.01
51.082	35.795	2135	572.3(B n B Y	1.3358	18.300	2784								•			
51.082	18 604	1807	432.50	7.81	1.3485	18.300	2573	1.028	2446	2.782	0.25213	10.038	n 1552	1807	1/1 515	17/1 0	4 // 4	0.02
COMBUSTOR	0	29	22 7	, 0-,	****	.01200	F 2 1 3		2043	EFICE	4.22222	14,030	0.1225	1073	14,515	13417	1 9 4 1	0 4 0 3
51.092			572.20	7a1)	1.3436	18.192	2692											
51.092	18,592	1642	432,30	642)	1.3567	18.192	2467	1.072	2646	2.746	0.35268	14.038	0.1554	1894	14.501	135.0	1.41	0.00
COMBUSTOR	0	30	23 4					•						•=	,			4,00
51,622	36,269	2082	563,5(825)	1,3382	18.277	≥753											
51.622	174958	1738	417.90	680)	1.3515	18.277	8528	1,068	2699	2.770	0.32984	14.038	0.1662	1942	13,837	138.3	1.41	0.03
COMBUSTOR		31																-
53.032	32,962	2342	542.30	932)	1,3252	18,489	2889			_								
53.032 - Combustor	12:344	1751	367.76	750)	1,3403	18.489	2642	1.119	2956	158.5	0.28111	14.038	0.1950	2058	12,914	146.6	1.41	0.08
55.132	29.484	32		0Es		40 757	2017											
55,132	11.500	2013	516.7(1	042]	1.3117	10,743	3017	4 244	7000	2 04 .								
COMBUSTOR	44427	33	281.86	0313	103315	101/25	2/40	1,200	2428	£,000	0.23040	14.038	0.2379	2197	12,273	156.5	1.41	0.14
55.632	29.085	2659	511.4(1	0443	1.3006	(R.745	2027											
55.632	10.800	2091	263.2(8.71	1.3070	18.745	2715	1.308	3000	2.677	0.000	4 / A Z B	0 3/190	2226	17 467	466 "	4 0.4	
COMBUSTOR	0	34	27 3	1 ,	****	,01103	E 12	145,0	2354	E+0/3	0 6 6 5 0 7 7	4.030	0.5400	2224	12.103	100.4	1.41	0,16
55.760	28.990	2665	510.1(1	047)	1.3092	18.772	3040	.										
55.760	10-562	2087	257.10	815)	1.3300	18.772	2711	1.312	3558	2.874	0.21872	14.038	0.2506	2210	12.092	150 0	4 /4	A 16
COMBUSTOR	0	35	28 5						0,500	F-014	4161012	*-*020	0 \$ 2 3 0 5	6630	16,076	12014	1 4 4 1	0.10
56.382	23.804	3175	503.9(12	285)	1.2844	19,170	3292											
56.382	9.403	5294	258.5(10	014)	1.3060	19.172	2950	1,259	3715	2.946	0-16866	14.058	0.3250	2403	9.736	171.2	1.41	0.26
COMBUSTOR	0	.56	29 4												.,,=0			
57.142	c5 • 147	5033	497.2(1	223)	1.2914	19.070	3196							•				
57,142 COMPUSTOR	7.042	2522	148.7(878)	1.3191	19.071	2783	1.501	4176	2.927	0.16116	14.038	0.3401	2435	10,458	173.5	1.41	0.23
COMBUSTOR 58,567	Ų	57	50 4															-
58.567	6. 27	2044	487.5(1	4U4)	1.2881	19.134	3218											
201001	01623	6631	110.66	070)	1,5151	14.135	2776	1.564	4343	2.934	0.14895	14.038	0.36/9	2482	10.054	176.8	1.41	0.25

READING = 0061 P	LOCK =	193	AINE =	273.36	Z MACI	1 6,0	, P(=	/45.	147	1 - 3001							
P	Ţ	н		GAMMA	MULWT	SONV	масн	VEL	5	M/A	M	A/AC	MUMTH	6	IVAC	PHI	ETAC
COMBUSTOR 0	38 3	1 4															
58,622 23,092	3552	487.3(រូផ្លូក(6)	1.2814	19.238	3568							2484	9.620	174 0	1 /14	0.28
50,622 7.039	2460	140.00	964)	1.3088	14.240	2884	1.445	4168	2.952	0.14851	14.030	0.3041	Zucn	7.020	1/047	1 4 4 1	0.450
COMBUSTOR 0	39 3	2 3	_														
58,762 23,027	3228	486,5(1307)	1,2812	19.241	3564						A =====	2167	4.589	177 3	4 /14	n 28
58,762 6.953	2457	136.60	963)	1,3089	19.244	2882	1.452	4184	2.425	0.14747	14.030	0.3/1/	2401	9,509	11145	1 4 4 1	0160
COMBUSTOR 0	40 3	3 6															
58.842 25.362	3050	486.0(1230)	1.2902	19,102	3201					44 475	0 = 4 9 0	5 (1 0 6	10.286	177 /		0 2//
58.842 5.895			841)	1,3218	19.104	2730	1.624	4434	2,926	0.14917	14.030	0.50/4	2409	10.200	11/13	1041	0 - 2 4
	41 3																
59,122 26.228	3006	484.2(1511).	1.2924	19.071	3182					44 070		2004	10.439	177 8	1.01	0.23
59,122 5.550			806)	1.3255	19.072	2683	1 . 603	4519	C. A10	0.14863	144030	0.3000	2470	10,437	11100	****	0 \$ 2 2
	42 3		_	_													
59.348 25.165		462.6(1249)	1,2880	19.142	3217							2501	10 330	178 5	1.81	n 25
59.34B 5.972			860)	1.3194	19.144	2754	14911	4457	5.431	0.14835	14,030	0.3043	\$341	10.229	Links	****	UBLS
	43 3																
	3362	477.20	1365)	1.2738	19,305	3310		***	2 26"	0 111605	4/1 038	A 7767	2217	9.431	170.7	1.41	0.31
60.072 7.325	5615	135.50	1027)	1,3013	19.370	2424	1,407	4175	Z • 404	0.14605	14,030	042193	6911	78424	11713	* * * *	
	44 3																
	3375	469.81	1370)	1,2729	19,588	3519			2 067		1/1 038	n #777	2611	9.519	180.%	1.41	0.31
61.092 7.125			1022)	1,3014	14.343	2740	1 * 11 5 3	4561	6.403	0.14511	144030	0.3117	2731	7021	,0043		
COMBUSTOR 0		8 6		4 55/#	40 000	7140											
		457.60	1160)	1,2964	19,040	2120		11.7 L.L	3 404		48.63R	0.3650	2526	11.122	179.0	5 . 41	0.23
63.102 4.775			7173	1,5548	14-041	2331	1.900	4/00	60070	0,15016	144030	0.3030	6.46.4		* 1 * * 7	* 4 - *	
COMBUSTOR 0		9 5		. 5575	40 687	71140											
64,522 22,160	3040	444,46	150()	1.2535	19,607	3410	1 420	1207	3 094	A (5/12)	14.018	0.1553	2822	7.894	179.6	1.41	0.39
			12013	1.6/6/	14.044	3640	1.050	2673	2,700	0.15423	144030	0 8 3 3 3 3	F (- F	,,,,,	,	• • • •	
COMBUSTOR O	47 4	10 3		. 2544	10 400	3/100											
66,986 20,982	2010	43343(14411	1.2541	10.711	3400	1.05%	2276	2.988	0.14620	14-038	0.3749	2516	7.671	179.2	1-41	0.39
			1581)	100143	174111	3641	18000	33.0	69700	401.4050							
	48 4		4/14/05	. 3075	10.707	THOR											
	2013	344 44	14471	1.2535	19.718	3316	1.030	2212	2.095	0,13591	14.038	0.4032	2515	6.998	179.2	1.41	0.39
67,362 10,358			1541)	100.30	174110	3610	. 9 0 5 0	2242		41,557.		0 4 4 5 5 6			• • • • •		
	49 4		46631	1,2339	19.483	2521											
67.362 19.482	2/101	307 64	10521	1 2600	10.714	2201	1.188	3012	3.040	0.13591	14.038	0-4032	2593	8,264	184.7	1.41	0.39
67,362 8,580 NOZZLE, AE		ຮາ/∎ສເ ∔3 3	19/9)	1 9 2 0 4 4	136194	2672			28040								
			4.8491	1,2535	19.707	3408											
89.598 0.521	1508 -	430101	5031	1 3178	19.722	2321	2.928	ATTA	2.995	0.02829	14.038	1.9370	3224	2.989	229.7	1.41	0.39
NOZZLE PO		14 3	2421	103310	* / # / 10 14	F-4 F-1	_,,,,,,	• 1 . •		******	• . • . •	- ,		-•-	• • • •		•
89.598 19.482			(499)	1,2535	19.707	3408											
89.598 0.390	1484 -	-537.A/	5.8	1.3437	19.722	2242	3.105	6962	2.995	0.02333	14.038	2.3495	3272	2.524	233.1	1.41	0.39
NOZZLE AE REGEN			4-,			4074				• • • • • • • • • • • • • • • • • • • •							- -
89.598 19.482			16521	1.2339	19-682	3531											
89.598 0.572	1828 =	14.005	6061	1.3269	19.722	2473	2.865	7084	3.040	0.02829	14.038	1.9371	3375	3.115	240.4	1.41	0.39
NOZZLE PO REGEN				* * * * * * * *		₩ → ! ₩				,,							-
89_599 19.482	4000	603-46	16#21	1.2339	19.682	3531											
89.598 0.390	1661 0	3467-11	6(9)	1.3346	19.722	2364	3.096	7319	3.040	0.02190	14,038	2.5024	3443	2.491	245.3	1.41	0.39
FICTIVE COMBUSTR			. 41.7	- D 1 O													•
67.362 252.216			121621	1.1926	21.00A	3803											
67.362 0.390	1300-1	1348.27	4561	1.3374	21,181	2020	4.670	9435	2.802	0.03874	14.038	1.4146	4258	5.681	303.3	1.41	1.00
FICTIVE NOZZLE	74 6						• •							•			
.89.59Å 18.741	3604	395-96	14661	1.2569	19,709	3380											
89.598 0.521	1575	501.6	5841	1.3389	19.722	2306	2,906	6702	2.990	0.02829	14.038	1.9371	3183	2.947	226.7	1.41	0.39
		6 4 4 4					•			* **	-		•	-			

							C A 4 A L 4	P#18/PS0	F=15/PT0	P+08/PS0	P#OB/PTO
YARS	Palt	₽₩OB	PDA	⊕o x	Re I B	Q+08	CAMALL				
6,452E 01	1.1924 01	1.192E 01	3.181E 01	-4 500E	03 -1.678E	03 02.620E 03	5.980E U3	3.059E 01	1.5986=02	3.059E 01	1.5986-02
6.699E 01	1.086E U1	1.086E 01	3.181E 01	04.524E	03 -1.728E	03 -2.796E 03	4.296E 03	2.7896 01	1.457E=02	2.789E 01	1.4576002
6.736E 01	1.001E 01	1.070E 01	3.181E 01		03 a1.7376		4.344E 03	2.57UE 01	1.3436=02	2.747E 01	1.4356-02
-			3.181E 01			03 -2.8252 03	4.349E 03	2.570E 01	1.343E=02	2.743E 01	1.433E-02
6.740E 01	1,001E 01	1.069E 01					4.375E 03	2.464E 01	1.287E-02	2.721E U1	1.4216=02
0.760E 01	9,597E 00	1.060E 01				03 42.838E 03					
6.926E 01	6.150E 00	5.190E 00	1.196E 02	m4.706E	03 =1.774E	03 -2.932E 03	4.591E 03	1.579E 01	8.247E=03	1.332E 01	6.959E=03
6,993E 01	4.438E 00	4.807E 00	2.238E 02	-4.746E	03 m1.784E	03 -2.963E 03	4.672E 03	1.139E 01	5,9516+03	1.234E 01	6.447E>03
7.070E 01	2.470E 00	3.705F 00				03 -2.996E 05	4.767E 03	6.340E 00	3.312E#U3	9.512E 00	4.969E=03
7.142E 01	1.926€ 00	2.675E 00				03 =3,026E 03	4.855E 03	4.944E 00	2.583E+03	6.667E 00	3.587E=03
						03 =3.051E 03	4 929E 03	3.761E 00	1.964E=03	5.752E 00	3.005E=03
7.203E 01	1.465E 00	2.2412 00						2.718E 00	1.420E=03	4.017E 00	2.099E=03
1.298E 01	1.0595 00	1.5658 00				03 -3.085E 03	5.043E 03				
7,341E 01	8.75UE=01	1.447E 00	5,092E 02	#4.908E	03 #1.810E	03 =3.098E 03	5.095E 03	2.246E 00	1.173E=03	3.713E 00	1.9406-03
7.494E 01	6.246E=01	1.025E 0o	5.552E 02	=4.949E	03 -1.816E	03 =3.133E 03	5,280E 03	1,603E 00	8.375E=04	2.631E 00	1.3746-03
7.509E 01	6.000E=01	9.358E-01	5.586E 02	=4.952E	03 =1.816E	03 -3.136E 03	5.2976 03	1.540E 00	8,046£#04	2.402E 00	1.2556-03
7.580E 01	6.523E=01	4.900E=01	5.817E 02	-4-971E	03 -1.819E	03 -3.152E 03	5.3626 03	1.674E 00	8.747E~04	1.258E OU	6.571E=04
7.585E 01	6.526E+01	4.876E.01				03 #3.152E 03	5.382E 03	1.675E 00	8.750t=04	1.252F 00	6.539E=04
7.717E 01	7.450E=01	0.000				03 m3.185E 03	5.434E 03	1.912E 00	9.990E=04	0.000	0.000
8.002E 01	1.000E 00	0.000				03 #3.185E 03	5.532E 03	2.567E 00	1.3410-03	0.000	0.000
8.392E 01	8.100E=01	0.000				03 -3.185€ 03	5.637E 03	2.079E 00	1.086E=03	0.000	0.000
						03 #3.185E 03	5.691E 03	2.682E 00	1.4016-03	0.000	0.000
8,673E 01	1.045E 00	0.000									
8,959E 01	1,555€ 00	0.000				03 =3.1858 03	5.714E 03	3.992£ 00	2.085E=03	0.000	0,000
8.960E 01	1.556E 00	0.000	7.230E 02	-5.048E	03 -1.863E	03 -3.185E 03	5.714£ 03	3.994E 00	2.087E#03	0.000	0.000

4.041E 01 1,861E-01 1.104E 02 3.945E-03 6.847E-104 4.065E 01 4.589E 00 1.237E 02 3.257E-03 7.261E-1 4.112E 01 8.656E 00 1.237E 02 3.257E-03 7.777E-1 4.150E 01 2.97E 00 1.237E 02 3.357E-03 8.015E-1 4.150E 01 2.907E 00 1.403E 02 3.352E-03 8.015E-1 4.165E 01 2.907E 00 1.403E 02 3.348E-03 6.049E-1 4.24EE 01 8.67E 00 1.403E 02 3.348E-03 6.049E-1 4.24EE 01 8.67E 00 1.403E 02 3.348E-03 6.049E-1 4.24EE 01 7.607E 00 1.403E 02 3.348E-03 6.049E-1 4.361E 01 2.517E 00 1.484E 02 3.512E-03 5.00E-1 4.361E 01 1.339E 01 1.616E 02 3.474E-03 5.108E-1 4.362E 01 1.067E-01 1.626E 02 3.474E-03 5.108E-1 4.362E 01 1.067E-01 1.626E 02 3.474E-03 5.108E-1 4.362E 01 1.339E 00 1.714E 02 3.774E-03 3.702E-1 4.362E 01 5.581E 00 1.714E 02 3.774E-03 3.702E-1 4.400E 01 3.372E-00 1.784E 02 3.774E-03 3.702E-1 4.625E 01 6.865E 00 1.783E 02 3.702E-03 3.702E-1 4.602E 01 2.575E-02 1.784E 02 3.594E-03 3.702E-1 4.602E 01 2.575E-02 1.784E 02 3.594E-03 3.702E-1 4.602E 01 3.983E 00 1.805E 02 3.902E-03 3.172E-1 4.602E 01 3.983E 00 1.805E 02 3.902E-03 3.172E-1 4.602E 01 1.028E 01 1.805E 02 3.902E-03 3.172E-1 4.602E 01 1.028E 01 1.805E 02 3.902E-03 3.172E-1 4.602E 01 1.028E 01 1.805E 02 3.902E-03 3.172E-1 4.602E 01 1.028E 01 1.958E 02 3.902E-03 3.703E-1 5.108E 01 7.803E 01 2.805E-0 2 3.605E-0 3.004E-1 5.505E 01 2.803E 01 2.805E-0 3.805E-0 5.505E 01 2.803E 01 2.805E-0 3.805E-0 5.505E 01 2.803E 01 2.805E-0 3.805E-0 5.505E 01 2.803E 01 2.805E-0 3.805E-0 5.505E 01 2.803E 01 2.805E-0 3.805E-0 5.505E 01 2.803E-0 01 2.805E-0 02 3.605E-0 3.805E-0 5.505E 01 2.803E-0 01 2.805E-0 02 3.605E-0 3.805E-0 5.505E-0 01 2.805E-0 01 2.805E-0 02 3.605E-0 3.805E-0 5.505E-0 01 2.805E-0 01 2.805E-0 02 3.605E-0 3.805E-0 5.505E-0 01 2.805E-0 01 2.805E-0 02 3.605E-0 3.805E-0 5.505E-0 01 2.805E		×	DORAG	CDRAG	CF	нс
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8.392E 01	1.260E 00 6,597E+01 3.266E+01	2.905E 02 2.911E 02 2.914E 02	2.991E=03 2.936E=03 2.963E=03 3.012E=03	3.866E=03 4.634E=03 6.130E=03

PAMJET PERFORMANCE

,	MANUEL PERF	HUNDLE			
ENGINE PERFORMANCE			INLET		
MEASURED THRUST	(LBF) (LBF) (LBF=SEC/LBM) (LBF=SEC/LBM)	MASS FLOW RATIO ADDITIVE DRAG COEFF	ICIENT.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0.4937 0.0981	(DEGREES)
CALCULATED THRUST COEFFICIENT		DELTA PT2 TOTAL PRESSURE RECO TOTAL PRESSURE RECO INLET PROCESS EFFIC	VERY = SUPERSONIC VERY = SUBSCNIC, IENCY = SUPERSONIC,	0.1130 0.3382 0.1532 0.8927	(981)
CALCULATED		KINETIC ENERGY EFFI	IENCY - SUBSONIC	0.9004	
	(LBF) (LBF=SEC/LBM)	ENTHALPY AT PO - SU	CIENCY - SUBSUNIC PERSONIC BSONIC	-3.28	(BTU/LBM) (BTU/LBM)
MOMENTUM AND FORCES			CUMBUSTOR		
INLET FRICTION DRAG	(LBF) (LBF) (LBF) (LBF) (LBF)	EQUIVALENCE RATIO., COMMUSTOR EFFICIENC TOTAL PRESSURE RATI COMBUSTOR EFFFCTIVE	Y	1.412 0.390 0.0772 0.5438	0,7700+ 0,6999
NOZZLE PRESSURE INTEGRAL	(L8F) (L8F) (L8F) (L8F)	NOZZLE COEFFICIENT PROCESS EFFICIENCY.	NOZZLE T COEFFICIENT - C5 CIENCY	0.9136	
Stations		FUE	L INJECTORS		
NOMINAL COML LEADING EDGE	4 (IN)	INJECTORS	STATION VA	LVE	
INLET THROAT	O (IN)	1 A 1 B	40,400 43,607	A B	
NOZZLE SHROUD TRAILING EDGE	- ·	50 57 10	44.300 51.082	D E	
STRUT TRAILING EDGE 67.36	5 (IN) 5 (IN) 5 (IN)	3A 3B 4	56,372 58,557 47,107		

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SUMMARY REPORT

Ċ.T. A/AC MONTH G IVAC PHI FTAC . GAPMA POLWT SONV MACH VEL S W/A н WIND TUNNEL 1 0 5 924.499 3019 676.8(802) 1.2933 28.832 2595 0.489 411 -30.5(99) 1.3988 28.831 995 5.977 5949 1.815 0.13226 33.326 0.9838 6285 12.228 188.6 SPIKE TIP NS 0 4 22,437 3019 676.8(802) 1,2932 28.831 2595 20.228 2948 655.5(782) 1.2954 28.831 2566 0.403 1033 2.072 0.13226 33.326 0.9838 6167 2.124 185.1 0.600 WIND TUNNEL 924,499 3019 676.8(802) 1.2933 28.832 2595 0.000 0.473 407 -31.4(98) 1.3988 28.831 990 6.010 5953 1.815 0.12920 32.554 0.9838 6143 11.953 188.7 0.000 SPIKE TIP NS 22.437 3019 676.8(802) 1.2932 28.831 2595 0.600 20.343 2952 656.6(783) 1.2953 28.831 2568 0.391 1005 2.072 0.12920 32.554 0.9838 6143 2.018 188.7 0,600 INLET THROAT 40.400 356.168 2990 668.2(794) 1.2942 28.831 2583 19,983 1483 238.3(368) 1.3500 28.831 1858 2.496 4638 1.878 1.16604 33.326 0.1116 5375 84.045 161.3 40.400 INLET UPNRSK 356.168 2990 668.2(794) 1.2942 28.831 2583 40.400 17,159 1425 223.0(352) 1,3533 28.831 1824 2,588 4720 1.878 1.06004 33.326 0.1227 5428 77.750 162.9 40.400 INLET DNNRSK 0 4 7 153.390 2990 668.2(794) 1.2942 28.831 2583 40.400 40.400 131,581 2887 637,1(764) 1,2974 28,831 2542 0,491 1247 1,936 1,06004 33,326 0,1227 5428 20,539 162,9 COMBUSTOR 0 8 40.410 355.308 2990 668.1(794) 1,2942 28.831 2583 238.6(368) 1.3499 28.831 1859 2.494 4636 1.878 1.16590 33.326 0.1116 5374 83.997 161.3 40.410 20.008 1484 COMBUSTOR 0 9 666.0(792) 1.2944 28.831 2581 41.300 282.118 2983 23,188 1632 278.1(408) 1.3421 28.831 1943 2.267 4406 1.894 1.16824 33.326 0.1114 5225 79.987 156.8 41,300 COMBUSTOR 0 10 41.365 277.854 2983 665.8(792) 1.2944 28.831 2580 23.484 1643 281.2(411) 1.3415 28.831 1949 2.251 4387 1.895 1.17013 33.326 0.1112 5213 79.781 156.4 41.365 COMBUSTOR 0 11 268.541 2981 665.4(791) 1.2945 28.831 2580 41.500 287.5(417) 1.3404 28.831 1962 2.216 4349 1.897 1.17060 33.326 0.1112 5189 79.112 155.7 41.500 24.038 1666 COMBUSTOR 0 12 42.460 233.981 2970 662.0(788) 1.2948 28.831 2575 25.977 1752 310.9(440) 1.3364 28.831 2009 2.086 4192 1.905 1.15964 33.326 0.1122 5088 75.538 152.7 42.460 -COMBUSTOR 0 13 44.085 215.026 2947 655.0(781) 1.2955 28.831 2566 44.085 25,810 1771 316.2(446) 1.3356 28.831 2020 2.039 4118 1.909 1.11938 33.326 0.1162 5034 71.630 151.0 COMBUSTOR 0 14 44.310 213.061 2944 654.1(780) 1.2956 28.831 2565 44.310 25.891 1775 317.1(447) 1.3354 28.831 2022 2.031 4106 1.909 1.11763 33.326 0.1164 5025 71.317 150.8 COMBUSTOR 8 5 0 15 44.800 208,073 2937 652.0(778) 1.2958 28.831 2562 44.800 26.111 1785 319.8(449) 1.3350 28.831 2027 2.011 4077 1.910 1.11296 33.326 0.1169 5005 70.518 150.2 COMBUSTOR 0 16 9 5 208.091 2937 652.0(778) 1.2958 28.831 2562 44.800 44.800 26.113 1785 319.8(449) 1.3350 28.831 2027 2.011 4077 1.910 1.11306 33.326 0.1169 5005 70.524 150.2 COMBUSTOR 0 17 10 5 46.260 188.098 2919 646.7(773) 1.2964 28.831 2555 25.242 1803 324.8(454) 1.3343 28.831 2037 1.970 4013 1.915 1.04830 33.326 0.1241 4959 65.376 148.8 46.260 COMBUSTOR 0 18 11 5 47.310 172.574 2907 643.1(770) 1.2968 28.831 2550 47.310 23.664 1805 325.31 455) 1.3342 28.831 2038 1.957 3988 1.920 0.97564 33.326 0.1334 4939 60.461 148.2

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MOMTM 0 IVAC PHI ETAC A/AC W/A GAMMA VOLWT SONV MACH VEL S 0 19 12 5 COMBUSTOR 172.341 2907 643.0(769) 1.2968 28.831 2550 47.325 23.613 1804 325.2(455) 1.3342 28.831 2037 1.958 3988 1.920 0.97391 33.326 0.1336 4939 60.361 148.2 0 20 13 5 COMBUSTOR 162.896 2899 640.5(767) 1.2970 28.831 2546 48.110 21.761 1787 320.5(450) 1.3349 28.831 2028 1.973 4002 1.923 0.90919 33.326 0.1431 4943 56.541 148.3 48.110 0 21 14 COMBUSTOR 156.337 2892 638.5(765) 1.2972 28.831 2544 48.775 19.353 1749 310.0(439) 1.3366 28.831 2008 2.020 4054 1.925 0.83728 33.326 0.1554 4970 52.756 149.1 48.775 COMBUSTOR 0 22 15 152.648 2887 637.0(764) 1.2974 28.831 2541 49.305 17.489 1711 299.8(429) 1.3382 28.831 1987 2.067 4107 1.926 0.78305 33.326 0.1662 4999 49.983 150.0 49.305 COMBUSTOR 0 23 16 141.781 2875 633.5(760) 1.2978 28.831 2537 50.715 13.945 1639 280.2(410) 1.3417 28.831 1947 2.159 4205 1.930 0.66737 33.326 0.1950 5052 43.607 151.6 50.715 COMBUSTOR 0 24 17 127.585 2861 629.2(756) 1.2982 28.831 2531 52.815 10.662 1564 259.8(389) 1.3456 28.831 1905 2.257 4299 1.936 0.54699 33.326 0.2379 5103 36.545 153.1 52.815 COMBUSTOR 0 25 18 125.683 2858 628.2(755) 1.2983 28.831 2529 53,315 10.034 1543 254.4(384) 1.3467 28.831 1893 2.285 4325 1.936 0.52464 33.326 0.2480 5117 35.263 153.6 53,315 0 26 19 4 COMBUSTOR 122.740 2853 626.9(754) 1.2984 28.831 2528 54.065 9.226 1517 247.3(377) 1.3481 28.831 1878 2.321 4358 1.938 0.49454 33.326 0.2631 5136 33.494 154.1 54.065 COMBUSTOR 0 27 20 119,675 2849 625.7(752) 1.2986 28.831 2526 54.825 8.540 1494 241.3(371) 1.3494 28.831 1865 2.352 4386 1.939 0.46766 33.326 0.2782 5151 31.874 154.6 54.825 COMBUSTOR 0 28 21 115.762 2845 624.3(751) 1.2987 28.831 2524 55.760 7.846 1472 235.3(365) 1.3506 28.831 1851 2.383 4412 1.941 0.43881 33.326 0.2965 5166 30.086 155.0 55.760 COMBUSTOR 0 29 22 4 100.589 2843 623.7(751) 1.2988 28.831 2523 56.250 6.026 1424 222.7(352) 1.3534 28.831 1823 2.457 4479 1.950 0.35369 33.326 0.3679 5208 24.621 156.3 56.250 COMBUSTOR o 30 23 100,481 2842 623.6(750) 1,2988 28.831 2523 56.305 6.005 1423 222.4(352) 1.3535 28.831 1822 2.459 4481 1.950 0.35275 33.326 0.3689 5208 24.563 156.3 56,305 COMBUSTOR 0 31 24 5 100.067 2842 623.4(750) 1.2988 28.831 2523 56.445 5.946 1421 221.8(351) 1.3536 28.831 1821 2.462 4483 1.950 0.35009 33.326 0.3717 5210 24.393 156.3 56.445 COMBUSTOR 0 32 25 101.397 2842 623.4(750) 1.2988 28.831 2523 56.525 6.006 1419 221.4(351) 1.3537 28.831 1820 2.464 4485 1.949 0.35408 33.326 0.3675 5211 24.678 156.4 56.525 COMBUSTOR 0 33 26 101.602 2841 623.0(750) 1.2988 28.831 2522 56.805 5.962 1415 220.3(350) 1.3539 28.831 1818 2.470 4489 1.949 n.35284 33.326 0.3688 5213 24.615 156.4 56.805 COMBUSTOR 0 34 27 101.788 2840 622.8(750) 1.2989 28.831 2522 57.031 5.935 1412 219.6(349) 1.3541 28.831 1816 2.473 4492 1.949 0.35218 33.326 0.3695 5214 24.584 156.5 57,031 COMBUSTOR 0 35 28 101.219 2837 622.0(749) 1.2989 28.831 2521 57.755 5.802 1405 217.6(347) 1.3545 28.831 1811 2.484 4499 1.949 0.34672 33.326 0.3753 5218 24.242 156.6 57.755 0 36 29 COMBUSTOR 58.775 101.390 2834 621.0(748) 1.2991 28.831 2520 5.729 1397 215.7(345) 1.3550 28.831 1807 2.492 4504 1.949 0.34451 33.326 0.3777 5219 24.112 156.6 58.775 COMBUSTOR υ 37 **3**0 5. 102.991 2828 619.3(746) 1.2992 28.831 2517 60.785 UT 5,985 1404 217.5(347) 1.3545 28.831 1811 2.475 4484 1.947 0.35650 33.326 0.3650 5204 24.840 156.1

A/AC MOMTM Q IVAC PHI ETAC W/A GANNA MOLWT SONV MACH VEL S Т LOMBUSTOR ... 0 38 31 5 104.145 2824 618.2(745) 1.2993 28.831 2516 பு 62.205 6.199 1411 219.3(349) 1.3541 28.831 1815 2.461 4468 1.946 n.36616 33.326 0.3553 5192 25.423 155.8 ආ 62.205 COMBUSTOR 0 39 32 4 96,208 2818 616.3(743) 1.2995 28.831 2513 64.669 5.958 1422 222.2(352) 1.3535 28.831 1822 2.437 4441 1.951 0.34708 33.326 0.3749 5172 23.951 155.2 64.669 0 40 33 2 COMBUSTOR 89.121 2817 616.0(743) 1.2996 28.831 2513 65.045 5,551 1424 222.6(352) 1.3534 28.831 1823 2.434 4437 1.956 0.32267 33.326 0.4032 5169 22.247 155.1 65.045 41 34 NOZZLE AE 87.281 89,121 2817 616.0(743) 1,2996 28.831 2513 48.5(178) 1.3931 28.831 1330 4.006 5329 1.956 0.06717 33.326 1.9371 5766 5.562 173.0 87.281 0.498 737 NOZZLE PO 42 35 3 89.121 2817 616.0(743) 1.2996 28.831 2513 87,281 0.489 733 47.7(177) 1.3933 28.831 1327 4.018 5333 1.956 0.06641 33.326 1.9591 5769 5.504 173.1 87.281 FICTIVE COMBUSTR 62 55 0 356.168 2817 616.0(743) 1.2996 28.831 2513 65.045 0.489 494 -10.2(119) 1.3990 28.831 1092 5.125 5598 1.860 0.10335 33.326 1.2589 5956 8.991 178.7 65.045 63 56 n FICTIVE NOZZLE 87,281 81,660 2796 609.8(737) 1,3002 28.831 2504 0.515 756 53.2(183) 1.3923 28.831 1347 3.918 5277 1.960 0.06717 33.326 1.9371 5722 5.509 171.7 87.281

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		1.315E 00	0.000	-5,469E-01			0.000	0.000	2.470E-02	2.687E 00	1.422E-03	0.000	0.000
	1.836E 01	1.315E 00	0.000	-4.378E 01			0.000	0.000	1.634E 02	2.687E 00	1,422E-03	0.000	0.000
	3.070E 01	2.690E 00	0.000	-2.061E 02			0.000	0.000	5.053E 02	5.497E 00	2.910E-03	0.000	0.000
	3.508E 01	4.810E 00	0.000	-4.492E 02			0.000	0.000	6.804E 02	9.829E 00	5.203E-03	0.000	0.000
	3.518F 01	4.820E 00		00 -5.308E 02			0.000	0.000	6.850E 02	9.849E 00	5,213E-03	1.474E 01	7.804E-03
	3.519E 01	4.820E 00		00 -5.309E 02			0.000	0.000	6.852E 02	9.851E 00	5.214E-03	1.465E 01	7.752E-03
	3.555E 01	4.855E 00		00 ~5.407E 02			0.000	0.000	7.214E 02	9.921E 00	5.251E-03	8.809E 00	4.663E+03
	3.585E 01 3.606E 01	4.810E 00 4.780E 00	3 000E	00 -5.595E 02 00 -5.739E 02		02	-1.198E	02 0.000	7.524E 02 7.734E 02	9.830E 00	5.203E-03 5.170E-03	3.883E 00	2.055E-03
	3.648E 01	5.217E 00	5.250F	00 -5,993E 02	-1.212E	02	-1.0000	02 0.000 02 0.000	8.171E 02	9.768E 00 1.066E 01	5.643E+03	6.129E 00 1.073E 01	3.244E-03 5.679E-03
	3.701E 01	5.185E 00	8.091E	00 -6.299E 02	-1.497F	ก็ว	-1.281E		8.732E 02	1.060E 01	5.608E-03	1.653E 01	8.752E-03
	3.731E 01	5.031E 00		00 -6,438E 02					9.0588 02	1.028E 01	5.442E-03	1.987E 01	1.052E-02
	3.803E 01	4.670E 0D		01 -6.606E 02					9.839E 02	9.543E 00	5.051E-03	3.332E 01	1.764E-02
	3.833E 0 <u>1</u>	6.493E 00	1.911E	01 -6.583E 02	-1.908E	02	-1.394E	n2 -5.135E 01	1.018E 03	1.327E 01	7.023E-03	3.906E 01	2.067E-02
	3.875E 01	8.975E 00		01 -6.591E 02					1,065E 03	1.834E 01	9.708E-03	3.818E 01	2.021E-02
	3.880E 01	9.303E 00		01 -6.593E 02					1.071E 03	1.901E 01	1.0068-02	3.806E 01	2.015E-02
	3.901E 01	1.053E 01		01 -6.589E 02					1.094E 03	2.152E 01	1.139E~02	3.900E 01	2.064E-02
	3.931E 01 3.950E 01	1.657E 01 2.024E 01		01 -6.648E 02 01 -6.752E 02					1.130E 03 1.151E 03	3.386E 01 4.136E 01	1.792E+02 2.189E+02	4.038E 01 2.902E 01	2.138E-02 1.536E-02
	3.980E 01	2.091E 01	5.050F	00 -7.051E 02	-2.536F	102	-1.700E	02 -7.703E 01	1.187E 03	4.272E 01	2.261E-02	1.032E 01	5.462E-03
	4.000E 01	2.133E Di	4.934E	00 -7.282E 02	-2.642E	02	-1.765E	02 -8.771E 01	1.209E 03	4.360E 01	2.308E-02	1.008E 01	5.337E-03
	4.040E 01	2.518E 01	4.697E	00 -7.780E 02	-2.874E	02	-1.909E	02 ~9.653E 01	1.256E 03	5.145E 01	2.723E-02	9.599E 00	5.081E-03
	4.041F 01	2.527E 01	4.691E	00 -7.792E 02	-2.880E	02	-1.912E	02 -9. 676E 01	1.257E 03	5.164E 01	2.734E-02	9.586E 00	5.074E-03
	4.130E 01	3.382E 01		00 -9.089E 02					1.363E 03	6.910E 01	3.658E+02	8.508E 00	4.504E-03
	4.136E 01	3.444E 01		00 -9.192E 02					1.370E 03	7.038E 01	3.725E-02	8.429E 00	4.462E=03
	4.150E 01	3.574E 01		00 -9.407E 02					1.387E 03	7.303E 01	3.866E#02	9.376E 00	4.963E-03
	4.246E 01 4.408E 01	1.342E 01		00 -1.021E 03 01 -1.041E 03					1.501E 03 1.698E 03	2.743E 01 3.632E 01	1.452E-02	1.610E 01	8.523E-03 1.455E-02
	4.431E 01	1.838E n1		01 -1.044E 03					1.725E 03	3.755E 01	1.923E-02 1.988E-02	2.749E 01 2.703E 01	1.431E-02
	4.480E 01	1.969E 01		01 -1.054E 03					1.785E 03	4.023E 01	2.129E-02	2.604E 01	1.378E-02
	4.480F 01	1.969E 01		01 -1.054E 03					1.785E 03	4.023E 01	2.130E-02	2.604E 01	1.378E-02
	4.626E 01	1.962E 01		01 -1.071E 03					1.965€ 03	4.009E 01	2.122E-02	2.310E 01	1.222E-02
	4.731E 01	1.957E 01		01 -1.071E 03					2.095E 03	3.999E 01	2.117E-02	2.098E 01	1.110E-02
	4.732E 01	1.946E 01		01 -1.070E 03					2.097E 03	3.977E 01	2.105E-02	2.095E 01	1.109E-02
	4.811E 01 4.877E 01	1.370E 01 1.292E 01		01 -1.053E 03 01 -1.014E 03					2.195E 03 2.278E 03	2.800E 01 2.640E 01	1,482E-02 1,397E-02	2.390E 01	1.265E-02
Ö	4.930E 01	1.389E 01		01 -9.772E 02					2.344E 03	2.839E 01	1.503E-02	2.640E 01 2.839E 01	1.397E-02 1.503E-02
RIG	5.071E 01	5.725E 00	5.725E	00 -9.047E 02	-1.443F	03	-6.084F	02 -8.350F 02	2.522E 03	1.170E 01	6.193E-03	1.170E 01	6.193E-03
٠ <u>٠</u>	5.281E 01	8.100E 00		00 -8.286E 02					2.788E 03	1.655E 01	8.761E-03	1.655E 01	8.761E-03
32	5.331E 01	7.197E 00		00 -8.087E 02					2.852E 03	1.471E 01	7.785E-03	1.471E 01	7.785E-03
₹ 🔂	5.406E 01	6.286E 00		00 -7.826E 02					2.948E 03	1.285E 01	6.799E-03	1.285E 01	6.799E-03
ž A	5.482E 01	5.362E 00		00 -7.600E 02					3.045E 03	1.096E 01	5.800E-03	1.096E 01	5.800E-03
ਪ੍ਰੇਸ਼	5.576E 01 5.625F 01	4.388E 00 3.878E 00	4 + JOSE	00 -7.372E 02	-1.749E	ยอ	-7.387E	02 71.010E 03	3.165E 03	8.968E 00	4.747E-03	8.968E 00	4.747E-03
	5.630E 01	2.100E 00	3.821E	00 -6.925E 02 00 -6.914E 02	-1.772E	03 03	=7.499E	02 -1 0225 03	3.209E 03 3.216E 03	7.925E 00 ' 4.291E 00	4.195E+03 2.271E+03	7.925E 00 7.808E 00	4.195E-03 4.133E-03
AG	5.644E 01	2.100E GO	3.675E	00 -6.890E 02	-1.777E	o3	-7.511E	02 -1.025E 03	3.234E 03	4.291E 00	2,271E-03	7.510E 00	3.975E-03
# E	5.652E 01	3.592E 00	3.592E	00 -6.875E 02	-1.781E	ე3	-7.524E	n2 ~1. 02aE 03	3.245E 03	7.340E 00	3.885E-03	7.340E 00	3.885E-03
3 53	5.680E 01	3.300E 00	3.300E	00 -6.830E 02	-1.791E	03	-7.568E	02 -1.034E 03	3.280E 03	6.744E 00	3.569E-03	6.744E 00	3.569E-03
1 02	5.703F 01	3.350E 00	3,350E	00 -6,798E 02	-1.799E	03	-7.602E	02 -1.039E 03	3.309E 03	6.846E 00	3.624E-03	6.846E 00	3.624E-03
	5.775E 01	3.510E 00	3.510E	00 -6,705E 02	-1.824E	03	-7.705E	02 -1.054E 03	3.402E 03	7.173E 00	3.797E-03	7.173E 00	3.797E-03
	5.877E 01 6.078E 01	4.875E no 2.925E no	2.00KE	00 -6.608E 02	-1.009E	03 03	-/.031E	02 =1.075E 03	3.532E 03	9.962E 00	5.273E-03	9.962E 00	5.273E-03
	6.220F 01	1.744E 00	1.744F	00 -6.599E 02	-1.950E	03	-8.150F	リエ ーエ・エ14E UO no =1.137E n3	3.790E 03 3.972E 03	5.977E 00 3.563E 00	3,164E-03 1,886E-03	5.977E 00 3.563E 00	3.164E-03
	6.467E 01	4.169E no	4.169F	00 -6.599E 02	-2.017F	n3	~8.381F	02 -1.17gF 03	4.289E 03	8.519E 00	4.509E-03	8.519E 00	1.886E-03 4.509E-03
ļ	6.504E 01	5.587E 00	4.539E	00 -6. 599E 02	2.027E	U3	-8.419E	02 -1.185E 03	4.337E 03	1.142E 01	6.044E-03	9.275E 00	4.909E-03
57	6.508E 01	5.587E 00	4.578E	00 -6.599E 02	-2.028E	03	-8.423E	n2 -1.186E 03	4.342E 03	1.142E 01	6.044E-03	9.356E 00	4.952E-03
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XABS	P-IB	P=0B	PDA	QOX,	Q-18	0-0B	CAWALL	P-IB/PS0	P-IB/PTO _*	P-08/PSo	P=08/PT0
6.528E 01	5.226E 00	4.775E 00	-6.599E 02	2 -2.0345	03 - 8.442E 0	2 -1.189E 03	4.368E 03	1.068E 01	5.653E-03	9.758E 00	5.165E-03
6.694E 01	2.230E 00	4.420E 00	-6.125E 02	2.074E	03 - 8.580E n	2 ~1.216E 03	4.583E 03	4.557E 00	2.412E-03	9.032E 00	4.781E-03
6.761E 01	2.183E 00					2 -1.225E 03	4.665E 03	4.462E 00	2.362E-03	1.145E 01	6.060E-03
6.838E 01	2.130E 00	4.066E 00	~4.480E 02	2 -2.104E	03 -8.664E 0	2 -1.237E 03	4.760E 03	4.353E 00	2.304E-03	8.310E 00	4.398E-03
6.910E 01	1.838E 00	2.630E 00	-3.807E 02	2.119E	0 3 - 8.697E ი	2 -1.250E 03	4.848E 03	3.755E 00	1.988E-03	5.374E 00	2.845E-03
6.971E 01	1.590E 00	2.419E 00	-3.354E 02	2.133E	03 -8. 721E 0	2 -1.261E 03	4.922E 03	3.249E 00	1.720E-03	4.943E 00	2.616E-03
7.066E 01	1.390E 00	2.090E 00	-2.770E 02	2.154E	03 –8.7 55E ი	2 -1.278E 03	5.036E 03	2.841E 00	1.504E-03	4.271E 00	2.261E-03
7.109E 01	1.300E 00	1.991E 00	-2.535E 02	2.163E	03 -8. 768E ი	2 -1.286E 03	5.088E 03	2.657E 00	1.406E-03	4.069E 00	2.154E-03
7.262E 01	9.676E-01	1.640E 00	-1.849E 02	2 -2.187E	03 -8. 809E 0	2 -1.306E 03	5.273E 03	1.977E 00	1.047E-03	3.351E 00	1.774E-03
7.277E 01	9.350E-01	1.425E 00	-1.797E 02	2.189E	03 - 8.812E ი	2 -1.308E 03	5.290E 03	1.911E 00	1.011E-03	2.912E 00	1.541F-03
7.352E 01	8+034E=01	3.500E-01	-1.498E 02	2 ~2.199E	03 -8. 828E 0	2 -1.316E 03	5.374E 03	1.642E 00	8.690E-04	7.152E-01	3.786E-04
7.353E 01	8.027E-01	3.443E-01	-1.491E 02	2.199E	იპ – 8.828E ი	2 -1.317E 03	5.375E 03	1.640E 00	8.682E-04	7.035E-01	3.724E-04
7.485E 01	5.700E-01	0.000				2 -1.335E 03	5.427E 03	1.165E 00	6.165E⊶n4	0.000	0.000
7.770E 01	2.900E-01	0.000	-1.174E 02	2 -2.224E	03 −8.889E ∩	2 -1.335E 03	5.525E 03	5.926E-01	3.137E-04	0.000	0.000
8.160E 01	5.150E-01	0.000	-1.002E 02	2 -2.227	03 -8.921E 0	2 -1.335E 03	5.630E 03	1.052E 00	5.571E-04	0.000	0.000
8.441E 01	5.950E-01	0.000	-8.785E 01	-2.229E	03 ⊸8.945⊑ ე	2 -1.335E 03	5.684E 03	1.216E 00	6.436E-04	0.000	0.000
8.727F 01	7.350E-01	0.880	-7.180E 01	-2.234E	0 3 -8.987E ი	2 -1.335E 03	5.707E 03	1.502E 00	7.950E-04	0.000	0.000
8.728E 01	7.353E-01	0.000	-7.180E 01	-2.234E	03 -8.987E ი	2 -1.335E 03	5.707E 03	1.503E 00	7.953E-04	0.000	0.000

X	ΔO	RAG	CDRAG		CF		HC	
4.040EEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEE	0112.9490.0466990.6411293.368559959838.6442.001001111111111111111111111111111111	021 021 161 161 161 161 161 161 161 1	1.35598EEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEE	00000000000000000000000000000000000000	2.158i 2.158i 2.128ii 2.28j 2.28j 2.398i 2.373i 2.375i 2.445i 2.450i 2.4	E-03 E-03	5.2844 5.2879 5.7911 5.7912 5.7912 5.7912 5.7912 5.8359 5.8359 5.8359 6.	C-022 C-
6.508E 6.528E 6.694E 6.691E 6.838E 6.910F 7.066E 7.109E 7.277E 7.352E 7.353F 7.485E 7.770E 8.160E 8.441E 8.727E	01 2.4 01 1.2 001 9.0 01 3.1 001 2.7 001 2.8 001 1.3 001 1.8 001 1.	80E-01 11E 00 01E 00 41E 00 61E 00 74E 00 72E 00 73E 00 22E 00 380E-01 39E 00 354E-01 21E-01 21E-01 30E-01	4.493E 4.505E 4.595E 4.627E	02 02 02 02	2.2268 2.2228 2.1428 2.1688	-03 -03 -03 -03 -03 -03 -03 -03 -03 -03	1.4136 1.3958 1.0256 1.1526	-02 -02 -03 -03 -03 -03 -03 -03 -03 -03 -03 -03

RAMJET PERFORMANCE

_		RAMULI PERFO	RMANCE			
<u>5</u>	ENGINE PERFORMANCE	•		IN FT		
	MEASURED THRUST			CCIENT	0.9838 0.0006 0.1636	
	NET THRUST	CLRF) (LBF) (LBF) (LBF-SEC/LBM)	TOTAL PRESSURE RECOVIOTAL PRESSURE RECOVINLET PROCESS EFFICINLET PROCESS EFFICINLETIC ENERGY EFFICINLETIC ENERGY EFFICINTHALPY AT PO - SUBSTITUTE OF SUBSTIT	/ERY - SUBSONIC IENCY - SUBSONIC IENCY - SUBSONIC IENCY - SUBSONIC IENCY - SUBSONIC IENCY - SUBSONIC PERSONIC	0.1659 0.8903 0.9035 0.9461 0.8967	(RTU/LBM) (BTU/LBM)
	MOMENTUM AND FORCES			COMBUSTOR		
	INLET FRICTION DRAG	(LBF) (LBF) (LBF) (LBF) (LBF) (LBF)	FUEL-AIR RATIOEQUIVALENCE RATIO COMBUSTOR EFFICIENCY TOTAL PRESSURE RATIC COMBUSTOR EFFECTIVEN INJECTOR DISCHARGE		0.000 0.000 0.2502	
	NOZZLE NOMENTUM CHANGE	(LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF)	VACUUM STREAM THRUST NOZZLE COEFFICIENT - PROCESS EFFICIENCY KINETIC ENERGY EFFIC	- CT	0.9498 0.9834	
	STATIONS		FUEL	_ INJECTORS		
	SPIKE TRANSLATION	34 (IN) 19 (IN) 10 (IN) 39 (IN) 29 (IN) 11 (IN) 15 (IN) 15 (IN)	INJECTORS S 1A 1B 1C 2A 2C 3A 3B 4	5TATION 40.400 41.290 44.300 48.765 46.250 54.055 56.240 44.790	VALVE	

t = 192.45 sec.

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SUMMARY REPORT

. •	P	ī	u		544244		001.11								_			
- 1	WIND TUNNEL	'i	, H		GAMMA	HOLVY	SUNV	мдСм	AEF	5	W/A	۴	A/AC	ין אטי	G	IVAC	PHI	ETAC
	U UUV GOF AND		0 5															
	0.000 925.749	2449	010-6	706)	1.2939	26.832	2586											
	0.000 p.486	406	=31,5(95)	1,3988	28,831	990	5,988	5927	1.813	0,13243	33.401	0.9847	6276	12.199	187.9		
	SLIVE IIL NO	~	0 4						*									
	0.600 22.487	2998	670.61	7061	1_2938	26.431	2546											
	0.000 20.294	2929	049.61	7761	1.2960	28.631	2550	0.000	1020	360	0.13243	77 // 11	0 0447	- 183	2 104			
i	MIND TUNNEL	3	0 0	, , , ,	1,2700	F01031	4337	0,400	1054	£ . UO7	0 * 1 3 5 4 3	22.401	0,404/	6102	2.100	105.1		
				*** / 4														
	.	2770	010.00	790)	1.2939	58.835	2586											
		403		97)	1,3987	28,831	986	6,014	5931	1.813	0.12999	32.784	0.9847	6163	11.980	188.0		
	SPIKE TIP NS	4	v v		-											•		
	0.600 22.487	2998	670,6(796)	1.2938	28,831	2586											
	U + Q U Q C U + 5 0 5	2932	650,5(777)	1.2959	26.831	2560	0.391	1002	2.069	0.12999	32.784	0.9847	6163	2.024	188.D		
,	INLET THROAT	5	0 4	, •				. ,	, , , ,	_,	• • • • • • • • • • • • • • • • • • • •	24,10	0 1 1 2	4,02		10040		
	40.400 352.741	2962	659.6(7461	1.2951	24 41	2572											
	40.400 20.056	1472	215.4	1453	1 3504	28 811	4063	2 000	* / * *	4 07.	1.17111	** "**						
	INLET UPNESK	6	0 3	302)	1.3300	501037	1025	8 400	4007	1.070	1+1/111	25,401	0.1114	2322	83.855	160.3		
				W											•			
	10 40 40 47 247	6706	659.6(/80)	1,4951	20,631	2575											
	40,400 17,217	1413	220.20	350)	1,3539	28,831	1617	2,580	4689	1.876	1.06464	33,401	0.1225	5408	77.584	161.9		
	tiare: Diagraph	- 1	v a												_	•		
	40.400 153.090	2962	659.71	7g6)	1.2951	.28.831	2572											
	*V**UU 151*545	2860	628.8(756)	1.2982	28.831	2530	0.491	1243	1.934	1.06464	33.401	0.1225	5408	20.571	161.0		
ε	COMBUSTOR 0	8	1 21			,,			10.0			22144.	041000	3400	201311	10144		
L	0.410 295.213	2916	659.81	8461	1 2074	27 681	2612											
Ĺ	0.410 15.304	1408	214.67	3.31	7555	27 580	1855	2 E##	# 3 A	1 054	1.17514	77 574						
	DYBUSTOR O	9	2 21	2021	1 4 3 2 3 3	E1.300	1000	61344	4/20	1 4 420	1=1/514	33,540	0.1114	5354	86.145	159.7	0.12	0.07
			661 21	0 - // 4	. 7040	24												
		5044	001.2(0 1 4 3	1,3014	20,404	5030											
		1301	200 4(424)	1,5483	26.484	1991	2.226	4433	2.031	1.18137	33,631	0.1111	5197	81.395	154.5	0.24	0.04
	tour and i Section	ŤΛ	3 C1															
	11.310 234.919	2804	661.21	802)	1,3033	26.442	2621											
	11.210 14.858	1525	268.9(412)	1.3508	26.442	1968	2.251	4430	2.024	1.18110	33.631	0.1112	5195	81.317	154.5	0.20	0 - 0 1
(COMBUSTOR 0	11	4 21	•			•	- • • •									0 8 6 4	0.01
4	114375 233.431	2797	661.01	800)	1.3036	26 416	2619											
- 4	11.375 20.155		272.21	4131	1.3506	26.416	1974	2.217	0.010	2 624	1.18289	22 421	0 4440	C 4 6 Y	01 071	450. 4		
		12	5 21	- 100	11000	841434	4 * * *		4410	E VE4	1110207	33.031	0 4 3 1 1 0	2102	01.010	124 • 1	0.24	0.00
7	41.500 228.059	2706	660.61	7.0.	. 7077	26 075	14.40											
	11.500 21.300	1546	251 71	1971	1.3037	20.435	2010											
7	41.500 . 21.304 Combustór o	1300	501.3(4561	1 - 2441	20.435	1 49 4	2.190	4357	2.025	1.18317	33,631	0.1110	5159	80.105	153.4	0.24	0.00
•		+ 3	0 61															-
	*C. 44	4103	656.7(795)	1.3040	26,435	2613									_		
	12.460 17.418	1551	278.7	420)	1.3495	26.434	1984	2,192	4349	2.039	1.17155	33.631	0.1121	5046	79.188	150.1	0.24	0 - 00
Ç	50.000 told 0	14	/ 3									• . •	4.5-5					
Ł	14.095 163.202	2873	648.0(8521	1.2996	26.558	2644											
4	44075 55.224	1990	371.5	5/18)	1.3294	26.558	2225	1.471	3710	J 057	1.13128	77 471	A 1141	0070	4E 70 1			
(COMBUSTOR 0	15	8 3						2117	C+031	**12150	33,031	0.1161	4734	034302	146.7	0.24	0.10
	14,310 156,220	2913	646.61	A+/13	1 2077	36 605	2450											
	14.310 37.414	2071	785 64	2-71	1 776 0	20,000	2030		.									
	Challeton of		308431	2723	1.3620	20.005	4400	1.004	3635	2.064	1.12931	33,631	0.1163	4914	65.795	146.1	0.24	0.14
-	00.003100	10	7 3															
	4.800 143.918			855)	1,2944	26,690	2681			*								
	44.800 42.400	2438	406.9((523	1,3190	26,690	2345	1.466	3437	2.075	1.12491	33.631	0.1167	4861	60.092	144.5	ور د	0 21
C	A 100 A 100 A	• 7	10 6					-					1	,		. ~ ~		- 1 - 1
4	4,810 143,832	2981	645.01	855)	1.2944	26.689	2681											
	4.810 42.413	2237	407-11	6221	1.3190	26.496	2345	1.065	2424	2.075	1.12492	77 /71	0 4424	****	10 010			
	OFBUSTOR 0	1 A	11 11	- 6 1			5273	.	J470	E (0 / 2	1016475	150,021	0 * 1 1 0 /	4854	00.005	144.5	0.24	0,21
	16,250 126,244			A-4.	1 7004	24 147	1676											
		コルフル	045 e41	420)	1.3740	54.503	\$0/Q											
•		2014	H4140(,	(c2o,	1,3500	c4.203	6578	1,359	5183	5.500	1.06860	33,892	0.1238	4759	52.852	140.4	0.51	0.04
															•		•	-

HEADING =	0063	អដ្ឋប្រជួន	= 71	TIME	= 192.4	54 MAC	н 6.	Q PI:	= 926	.749	TT 8 299	e.3						•
	P	T	н		GAMMA	MOLWI	SONV	MACH	VEL	s	W/A	H	AZAC	MIMUM	c c	IVAC	PHI	E T
COMBUSTOR	0	19	12 2										,		-			-
			643.4	(826)	1.3096	24.264	2678											
46.260									3181	2.200	1.05/94	43.897	0.1239	4759	52.800	140.4	6.51	0 - 0
COMBUSTOR			13 4		.,,,,,							23.4.1	. 1 7 7 7 7	7,57	25.000	1-01-	V # J 1	1. 0
			634.5		1 1000	24.422	2772											
7.310	45.785	2261	00000	4 6031	1 2316	24 422	21142	1 757	2000	2 220	A 00740	77 003	0 4 4 7 7		47 470			
	434193			(884)	1.3510	24.466	2406	1.591	3075	2.240	0.99368	22,046	0.1225	4022	47./89	142.5	0 . 51	0 . 1
OMEUSTOR		15																
17.335	116:091	2010	634.2	(872)	1.3028	24,425	2733											
47.335	45.823	2257	443.1	(6 83)	1.3215	24.425	5464	1,255	3093	2.221	0.99257	33,892	0.1333	4823	47.709	142.3	0.51	0.1
CUMBUSTOR	0	22	15 4															•
48,110			0.850		1.2976	24.550	2773											
48.110									3164	2.214	0.92591	11.802	0.1/120	лотъ	45.590	4.04	A E 1	Α.
COMBUSTOR		23		() [()	1.51,0	644550	2000	19500	3100	E 0 E 3 M	0 4 7 5 3 7 1	33,075	041454	4713	436370	145.0	A . 21	0.
48.775	104.015	2/31	633.0	(4193	1,3078	22,445	2810											
48.775	34*600	2164	425.0	(706)	1,3271	22,492	2519	1.261	3556	2.367	0.85951	34.167	0.1552	5000	43.090	146.3	0.80	0,
COMBUSTOR			17 2															
18.785	105,925	2733	632,9	(914)	1.3077	22.494	2810											
48.785	39.568	2165	424.7	£ 7071	1 - 3270	22.494	2520	1.281	3227	2.847	0.85839	34.167	0-1554	5002	43.052	1 // 4 . //	n an	Λ
COMBUSTOR		25	18 //			14 14 14 14 14 14 14 14 14 14 14 14 14 1	~ ~ ~ ·		- L .	F 9 4 4 1	V • O > O > O	341101	0 1 1 2 2 4	2005	424015	14094	4 8 0 0	۷.
19.315				4 0071	4 700/	33 407	2000											
	37.5/4	2047	629,2	(753)	1.3050	22,003	2022	4 -00										
49.315	3/+340	4621	411.7	(/30)	1.3223	55.003	2205	1.288	3599	2.382	0.80280	34.167	0.1662	5101	41,157	149.3	0.80	0,
COMBUSTOR		26																
50.729	89,115	3141	620.3	(1058)	1.2885	22.895	2965											
10.725	33.437	2506	380.9	(8535	1.3097	22.896	2670	1-297	3461	2.417	0.68420	34.167	0.1950	5345	36,803	156-0	0.80	Α.
COMBUSTOR	0	27	20 //	6 7				****			*******	244,01	0 3 2 7 2 0	4275	20,000	12014	0.00	V .
2.825					. 5000	77 065	7041											
	22.410	2672	609.0	(1115)	1,2000	23.000	2010											
2.825	631305	2400	244.4	(602)	1-3088	23.070	2637	1,503	3964	2.433	0.56079	34.167	0.2379	5633	34.547	164.9	0.80	0,
COMBUSTOR	Ç	85																
3,325	80.431	3376	606.6	(1142)	1.2767	23,152	3042											
33.325	22.907	2543	289.2	8325	1.3050	23.155	2670	1.493	1985	2.442	0.53787	34.167	0.2480	5487	33,313	144.5	0 8 0	Λ
COMBUSTOR	0	20	22 4					• • • • •	_,,,,	# 4 P	4945101	244.01	400	500,	225213	10035	4600	ν.
4.075					1 2770	37 767	7050											
	70,301	2730	603.2	(1,01)	100/37	53.613	2024											
4.075	E1+002	6222	200,4	(632)	1.3030	C3.C1/	50/1	1.531	4040	2.448	0.50701	34.167	0.2631	5764	32.224	168,7	0.80	0.
ROIBURNO	0	30	23 3															
64.835	76.887	3460	599.9	(1172)	1.2723	23.251	3068											
4.835	19.237	2537	246.9	(828)	1.3039	23.256	2660	1.580	4202	2.451	0.47946	34.167	0.2782	5834	31.313	170-7	0.86	۸
COMBUSTOR	0	31	24 4		,,,,,,				- 10 7 Ng		• • • • • • • • • • • • • • • • • • • •	.,,		2024			0,00	v #
5.760				/ 1 1 4 5	1 3461	21 200	1 A a A											
	13 5030	2500	596.1	111901	1,4701	23.677	2000											
55.760	11.6203	6767	254631	(024)	1.3033	C3+302	2025	1.060	4315	2.455	0.45017	34 0 1 0 7	0.2963	5909	30.176	172.9	0.80	0.
OMBUSTOR			25 5															
56.260	58.616	3893	594,3	(1330)	1.2473	23,705	3191											
005.00	16.566	2989	231.2	9963	1.2822	23.727	2834	1.504	4262	2.499	0.36267	34.167	0.3678	6087	24.022	178-1	0.80	۸.
TOMBUSTOR		33	26 5	,			M - M -				4444201	5-4107	0 2 3 0 7 0	0001	241015	4,011	0100	
6.315			594.0		1 3401	27 174	7000											
	10,303	2422	374401	111401	1.2001	60,001	3007	4 6 "		<u> </u>								
6.315	12,401	2413	10040	(181)	1.5071	23.544	5245	1,784	4624	2.465	0.36152	34.167	0.3690	6091	25.901	170.3	0.80	0.
OKHUSTOR		34																
56,455	68,454	3538	593,5	(1200)	1.2679	23.543	3091											
io,45g	12.356	2412	163.8	t 7air	1.3070	23.350	2591	1.790	4637	2.465	0,39892	34-167	0.3717	6100	25.864	174.5	0.80	n.
ADTEUBNO:	6	35	28 6	,						D # 11 W B		# - p . C .	V # 37 4 1	5.00	F 2 4 0 0 4	71000	V 8 G O	0.8
6.535					4 3/107	3 * 4 ac	7101											
	14 000	2016	593.2	(1254)	10001	E30005	2100								_			
5.535	10.020	4432	214.0	(466)	1.2843	23.705	5915	1,539	4327	2.496	0.36294	34.167	0.3675	6106	24.407	178.7	0,80	0.
COMBUSTUR	0	36	29 3														-	-
6.815	60.839	3851	592.21	(1314)	1.2500	23.066	3180											
56.815	15.525	2885	207.2	9/185	1.2864	23.484	2701	1.571	4384	2.002	0.36174	34.167	0 1608	4120	34.483	170 2	A 4A	^
OFBUSTOR	7 7 7 7 7	37	30 3				in 1 7 €		-300	6 8 Y7 J	0 # 30 F L d	348101	A # 1000	0124	24.65/	114.5	V.00	0.
57.041	06.614	2014	591.4	(1300)	1 6 2 5 3	25.029	3170											
57.041	14.915	5915	195.6	(158)	1.2894	25.646	2761	1.615	4450	2.489	0.36119	34.167	0,3693	0137	24.980	179.6	0.80	0.4
											-			•		_ ,		

GARMA MOLHT SONV MACH VEL S ~/4 N A/AC -MUM1M R IVAC PHI ETAC U 38 31 4 - COMBUSTOR an 57.765 65.609 3679 589.0(1251) 1.2601 23.498 3132 F 57.765 12.960 2571 159.6(836) 1.2995 23.509 2658 1.744 4635 2.475 0.35546 34.167 0.3753 6168 25.605 180.5 0.80 0.45 COMBUSTOR 0 39 32 7 58.785 120.541 2985 586.1(1001) 1.2947 22.833 2901 58./85 6.787 1477 45.2(464) 1.3523 22.833 2086 2.494 5202 2.374 0.35320 34.167 0.3777 6181 28.555 180.9 0.80 0.22 COMBUSTOR 0 40 33 6 60.795 55,800 4265 581,0(1465) 1,2219 24,139 3276 60.795 20,650 3529 262.8(1180) 1,2550 24,195 3017 1,323 3990 2,517 0,36549 34,167 0,3650 6167 22,662 180,5 0,80 0,67 COMBUSTOR 0 41 34 62,215 58,384 4167 577,2(1429) 1,2291 24,041 3254 62.215 19.800 3370 241.2(1122) 1.2633 24.066 2965 1.383 4100 2.509 0.37539 34.167 0.3555 6156 23.917 180.2 0.80 0.63 COMBUSTOR 0 42 35 4 64.679 52.447 4361 569.8(1500) 1.2139 24.275 3293 64.679 22,700 3742 292,6(1259) 1,2431 24,543 3082 1,208 3724 2,524 0,35583 34,167 0,3749 6134 20,594 179,5 0,80 0,72 COMBUSTOR 0 43 36 65.055 47.956 4452 568.6(1534) 1.2057 24.380 3308 65.055 23.834 3941 329.9(1333) 1.2307 24.459 3140 1.101 3456 2.535 0.33080 34.167 0.4032 6132 17.766 179.5 0.80 0.76 COMBUSTOR REGEN 44 37 21 65.055 47.956 4580 637.8(1585) 1.1975 24.339 3347 65.055 24.627 4104 404.8(1397) 1.2208 24.436 3193 1.069 3414 2.550 0.33080 34.167 0.4032 6190 1/.552 181.2 0.80 0.76 NOZZLE AE 45 38 87.291 47.956 4452 568.6(1515) 1.2057 24.380 3308 1.365 2146 -362.9(668) 1.3032 24.502 2382 2.866 6627 2.535 0.06886 34.167 1.9371 7927 7.307 232.0 0.80 0.76 87.201 NUZZLE PO 46 39 87.291 47.956 4452 568.6(1515) 1.2057 24.380 3308 87.291 0.486 1677 -522.2(509) 1.3241 24.502 2123 3.480 7388 2.535 0.03397 34.167 3.9264 8335 3.901 243.9 0.80 0.76 NOZZLE AE REGEN 47 40 87.291 47,956 4580 637,8(1585) 1,1975 24,339 3347 87.291 1.416 2260 -322.6(709) 1.2987 24,502 2441 2.840 6932 2.550 0.06886 34.167 1.9371 8064 7.419 236.0 0.80 0.76 NOZZLE PO REGEN 48 41 5 87.291 47.956 4580 637.8(1585) 1.1975 24.339 3347 0.486 1756 -495.9(536) 1.3201 24.502 2169 3.473 7532 2.550 0.03308 34.167 4.0326 8501 3.872 248.8 0.80 0.76 67.291 FICTIVE COMBUSTR 168 61 0 65.055 352,741 5077 568,6(1766) 1,1882 25,091 3457 65.055 0.486 1278 =936.3(372) 1.3396 25.340 1833 4.734 8678 2.384 0.05416 34.167 2.4632 9522 7.303 278.7 0.80 1.00 FICTIVE NOZZLE 69 62 0 87.291 30.198 4400 550.1(1513) 1.2031 24.373 3286 87.291 1.715 2484 =242.8(788) 1.2904 24.502 2551 2.470 6299 2.568 0.06886 34.167 1.9371 7539 6.741 220.7 0.80 0.76

XABS	P=18	P=08	AGS	aox	G =1B		0=0b	CAWALL	P=I8/PS0	P=18/PT0	P=08/P80	P#08/P10
5.981E=								2.4708-02	2.714E 00			
		0.000	-5,480E-01		0.000		0.000			1.424E=03	0.000	0.000
1.636E		0.000	=4.395E U1	0.000	0.000		0.000	1.0346 02	2,714E 00	1.424E+03	0.000	0.000
3.070E		0.000	-2.075E UZ		0.000		0.000	5.053E 02	5.581E 00	2.9306=03	0.000	0.000
3.508E		0.000	-4.517E 02		0.000		0.000	6.804E 02	9.910E 00	5.202E=03	0.000	0.000
3,519E			0 - 5.339E 02		0.000		0,000	6,854E 02	9 9545 00	5.2256-03	1-475E 01	7.740E=03
5.520E		7-126E 0	0 45.340E 02	0.000	0.000		u.000	6.857E U2	9,457E 00	5.726£#03	1.465E 01	7.690E+03
3.555E		4.3848 0	0 -5.438£ 02	0.000	0.000		0.000	7,2098 02	1.009E 01	5.248L=U3	4.612E 00	4.730E=U3
3.586E	01 4.867E 00	1.425E 0	0 =5.633t 02	-1.639E	02 #1.839E	υZ	0.000	7.529E 02	1,001E 01	5.251E=U3	3.457E UO	2.077E=U3
3.606E	01 4,840E 00	2.969E 1	0 -5.773E 02	-1.860E	02 -1.860E	0.2	0.000	7.729E 02	9.950E 00	5.2231-03	6.104E 00	3.204E=03
3.648E	01 5.224E 00	5.217E 0	6.030E 02	#1.905E	02 -1.905E	02	0.000	8.164E 02	1.0748 01	5,637E#U3	1.072E 01	5.629E=03
3.701E	01 5.210E 00	8.053E 0	0 =6.338E 02	-2.181E	02 -1.965E	02 •	2.154E 01	8.726E 02	1.071E 01	5.622E=03	1.655E 01	8,689E=03
3.732E	01 5.046E 00		0 -6.483E 02						1.037E 01	5.445E-03	2.002E 01	1.051E=02
3.8032	01 4.680E 00		1 -6.6528 02						9.621E 00	5.050£=03	3.340E 01	1.753E=02
3.834E			6.634E 02						1.381E 01	7.251E=03	3.937E 01	2.0666=92
3.875E			-6.659E 02						1.921E 01	1.008E-02	3-813E 01	2.0016-02
3.881E			#6.665E 02						2.008E 01	1.054E=02	3.793E 01	1.991E-02
	01, 1 103E 01		-6.673E 02						2.268E 01	1.190E=02	3.905E 01	2.050E=02
3.932E			-6.749E 02						3.525E 01	1.850E=02	4.086E 01	2.145t=02
3.950E			₩6.850E 02						4.225E 01	2.217E=02	3.006E 01	1.578E=02
3.981E			-7.155E 02						4.339E 01	2.277E+02	1.064E 01	5.5848-03
4.000E			7.378E 02						4.406E 01	2.313E=02	1 039E 01	5.453E=03
4.040E			-7.88ZE 02						5.287E 01	2.7756-02		5.169E=03
4.0416			7.894E 02								9.846E 00	5.162E=03
4.130E			#9.242E 02						5.309E 01	2.7868.02	9.835E 00	
									7.3668 01	3.815E=02	8 633E 00	4.551E=03
4.131E 4.137E			-9.258E 02						7.290E 01	3.827E=02	8,619E 00	4.524E=03
	,		9.365E 02						7,434E 01	3.9026=02	8.532E 00	4,478E=03
4.150E			69.575E 02						7.709E 01	4.046E#02	1.050E 01	5.511E-03
4.246E			=1.049E 03						4.602E 01	2.416E=02	2.559E 01	1,343E=02
4.409E			-1.126E 03						9.353E 01	4.9095.02	5.130E 01	2.6934.02
4 - 431E			1.143E 03						9,978E 01	5.237E=02	5.405E 01	2.837E-02
4.480E			-1.186E 03						1.140E 02	5.985E-02	6.031E 01	3.166E=02
4.481E			1 .187E 03						1.139E 02	5.9016-02	6.044E 01	3.172E=02
4.625E			-1.250E 03						1.035E 02	5.434E-02	7.685E 01	4.139E+02
4.626E			1 -1.550E 03						1.032E 05	5-4306-02	7.898E 01	4 . 1 45E = 02
4.7318			1 mi.141E 03						9.585E 01	5,031E=02	9.240E 01	4.850E=02
4 a 7 3 3 E			1 -1.139E 03						9,569E 01	5.022E-02	9.272E 01	4-866E=02
4.811E			1 -1.035t 03						9.056E 01	4. 7 53E=02	8.664E 01	4,547E=02
4.877E			1 -9.067E 02						8,142E 01	4.274E=02	8.142E 01	4.274E=02
4.878E			1 =9.046E 02						8.134E 01	4.2/0F=05	8.134E 01	4.270E=02
4.931E			-7.981E 02						7.719E 01	4.051E=02	7.719E 01	4.0516-92
5.072E			45.357€ 02						6.874E 01	3.608E#02	6.874E 01	3.608E=02
5.282E			2.230E 02						4.803E 01	2.521E=02	4.803E 01	2,521E=02
5.332E			1 -1.62BE 02						4.709E 01	2.472E=02	4.709E 01	2.472E=02
5.407E	01 5*108E 01	2.108E 0	-7.772E 01	#3,158E ()3 #1#435E	03 •	•1.723E 03	2,948E 03	4.335E 01	2.2/5E=02	4.335E 01	2.275E=02
5.483E		1.924E 0	4.353E=01	*3.271E	3 -1.482E	03 =	1.789E 03	3.046E 03	3,955E 01	2.076E=02	3.955E 01	2.076E=02
5,576E		1.750E 0:	8,565E 01	=3.349E)3 +1.535E	03 =	.1.865E 03	3.164E U3	3.598E 01	1.889E=02	3.598E 01	1.889E#92
5.626E		1.657E 0;	5.998E 05	03.464E (3 -1.560E	03 e	1.904E 05	3,209E 03	3,406E 01	1.7876-02	3.406E 01	1.787E=02
5.631E		1.646E 0:	2.715E 02	-3.47UE (3 -1.563E	03 =	1.908E 03	3,216E 03	1.750E 01	9.185E=03	3.384E 01	1.7766.02
5.645E		1.620E 0		03.45BE)3 =1.569E	03 •	1.919E 03	3,234E 03	1.750E 01	9.1856.03	3.330E 01	1.7486=02
5,6538	01 1.605E 01	1.605E 0	2,8865 02		3 -1-573E				3,300E 01	1.7326-02	3.300E 01	1.732E=02
5.6818		1.552E 0		=3.531E (3 -1.585E	03 -	1.946E 03		3.192E 01	1.675E+02	3.192E 01	1.675E-02
5.704E	01 1.491E 01	1.491E 0	3,241E 92	♥3.558E	3 -1.5956	03 •	1.963E 03		3,066E 01	1.609E=02	3.066E 01	1.609E=02
5.776E	01 1.295E Q1	1.296E 0			3 +1.623E				2.664E 01	1.3981=02	2.664E 01	1.3986=02
F 07.5		6.787E 0			3 -1.658E				1.395E 01	7.324E=03	1.395E 01	7.324E=03
5.078€ 5.079€		2.065E -0			3 -1.713E				4.245E 01	5.558F=05	4.245£ 01	2.228E-02
C) 6.221E	* * * * * * * * * * * * * * * * * * * *	1.980F 0			3 =1.749E				4.070E 01	2.136E=02	4.070E 01	2.136E=V2
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ABS P=18 P=08 PPA GOX G=18 G=06	CANALL	P=16/P80	F-18/P10	P=08/P80	D-08 (DTA
6.866E 01 3 370E 01 3 37.8 0. W 048E WM		- • ·			P#OB/PTO
The state of the s	4.2896 03	4,667E 01	2.4496-02	4.617E 01	2.4495*02
TO THE TO THE TO THE TO THE TOTAL THE THE THE THE THE THE THE THE THE THE	4.357E U3	5.042k 01	2.646E=02	4.758E 01	2.497E=02
- 1 TTTT TE TATE TO THE TO THE TOTAL OF THE TATE OF THE TOTAL TO THE TOTAL TOT	4.342E 03	5.042E 01	2.646E=02	4./67E 01	2.502E=02
- 0.7696 01	4.368E 03	4.777E 01	2.507E=02	4.816E 01	2.528E=02
6.69%E 01 1.254E 01 1.195% 01 5.856% 02 04.521% 03 01.893% 03 02.628% 03	4.583E 03	2.578E 01			
			1.3536-02	2.457E 01	1.2896=02
TO WALL AND THE TAXABLE OF TAXABLE OF TAXABLE OF TAXABLE OF	4.665E 03	1.887E 01	9.906E=03	2,328E 01	1,222E,02
- 1 Miles 12 Tailing at the section of the section of the section of the section of	4.760E 03	1.094E 01	5.740E=03	1.770E 01	9.293Lp03
6-911E 01 4-218E 00 6-075E 00 1-201E 03 -4-675E 03 -1-933E 03 -2-742E 03	4.848€ 03	8.672E 00	4.552E+03	1.249E 01	6.555E=03
- 9.47/20 01 3.285E 00 5.000E 00 1.300E 03 44.714E 03 41.940E 03 42.774E 03	4.922E 03	6.753E 00	3.545t=03	1.028E 01	5.3956-03
7.0678 01 2.3288 00 3.3258 00 1.4098 03 -4.7688 03 -1.9498 03 -2.8208 03	5.036E 03	4.786E 00	2.512E-03		
7.110E 01 1.895E 00 3.090E 00 1.446E 03 -4.790E 03 -1.952E 03 -2.838E 03				6.836E 00	3,588E-03
	5.08BE 03	3.896E 00	2.045E=03	6,353E 00	3.334E-03
FEET VI 1-11VE I' ALLIAC IO SANUE AN MARGRAD ON AVAIDE ON AUTODAD ON	5.273E 03	2,445E 00	1.283E=03	4.636E 00	2,433E+03
- " "TITE TO THE TO THE TO THE TO THE TO THE TOTAL OF WINTER OF WINTER OF WENDING US	5.290E 03	2.302E 00	1.209E=03	4.029E 00	2.115E=03
7-353E 01 1-079E 00 4-850E-01 1-590E 03 -4-880E 03 -1-966E 03 -2-915E 03	5.374E 03	2.199E 00	1.154E=03	9.971E=01	5.233E=V4
- / • 3 3 4 1 1 1 2 6 4 E 00 4 2 7 7 1 5 2 1 1 2 5 9 1 E 03 4 4 8 8 1 E 03 4 4 4 9 6 6 F 0 7 4 2 1 9 5 5 F 0 3	5.375E 03	2.1985 00	1.154E=03		
7.486E 01 9.800E-01 0.000 1.613E 03 -4.932E 03 -1.971E 03 -2.960E 03				9.808E=01	5.148E=04
THE BEST OF THE STATE OF THE ST	5.427E 03	2.015E 00	1.057E=03	0.000	0.000
The state of the s	5,525E 03	5,170E 00	2.714E=03	0.000	0,000
- 9 3325 72 1.7275 03 AS\$4000 03	5.630E 03	3.598E 00	1.888E=03	0.000	0.000
8.442E 01 1.300E 00 0.000 1.808E 03 -4.957E 03 -1.996E 03 -2.960E 03	5.684E 03	2.673E 00	1.403E=03	0.000	0.000
- 0 1 1 2 4 0 0 0 0 0 0 0 0 0 0 1 8 4 7 E 03 - 4 4 9 6 9 E 03 - 2 - 0 0 8 E 0 1 - 2 - 9 6 0 E 0 1	5.707E 03	3.906E 00			•
8,729E 01 1,901E 00 0,000 1,847E 03 -4,969E 03 -2,008E 03 -2,960E 03			2.050E=03	0.000	0.000
CO SOCIAL CO SECURE CO SECURE CO SECURE CO	5.707E 03	3.909E 00	2.0526-03	0.000	0.000

X	DORAG	CDPAG	CF	HC
44.0116 0011	20110100011000110000110001100011000110	22222222222222222222222222222222222222	33333333333333333333333333333333333333	22222222222222222222222222222222222222
011011011011011011011011011011011011011	1.2394EE 000 000 000 000 000 000 000 000 000	00000000000000000000000000000000000000	2.650E=0033 2.65E=0033 2.65E=0033 2.65E=0033 2.65E=0033 2.65E=0033 2.65E=0033 2.65E=0033 2.65E=0033 2.766E=0033	2.607762=0022 2.6077
7,771E 01 8,161E 01 8,442E 01 8,728E 01 8,729E 01	2.214E 00 2.744E 00 1.158E 00 4.926E=01 0.000	5.099E 02 5.127E 02 5.138E 02 5.143E 02	2.833E+03 2.762E+03 2.706E+03 2.750E+03 2.750E+03	8.470E=03 6.407E=03 5.076E=03 6.755F=03 6.758E=03

RAMJET FERFORMANCE

	1	RAMJET FER	RAMJET FERFORMANCL							
- 6: - 6:										
8				INLET						
	CALCULATED THRUST	BF) BF=SFC/LAM)	HASS FLOW RAT ADDITIVE DRAG LIMITING PRESS	CK	0.9847					
	MEASURED THRUST COEFFICIENT		DFLTA PT2 TOTAL PRESSURI TOTAL PRESSURI INLET PROCESS	E RECOVERY - SUPERSUNIC E RECOVERY - SUBSUNIC EFFICIENCY - SUPERSONIC.	0.1487 0.3806 0.1652	(PSI)				
	REGENERATIVE=COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	0.F.)	KINETIC ENERGY	EFFICIENCY - SUBSONIC Y EFFICIENCY - SUPERSONIC	0.9428					
	STREAM THRUST	AF)	ENTHALPY AT P	Y EFFICIENCY = SUBSGNIC D = SUPERSONIC D = SUBSONIC D = BUBSONIC	-2.35	(BTU/LBM) (BTU/LBM)				
_	. MOMENTUM AND FORCES			_ COMBUSTOR						
	INLET FRICTION DRAG	0F) 0F] 0F] 0F] 0F] 0F]	EQUIVALENCE RACOMBUSTOR EFF TOTAL PRESSUR COMBUSTOR EFF	OATIO	0,799 0.757 0.1360 0.7150	0.7703. 0.7033				
	NOZZLE PRESSURE INTEGRAL EXTERNAL FRICTION DRAG. EXTERNAL PRESSURE INTEGRAL. TOTAL EXTERNAL DRAG	8F) 8F) 8F) 8F) 8F) 8F) 8F)	VACUUM BIREAM THRUST COEFFICIENT = CS 0.9510 NOZZLE COEFFICIENT = CT							
	STATIONS			FUEL INJECTORS						
	NOMINAL COMPLEADING EDGE	IN) IN) IN) IN) IN) IN) IN)	INJECTORS 1 A 1 B 1 C 2 A 2 C 3 A 3 B	37ATION 40,400 41,300 44,300 48,775 46,250 54,065 56,250 44,800	VALVE A B D E					

t = 216.75 sec.

SUPHARY REPORT

H GAMMA MOLAT SONV MACH VEL S A/A AZAC MUNTH D IVAL PHI ETAC WIND TUNNEL 0.000 925,749 2981 665,2(791) 1,2945 28,832 2579 - 0.000 0.483 402 -32.5(97) 1.3987 25.831 985 5.998 5909 1.811 0.13219 33.392 0.9862 6254 12.138 187.3 SPIKE TIP NS 2 0.600 22.512 2980 665.2(791) 1.2944 28.831 2579 0.600 20.346 2912 644.7(771) 1.2965 28.831 2552 0.397 1014 2.068 0.13219 33.392 0.9862 6192 2.084 185.4 WIND TUNNEL 0.000 925.749 2981 665.2(791) 1.2945 28.832 2579 0.474 400 -33.0(96) 1.3987 26.831 983 6.015 5911 1.811 0.13057 32.982 0.9862 6179 11.993 187.3 0.000 SPIKE TIP NS 0.600 22,512 2960 665,2(791) 1,2944 28,831 2579 0.600 20,407 2914 645.3(772) 1.2965 28.831 2553 0.392 999 2.068 0.13057 32.982 0.9862 6179 2.028 187.4 INLET THROAT 355,200 2929 649,6(776) 1,2961 28,831 2559 40.400 40.400 19.726 1444 226.1(357) 1.3522 28.631 1835 2.502 4593 1.872 1.17028 33.392 0.1114 5329 83.525 159.6 INLET UPNRSK 40.400 355.200 2929 649.6(776) 1.2961 28.831 2859 40.400 16.938 1388 213.2(343) 1.3555 28.831 1801 2.594 4673 1.872 1.06389 33.392 0.1225 5381 77.261 161.2 INLET DNNRSK 152.317 2929 649.6(776) 1.2961 28.831 2539 40.400 40.40m 130.653 2828 619.10 746) 1.2992 28.631 2517 0.490 1234 1.930 1.06389 33.392 0.1225 5381 20.403 161.2 CUMBUSTOR 1 21 40.416 295,126 2893 652,5(798) 1,2983 27,602 2601 40.410 15.599 1403 213.2(362) 1.3556 27.601 1851 2.533 4688 1.952 1.17423 33.508 0.1114 5328 85.554 189.0 0.12 0.07 COMBUSTOR 5 51 41.298 220,964 2828 656,2(809) 1,3019 26,478 2630 19,993 1569 41.298 268.0(424) 1.3481 26.478 1993 2.209 4403 2.031 1.18056 33.621 0.1112 5170 80,774 153.8 0.24 0.04 COMBUSTOR 0 10 41.30A 231,010 2788 656,1(797) 1,3038 26,436 2615 41.308 20.042 1586 269.3(412) 1.3508 26.435 1969 2.234 4400 2.024 1.18091 33.621 0.1112 5168 80.743 153.7 0.24 0.01 COMBUSTOR 0 11 4 21 229,460 2781 655,9(795) 1,3041 26,429 2612 41.373 41.373 20.364 1531 272.66 414) 1.3506 26.429 1972 2.221 4380 2.024 1.18223 33.621 0.1110 5156 80.463 153.3 0.24 0.00 COMBUSTOR 0 12 5 21 41.500 225.220 2778 655.3(794) 1.3042 26.428 2611 41.500 - 22.267 1972 289.00 426) 1.3484 26.428 1997 2.195 4305 2.025 1.18224 33.621 0.1110 5132 79.093 192.6 0.24 0.00 COMBUSTOR 0 13 195.693 2790 650.3(797) 1.3034 26.457 2614 42.460 30.724 1778 42.460 336.9(486) 1.3386 26.456 2115 1.872 3960 2.036 1.17116 33.621 0.1121 5020 72.069 149.3 0.24 0.02 COMMUSTOR 0 14 44.091 137.047 3395 639.4(981) 1.2749 27.156 2815 44.093 57,330 2799 442.3(790) 1.2948 27.159 2576 1.214 3140 2.106 1.13041 33.621 0.1161 4986 55.159 148.3 0.24 0.60 COMBUSTOR 0 15 44.310 135,866 3414 637.7(987) 1.2739 27.183 2820 44.310 59.225 2842 448.2(804) 1.2930 27.186 2592 1.188 3079 2.107 1.12878 33.621 0.1163 4982 54.012 148.2 0.24 0.62 COMBUSTOR 0 15 44.800 133,549 5441 633.6(995) 1.2725 27.228 2827 44.000 93.500 2923 461.2(829) 1.2898 27.231 2624 1.114 2936 2.109 1.12421 33.621 0.1168 4968 51.304 147.8 0.24 0.66 COMBUSTOR 0 17 10 44.808 133.503 3440 633.5(995) 1,2725 27.228 2827 44.808 63,503 2923 461.2(829) 1.2898 27.231 2624 1.119 2936 2.109 1.12588 33.621 0.1168 4968 51.275 147.7 0.24 0.66 COMBUSTOR 0 18 11 46.250 125.169 3021 643.5(966) 1.2942 23.939 2850 46.250 64.089 2587 487.9(.813) 1.3085 23.940 2651 1.052 2790 2.283 1.07073 33.974 0.1239 4979 46.423 146.6 0.61 0.19

GAMMA MOLHT SONV MACH VEL S AZAC MOPIM R IVAC PHI ETAC */A COMBUSTOR 0 19 12 2 125.144 3023 643.4(967) 1.2941 23.941 2850 64.093 2589 487.8(814) 1.3084 23.942 2652 1.052 2790 2.283 1.07015 33.974 0.1239 4961 45,403 146,6 0.61 0.19 COMBUSTOR 0 20 13 47.310 120.128 3246 632.6(1042) 1.2834 24.189 2926 47.310 64.520 2822 477.9(891) 1.2974 24.191 2743 1.014 2782 2.303 0.99579 33.974 0.1332 5139 43.058 151.5 0.61 0.29 COMMUSTOR 0 21 14 47.333 120.115 3248 632.4(1043) 1.2833 24.192 2927 47.333 64.687 2826 478,2(892) 1,2973 24.194 2745 1.012 2778 2.303 0.99539 33,9/4 0.1335 5141 42,967 151.5 0.61 0.30 COMBUSTOR 0 122 15 48.110 115.368 3462 624,9(1115) 1.2727 24.430 2994 48.110 64.547 3049 471.3(967) 1.2867 24.433 2826 0.981 2772 2.320 0.92789 33.974 0.1430 5291 39.978 155.7 0.01 0.39 COMBUSTOR 0 23 16 48,773 108,887 3143 638,4(1116) 1,2899 21,685 3049 48.773 53,295 2668 448,5(929) 1,3056 21,686 2826 1,091 3082 2,505 0,86420 34,353 0,1552 5410 41,395 157,5 1,00 0,21 COMBUSTOR 0 24 17 48.783 108,812 3145 638,3(1117) 1,2898 21,688 3050 48.783 53.185 2669 448.0(930) 1.3055 21.689 2826 1.092 3086 2.505 0.86307 34.353 0.1554 5412 41.394 157.5 1.00 0.22 COMBUSTOR 0 '25 18 49.313 105.193 3278 634.2(1167) 1.2834 21.815 3097 49.313 47.350 2737 416.0(953) 1.3014 21.817 2849 1.160 3304 2.519 0.80718 34.353 0.1662 5543 41.450 161.4 1.00 0.25 COMBUSTOR 0 26 19 96,611 3591 624,3(1286) 1.2677 22,126 3198 50.723 36.394 2937 354,4(1025) 1.2903 22.132 2918 1.259 3674 2.548 0.66794 34.353 0.1950 5841 39.284 170.0 1.00 0.35 50.723 COMBUSTOR 0 27 20 52.823 89.200 3838 611.5(1380) 1.2539 22.391 3269 52.823 27.712 2996 258.3(1042) 1.2845 22.406 2922 1.459 4204 2.569 0.56385 34.353 0.2379 6177 36.835 179.8 1.00 0.43 COMBUSTOR 0 28 21 53.323 88.329 3857 608.8(1387) 1.2527 22.417 3274 53.323 25.570 2967 235.3(1031) 1.2651 22.433 2907 1.467 4323 2.571 0.54080 34.353 0.2480 6240 36.328 181.6 1.00 0.44 COMBUSTOR 0 29 22 54.073 86,757 3893 604,8(1401) 1,2505 22,461 3283 54.073 23,114 2944 200,5(1021) 1,2852 22,479 2893 1,543 4464 2,574 0,50978 34,353 0,2631 6324 35,366 184,1 1,00 0,45 CORBUSTOR 0 30 23 54.033 86.276 3893 601,0(1401) 1,2504 22,470 3202 54.833 20.625 2875 175.0(993) 1.2875 22.488 2860 1.614 4617 2.574 0.48207 34.353 0.2782 6399 34,588 186,3 1,00 0,45 COMBUSTOR 0 31 24 55.760 83.925 3944 596.7(1420) 1,2472 22.531 3295 55.760 18,922 2882 150.7(995) 1,2864 22,553 2859 1.652 4724 2,579 0.45257 34,353 0.2964 6480 33.224 188.6 1.00 0.47 COMBUSTOR 0 32 25 5 56.258 65.401 4393 594.5(1594) 1.2155 22.995 3398 56,258 18,007 3441 159,5(1205) 1,2584 23,072 3055 1,927 4666 2,622 0,36452 34,353 0,3679 6679 26,431 194,4 1,00 0,62 COMBUSTOR 0 35 26 76.458 3997 594,3(1440) 1.2435 22.589 3307 56.313 50.313 13.697 2783 85.2(955) 1.2889 22.616 2808 1.797 5047 2.590 0.36349 34.353 0.3690 6683 28.511 194.6 1.00 0.49 COMBUSTOR 0 34 27 76.264 4004 593.7(1443) 1,2430 22.597 3309 56.453 56,453 13.568 2785 82.2(956) 1.2887 22.624 2808 1.802 5059 2.590 0.36088 34.353 0.3717 6694 28.374 194.8 1.00 0.49 COMBUSTOR 0 35 28 56.533 66.764 4372 593.4(1586) 1.2173 22.976 3394 56.533 17,502 3385 146,0(1183) 1,2611 23.049 3034 1,559 4732 2,619 0,36492 34,363 0,3675 6700 26,834 195.0 1,00 0,61 COMBUSTOR 0 36 29 56.813 67.792 4352 592.3(1578) 1,2189 22.458 3389 56.813 16.987 3334 133.7(1163) 1.2634 23.028 3016 1.588 4790 2.617 0.56372 34.353 0.3686 6719 27.075 195.6 1.00 0.60 COMMUSTOR 0 37 30 57.039 69.719 4243 591.4(1555) 1.2233 22.899 3377 57.039 10.154 3222 110.6([120] 1.2667 22.959 2975 1.638 4874 2.611 0.36303 34.353 0.3695 6733 27.497 196.0 1.00 0.58

GAMPA MOLWT BONY, MACH VEL S AZAC POPTH Q #/A IVAC PHI ETAC COMBUSTOR 0 38 51 4 57.763 76.981 4080 588,5(1472) 1,2383 22,686 3327 13.485 2841 64.3(976) 1.2856 22.719 2827 1.812 5122 2.592 0.35741 34.353 0.3753 6765 26.448 196.9 1.00 0.52 COMBUSTOR 0 39 32 58.783 137.782 3348 585.1(1191) 1,2789 21,987 3111 58.783 7.350 1673 -59.9(553) 1.3396 21.989 2251 2.524 5681 2.494 0.35513 34.353 0.3777 6777 31.354 197.3 1.00 0.31 COMBUSTOR 0 40 33 60.793 63,729 4680 579.0(1705) 1.1918 23.337 3447 20.750 3874 171.9(1371) 1.2317 23.488 3178 1.420 4514 2.632 0.36748 34.353 0.3650 6759 25.778 196.6 1.00 0.73 60.793 0 41 34 COMBUSTOR 62.213 66,501 4593 574,6(1671) 1,1995 23,255 3432 62,213 20.244 3725 153,3(1313) 1.2414 23.379 3136 1.464 4591 2.625 0.37744 34.353 0.3553 6745 26.931 196.3 1.00 0.70 COMBUSTOR 0 42 35 64 - 677 58.579 4857 566.1(1774) 1.1739 23.559 3469 64.677 25.889 4256 222.9(1521) 1.2017 23.770 3271 1.207 4144 2.642 0.55777 34.353 0.3749 6719 25.041 195.6 1.00 0.83 COMBUSTOR 0 43 36 65.053 53.222 4983 564.7(1824) 1.1608 23.694 3484 65.053 25,254 4525 269,0(1628) 1,1759 23,944 3324 1,157 3846 2,652 0,33261 34,353 0,4032 6715 19,880 195,5 1,00 0,91 COMBUSTOR REGEN 44 37 65.053 53.222 5054 625.0(1855) 1,1576 23,621 3509 65,053 26.633 4636 344.3(1676) 1,1692 23.874 3360 1.115 3748 2.664 0,33261 34.353 0.4032 6752 19.372 196.6 1.00 0.91 NOZZLE AE 45 38 " 87.289 93.222 4983 564.7(1794) 1,1608 23.694 3484 87.259 1.632 2756 ~551.0(917) 1.2709 24.205 2683 2,784 7472 2.652 0,08924 34.353 1.9371 8787 8.040 255.8 1.00 0.91 NOZZLE PO 87.289 53.222 4983 564.7(1794) 1.1608 23.694 3484 87.289 0.483 2109 -793.3(676) 1.2946 24.206 2368 3.481 8243 2.652 0.02955 34.353 4.5396 9363 3.785 272.5 1.00 0.91 NOZZLE AE REGEN 47 40 5 87.289 53.222 5054 625.0(1855) 1.1576 23.621 3509 87.289 1.678 2862 #510.8(957) 1.2670 24.204 2729 2.762 7539 2.664 0.06924 34.353 1.9371 8882 8.112 258.5 1.00 0.91 NOZZLE PO REGEN 48 41 53.222 5054 625.0(1855) 1,1576 23.621 3509 87.289 37.289 0.483 2180 -767.6(702) 1.2918 24.206 2405 3.471 8347 2.664 0.02894 34.353 4.6340 9486 3.755 276.1 1.00 0.91 FICTIVE COMBUSTR 68 61 0 65,053 355.200 5312 564.7(1955) 1.1695 24.044 3584 05.05¥ 0.485 1469-1148.2(449) 1.3233 24.578 1983 4.669 9258 2,492 0.04838 34.353 2,7724 10228 6.960 297.7 1.00 1.00 FICTIVE NOZZLE 69 62 0 87.289 29.714 4893 540.9(1787) 1.1563 23.657 3448 87.289 - 2.165 3266 -348.5(1114) 1.2483 24.194 2894 2.305 6671 2.696 0.06924 34.353 1.9371 8197 7.179 238.6 1.00 0.91

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XABs	P=1B	P≖OR	PDA	GOX	Q=IB	Q#ባ <u>ፀ</u>	CAMALL	P=18/P50	P=18/PT0	P=08/PS0	P=08/P10
6.981E=01	1.325E 00	0.000	-5.484E-01	0.000	0.000	0.000		2.746E 00	1.451E=03	0.000	0.000
1.836E 01	1.325E 00	0.000	-4.411£ 01	0.000	0.000	0.000	1.634£ 02	2 7468 00	1.431t=03	0.000	0.000
3.070E 01	2.730E 00	0.000	-2.085E 02	0.000	0.000	0.000	5.053E 02	5.658E 00	2.949E=03	0.000	0.000
3.508E 01	4.829E 00	0.000	-4.534E 02	0.000	0.000	0.000	6.804E 02	1.001E 01	5.210E-03		
3,519E 01			_ •	- •		•	• •			0.000	0.000
3.520E 01	4.850E 00		-5.349E 02	0.000	0.000	0.000	6.8538 02	1.0058 01	5.2396-03	1.475E 01	7.686E#03
	4.8518 00		-5.350k 02	0.000	0,000	0,000	6,856E 02	1.005E 01	5.241L=03	1,465E 01	7.637E=03
3.555E 01	4.920E 00		-5,450E 02	0.000	0.000	0,000	7.210E 02	1.050E 01	5.315E-03	9.109E 00	4.748E=03
3.586F 01	4.874E 00		-5.643E 02				7,548E 02	1.0106 01	5.265E+03	4.197E 00	2.187£=03
3,606E 01	4.845E 00		5.782E 02				7.730E 02	1.004E 01	5.234E=03	6.362E 00	3.316E=03
3-6488 01	5.228E 00		-6.037E 02				8,166E 02	1.084E 01	5.647E=03	1.098E 01	5.720E=03
3.701E 01	5.260£ 00					02 #2,196E 01	8.725E 02	1.090E 01	5.682E=03	1.680E 01	8,755E=03
3.732E 01	5.085E 00					02 +2.926E 01	9.0625 02	1.054E 01	5.4936-03	5.057E 01	1.055E-02
3.803E 01	4.690E 00		-6.661E 02				9.835E 02	9.720E 00	5.066E=03	3.396E 01	1.770E=02
3-834E 01	6.781E 00					10 3985.5# 50	1.018E 03	1.405E 01	7.325£~03	4.005E 01	5.080F=0S
3.875E 01	9.502E 00					02 06.149E 01	1.064E 03	1.969E 01	1.0266=02	3.893E 01	5.054E+05
3.881E 01	9.92SE 00					05 -0.5896 01	1,072E 03	2.0566 01	1.0726-02	3.870E 01	5.050E=05
30901E 01	1.124E 01					02 46,725E 01	1.094E 03	2.330E 01	1.214E=02	3.980E 01	2,07#E+02
3.932E 01	1.740E 01	5.000E 01	. ≈6.763£ 02	## 555E (02 =3. 814E	02 97.415E 01	1.130E 03	3.606E 01	1.880E=02	4.145E 01	2.160E=02
3.950E 01	2.089E 01					02 07.8025 01	1.151E 03	4.329E 01	2.256E=02	3.058E 01	1.5946=02
3.981E 01	S.146E 01	5.500g 00	-7.177E 02	-4.840E (02 -3.993 E	02 →8.474€ 01	1.187E 03	4.44BE 01	2.318E.02	1.140E 01	5.941E-03
4.000E 01	2,181E 01	5.334E 00	₩7,404E 02	⊕4.956E (02 -4. 069E	10 3698°96 20	1,209E 03	4.519E 01	2.356E=02	1.105E 01	5.7616-03
4.OHOE DI	S.01SE 01	4.978E 00	97.913E 02	9055.60	02 64.241E	02 09.786E 01	1,256E 03	5.414E 01	2.822E=02	1.032E 01	5.3776-03
4.041E 01	2.683E 01	4.9695 00	-7.925E 02	2655°C	02 - 4.245E	02 =9.811E 01	1.257E 03	5,436E 01	2.833E=02	1.030E 01	5.367E-03
4,130E 01	3.581E 01	4.179E 00	#9.287E 02	06.131E (02 04.670 E	02 -1.461E 02	1,362E 03	7.421E 01	3,868E=Q2	8.6612 00	4.514E>U3
4.131E 01	3.591E 01	4.170E 00	-9.303E 02	-6.144E (02 =4.675E	02 #1.469E 02	1,363E 03	7.443E 01	3.879t-02	6.643E 00	4.505E-03
4.1378 01	3.662E 01	4-112E 00	-9.414E 02	-6.233E (02 - 4.708E	02 -1.529E 02	1.371E 03	7.589E 01	3.955E-02	6.523E 00	4.4426=03
4.150E 01	3.799E 01					02 -1-640E 02	1.386E 03	7.873E 01	4.103E-02	1.357E 01	7.072E=U3
4.246E 01	3.652E 01					02 -5.421E 05	1.5016 03	7.570E 01	3.9454=02	5,165E 01	5.6924=02
4.409E 01	5.848E 01					05 44.943E 05	1.699E 03	1.2128 02	6.317E-02	1.164E 02	6.069E=V2
4.431E 01	6.140E 01					05 -243E 05	1,725E 03	1.273E 02	6.632L=02	1.182E 02	6.1636=02
4.480E 01	6.799E 01					02 #6.035E 02	1,785E 03	1.409E 02	7.344E-02	1.233E 02	6.374E=02
4.481E 01	6.796E 01					02 #6.049E 02	1.7868 03	1.409E 02	7.3416-02	1.284E 02	6,378E=U2
4.625E 01	6.336E 01					02 =8.995E 02	1,963E 03	1,313E 02	6.844E-02	1.343E 02	7.001E=U2
4.026E 01	6.333E 01					20 3810°6 8	1,464E 03	1.313E 02	6.8416=02	1.344E 02	7.006E=02
4.731E 01	5.998E 01	6.906E 01	97.915E 02	05.551E (03 01.0785	03 #1.144E 03	2,094E 03	1.243E 02	6.479E+02	1.431E 02	7,440E=0a
4.733£ 01	6.022E 01					03 -1-149E 03	2.097E 03	1.548E 05	6.505E-02	1.433E 02	7.470E=02
4.8116-01	6.850E 01					03 *1.316E 03	2,194E 03	1.420E 02	7,399E=02	1.256E 02	6.5458=02
4.877E 01	5.330E 01					03 41.441E 03	2,277E 03	1.105E 02	5,757E-02	1,105E 02	5.757E=02
4.878E 01	5.319E 01					03 -1 442E 03	2,2788 03	1.102E 02	5.7456-02	1.102E 02	5,745E-02
4.931E 01	4.735E 01	4.735E 01				03 #1.529E 03	2,345E 03	9.813E 01	5.115E-02	9.813E 01	5.115E#U2
5.072E 01	3.839E 01	3.639E 01				03 -1.734E 03	2.5228 03	7 - 957E 01	4.1476=02	7.957E 01	4.147E>U2
5.2828 01	2.771E 01	2.771E 01				03 -1.9948 03	2.789E 03	5.743E 01	2.994E=02	5.743E 01	2.994E=02
5.3325 01	2.557E 01	2.557F 01				03 -2.049E 03	S.852E 03	5.299E 01	2.762E=02	5.299E 01	2.762E+V2
5.407E 01	2.311E 01	2.311E 01				03 -5.129E 03	2.94BE 03	4.790E 01	2.4976-02	4.790E 01	2,4976=02
5.483E 01	2.062E 01	5.095E 01				03 -2.207E 03	3.045E 03	4.275E 01	5.558E=05	4.275E 01	2.2588=05
5.576E 01	1.892E 01	1.892E 01				03 =2.298E 03	3,165E 03	3.9228 01	2.0445-05	3.925E 01	2.0446-02
5+626E 01	1.801E 01	1.801E 01				03 -2.344E 03	3,209E 03	3.732E 01	1.945E-02	3.732E 01	1.945E=U2
5.6318 01	9.487E 00	1.791E 01		=4.1755 (05 =1.5436	03 02.349E 03	5.216E 03	1.966E 01	1.0256=02	3.711E 01	1.934€=02
5.645E 01	9,487E 00	1.765E 01	Y.295E 02	-A.212E (05 -1.850E	03 -2.362E 03	3.234E 03	1.966E 01	1.025E-02	3,658E 01	1.906E#02
5.653E 01	1.750E 01	1.750E 01	7,3051 02	04+224E (05 = 1 · 054E	03 *2.370E 03	3,2456 03	3.627E 01	1.8916=02	3.627E 01	1.891E=02
5.681E 01	1.699E 01	1.6998 01		₹4.263E (U1.067E	03 *2.395E 03	3,2806 03	3.521E 01	1.835E=02	3.521E 01	1.835E=02
5,704E 01	1.615E 01	1,615E 01	7.7566 02	-4.644E (0.5 = 1 = 078E	03 =2,416E 03	3,309E 03	3,348E 01	1.745E=02	3.348E 01	1.7458-02
5.776E 01	1.348E 01	1.348E 01				03 m2.483E 03	3,402E 03	2.795E 01	1.4578-02	2.795E 01	1.457E=02
5.878E 01	7.350E 00	7.3500 00				03 #2.561E 03	3,532E 03	1.523E 01	7.940E-03	1.523E 01	7,940E-V3
6.079E 01	2.075E 01	2.075E 01				03 #2.709E 03	3,790E 03	4.300E 01	5.5416-05	4.300E 01	2.241E-02
6.221E 01	2.024E 01	2.024E 01	1.0432 03	#4.0/0E (U⇒ □2.047E	03 =2,823E 03	3,972E 03	4.196E 01	2.1676-02	4,196E 01	2.187E=02

ORIGINAL' PAGE IS OF POOR QUALITY

	XABS	₽=18	P=08	PDA	ROX	W=IB		₩≈08		LAWALL	P=16/P8v	P#18/P10	P#08/P80	P=08/P/10
	6-468E 01	2.389E 01	2.389E 01	1.043t 03	-5.163E 03	=2.133E	03	≈3.030F	03	4.289Ł 03	4.9516 01	2.580E=U2	4.951E 01	2.580E=U2
7	6.505E 01	S.606E 01	2.444E 01	1.043E 03	-5.211E 03	-2.148£	03	93.063E	03	4.3576 03	5.402E 01	2.615E=02	5.066E 01	2,641E=02
2	6.509E 01	2.6068 01	2.450E 01	1.0435 03	•5,216E 03	-2,149E	0.3	□3.067€	03	4,342E V3	5.402E 01	2,815t=02	5.0798 01	2.647E-02
	6.529E 01	2.474E 01	2.480E 01	1.043E 03	-5.219E 03	a2.157€	03	□3.082E	03	4.368E 03	5.128E 01	2.6736-02	5.140E 01	2.6791-02
	6.695E 01	1.377E 01	1.199E 01	1.251E 03	-5,409E 03	#2.213E	03	-3.195E	03	4.583£ 03	2,854E 01	1.487E=02	2.485E 01	1.295E=UZ
	6.762E 01	9.894E 00	1.195E 01	1.490E 03	5.470€ 03	-2.431E	G 3	-3.239E	0.5	4,665E 03	2.051E 01	1.069E=02	2.408E 01	1.255E=UZ
	6.839E 01	5.440E 00	8.818E 00		+5.540E 03					4,760E 03	1.127E 01	5.876E=03	1.827E 01	9,525E=03
	6.911E 01	4.260E 00	6.500E 00		-5.6∪7E 03					4.848E 03	00 3PS#.8	4.602E=03	1.285E 01	6.697E=03
	6.972E 01	3.260E 00	5.129E 00		■5,661E 03					4.922E 03	6.756E 00	3.521E=03	1.063E 01	5.540E=03
	7.067E 01	2.3518 00	3.460F 00		-5.734E 03					5.0366 03	4.873E 00	2,540E=03	7.171E 00	3.7386=03
	7.110E 01	1.940E 00	3.211E 00		•5.770E 03					5.088E 03	4.021E 00	2.0966-03	6.655E 00	3.469E=03
	7.263E 01	1.284E 00	2.325E 00	2.242E 03	-5.851E 03	=2.296E	03	#3.555E	03	5.273E 03	2.662E 00	1.387E=03	4.819E 00	2.511E=03
	7.278E 01	1.220E 00	2.033E 00		*5.857€ 03					5.290E 03	2.528E 00	1.318E=03	4.214E 00	2.196E=03
	7.353E 01	1.305E 00	5.7508.01		-5.840E 03					5.374E 03	2,704E 00	1.4098-03	1.192E 00	6.211Em04
	7.354E 01	1.305E 00	5.672E=01		=5.890E 03					5.375E 03	2.705E 00	1.410E=03	1 m 1 7 o E 00	6.127E=04
	7.486E 01	1.455E 00	0.000		•5,956E 03					5.427E 03	3.016E 00	1.5726+03	0.000	0.000
	7.771E 01	2.705E 00	0.000		-5,970E 03					5,525E 03	5.606E 00	2.922E=03	0.000	0.000
	8-161E 01	1.840E 00	0.000		-5.986E 03					5.630E 03	3.813E 00	1.988E=03	0.000	.0.000
	8.442E 01	1.425E 00	0.000		=6.001E 03					5.684E U3	2.953E 00	1.539E=03	0.000	0.000
	8.728E 01	5.090E 00	0.000		-6.025E 03					5.707E 03	4.332E OU	2.258E=03	0.000	0.000
	8.729E 01	2.091E 00	0.000	2.582E 03	-6.025E 03	□2.378E	03	#3,647E	03	5.707E 03	4.334E 00	2.259E=03	0.000	0.000

×	DDRAG	CORAG	ÇF	нс
4.1301E 01 4.1301E 01 4.1301E 01 4.1306E 01 4.1506E 01 4.1546	1.364£ 01 2.267£ 01 2.267£ 01 2.247£ 01 2.803£ 01 2.8047£ 01 3.8047£ 01 3.874£ 01 1.446£ 01 1.446£ 01 1.446£ 01 1.46£ 01	1.3645EEE 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2-12-03 	144222
4.9372EE 001 4.9372EE 001 4.9372EE 001 5372EE 001 537465EE 001 557465EE 001 55766666666666666666666666666666666666	1.545E 01 7.717E 01 1.769E 00 1.769E 00 1.769E 00 1.1651E 00	00000000000000000000000000000000000000	28E = 003 2877E = 003 27726E = 003 22805E = 003 2805E	7.6022 5.602 5.6022 5.6022 5.6022 5.6022 5.6022 5.6022 5.6022 5.6022
6.079E 01 6.221E 01 6.2265E 01 6.5029E 01 6.5029E 01 6.5029E 01 6.5029E 01 6.5029E 01 7.7010E 01 7.210E 01 7.210E 01	1.898E 01 1.318E 01 2.385E 00 3.385E 00 3.385E 00 1.436E 00 1.4476E 00 5.524E 00 4.8796E 00 4.8796E 00 4.8796E 00 4.8796E 00 5.8298E 00 5.8298E 00 6.836E 00 6.83	9.3256 9.3256	2.456E003 3.010E003 3.029E003 3.197E003 3.334E003 3.240E003 3.161E003 3.161E03 3.161E03 3.161E03 3.089E003 3.089E003 3.089E003	4.427EmQ2 3.637EmQ2 3.650EmQ2 3.650EmQ2 3.650EmQ2 2.6792EmQ2 1.8597EmQ2 1.277EmQ3 8.734EmQ3 8.734EmQ3
7.278E 01 7.353E 01 7.354E 01 7.476E 01 8.161E 01 8.442E 01 8.728E 01 8.729E 01	4,239E-01 1.707E 00 2.698E-03 1.003E 00 3.655E 00 3.007E 00 1.274E 00 5.500E-01	5.109E 002 5.209E 002 5.209E 002 5.209E 002 5.209E 002 758E 002 75	2.9646.03 2.8906.03 2.8906.03 2.9396.03 2.9336.03 2.9336.03 2.8876.03 2.9236.03	6.296E=03 4.106E=03 4.093E=03 5.755E=03 9.166E=03 6.804E=03 7.427E=03 7.4451E=03

RAMJET" PERFORMANCE.

17	KEMPEL FORFUMANUE											
76	ENGINE PERFORMANCE			INLET								
	CALCULATED THRUST	(LBF) (LBF*SEC/LBM)	MASS FLOW HATIO ADDITIVE DRAG COEF LIMITING PRESSURE DELTA PTZ TOTAL PRESSURE REC	FIGIENY	0.9862 0.0004 0.1622 0.1474 0.3837							
	REGENERATIVE COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	(LBF)	INLET PROCESS EFFI INLET PROCESS EFFI KINETIC ENERGY EFF KINETIC ENERGY EFF ENTHALPY AT PO = 8	OVERY - SUBSONIC CIENCY - SUPERSONIC CIENCY - SUBSONIC ICIENCY - SUBSONIC UPERSONIC UBSONIC	0.8934 0.9050 0.9378 0.8888 -4.68							
	MOMENTUM AND FORCES		COMBUSTGR									
	INLET FRICTION DRAG	(LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF)	FUEL#AIR RATID									
	CALCULATED LOAD CELL FORCE	(LBF) (LBF)										
	8NO1TAT8		FU	EL INJECTORS								
	NOMINAL CUML LEADING EDGE	(in) (in) (in) (in) (in) (in) (in) (in)	INJECTORS 1 A 1 B 1 C 2 A 2 C 3 A 3 B 4	STATION 40.400 41.298 44.300 48.773 46.250 54.063 56.248 44.798	ALVE B D E							

t = 249.15 sec.

SUMMARY REPORT

ت							• •	•	, ,	., .	A 1.							
8	Р	Ť	h		GAMMA	MOLMI	SOLV	MACH	VEI	5	W/A	H	A/AC	MINOW	G.	IVAL	041	ETAE
1	WINC TUNNEL	1	0 5		•		5 ~ (1 ·	1124	,	U	11/15	**	4/40	mor pr	t3	1426	501	CIAL
	0.000 472.999	2988	667.50	7031	1.2943	28.841	2582											
	0.000 0.247		-32.17	071	1 3047	28.834	902	E 00/	E04.	. 0.6.0	0 24754	. 4 . 0 15 "		7.00				
,	SPIKE TIP NS	2		4,,	143407	50.027	707	34444	2410	1+050	0.06756	17,034	11.4422	3199	6.212	187.6		
•	**		0 3	a v .													,	
	0.600 11.350		667.51															
	0,600 10,220	5411		772)	1,2963	26.631	2554	0,405	1034	2.115	0.06756	17.054	0.9855	8ء 1 د	1.085	183,4		
'	IND TUNNEL		0 0															
	0.000 472,999		667,5(
	0,000 0,238	399	-33,2(96)	1.3987	28.831	982	6.033	5921	1.858	0.06572	16.589	0.9855	3113	6.047	187.7		
;	SPIKE TIP NS	4	O Q						-	_		-						
	0,600 11,350	5988	667,5(793)	1.2941	28,831	2582											
	0.600 10.289	2922	647.5(774)	1.2962	28.831	2596	0.391	1000	2.115	0.06572	16.589	0.9855	3113	1.022	187.7		
	INLET THROAT	5	0 4	•	• • • • • • • • • • • • • • • • • • • •	,			• •				******	5.15	.,	10/9/		
	40,400 189,740	2926	648.7(775)	1.2962	28.831	2557											
	40.400 9.803	1416	220.5	350)	1.3539	28.831	1818	2.546	4620	1-915	0.59795	17.054	0.1114	2722	43.013	146 3		
	INLET UPNESK		0 3	- 2 .							043/1/3	111034	A 1 1 1 -	6133	421013	100.03		
	40.400 189.740		648.71	7951	1.2942	28.831	>==7											
	40.400 8.422		206.00	3455	1.3572	28.831	1741	2 478	4707		0 50750	17 054	0.1225	2850	30 846			
	INLET DNNRSK	7	0 4	-3-7	143215	201031	1704	£ 60 % C	4/0/	74415	0.54534	114034	A.1552	6/54	39,760	101.0		
	40.400 78.229			7-51	1 2062	20 04.	2 F C N											
	40.400 67.258		648.70	777	1 2004	20.031	₹22/											
	COMBUSTOR 0	2020	010911	740}	1.5442	50.031	5210	0.401	1224	1.476	0.54359	17.054	0.1225	2759	10.342	161.8		
		-	1 4	7-6	. 50/5		~											
			648.6(772)	1.2902	50.021	2557											
			E20.0(350)	1.3538	€0,031	1814	2.544	4627	1.915	0.59787	17.054	0.1114	2732	42,989	160.2		
	COMBUSTOR 0	2013	2 3	*-0.														
	41,310 148,227		646.1	72)	1.2905	28.831	2554											
	41.310 11.441			390)	1.3455	28.831	1409	2.305	4393	1.931	0.59894	17.054	0.1112	2654	40,890	155.6		
		10	3 3															
	41,375 145,864		645.8(772)	1,2965	28,831	2553											
	41.375 11.590	1577	263.4(393)	1,3449	28.831	1912											
								2.287	4375	1.932	0.59984	17.054	0,1110	2648	40.779	155.3		
		11	4 2							•		• • • •	.,					
	41.500, 141.040	2915	645.31	772)	1.2965	28.831	2553											
	41.500 11.851	1599	269.3(399)	1.3437	28.831	1925	2.254	4338	1.934	0.59998	17.054	0-1110	2636	40,450	154.6		
- 1	COMBUSTOR 0	12	5 5							• • • •				2020				
	42.460 - 122.309	2900	640,91	7673	1.2970	28.831	2547											
4	42.460 12.805	1681	291.60	4211	1.3396	28.831	1971	2.121	4181	1.941	0.59409	17.050	0.4121	259/	36,599	121 6		
(13	6 4		••••		• • •	-,			4457407	2.4004	A 1 1 6 7	6304	301277	15115		
	14.095 112.474	2869	631.60	7681	1.2979	28.831	2534											
	44.095 12.678		294.86	4543	1.3391	28.831	1977	2.077	4104	1.005	0.57367	17 054	A 1141	3657	74 407	1.00		
		14	7 4	2.,		,,		E V V V	-100	117-3	0.31301	111034	0.01707	6223	36,603	144.1		
	14.310 111.439		630,40	7671	1 2QA1	28.831	2572											
	14.310 12.700		299.46	4251	1 3300	20.83	1078	2 440	# A C #	4 045	0.57268	43 65"						
		15	8 4	-2-1	1,0370	FO3031	1110	GEUNT	4074	11743	0.3/200	17,094	0.1163	2244	36,438	149.4		
	44,800 108.625		627.7(7041	. 2040	20 97.	3530											
	4.800 12.826		207 04	1571	1 7704	20 021	6267	4 6/10										
		16	C7187(4211	1 9 3 3 0 0	20.031	1407	8.040	4003	1.440	0.57044	17.054	0,1167	2537	36,015	148.8		
			9 4	W /1 *	. 20-"	35 A												
		1700		7541	1,2984	60.031	4250											
		1/04	44/445	427)	1,3365	59.671	1984	6.046	4062	1.946	0.57045	17.054	0.1167	2537	36,008	148.7		
	COMBUSTOR 0	17	10 4	m . r			_											
	16.260 97.966	4033	620.60	748)	1,2991	28,831	2519											
	46,260 12,388	1/18	\$91.7C	431)	1.3379	28,831	1991	5.006	3995	1.951	0.53738	17.054	0.1239	2511	35.362	147.2		
,	COMBUSION U	10	11 4											* -				
	47.310 90.081	2017	616.0(.	743)	1,2996	28.831	2513											
	47.310 11.570	1/15	500.8(430)	1.3381	58.831	1989	1.997	3972	1,955	0.50001	17.054	0,1332	2500	30.864	146.6		
													,					

	KENGING #	(003	CLUCK	9 134	1 The	= 54491	DH MHC	L 0.	U P1 1	4/6	• 777	11 = 540	0.0						,
		ρ	Т	H		GAMMA	MULWT	SONV	масн	VEL	s	*/A	H	A/AC	MTHOM	G	IVAC	PHI	ETAC
	COMBUSTOR		19			B · (· · · · · · · · · · ·		• • • • • • • • • • • • • • • • • • • •	7,1- 4	,	•		,-	.,,,,,	• • •	-	• / •		
	47.335	89.907	2817	615.9	(743)	1,2996	28,831	2513											
	47.335	11.563	1715	300.8	(430)	1,3381	56.831	1989	1.996	3971	1.955	0.49945	17.054	0.1333	2500	30.820	146.0		
	COMBUSTOR		20				_												
	48.110	85.322	2806	612,7	(740)	1,2000	28.831	2508							3503	20 041			
	48,110				(424)	1,5391	58.821	1977	5.017	3988	1.958	0.46591	17.054	0.1429	2002	28,876	140.7		
	COMBUSTUR 48.785		21 2797	-	7771	1 3002	28.831	2504											
	48.785	9.381	1651	283.5	4(3)	1.3411	28.831	1954	2.069	0043	1,959	0.42846	17-054	0.1554	4516	26,918	147.5		
	COMBUSTOR		22							-0-3		0 4 - 2 4 - 5		~ 4.254					
	49.315	40.532	2791	608.2	(735)	1.3004	28.831	2502											
	49.315	8,458	1613	273.1	(402)	1.3430	28.831	1933	2.119	4095	1.960	0.40071	17.054	0.1662	2531	25,503	148.4		
	COMBUSTOR	0	23	16 5															
	50.725						28,831												
	50.725	0.696	1535	252.2	(382)	1.3071	28.831	1888		4400	1 047	A 78163	17 AE/	0 1050	255.0	22 245	150 A		
	COMBUSTOR	ď	24	17 4					C.CE1	4175	14703	0.34152	11000	0.1450	2000	22.265	13010		
	52,825	68.700			(726)	1.3014	28.631	2488											
	52.825	5.087	1455	230.8	360)	1,3516	28.831	1841	2.350	4290	1,967	0.27991	17.054	0.2379	2584	18,660	151.5		
	COMBUSTOR		25		•	- •	•												
	53.325						28.831												
	53.325				(355)	1.3528	28.831	1829	2.359	4315	1.968	0.26847	17,054	0.2460	2591	18.002	151.9		
	COMBUSTOR 54.075		26 2740		7 7 7 7 3	1 2017	28 824	2/18/1											
	54,075						28.831			4347	1.940	0.25307	17.054	0.2631	2600	17,096	152.4		
	COMBUSTOR		27		5 3417	113344	200001	1013	21310	7341	41707	4455501	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	4.6507.	2000	. 1 3 0 7 0	* ~ * * ~		
	54,835	64.753			(722)	1.3019	28,831	2482											
	54,835	4.064		212.3	(342)	1.3557	28,831	1799	2.429	4371	1.970	0.23932	17.054	0.2782	2607	16,257	152.8		
	COMBUSTOR		28																
	55.760	62.604		592.51	(720)	1,3021	28.831	2480	n "Łn						5448	46 90.04			
	55.760 COMBUSTOR		59		(330)	1,35/0	20.031	1100	2 0 0 7	4343	1.7/2	0.22470	118054	0,2703	2012	15.341	129.5		
	56.260				7491	1.3021	28.831	2478											
	56,260									4478	1,979	0.18102	17.054	0.3678	2640	12.599	154.8		
	COMBUSTOR		30	23 4	·			,					• •				•		
	56,315						28,831										_		
3	56,315	5.810	1305	190.6	(350)	1,3608	28.831	1748	2,563	4480	1.979	0.18045	17.054	0.3690	2640	12.562	154.8		
3	COMBUSTOR		31		. 7.0.	1 7000	20 624	2/170						-					
Ş	56.455 56.455						28,631			anso	1.070	0.17915	17.054	0.3717	2641	12.479	150.A		
!	COMBUSTOR		32		25.7	14200,	201021	1,40	CEDMI		*****	0	*1 #0 #4	V # 3 1	4441	*****	*>=10		
,	56,535	56,424	2734	591.3	(719)	1,3022	28,831	2478											
	56.535	2.810	298	189.6	(319)	1.3610	28.831	1745	2.569	4484	1.978	0.18116	17.054	0.3675	2641	12,623	154.9		
	COMBUSTOR		33																
	56,815	56.594	2733	590.9	(718)	1.3022	28 831	2477	0 674			0 45054	4 % A C //	0 11/04	2422	43 607			
	56,815 COMBUSTOR		34		(310)	1.5013	50.027	1742	2.510	4408	14419	0.18056	17*054	0.5666	6046	12.593	124.4		
	57,041	_			7181	1.3023	28.831	2477											
	57.041									4491	1.978	0.18029	17.054	0.3693	2643	12.582	155.0		
	COMBUSTOR		35		• •		•	•		•							- • •		
	57,765						28.831					_							
	57.765				(314)	1.3621	28,631	1734	2,595	4500	1.977	0.17742	17.054	0.3753	2645	12.407	155.1		
	COMBUSTOR		36	_	. 7.4.	. 70.2	20 uz-	2024											
<u> </u>	58.785 → 58.785						28,631			4504	1.974	0.17630	17.05/	0.1177	2646	12.345	155.5		
	COMBUSTOR	0			(-1r)	112061	201031	1150	F # 0 0 0	- 2v0	44770	A411030	118034	V # 3	2040	*****	73765		
Ç	0 60.795				(713)	1,3028	28,631	2470											
•	60.795						28.831												
									2.590	4484	1,975	0.18243	17.054	0.3650	2657	12,714	154,6		

	Þ	7	н		GAMMA	MOLHT	SONV	MACH	VEL	১	-/4	4	A/AC	HOMIM	o.	IVAC	PHI	ETAC
► COMBUSTOR	> 0	38	31 5															
CD 62.215	50,302	2712	584.7(712)	1.3029	28.831	2468											
C 62.215									4467	1.974	0.18738	17.054	0.3553	2651	15.008	154.2		
COMBUSTOR	₹ (J		32 4	•		-		-				•	• -					
64,679	53,651	2704	582.3(710)	1.3031	28,831	2465											
64.679	2.776	1294	188.7(318)	1.3612	28.831	1743	2,546	4438	1.976	0.17761	17.054	0.3749	2619	12.250	153.6		
COMBUSTOR	ŧ u	40	33 3										• -					
↑5• 0\$5	49.674	2702	581,9(7101	1.3032	28,831	2464											
65.055	2.586	1296	189.16	318)	1.3611	28.831	1744	2.542	4434	1.984	0.16512	17.054	0.4032	2617	11.377	153.5		
- NOZZLE A	\E	41	34 3									-						
87.291	49.674			710)	1,3032	28,831	2464											
87.291	0.234	668	31.7(161)	1.3957	20,831	.1599	4.139	5247	1.984	0.03437	17.054	1.9371	2898	2.603	169.9		
NOZZLE F	90	42	35 3					-					•			-		
87.291	49.674			710)	1.3032	28.831	2464											
87.291	0.247	678	34.2(164)	1.3953	28.831	1277	4.099	5235	1.984	0.03563	17.054	1.8687	2893	2.899	169.7		
PICTIVE C	COMBUSTR	65	55 0					_										
65.055	189,740	2702	581,9(710)	1,3032	28,831	2464											
65.055	0.247	463	-17.9(112)	1.3991	26,831	1057	5.184	5478	1.891	0.05460	17.054	1.2194	2981	4,649	174.8		
FICTIVE N	VOZZLE	63	56 O															
67.291	58,888			709)	1.3033	28.831	2463											
87.291	0,216	951	20,3(150)	1.3970	28.831	1223	4.332	5297	1.972	0.03437	17.054	1.9371	2915	2.830	170.9		

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XABS	PalB	Р•ОВ РО	A GOX		Q=18	Q=08	CAWALL	P+IH/PSO	P=IH/PTO	P#G8/P80	P#08/P10
6.981E=01	6.750E=01		766E=01 0.00		0.900	0.000	2.470E+02	2.73UE 00	1.4278-03	0.000	0.000
1.8368 01	6.750E=01		47E 01 0.00		0.000	0.000	1.634E 02	2.730E 00	1.427t=03	0.000	0.000
3.070E 01	1.405E 00		68E 02 0.00		0.000	0.000	5.053E V2	5.6826 00	2.9106-03	0.000	0.000
3.508E 01	2.486E 00		29E 02 0.00		0.000	0.000	6.804E 02	1.006E 01	5,256£ 03	0.000	0.000
3,519E 01	2.491E 00	3.640E 00 #2.7		-	0.000	0.000	6.854E 02	1.007E 01	5.2666-03	1.4728 01	7.695E=03
3.520E 01	2,491E 00	3.623E 00 -2.7		0	0.000	0.000	6.857E 02	1.007E 01	5.2068.03	1.465E 01	7,699E=03
3.555E 01	2.505E 00	2.635E 00 =2.7			0.000	0.000	7,209E 02	1.013E 01	5.296E-03	1.066E 01	5.5716=03
3.586E 01	2,483E 00	1.750E 00 =2.8	170E 02 #2.02	3E 02	2 -2.023E 0.	2 0.000	7,529E 02	1.0048 01	5.250E=03	1.078E 00	3.700E=03
3.606E 01	2.470E 00	2.169E 00 =2.9	127E 02 =2.04	SE 02	2 +2.045E 0	2 0.000	7.729E 02	9.990£ 00	5.2221-03	8./74E 00	4.587E=03
3.648E 01	5.666E 00	3.072E 00 -3.0	35£ 02 - 2.04	SE 0	2 -2.095E 0	2 0.000	8.164E 02	1.076E 01	5.6365-03	1,242E 01	6.495E=03
3.701E 01	2,605E 00	4.211E 00 =3.1	79E 02 -2.26	5E 0	0 3161.5m	2 -1.041E 01	8.726E 02	1.054E 01	5.507£#03	1.703E 01	8.903E#U3
3.732E 01	2.559E 00	4.887E 00 -3.2					9.063E 02	1.035E 01	5,410E=03	1.977E 01	1.033E=02
3.803E 01	2.455£ 00	8.197E 00 =3.3					9.634E 02	9.929E 00	5,190E=03	3.315E 01	1.733E=02
3.834E 01	3.500E 00	9.675E 00 -3.3					1.0186 03	1.318E 01	6.845F=03	3,913E 01	2.045E=02
3.875E 01	4.295E 00	9.804E 00 =3.3					1.064E 03	1.737E 01	9.001E=03	3.965E 01	2.073E=02
3,881E 01	4.461E 00	9.825E 00 =3.3				_ * *	1.072E 03	1,804E 01	9,432E=03	3.974E 01	2.0775-02
3.901E 01	4.9608 00	9.882E 00 =3.3					1.094E 03	5.000F 01	1.0491-02	3.997E 01	2.0895-02
3.932E 01	8.367E 00	9.9756 00 =3.3					1.130E 03	3,384E 01	1.769E=02	4.034E 01	2.1095002
3.950E 01	1.026E 01	7.553E 00 =3.3					1.150E 03	4.151E 01	2.1706=02	3.055E 01	1.597E=02
3.981E 01 4.000E 01	1.082E 01	3.200E 00 =3.5 3.112E 00 =3.6					1.187E 03	4.577E 01 4.511E 01	2.288E=02 2.358E=02	1.294E 01 1.258E 01	6.765E=03 6.579E=03
4.040E 01	1.3215 01	3.921E 00 a3.8					1.256E 03	5.342E 01	2.793E=02	1.181E 01	6.1756#03
4.041E 01	1.326E 01	2.916E 00 =3.8					1.257E 03	5.363E 01	2.8036-02	1.179E 01	6.165E=03
4.13 E 01	1.789E 01	2.487E 00 -4.5					1.363E 03	7.233E 01	3.781E-02	1.006E 01	5.2586=03
4.137E 01	1.822E 01	2.456E 00 =4.6					1.371E 03	7.369E 01	3.8526=02	9.9342 00	5.193E=03
4.150E 01	1.886E 01	2.678E 00 =4.7					1.386E 03	7.629E 01	3.9886-02	1.083E 01	5.662E=03
4.246E 01	7.125E 00	4.379E 00 -5.1					1.501E 03	10 3586.5	1.506E=02	1.771E 01	9.257E=03
4,409E 01	9.824E 00	7.275E 00 -5.2					1.699E 03	3.973E 01	2.0776-02	2.9428 01	1.538E=U2
4.4318 01	1.018E 01	7.157E 00 =5.2	608 02 =6.32	7E 02	2 ≈3.871E 0	2 -2 456E 02	1.725E 03	4.117E 01	2.1526#02	2.895E 01	1.513E=02
4,480E 01	1,099E 01	6.889E 00 =5.3					1.785E 03	4.444E 01	5.236-05	2.786E 01	1.4566=02
4 4 4 8 1 E 01	1:09BE 01	6.883E 00 =5.3					1.786£ 03	4.442E 01	2.322E=02	2.784E 01	1.4556-02
44656E 01	1.047E 01	6.089E 00 -5.4					1.964E 03	4.241E 01	2.2176-02	2.463E 01	1.2876-02
4.731E 01	1.01 SE 01	5.514E 00 -5.4					2.094E 03	4.095E 01	2.141E=02	2.230E 01	1.1662=02
4./33E 01	1.002E 01	5.500E 00 =5.4					2.097E 03	4.054E 01	2,119E=02	2,224E 01	1,163E=02
4.8112 01	6.900E 00	6.148E 00 =5.3					2.194E 03	3.791E 01	1,4596=02	2.486E 01	1.300E=02
4.878E 01	6.711E 00	6.711E 00 -5.1					2,2788 03	2.7146 01	1.4196-02	2.714E 01	1,4198=02
4.931E 01 5.072E 01	7.154E 00 3.219E 00	7.154E 00 =4.9 3.219E 00 =4.5					2.345E 03 2.522E 03	2.893E 01 1.302E 01	1.513E=02 6.805E=03	2.893E 01 1.302E 01	1.513E=02 6.805E=03
	3.937E 00	3.937E 00 #4.1					2.789E 03	1.592E 01	8.325E=03	1.592E 01	8.3251-03
5.335E 01	3.750E 00	3.750E 00 04.0					2.852E 03	1.517E 01	7.9281-03	1.517E 01	7.926E+03
5.407E 01	3 079E 00	3,0795 00 -3.9					2.948E 03	1.245E 01	6.5116-03	1.245E 01	6.5115-05
5.483E 01	2.400E 00	2.400E 00 a3.7					3.046E 03	9.707E 00	5.0746.03	9,707E 00	5.074E=03
5.576E 01	2.102E 00	2.1028 00 =3.6					3.164E U3	8.502E 00	4.444E=03	8.502E 00	4.444E=03
5.626E 01	1.941E 00	1,941E 00 =3,4					3.209E 03	7.851E 00	4.104E+03	7.851E 00	4.104E=03
5.631E 01	1.462E 00	1.9235 00 -3.3					3.216E 03	5.915E 00	3.092E-03	7.779E 00	4.067E=03
5.645E 01	1.4626 00	1.878E 00 =3.3					3,234E 03	5.915E 00	3,092E=03	7.597E 00	3.971E+03
5.653E 01	1.853E 00-	1,8538 00 -3.3	179E 02 =1.29	9E 03	96,277E 0	S #6.711E 02	3.245E 03	7.493E 00	3.917E-03	7.493E 00	3.917E=03
5.681E 01	1.762E 00	1.762E 00 =3.3					3.280E 03	7,128E 00	3.726E=03	7.128E 00	3.7262-03
5.704E 01	1.B71E 00	1.871E 00 =3.3					3.309E 03	7,568E 00	3,956E=03	7.568E 00	3.956E#U3
5.776E 01	5.550E 00	2.220E 00 -3.2					3.402E 03	8,979E 00	4.6938=03	8,979E 00	4.693E=03
5.878E 01	2.625E 00	3.025E 00 =3.2					3.532E 03	1.062E 01	5 550E-03	1.062E 01	5.550E=03
6.079E 01	1,5756 00	1.975E 00 =3.2					3.790E 03	6.370E 00	3.330t=03	6.370E 00	3.330E=03
6.221E 01	1.106E 00	1.1068 00 =3.2					3.972E U3	4.474E 00	2,3396-03	4.474E 00	2.339E=03
6,468E 01	2.061E 00	2.061E 00 =342					4.289E 03	8.336E 00	4.358E-03	8.336E 00	4.358E=03
6,505E 01	2.850E 00	2.2075.00 -3.2					4.337E 03	1.153E 01	6.0256=03	8.926E 00	4.666E=03
6,509E 01	2,850E 00	2.222E 00 03.2	1818 05 a1.40	nc 03	96.160E 0	€ =7.838E 02	4.342E 03	1.153E 01	6,0256=03	8.989E 00	4,6996=03

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V.)

	ZABS	P+I8	P=0B	PDA	G O X	GeIB	90=0	CAWALL	P#16/P80	L-15/014	0.00.700	
فجط	6.529E 01	2.693E 00	-							F=LB/PTO	P=08/PSU	P+06/PI0
င်ာ			ENDOUG VU	-345675 /	E -184035 03	001/15	02 #7.862E 02	4.368E U3	1.089E 01	5.693L003	4.302E 00	4,8632#43
N	6.695E 01	1.390E 00	3.400E 00	•2.939€ (5 +1*4PRE 03	#6.044 <u>F</u>	02 -8.038E 02	4.5035 03	5.622E 00	2.9396-03	1.375E 01	7.1886.03
	6.7628 01	1.260E 00	2.437E 00	-2.511E (2 =1.497E 03	3668168	20 3501.80 SO	4.665£ 03	5.095F 00	2.663E+03	9.858E 00	5.153E=03
	6.839E 01	1.110E 00	1.852F 0a	#2-067E (2 m1-507F 07	-6-BARE	02 -8.179E 02	4.760E 03	4 4898 00			
	6.911E 01	9,2866-01	L. Thee na	_1 7795	3 m4 C14C AT		05 -01/70 02		•	2.347E+03	7.491E 00	3,916E=03
			193036 00	41912 C	E attator of	MU-204F	02 #8.259E 02	4.848E 03	3.756E 00	1.963E#03	5.278E 00	2.759£=03
	6.972E 01	7.750E=01	TOUCAE DO	#1*211E (2 -1.5458 03	=6.717E	02 -8.330E 02	4.922E 03	3.134E 00	1.6382.03	4.970E 00	2.598E=03
	7.067£ 01	6.717E=01	1.110E 00	-1.218E (2 *1.558E 03	#6.933E	02 -8,443E 02	5.036E 03	2.717E 00	1.420E=03	4.489E 00	2.347E=03
	1.110E 01	6.250E=01	1.002F 00	-1.099F	2 41.5436 01	-4.930E	02 -8.491E 02	5.088E 03	2.528E 00			
	7.263E 01	8.162E=01	8.000= 01	-7 (075	4 -4 6606 42	0007345	02 40,471C 0E			1.321E=03	4.214E 00	2.203E=03
	7.278E 01		O COUNTROL	WIND TO THE	1 -1.0094 03	#01.42AF	02 =8.626E 02	5.273E 03	3.301E 00	1.726E=03	3.236E 00	1.691E=03
		8.350E=01	1.050Em01	#0:757t (1 =1.560E 03	-6.76UE	02 =8.637E 02	5,290E 03	3.377E 00	1.765E-03	2.851E 00	1.490E+03
	7.353E 01	0.565€ =01	2.300E#01	□4.817E (1 =1.567E 03	06.968E	02 #8,7028 02	5.374E 03	2.695E 00	1.388E-03	9.302E=01	4.863E=04
	7.354E 01	6.556E#01	2.2756-01	#4.770F C	1 -1-567# 03	MA-948E	02 #8.702E 02	5.375E 03	2.651E 00	1 306E=03		,
	7.486E 01	3.400E=01	0.000	- 1 7 I A E	1 mi EMDE A	-4 Goan	02 -8 4746 02			,,,	9 199E=01	4.809E#04
	7.771E 01	1.750E=01		7 4004	1 -100056 03	08 70 VE	05 #8,8366 05	5.427E 03	1.375E 00	7.188E-04	0.000	0.000
			0.000	445.00AF	1 =1.540E 01	07.000E	02 -8.458E 02	5.525E 03	7.078E=0:	3.700E=04	0.000	0.000
	8.161E 01	S-600E=01	0.000	■1.759E (1 =1.547E 03	•7.018E	02 98.456E 02	5.630E 03	1.052E 00	5.497E=04	0.000	0.000
	8.442E 01	2,850E=01	0.000	#1.153E (1 mi.472E 03	a7.033F	02 -7.684E 02	5.684E 03	1.1536 00	6.025E=04		
	8.728E 01	3.400E=01	0.000	-1.00#F	0 -1.0705 01	-1.0400	02 -7.684E 02				0.000	0.000
	8,729E 01	3.401E=01		- 7 ADDE	A -14414E 03	2/1000E	A 41.004E A	5.707E 03	1.375E 00	7,188E=04	0,000	0.000
	~ # · # 7 # V &	20401C-01	0.000	43.4456 (O -1-414F 03	■7.060E	02 -7.684E 02	5.707E 03	1.376E 00	7.191E=04	0.000	0,000

×	UDRAG	CDRAG	CF	нс
4.041E 01 4.137E 01 4.137E 01 4.137E 01 4.137E 01 4.137E 01 4.2409E 01 4.431E 01 4.480E 01 4.480E 01 4.480E 01 4.731E 01 4.731E 01 4.731E 01 4.731E 01 4.731E 01 5.731E 01 6.731E 01	7.839E 01 1.208E 01 1.008E 01 1.008E 01 1.008E 01 1.008E 01 1.008E 00 1.1370E 01 1.137E 01 1.137E 01 1.127E 01 1.127E 01 1.127E 01 1.127E 01 1.127E 01 1.127E 01 1.127E 00	7.89182EEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEE	33333333333333333333333333333333333333	2.9200000000000000000000000000000000000
5.631E 01 5.645E 01 5.653E 01 5.661E 01 5.704E 01 5.776E 01 5.878E 01	2.087E=01 5.236E=01 3.017E=01 1.053E=00 8.473E=01 2.473E=00 3.740E	2.202E 02 2.208E 02 2.211E 02 2.231E 02 2.230E 02 2.257E 02 2.257E 02	2,354E-03 2,352E+03 2,345E-03 2,337E-03 2,331E-03 2,316E-03 2,305E-03	6.761E=03 8.687E=03 8.757E=03 8.694E=03 6.655E=03 6.457E=03 8.348E=03
6.079E 01 6.221E 01 6.468E 01 6.505E 01 6.509E 01 6.529E 01 6.695E 01	7.446E 00 5.397E 00 9.262E 00 1.340E 00 1.372E=01 6.777E=01 5.597E 00	2.368E 02 2.422E 02 2.518E 02 2.538E 02 2.530E 02 2.537E 02 2.593E 02	2.304E=03 2.303E=03 2.336E=03 2.366E=03 2.356E=03 2.352E=03 2.337E=03	8.630E=03 8.869E=03 8.545E=03 6.093E=03 7.912E=03 7.818E=03 7.555E=03
6.762E 01 6.839E 01 6.911E 01 6.972E 01 7.067E 01 7.110E 01 7.263E 01 7.278E 01	1.935E 00 1.931E 00 1.526E 00 1.127E 00 1.616L 00 6.900E=01 2.362E 00 2.150E=01	2.612E 02 2.631E 02 2.646E 02 2.658E 02 2.674E 02 2.704E 02	2.287E=03 2.242E=03 2.166E=03 2.166E=03 2.119E=03 2.119E=03 2.119E=03	6.221E=03 5.259E=03 4.243E=03 3.904E=03 3.564E=03 3.360E=03
7.353E 01 7.354E 01 7.486E 01 7.771E 01 8.161E 01 8.442E 01 8.728E 01 8.729E 01	8.700E=01 1.358E=03 3.973E=01 5.500E=05 5.237E=01 3.197E=01 1.456E=01 0.000	2.715E 02 2.715E 02 2.719E 02 2.725E 02 2.730E 02 2.735E 02 2.735E 02	2.014E.03 2.013E.03 1.966E.03 1.854E.03 1.899E.03 1.922E.03 1.922E.03	2.007E=03 2.081E=03 1.702E=03 1.023E=03 1.370E=03 1.462E=03 1.662E=03

			RAMJET PERF	ORMANCE			
18	ENGINE PERCORMANCE	•			INLET		
4	•				INCET		
	MEASURED IMPUST	#285.	(LBF) (LBF#SFC/LBM)	MASS FLOW RATION ADDITIVE DRAG (K	0.9855	(DEGREES)
	MEASURED THRUST COEFFICIENT	.1794 .2325		TOTAL PRESSURE	RECOVERY - SUPERSUNIC RECOVERY - SUBSUNIC. 1FFICIENCY - SUPERSON	U.0747 C V.4011	(PSI)
	REGENERATIVE COOLED ENGINE PERFO			INLET PROCESS E	EFFICIENCY = 8UB8ONIC. EFFICIENCY = SUPERSON	0.9059	
	STREAM THRUST	9809.	(LRF)	KINETIC ENERGY	EFFICIENCY - SUBBONIO - SUPERSONIC	0.8856	(RTUZERM)
	SPECIFIC IMPULSE	2109.	(LBF=SEC/LBM)	ENTHALPY AT PO	- SUBSONIC	29,15	(BTU/LBM)
	MOMENTUM AND FURCES				CUMBUSTUR		
	INLET FRICTION DRAG	78.4 467.0 174.4 7.92 =116. 20.62	(LBF) (LBF) (LBF) (LBF) (LBF)	EQUIVALENCE RAT COMBUSTOR EFFIC TOTAL PRESSURE COMBUSTOR EFFEC	TIO	0,000 0,000 0,000 0,2618	
	NOZZLE PRESSURE INTEGRAL	298. 318.			NOZZLE		
	EXTERNAL PRESSURE INTEGRAL TOTAL EXTERNAL DRAG	27.80 =640. =668. 7.92 =597. 1550.	(LBF) (LBF) (LBF) (LBF) (LBF)	NOZZLE COEFFICI	THRUST COEFFICIENT = (IENT = CT ENCY EFFICIENCY	0,9650 1.0477	
	STATIONS				FUEL INJECTORS		
	COWL LEADING EDGE	34.884 0.3146 40.400 35.199 73.539 87.291 56.455 65.055	CIN) CIN) CIN) CIN) CIN) CIN) CIN)	INJECTORS 10 10 10 20 20 30 30 4	8TATION 40.400 41.300 44.300 48.775 46.250 54.065 56.250 44.800	VALVE	

t = 275.25 sec.

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SUPHARY REPORT

00							V W	, ,, ,,	., .		J							
C)	P	T	н		CAMMA	MOLPT	VAUS	мася	VFI	S	+/4	Hr.	A/AC	MONTH	Q	* 1. 4 e	PHI	ETAC
	WIND TUNNEL	1	0 5		() IV	11.00	9	11,00	1-6	3	. , , ,	•	*/*6	In Day 1	ų.	TAHP	LUT	C I # C
	0.000 471.249			7051	1.2941	28.831	2585											
	0.000 0.247			081	7087	28 83	0.00	5 000	E027	1 050	0.06733		4 4055	2 4 0 0	4 400	407 0		
	SPIKE TIP NS	ž	0 4	403	143707	201031	707	2.440	2763	11024	0.00133	10.404	0.4625	2140	6.198	101.0		
		_		W . C .														
			507.4((93)	1.2939	28.621	2505											
	0.000 10.226	2454		774)	1.2961	28.631	2556	0 404	1032	2.110	0.06733	16,989	0.9852	3125	1.080	184.0		
	WIND TUNNEL	3	0 0															
	U.000 471.249	2994	669.4(795)	1.2941	28.831	2585											
	0.000 0.238	401	□32,8 (97)	1,3987	28.831	984	650.6	5928	1.859	0.06564	16.564	0.9852	3112	6.047	187.9		
	SPIKE TIP NS	4	0 0					-			•		•					
	0.600 11.350	2994	669,4(705)	1.2939	28.831	2585											
	0.600 10.289	2928						0.391	1001	2-116	0.06564	16.564	0.0852	5112	1.021	187.9		
	INLET THROAT	5	0 3		• • • • • •						.,	,		* ~	****	**1*/		
	40.400 183,599	2931	650.30	7773	1.2960	28.831	2550											
	40.400 9.950		226.01	1:91	1 3527	28.431	(22)	2 517	// A O B	1 010	0.59543		A 444#	2747	42.638	480 0		
	INLET UPNESK	- 4	0 3	-3-7	* * * * * - 1	201031	1031		4000	***10	V & 37343	104 404	041114	2111	46.030	13444		
	40.400 183.599	2931	450-31	7-71	1.2960	28.88.	2550											
	40.400 8.545							3 460	4400		0 64470							
	INLET DNNRSK	1500	6 - 1 - 5 (2411	1.3300	F0 * 62 1	1141	E . 0 V 7	4007	1.410	0.54130	10.404	0.1225	2743	39.431	101.5		
	40,400 77,685	2011	480 74			no na.												
			650.3(1777	1,2700	\$0.031	5224						_					
			DE0 . U (7473	7.5445	59 921	2518	0.484	1521	1.977	0.54130	16.989	0.1225	2743	10.358	161.5		
	COMBUSTOR		1 21															
	40,410 154,266		653.1(001)	1,8484	27.489	2000											
	40.410 9.152		224.3(375)	1.3535	27,489	1880	2.463	4632	2.005	0.59764	17.054	0.1114	2716	43.021	159.3	0.13	0.07
	O ROTEUR O	200	2 21												• .			
	41.298 115.108				1,3023										•			
	41.298 11.513			434)	1.3470	26.333	5014	2,164	4358	2.087	0.60094	17.114	0.1112	2646	40.703	154.6	0.26	0.04
		10	3 51			_												
	41,308 123,502		656,8(799)	1,3042	26,289	2618											
	41.308 11.539		277.7(422)	1.3497	26,289	1989	2,190	4356	2.079	0.60111	17,114	511110	2645	40.688	154.6	0.26	0.01
		11	4 21															• -
	41.373 122.824	2773	656,51	796)	1.3046	26,283	2616											
	41.373 11.712	1554	280.86	423)	1.3496	26,283	1992	2.177	4336	2.079	0.60178	17.114	0.1110	2640	40.555	154.2	0.26	0.00
	COMBUSTOR 0	12	5 21		- •		•							•	.,	40.00	-,	-,
	41.500 119.877	2770		796)	1.3047	26.282	2615											
	41.500 . 12.219	1579	288.41	430)	1.3483	26.282	2007	2.137	4289	2.080	0.60179	17-114	0.1110	2629	40.107	153.6	N-26	0.00
	COMBUSTOR O	13	6 21										*****	846			4120	
	42.460 100.987	2753		7001	1,3052	26.282	2607											
	42.460 9.354		274.21	4 6	1.3508	26.281	1977	7.195	4346	2-004	0.59615	19 114	0 4134	2677	40 211	457 4	n 54	0.00
		14	7 21	-,	*****	401401	4 - 1 1		4340	68071	0437013	1.4112	041151	0211	40,211	10010	V . CO	0 4 9 0
	44.093 96.470			7001	1.3062	26.384	2501											
	44.093 14.450		125.7/	4.8	1 3/121	24 286	3097	1 001	IDEA	3 401	a 57544	. ~		0877				
		15	8 3	7007	1.9467	201203	2003	19401	3434	20041	0.57541	1/,110	0.1161	2230	35,405	148.5	0.25	0 # 0
	44.310 92.762			7083	4 3048	24 734	24.07											
	44.310 15.376		637.20	447	1.3040	EGRAET	2003											
	~		9 4	4011	1,3304	200367	erto	1.930	2647	2.047	0.57498	17,114	0.1163	2529	34.764	147.8	0.26	0.03
	44.800 83.758	16 28//4		4.0	1 7000	24 000	1470											
				0101	1 2 2 0 0 0	CD 0 440	2034											
	44400 TIENDU	1,420	352.1(240)	1,5505	C0 • 440	4515	1,693	5745	4.115	0.57225	17.114	0.1168	2515	33,309	146.9	0.26	0.13
		17		0.0-														
	44.808 83.621	4000	632.40	0141	1.2000	66.442	6639			_								
	44.808 17.495	1.424	352.4(541)	1.3304	26.442	2213	1,691	3743	2.113	0.57208	17,114	0.1168	2514	33,278	146.9	0.26	0.13
	COMBUSIUM 0	18	11 7												- "			
	46.250 65.888	2730	636.3(867)	1.3071	23.682	2737											
	46.250 23.176	5155	424.5(657)	1.3278	23.682	2432	1,358	3255	2,509	0.54478	17.285	0.1239	2484	27.560	143.7	0.61	0.09

MIMOM IVAL PHI ETAC A/A A/AC GAMMA MOLHT SONV MACH VEL S 0 19 12 2 COMBUSTOR 46.260 65.818 2733 636,2(868) 1.3070 23.685 2738 23.215 2126 424.7(658) 1.3277 23.685 2434 1.335 3253 2.309 0.54448 17.285 0.1239 2485 27.525 143.7 0.61 0.09 46.260 COMBUSTOR 0 20 13 59.586 2976 623.5(950) 1.2954 23.949 2829 47.310 27.351 2482 447.6(776) 1.3116 23.949 2600 1.141 2967 2.339 0.50665 17.285 0.1332 2527 23.362 146.2 0.61 0.20 47.310 COMBUSTOR 0 21 14 47.333 59,529 2979 623,2(951) 1,2952 23,452 2830 27.472 2488 448.3(778) 1.3116 23.952 2603 1.157 2959 2.339 0.50644 17.285 0.1333 2527 23.288 146.2 0.61 0.20 47.333 COMBUSTOR 0 22 15 48.110 56.232 3137 614.4(1004) 1.2874 24.130 2885 28,168 2679 449,1(842) 1,3028 24,131 2682 1,072 2876 2,355 0,47210 17,285 0,1430 2576 21,099 149,1 0,61 0,27 46.110 0 23 16 COMMUSTOR 48.773 54.122 2744 621.4(962) 1.3074 21.464 2883 21.230 2191 408.4(750) 1.3264 21.465 2594 1.259 3265 2.521 0.43950 17.471 0.1552 2617 22.299 149.8 0.99 0.12 48.773 COMBUSTOR 0 24 17 48.783 54.086 2746 621.3(962) 1.3073 21.466 2883 21.190 2191 407.9(751) 1.3263 21.466 2595 1.259 3268 2.521 0.43892 17.471 0.1554 2618 22.289 149.8 0.99 0.12 48.783 COMBUSTOR 0 25 18 49.313 52.397 2820 616.4(990) 1.3037 21.540 2913 19.067 2215 362,5(758) 1.3245 21.540 2602 1.315 3421 2.531 0.41050 17.471 0.1662 2669 21.823 152.8 0.99 0.14 49.313 COMBUSTOR 0 26 19 46,873 3102 604,5(1095) 1,2902 21,811 3021 50.723 16.994 2453 348.6(843) 1.3122 21.812 2709 1.321 3578 2.566 0.34986 17.471 0.1950 2791 19.454 159.8 0.99 0.23 50.723 COMBUSTOR 0 27 20 52.823 43.924 3240 589,4(1146) 1.2830 21.967 3067 11.887 2400 257.9(820) 1.3119 21.969 2670 1.526 4073 2.582 0.28675 17.471 0.2379 2936 16.149 168.0 0.99 0.28 52.823 COMBUSTOR 0 28 21 53,323 41,619 3361 586,3(1191) 1,2767 22,085 3108 12.117 2544 260,1(872) 1.3052 22.089 2734 1.478 4040 2.595 0.27503 17.4/1 0.2480 2964 17.269 169.6 0.99 0.31 53,323 COMBUSTOR 0 29 54.073 40.794 3397 581.8(1205) 1.2747 22.128 3119 10.979 2528 234.5(865) 1.3052 22.133 2722 1.531 4168 2.599 0.25925 17.471 0.2631 3003 16.795 171.9 0.99 0.32 54:073 COMBUSTOR 0 30 40,430 3403 577,3(1207) 1,2742 22,144 3120 54,633 9,825 2474 206.7(844) 1,3069 22,149 2694 1,599 4307 2.600 0.24516 17.471 0.2782 3039 16.409 173.9 0.99 0.33 54.833 COMBUSTOR 0 31 24 55,760 39,180 3455 572,3(1226) 1,2713 22,204 3136 9.052 2488 185.2(848) 1.3055 22.210 2696 1.632 4401 2.605 0.23016 17.471 0.2964 3077 15.741 176.1 0.99 0.35 55.760 COMBUSTOR 0 32 25 56,258 30,542 3861 569,7(1381) 1,2461 22,603 3253 8.037 2965 192.2(1024) 1.2830 22.627 2891 1.503 4346 2.652 0.18538 17.471 0.3679 3174 12.522 181.7 0.99 0.47 56.258 COMBUSTOR 0 33 26 56,313 35,273 3531 569,5(1255) 1,2668 22,282 3159 0.640 2432 129.1(826) 1.3064 22.290 2662 1.703 4694 2.619 0.18486 17.471 0.3690 3176 13.485 181.8 0.99 0.37 56,313 COMBUSTOR 0 34 27 56.453 35.161 3538 568.8(1258) 1.2664 22.290 3161 0,581 2434 126,4(826) 1,3062 22,299 2663 1,767 4705 2,620 0,18353 17,471 0,3717 3181 13,419 182,1 0,99 0,37 56.453 COMBUSTOR 0 35 28 6 56,533 31,132 3846 568,4(1375) 1,2472 22,591 3249 8.408 2921 180.4(1007) 1.2848 22.613 2873 1.534 4406 2.649 0.18559 17.471 0.3675 3184 12.708 182.3 0.99 0.47 56,533 COMBUSTOR 0 36 29 56,813 31,558 3832 567.0(1370) 1.2481 22.580 3245 8.175 2862 169.8(992) 1.2864 22,602 2856 1.561 4459 2.647 0.18497 17.471 0.3688 3193 12.617 182.8 0.99 0.46 56,813 COMBUSTOR 37 30 0 57.039 32.371 3785 566.0(1352) 1.2513 22.536 3232 7./95 2794 155.1(959) 1.2902 22.555 2819 1.609 4534 2.642 0.18462 17.471 0.3695 3200 13.009 183.1 0.99 0.45 57.039

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GAPMA MOLHT SONV MACH VEL 8 4/4 AZAC MUNIM D IVAL PHI ETAC COPBUSTOR 0 38 51 4 57.763 35.342 3612 562.6(1285) 1.2620 22.375 3182 57.763 6.570 2491 110.4(846) 1.3031 22.386 2685 1.772 4757 2.623 0.1817/ 17.4/1 0.3753 3215 13.436 184.0 0.99 0.40 COPBUSTOR 0 59 32 58.783 59,917 2993 558,6(1052) 1.2940 21.815 2971 58,783 3.675 1515 2.5(499) 1.3504 21.816 2160 2.443 5275 2.529 0.18060 17.471 0.3777 3220 14.806 184.3 0.99 0.23 - COPBUSTOR 0 40 33 60.793 33.074 4076 551.3(1463) 1.2302 22.863 3302 60.793 9,650 3253 190,3(1131) 1,2681 22,907 2992 1,420 4250 2,661 0,18689 17,471 0,3650 3210 12,344 183,7 0,99 0,55 COMBUSTOR 0 41 34 3 62,213 30.513 4091 545.9(1468) 1.2290 22.891 3304 10.150 3293 194.1(1146) 1.2661 22.936 3006 1.396 4196 2.659 0.19195 17.471 0.3593 3202 12.516 183.3 0.99 0.56 62.213 COMBUSTOR 0 42 35 u 64.677 27.632 4221 535.7((518) 1.2173 25.052 3329 64.677 11.030 3554 226.5(1247) 1.2515 23.114 3093 1.267 3920 2.672 0.18195 17.471 0.3749 3188 11.085 182.5 0.99 0.61 COMBUSTOR 0 43 36 4 25.044 4343 533.9(1565) 1.2084 23,185 3351 65.053 65.053 11.607 3805 271.9(1344) 1.2352 23.264 3169 1.145 3621 2.685 0.16915 17.471 0.4032 3186 9.519 182.3 0.99 0.66 COMBUSTOP REGEN 44 37 21 05.053 25.044 4516 633.9(1637) 1.1929 23.125 3403 65.053 9.516 3836 287.6(1357) 1.2313 23.258 3178 1.310 4163 2.708 0.16915 17.471 0.4032 3243 10.943 185.6 0.99 0.66 NOZZLE AE 45 38 87.289 25.044 4343 533.9(1537) 1.2054 23.185 3351 87.250 0.698 2068 -423.0(674) 1.3076 23.300 2402 2.881 6920 2.685 0.03521 17.471 1.9371 4104 3.787 234.9 0.99 0.66 NOZZLE PO 46 39 87,289 25.044 4343 533.9(1537) 1.2054 23.185 3351 87.289 0.247 1609 -585.2(511) 1.3290 23.300 2136 3.503 7483 2.685 0.01732 17.471 3.9393 4313 2.014 246.9 0.99 0.66 NOZZLE AE REGEN 47 40 87.289 25.044 4516 633.9(1637) 1.1929 23.125 3403 87.269 0.736 2227 =364.9(731) 1.3012 23.299 2486 2.843 7070 2.708 0.03521 17.471 1.9371 4204 3.869 240.6 0.99 0.66 NOZZLE PO REGEN 48 41 87.289 25.044 4516 633.9(1637) 1.1929 23.125 3403 87.289 0.247 1717 -547.7 (549) 1.3234 23.300 2202 3.492 7689 2.708 0.01667 17.471 4.0915 4434 1.992 253.8 0.99 0.66 FICTIVE COMBUSTR 68 61 183.599 5194 533.9(1899) 1.1654 24.092 3534 65.053 65.053 0.247 1436+1143.6(437) 1.3255 24.652 1959 4.677 9162 2.532 0.02515 17.471 2.7127 5147 3.580 294.6 0.99 1.00 FICTIVE NUZZLE 59 52 0 87.289 16.412 4278 506.4(1538) 1.2084 23.184 3324 87.289 - 0.854 2350 #319.1(777) 1.2965 23.299 2550 2.520 6427 2.715 0.03521 17.471 1.9371 3914 3.517 224.0 0.99 0.66

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XABS	P= I B	P⇔OU	PDA	ΧUΩ	O-IB		6 → 03		CAHALL	P=IB/PSU	P#18/P10	P=05/P8v	P=0B/P[0
6.981E=01		0.000	-2.766E=U1	0.000	0.000		0,000		2.470E=02	2.794E 00	1.464E#03	0.000	0.000
1.636E 01	6.900E=01	0.000	■2.296E 01	0.000	0.000		0.000		1.6346 02	2.794E 00	1.4646=03	0.000	0,000
3.070E 01	1.435E 00	0.000	#1.091E 02	U . 0 U O	0.000		0.000		5.053£ 02	5.810E 00	3.045E=03	0.000	0.040
3.508E 01	2.539E 00	0.000	-2,379E 02	0.000	0.000		0.000		6.804E 02	1.028E 01	5.387E=03	0.000	0.000
3.519E 01	2.550E 00	3.633E 00	#2.797E 02	0.000	0.000		0.000		6.853E 02	1.032E 01	5.410E=03	1.4718 01	7.7096=03
3.520E 01	2.550E 00	3.618E 00	-2.798E 02	0.000	0.000		0.000		6.856E 02	1.033E 01	5.412E=03	1.465E 01	7.678E=03
3.555E 01	2.585E 00		-2.843E 02		0.000		0.000		7.210E 02	1.047E 01	5.485E-03	1.123E 01	5.885E+03
3.586E 01	2.551E 00		=2.919E 02			5 0 2	0.000		7.528E 02	1.033E 01	5.414E-03	6.199E 00	4.297E+03
3.606E 01	2,530E 00		-2.973E 02				0.000		7,730E 02	1.024E 01	5.3698-03	9.792E 00	5.132E-03
3.648E 01	2.707E 00		#3.078E 02						8 166E 02	1.096F 01	5.744E=03	1.318E 01	6.910E=03
3.701E 01	2.810E 00		*3.228E 02					0.1	8 725E 02	1.138E 01	5,963E=03	1.747E 01	9.153E+03
3.732E 01	2.716E 00	4.937F 00	-3.311E 02	-2.339E	02 -2.197	- 02	-1.420F	01	9.062E 02	1.100E 01	5.764E+03	1.999E 01	1.048E-02
3.803E 01	2.505E 00	8-309F 00	-3.416E 02	#2.513F	02 02.2031	7 02	-2.198F	01	9.835E 02	1.014E 01	5.316E=03	3.364E 01	1.763E=02
3.834E 01	3.490E 00	9-8009 00	-3,412E 02	-2.543F	02 -2.3400	. 02	-2 STAF	0.1	1.018E 03	1.413E 01	7.406E-03	3.968E 01	2.080E=02
3.875E UI	4.772E 00		=3,420E 02					01	1 064E 03	1.932E 01	1.013E=02	4.038E 01	2.116E=02
3 . 60 1E 01	4 969E 00		₩3.421€ UZ						1.0726 03	2.012E 01	1.055E-02	4 049E 01	2.122E#U2
3.901E 01	5.590E 00	1.0136 0	-3.418E 02	₩2.7MOE	12 -2.455	7.5	-3 -3635	01	1.094E 03	2.2635 01	1.186E=02	4-100E 01	2.149E=02
3.932E 01	8.821E 00	1.032F 0.	=3.451E 02	#2.876F	NO -5-5176	. ^2	-1.55JE		1.130E 03	3.572E 01	1.872E=02	4-181E 01	2.191E=02
3.950E 01	1.065E 01		-3.500E 02						1.151E 03	4.312E 01	2.2608#02	3.383E 01	1.773E#02
3.981E 01	1.104E 01		-3.631E 02					οi	1.187E 03	4.471E 01	2.343E=02	1.974E 01	1.0346=02
4.000E 01	1 127E 01		-3.725E 02						1.209E 03	4.565E 01	2.393E-02	1.963E 01	1.0292+02
4.040E 01	1.346E 01	4.793F GA	#3.936E 02	a1.250F	12 = 2.7786		ma.7455	01	1.256E 03	5.449E 01	2.856E=02	1.9418 01	1.0178+02
4.041E 01	1.351E 01	4.7915 00	≈3,941€ 02	43.254E	12 -2.7616		0/1 723E	01	1.2978 03	5.471E 01	2.8676-02	1,940E 01	1.017E#02
4.130E 01	1.836E 01	4 667# 00	-4.521£ 02	*3.742F	12 -1-0416	. ^5	-7.010F	01	1.362E 03	7.434E 01	3.896E-02	1.890E 01	9.903E=03
4 . 13; E 01	1.841E 01		#4,528E 02						1.363E 03	7.456E 01	3.907E-02	1.889E 01	9.900E=03
4-137E 01	1 877E 01	4-656F A	-4.577E 02	-3-797F	12 -3-0646	, A >	-7. T.OF	01	1.371E 03	7.599E 01	3.963E=02	1.885E 01	9.881E=03
4.150E 01	1.946E 01		=4.671E 02						1.3866 03	7.880E 01	4 130E-U2	2.014E 01	1.0566-02
4.246E 01	1.132E 01	7.383E 00	-5.065E 02	-4.796E	2 43.4666	0.2	01.330F	دَه	1.501E 03	4 586E 01	2.403E=02	2 989E 01	1.5476=02
4.409E 01	1.742E 01	1.148F 0	■5.279E 02	ab.810E	2 ~4.3156	0.5	-2-47AF	02	1.6998 03	7.054E 01	3.697E=02	4.648E 01	2.436E+02
4.431E 01	1.823E 01	1.2526 01	95.324E 02	97.120E	12 24.4776		#2.601F	05	1.725E 03	7.383E 01	3.809E=02	5.069E 01	2.656E=02
4.480E 01	2.006E 01	1.4878 01	⊕5,411E 02	-7.924E	02 64.8208	20	-1-108E	02	1.785E 03	8.123E 01	4.257E=02	6.019E 01	3.155E=02
4.481E 01	2.009E 01	1 490E 0	-5.412E 02	=7.938E	12 -4.826	0.2	#3.112E		1.786E 03	8.133E 01	4.262E=02	6.034E 01	3.1636=02
4.625E 01	2.454E 01		-5.274E 02						1.963E 03	9.936E 01	5.207E-02	8.832E 01	4.629E=02
4.626E 01	2.457E 01		-5.269E 02						1.9648 03	9.949E 01	5.214E-02	8.851E 01	4,6396-02
4.731E 01	2.781E 01		-4.744E 02					02	2.094E 03	1.1268 02	5.9026-02	1.089E 02	5.706E=02
4.733E 01	2.7948 01		-4.7418 02						2.097E 03	1,132E 02	5.930E=02	1.093E 02	5.729E=02
4.811E-01	3.245E 01	2 389F 0	-4,183E 02	-1.455F	13 -7-0526	0.2	-7./195F	02	2.194E 03	1.314E 02	6.8865.02	9.672E 01	5.069E=02
4 877E 01	2.123E 01	2 1235 0	-3.502E 02	#1.573E	3 47.4556	60	#8.274F	02	2.2776 03	8.596E 01	4.505E-02	8.596E 01	4.505E+02
4.878E 01	2.119E 01	2.119E 0	-3.491E 02	=1.575E	3 -7.4616	0.2	#8.285E		2.278E 03	8.580E 01	4.497E=02	8 580E 01	4.497E=02
4.931E 01	1.907E 01		₽2.935E 02					ōZ	2.345E 03	7.720E 01	4.046E=02	7.720E 01	4.046E=02
5.072E 01	1.699E 01		-1.60ZE 02					03	2.522E 03	6.881E 01	3,606E=02	6.881E 01	
5.282E 01	1.189E 01		-1.201E 00						2.789E 03	4.813E 01	2.523E-02	4.815E 01	2.923E=V2
5.332E 01	1.2126 01	1.2126 01	3,000E 01					03	2.852E 03	4.906E 01	2.571E=02	4.906E 01	2.571E=02
5.407E 01	1.098E 01	1.098E 01	7.469E 01	#2.266E	3 m1.014F	03	a1.292E		2.9486 03	4.445E 01	2.330E-02	4.445E 01	2.3306=02
5.483E 01	9.825E.00	9.825E 00	1.150E 02	-2.343E	3 -1.045	0.3	#1.298E	03	3.045E 03	3.978E 01	2.0856-02	3.978E 01	2.085E-02
5.576E 01	9.052E 00	9.052E 00	1.589E 02	#2.432E	3 -1.080F	03	#1.352E		3.165E 03	3.665E 01	1.921E-02	3.665E 01	1.921E=02
5.626E 01	8.637E 00	8.637E 00							3.209E 03	3.497E 01	1.833E=02	3.497E 01	1.833E-02
5.631E 01	4.686E 00	5.592E 00	3.606E 02	-2.481E	13 -1.098	7.3	-1.383F	03	3.216E 03	1 898E 01	9.947E=03	3.479E 01	1.823E=02
5 645E 01	4.688E 00	8.475E 00	2.6612 02	#2.493E	03 -1.1026	0.3	-1-390F	03	3.234E 03	1.8986 01	9 947£=03	3.432E 01	1.798E=02
5,653E 01	8.408E 00	8.4082 00	2.695E 02						3.245E 03	3.405E 01	1.784E=02	3.405E 01	1.784E=U2
5.681E 01	8.1752 00	8-175F 0n	2.803E 02	#2.523F	03 -1.11%	0.3	=1.410=	03	3.280E 03	3.310E 01	1.735E=02	3.310E 01	1.735E+02
5.704E 01	7.793E 00	7.793E 00	2,881E 02					03	3.309E 03	3.155E 01	1.6846-02	3.155E 01	
5.776E 01	6.570E 00	6.570E 00	3.076E 02	#2.600F	3 -1-170	. 0%	-1.462E		3.402E 03	2.660E 01	1.394E=02		1.6545=92
5.878E 01	3.675E 00	3,6758 00	3.194E 02	#2.670F)3 miliant		- 4 3 4 U C C	0.3	3.532E 03	1.488E 01	7.798E=03	2.660E '01 1.488E 01	1,3946.02
6.079E 01	9.650E 00	9.650E-00	3.210E 02						3.790E 03	3.907E 01	2.048E=02	3.907E 01	7,798E=03
6,821E 01	1.015E 01	1,015E 01	3.2106 02	-2.892F	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	. 03	-10373E	ú š	3,972E Q3	4.110E 01	2.154E-02	4.110E 01	2,048E=02
· •				to a - i bit on i			10010	~ ~	-1.1-6 43	- F V - V - V -		-411AE 0]	2,1546=02

XABS	Pal8	P=0b	POA	QUX	6=18	G#08	CANALL	P=Ib/PSQ	P=18/P10	P=OB/PSO	P=08/PT0
6.46pE 01	1,103E 01	1.103E 01	3.210F 05	=3.071E 03	-1.291E 03		4.289E 03	4.466E 01	2.341E-02	4.468E 01	2.341E=02
6.505E 01	1.245E 01	1.116E 01	3,210E 02	-5.102E 03	-1.502E 03	-1.800E 03	4.537E U3	5.041E 01	2.6426-02	4.520E 01	2.369E=02
6.509E 01	1.245E 01	1.118E 01	3.210E 02	-3.105E 03	■1.303E 03	E0 3508.10	4.342E 03	5.041E 01	2.6426=05	4.526E 01	2.372E-02
6.529E 01	1.180E 01	1.125E 01	3.5106 05	-3,121E 03	•1.309E 03	■1.812E 03	4.368E U3	4.780E 01	2.505£#02	4.555E 01	2.387E#02
6.6958 01	6.450E 00	6.030E 00				•1.885E 03	4.5836 03	2.612E 01	1.369E=02	2.442E 01	1.280E=U2
6.7628 01	4.742E 00	5.820E 00	5.358E 02	-3,268£ 03	=1.358E 03	*1.911E 03	4,665E U3	1.920E 01	1.006E=02	2.357E 01	1.2356-02
6.839E 01	2.780E 00	4.427F 00				#1.940E 03	4.760E 03	1.126E 01	5.899k=03	1.795E 01	9,395E=03
6.911E 01	2.179E 00	3.125E 00				-1.969E 03	u•848E 03	8.823E 00	4.624E=03	1,265E 01	6.631E=03
6.972E 01	1.670E 00	2.601E 00				-1,493E 03	4.922E 03	6.762E 00	3.544E-03	1.053E 01	5,5196-03
7.067E 01	1.195E 00	1.785E 00				-2.027E 03	5.036E 03	4.839E 00	2,536E+03	7.228E 00	3.788E+03
7.110E 01	9.800E=01	1.643E 00				#2,041E 03	5.088E 03	3.9688 00	2.080£-03	6.655E 00	3.488E-03
7.263E 01	7.022E=01	1-140E 00				078€ 03	5,273E 03	2.843E 00	1.490E=03	4.616E 00	2,419E=03
7 278E 01	6.750E=01	1.013E 00				-2.081E 03	5.2908 03	2.733E 00	1.432E=03	4.103E 00	2.150E=03
7.3538 01	6.786E=01	3.800F=01	9.422E 02	-3,496E 03	i ∞1.3 98€ 03	=2.097E 03	5.374E 03	2.748E 00	1.4406=03	1.539E 00	8.064E+04
7.354E 01	6.786E=01	3.766E-01				#2.097E 03	5,375E 03	2.748E 00	1.4406-03	1.525E 00	7.9925-04
7.486E 01	6.850E=01	0.000	9.573E 02	-3,534E 0	01.403E 03	-2.131E 03	5.427£ 03	2.774E 00	1.4546-03	0 + 0 0 0	0.000
7.771E 01	1.175E 00	0.000				-2.131E 03	5.525E 03	4.758E 00	2.443E=03	0.000	0.000
8.161E 01	9.300E=01	0.000	1.040E 03	-3.554E 03	5 -1.424E 03	-2.131E 03	5.6302 03	3,766E 00	1.973E=03	0.000	0.000
8.442E 01	7.100E=01	0.000	1.058E 03	- -3,565€ 03	5 -1.434E 03	#2.131E 03	5.684E U3	2.875E 00	1.5076-03	0.000	0.000
8.728E 01	9.900E=01	0.000				+2-131E 03	5.707E 03	4.009E 00	2.1016-03	0.000	0,000
8.729E 01	9,906E=01	0.000	1.078E 03	■3,583E 03	5 =1.452E 03	-2.131E 03	5.707E 03	4.011E 00	2.102E=03	0.000	0.000

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4.040E 01 4.040E 01 4.131E 01 4.137E 01 4.137E 01 4.150E 01 4.246E 01 4.409E 01	8.117E 01 1.28E=01 1.222E 01 1.298E=01 8.181E=01 1.589E 00 1.211E 01 1.994E 01 2.496E 00	8.117E 0f 8.152E 01 9.355E 01 9.365E 01 9.446E 01 1.605E 01 1.082E 02 1.281E 02 1.306E 02	2,377E=03 2.711E=03 2.847E=03 2.618E=03 2.601E=03 2.647E=03 2.647E=03 2.703E=03	2.9/UE=02 2.695E=02 3.154E=02 3.154E=02 3.420E=02 3.510E=02 2.854E=02 3.729E=02 5.857E=02
4.480E 01 4.481E 01 4.625E 01 4.626E 01 4.731E 01 4.811E 01 4.871E 01 4.878E 01 4.878E 01	5.548£ 00 9.006E=02 1.659E 01 1.072E=01 9.901E=00 2.001E=00 6.742£ 00 9.000E=02 4.414E 00	1.361E 02 1.362E 02 1.528E 02 1.528E 02 1.628E 02 1.6498E 02 1.758E 02 1.758E 02	2.747E=03 2.829E=03 3.328E=03 2.983E=03 2.994E=03 3.144E=03 3.132E=03 3.037E=03 2.983E=03	4.0946=02 4.125E=02 4.125E=02 4.649E=02 4.649E=02 4.5573E=02 4.5573E=02 4.2633E=02 4.042E=02
5.072E 01 5.282E 01 5.327E 01 5.4872E 01 5.4872E 01 5.621E 01 5.623E 01 5.653E	1.083E 01 1.469E 01 3.364E 00 4.953E 00 4.913E 00 5.776E 00 1,893E 00 2.806E=01 7.311E=01 4.265E=01	911E 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2.929E=03 2.938E=03 3.048E=03 3.048E=03 3.030E=03 3.975E=03 3.151E=03 2.975E=03 3.415E=03	3.694E=02 2.857E=02 2.779E=02 2.500E=02 2.373E=02 2.029E=02 1.641E=02 1.719E=02 1.743E=02
5.681E 01 5.704E 01 5.776E 01 5.878E 01 6.221E 01 6.268E,01 6.505E 01 6.509E 01	1.49ZE 00 1.165E 00 3.781E 00 5.527E 00 9.824E 00 4.683E 00 1.213E 01 1.692E=01 8.605E=01	296E 022 207E 022 2.307E 022 2.4499E 022 2.4499E 022 2.703E 022 2.714E 02	3.139E-03 3.117E-03 3.032E-03 2.932E-03 2.680E-03 3.281E-03 3.281E-03 3.509E-03	1.859E=02 1.815E=02 1.653E=02 2.5348E=02 2.037E=02 1.969E=02 1.969E=02 1.948E=02
6.695E 01 6.762E 01 6.876E 01 6.972E 01 7.067E 01 7.110E 01 7.263E 01 7.353E 01	7.257E 00 2.662E 00 2.662E 00 1.712E 00 2.262E 00 2.262E 01 2.791E 00 2.791E 00 2.457E 01	22222222222222222222222222222222222222	3.368E=03 3.337E=03 3.24E=03 3.190E=03 3.15E=03 3.115E=03 3.058E=03 3.044E=03 2.970E=03	1.404E=02 1.327E=02 1.042E=03 7.280E=03 5.616E=03 5.113E=03 3.670E=03 2.506E=03
7.354E 01 7.486E 01 7.771E 01 8.161E 01 8.442E 01 8.728E 01 8.729E 01	1.546E=03 5:387E=01 1:313E 00 1:519E 00 6:738E=01 2:845E=01 0:000	2.953E 02 2.959E 02 2.959E 02 2.987E 02 2.997E 02 2.997E 02	2.969E=03 3.000E=03 3.003E=03 3.007E=03 2.954E=03 2.969E=03 2.969E=03	2.559E=03 3.118E=03 4.654E=03 3.679E=03 5.145E=03 4.045E=03 4.047E=03

92	LNGINE PERFORMANCE			INLET		
			MASS FLOW RATIO ADDITIVE DRAG COELIMITING PRESSURE DELTA PTZ TOTAL PRESSURE HE TOTAL PRESSURE RE	FFICIENT	0.9852 0.0005 0.1625 0.0748 0.3896	
	REGENERATIVE COLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	_BF)	INLET PROCESS EFF KINETIC ENERGY EF KINETIC ENERGY EF ENTHALPY AT PO =	ICIENCY - SUBSONIC FICIENCY - SUPERSONIC FICIENCY - SUBSONIC SUPERSONIC SUPERSONIC	0.9056 0.9344 0.8850 =4.90	
	MOMENTUM AND FURCES			COMBUSTOR		
	INLET FRICTION DRAG	LBF) LBF) LBF) LBF) LBF) LBF) LBF) LBF)	EQUIVALENCE RATIO COMBUSTOR EFFICIE TOTAL PRESSURE RA COMBUSTOR EFFECTI INJECTUR DISCHARG VACUUM STREAM THR NOZZLE COEFFICIEN PROCESS EFFICIENCE	NCY	0.988 0.655 0.1364 0.6568 0.7484,	0.7696. 0.6728
	R GDITAT8		F	FUEL INJECTORS		
	NOMINAL COME LEADING EDGE	(ÎN) (IN) (IN) (IN) (IN) (IN)	INJECTORS 1A 1B 1C 2A 2C 3A 3B	STATION V 40.400 41.298 44.300 48.773 46.250 54.063 56.248 44.798	ALVE A B D E	

t = 156.11 sec.

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9 1

SUMMARY REPORT

GAMMA MOLWT SONV MACH VEL S W/A A/AC M M 404 IVAC PHI ETAC MIND WONKER 0 5 747.999 2956 657.5(783) 1.2951 26.652 2568 0.366 397 -33.76 96) 1.3987 28.651 979 6.010 5881 1.825 0.10666 26,978 0.9875 5029 9.748 186.4 0.000 SPIKE TIP NS 2 0 5 0.600 18.112 2956 657.5(783) 1.2950 28,851 2568 0.6,00 16,376 2889 637.2(764) 1.2971 28.851 2541 0.397 1008 2.080 0.10666 26.978 0.9875 4987 1.670 184.9 WIND TUNNEL 747.999 2956 657.5(783) 1.2951 28.852 2568 0.000 0.000 0.380 396 =34.i(95) 1.3986 28.851 976 6.025 5883 1.823 0.10556 26.700 0.9875 4978 9.650 186.4 SPIKE TIP NS 0.600 18,112 2956 657.5(783) 1.2950 28.851 2568 0.600 16,417 2890 637.7(764) 1.2970 28.851 2542 0.392 995 2.080 0.10556 26.700 0.9875 4978 1.633 186.5 INLET THROAT 40,400 264.633 2927 648.8(775) 1,2960 28.851 2557 40.400 16.027 1449 229.2(358) 1.3518 28.651 1837 2.494 4582 1.687 0.94629 26.978 0.1113 4299 67.387 159.4 INLET UPNESK 40.400 284.633 2927 648.8(775) 1.2960 28.651 2557 214.2(344) 1.3551 28.851 1803 2.586 4663 1.887 0.86026 26,978 0.1224 4342 62.342 160.9 40.400 13.759 1392 INLET DNNRSK 40.400 122,955 2927 648.6(775) 1.2960 26.65; 2557 40.400 - 105.422 2826 -618.3(745) 1.2991 26.851 2515 0.491 1239 1.945 0.86026 26.978 0.1224 4342 16.510 160.9 COMBUSTOR 40.410 283.945 2927 645.8(775) 1,2960 28,851 2557 40.410. 16:047 1450 229.5(359) 1.3517 28.651 1838 2.492 4580 1.887 0.94617 26.978 0.1113 4298 67.349 159.3 COMBUSTOR 41.312 224.708 2920 646.6(773) 1.2962 28.881 2554 41.312 18.672 1597 266.8(398) 1.3436 28.881 1923 2.261 4348 1.903 0.94878 26.978 0.1110 4177 64.106 154.8 COMBUSTOR 0 10 41.377 220,912 2919 646,4(773) 1.2962 28,851 2553 41.377 18.881 1609 271.8(401) 1.3431 28.851 1930 2.244 4329 1.904 0.94881 26,978 0.1110 4167 63.836 194.5 COMBUSTOR 41.500 214.063 2918 646.0(772) 1.2963 28.851 2553 41.500 19,294 1630 277.5(407) 1.3420 28.851 1941 2.212 4294 1.906 0.94912 26.978 0.1110 4149 63.335 153.8 COMBUSTOR 0 12 42.460 186.164 2906 42.460 20.867 1715 642.4(769) 1.2966 28.851 2548 300.6(430) 1.3379 28.851 1986 2.080 4136 1.914 0.93974 26.978 0.1121 - 4067 60.400 150.7 COMBUSTOR 44.097 171.003 2882 635.1(762) 1.2974 28.851 2538 44.097 20,765 1734 305.7(435) 1.3371 28.851 1999 2.031 4060 1.917 0.90794 26.978 0.1160 4021 57.283 149.1 COMBUSTOR 0 14 44.310 169,418 2878 634.1(761) 1.2975 28.851 2537 44.310 20,821 1737 306,6(436) 1.3369 26.851 2000 2.024 4048 1.918 0.90624 26.978 0.1162 4015 57.017 148.8 COMBUSTOR 44.800 165.451 2871 632.0(759) 1,2977 28,851 2534 44.800 309.2(438) 1,3365 28.851 2005 2.004 4019 1.919 0,90263 26.978 0.1167 3998 56.378 148.2 21.004 1746 COMBUSTOR 0 16 44.812 165.319 2871 631,9(759) 1,2977 28,851 2534 21.015 1747 309.3(439) 1.3365 28.851 2006 2.003 4018 1.919 0.90261 26.978 0.1167 3997 86.362 148.2 44.812 COMBUSTOR 0 17 10 46.260 149.600 2852 626.3(753) 1.2983 28.651 2526 46.260 20.303 1763 313.8(443) 1.3358 28.851 2014 1.903 3955 1.924 0.85034 26.978 0.1239 3960 52,262 146.8 COMBUSTOR 0 18 11 47.310 137.334 2840 622.6(749) 1.2987 28.851 2521 47.310 19.008 1763 313.9(443) 1.3358 28.851 2015 1.951 3931 1.928 0.79120 26.978 0.1331 3944 48.330 146.2

PUPTH D GAMMA MOLWT SUNV MACH VEL S A/AC IVAC PHI ETAC COMBUSTOR 0 19 12 5 47.337 137.037 2840 622,5(749) 1.2987 28.851 2521 47.337 18,994 1764 314.0(443) 1.3357 28.851 2015 1.950 3929 1.928 0.79008 26.978 0.1333 3943 48.246 146.2 COMBUSTOR 0 20 13 5 48,110 129.768 2831 619.9(747) 1.2990 28.851 2517 48.110 17.458 1745 308.7(438) 1.3366 28.851 2005 1.968 3946 1.931 0.73724 26.978 0.1429 3947 45.209 146.3 COMBUSTOR 0 21 14 48.787 124.659 2824 617.8(745) 1.2992 28,851 2514 48.787 15,464 1704 297,8(427) 1,3384 28,851 1983 2,018 4001 1,933 0,67778 26,978 0,1554 3971 42.146 147.2 0 22 15 COMBUSTOR 49.317 121,892 2819 616,2(743) 1,2994 28,851 2512 49.317 13.955 1667 287.6(417) 1.3402 28.851 1962 2.067 4055 1.934 0.63389 26.978 0.1662 3994 39.948 148.1 COMBUSTOR 0 23 16 50.727 113,450 2806 612,6(740) 1,2997 28,851 2507 50.727 11.105 1594 267.9(397) 1.3438 28.851 1921 2.162 4153 1.938 0.54025 26.978 0.1950 4037 34.869 149.6 COMBUSTOR 52.627 102.170 2791 608.1(735) 1.3002 28.851 2501 52.827 8.482 1519 247.7(377) 1.3478 28.851 1878 2.261 4246 1.943 0.44279 26.978 0.2379 4077 29.221 151.1 COMBUSTOR 0 25 18 53:327 100.707 2788 607.1(734) 1.3003 28.851 2499 7,979 1499 242.3(372) 1,3489 28.851 1866 2.289 4272 1.944 0.42470 26.978 0.2480 53.327 4069 28,198 151.6 COMBUSTOR 0 26 19 54.077 98,478 2783 605,7(733) 1,3005 28,851 2498 54,077 7.329 1472 235.2(365) 1.3505 28.851 1851 2.327 4306 1.945 0.40034 26.978 0.2631 4104 26.790 152.1 COMBUSTOR 0 27 20 54,837 96.153 2779 604.4(732) 1.3006 28.651 2496 54.837 6.776 1448 229.0(358) 1.3518 28.851 1837 2.359 4334 1.946 0.37858 26.978 0.2782 4117 25.499 152.6 0 28 21 COMBUSTOR 93,186 2774 605,0(730) 1,3008 28,851 2494 55.760 55.760 6.225 1426 223.0(352) 1,3531 28,851 1823 2,392 4361 1,948 0,35550 26,978 0,2963 4129 24.091 153.0 COMBUSTOR 0 29 22 56.262 81.587 2772 602.4(730) 1.3008 28.851 2493 56.262 4.751 1374 209.4(359) 1.3562 28.851 1792 2.474 4434 1.957 0.28626 26.978 0.3679 4166 19,726 154.4 COMBUSTOR 0 30 23 56,317 81,491 2772 602,3(729) 1,3008 28,851 2493 56.317 COMHUS 4.733 1373 209.2(338) 1.3562 28.851 1791 2.476 4435 1.957 0.28546 26.978 0.3690 4166 19.676 154.4 TGINALI PAGE IS COMBUSTOR 0 31 24 56.457 81.198 2771 602.1(729) 1.3009 28,851 2492 56,457 4.688 1371 208.5(338) 1.3564 28.851 1790 2.480 4438 1.957 0.28341 26.978 0.3717 4168 19.547 154.5 COMBUSTOR 0 32 25 56,537 82,279 2771 602.0(729) 1.3009 28.851 2492 56.537 4,734 1369 208,1(337) 1.3565 28,851 1789 2.482 4440 1.956 0.28663 26.978 0.3675 4168 19.776 154.5 COMBUSTOR 0 33 26 56,817 82.455 2770 601.7(729) 1.3009 28.851 2492 56.817 4.700 1365 207.1(336) 1.3567 28.851 1787 2.487 4444 1.956 0.28563 26.978 0.3688 4170 19.725 154.6 COMBUSTOR 0 34 27 57.043 82,649 2769 601,4(729) 1,3009 28,851 2492 57.043 4.679 1362 206,3(336) 1,3569 28,851 1785 2,491 4446 1,956 0,28520 26,978 0,3693 417! 19.707 154.6 COMBUSTOR 0 35 28 57.767 82,317 2766 600,6(728) 1,3010 28,851 2490 57.767 4.568 1354 204.1(333) 1.3574 28.851 1779 2.504 4455 1.956 0.28068 26.978 0.3753 4174 19.431 154.7 COMBUSTOR 0 36 29 58.787 82.547 2763 599.6(727) 1.3011 28.851 2489 58,787 4.507 1346 202.0(331) 1.3579 28.851 1775 2.513 4460 1.955 0.27888 26.978 0.3777 4176 19.330 154.8 COMBUSTUR 0 37 30 83.750 2757 597.6(725) 1.3013 28.851 2486 60.797 60.797 4.711 1353 203.9(333) 1.3575 28.851 1779

2,495 4439 1,953 0.28859 26,976 0.3650 4163 19,910 154,3

GAMMA MOLNT SONV MACH VEL S A/AC MOMTH G IVAC PRI ETAC H/A COYBUSTOR 0 38 31 5 CD 62.217 84.610 2753 596,7(724) 1,3014 28,851 2485 O 62.217 4.882 1360 205.8(338) 1,3570 28.851 1783 2.480 4423 1.952 0.29641 26.978 0.3553 4153 20.373 153.9 COMBUSIOR 0 39 32 4 78.037 2746 594.7(722) 1.3016 28.851 2482 64.631 64.681 4.696 1371 208.7(338) 1.3563 28.691 1790 2.455 4395 1.957 0.26096 26.978 0.3749 4136 19.189 153.3 COMBUSTOR 0 40 33 65.057 72.273 2745 594.4(722) 1.3017 28.851 2482 65.057 4.374 1373 209.1(338) 1.3563 28.851 1791 2.451 4391 1.962 0.26120 26.978 0.4032 4133 17.823 153.2 NOZZLE AE 41 34 3 72.273.2745 594.4(722) 1.3017 28.851 2482 87.293 87.293 0.392 708 41.6(171) 1.3942 28.851 1305 4.031 5259 1.962 0.03438 26.978 1.9371 4604 4.444 170.7 NOZZLE PO 42 35 3 87.293 72.273 2745 594.4(722) 1.3017 28.851 2482 87.293 0.386 705 40.8(170) 1.3943 28.851 1302 4.044 5263 1.962 0.05378 26.978 1.9585 4607 4.399 170.8 FICTIVE COMBUSTR 61 54 65.057 484.633 2745 594.4(722) 1.3017 28.851 2481 65.057 0.386 477 -14.3(115) 1.3991 28.851 1073 5.144 5519 1.868 0.08328 26.978 1.2647 4753 7.143 176.2 FICTIVE NUZZLE 62 55 0 87.293 113.747 2724 587.9(715) 1.3024 28.851 2472 87.293 - 0.313 579 10.2(140) 1.3979 28.851 1181 4.554 5377 1.929 0.05437 26.978 1.9371 4664 4.544 172.9

XABs	P#18	P=OB	PDA .	QOX	⊍⇔រដ	9≈0	P	CAWALL	P#18/PS0	P#18/PT0	P#08/PS0	P=08/PT0
	•		-		-		-					
6.981E=01	1.040E 00	0.000	-4.412E=01	0.000	0.000	0.00	U	2,470E=02	2.695E 00	1.390t=03	0.000	0.000
1.836E 01	1.040E 00	0.000	-3.463E 01	0.000	0.000	0.00	C)	1.634E 02	2.695E UU	1.390E+03	0.000	0.000
3.070E 01	2.175E 00	0.000	-1.650E 02	0.000	0.000	0.00	'n	5.053E 02	5.636E 00	2.908E=03	6.000	0.000
3.508E 01	3.881E 00	0,000	□3.612E 02	0.000	0.000	0.00	U	6,804E 02	1.00bE 01	5.189E=03	0.000	0.000
3.519E 01	3.869E 00	5.696E 00	04.268E 02	0.000	0.000	0.00	0	6.855E 02	1.003E 01	5.172E=03	1.476E 01	7.615E=V3
3.520E 01	3.868E 00		50 3865.Pe	0.000	0.000	0.00		6.858E 02	1.002E 01	5.171E=03	1.467E 01	7.5685#03
3.555E 01	3.830E 00	3 010E 00	=4.341E 02	0,000	0.000	0.00	U	7.208E 02	9,9258 00	5.1206-03	9.356E 00	4,827£-03
3.587E 01	3.864E 00	1.750E 0n	₩4.489E 02	□1.040E □	02 -1.040E	02 0.00	0	7.530£ 02	1.001E 01	5.166£=03	4.5351 00	2.340E+U3
3.606E 01	3,885E 00	2.569F 0n	#4.595E 02	-1.051E	02 -1.0518	00.00	ñ	7.727E UZ	1.007E 01	5,194b=03	6.656E 00	3.454E=U3
3.648E 01	4,221E 00						-					
			#4.796E 02					8.164E 02	1.0948 01	5,643E=03	1.127E 01	5.8146-03
3.701E 01	4,205E 00	4.595E 00	-5.042E 02	=1.561E	05 =1*111E	02 =1.30	2E 01	8,722E 02	1.090% 01	5.622E+03	1.709E 01	8 ₄ 817€ ≈03
3.733E 01	4.070E UO		-5.155E 02					9.064E 02	1.055E 01	5.441E-03	2.057E 01	1.061E=02
3.803E 01	3.770E 00		-5.285E 02					9.832E 02	9.769E 00	5.040E=03	3.444E 01	1.777E=02
3.835E 01	5.199E 00		■5.261E 02					1.019E 03	1.347E 01	6,951E=03	4.068E 01	2.099E=02
3.8756 01	7.017E 00	1.529E 01	-5.251E 02	=1.603E	02 -1.261E	02 -4.22	4E 01	1.064E U3	1.8186 01	9,382E=03	3.963E 01	2.044E=02
3.882E 01	7.319E 00	1.522F 01	-5.250E 02	w1.704F	12 a1.271F	12 =4.32	7 F O 1	1.072E 03	1.897E 01	9.7856-03	3.945E 01	2.035E=02
3.901E 01	8,190E 00											
			-5.239E 02					1.094E 03	5.155E 01	1.095E=02	4.027E 01	2.078E=U2
3.933E 01	1.3628 01	1.006E 01	-5.281E 02	₽1.876E (02 *1.365E	02 =5.10	7E 01	1.130E 03	3,529E 01	1,821E-02	4.1628 01	2.147E=02
3.950E 01	1.659E 01	1.206E 01	m5.363E 02	-1.941E	02 -1.404E	02 =5.37	2E 01	1.150E 03	4.298E 01	2.218E=02	3.126E 01	1.613E002
3.982E 01.	1.710E 01		-5.603E 02					1.187E 03	4.431E 01	2.2866=02	1.231E 01	6.350E=03
4.000E 01	1.740E 01											
		4 9 0 1 4 5 0 0	≈5.777E 02	acetobe (15 010345F	05 =0 * 11	5F 01	1.2098 03	4.508E 01	5.350E-05	1.197E 01	6.176E=03
4.040E 01	5.096E 01	4+224E 00	66.170€ 02	□2.345E (32 -1.6728	Q2 ×6.73)E 01	1.256E 03	5.327E 01	2.748E-02	1.123E 01	5.794E=03
4.041E 01	2.064E 01	4.327E 00	50 3971.6 o	#2.350E (12 -1-675F	02 -6.70	SE 01	1.257E 03	5.348E 01	2.759E=02	1.121E 01	5.785E=03
4.131E 01	2.776E 01		₽7,235E 02					1.363E 03	7.194E 01	3.712E=02		4.9256-03
	•										9.546E 00	
4+138E 01	2,8286 01		=7.318€ 02					1.371E 03	7.327E 01	3,780E=02	9,426E 00	4,863E+U3
4.150E 01	2.925E 01	3.963€ 00	47.477E 0≥	™3.103E (02.080E	02 -1.02	1E 02	1.386E 03	7.580E 01	3.910E=02	1.027E 01	5.2986-03
4.246E 01	1.102E 01		-8.125E 02					1.501E 03	2.837E 01	1.474E-02	1.684E 01	8.689E=03
4.410E 01	1.449E 01		-8.296E 02					1.699E 03				
									3.754E 01	1.937E=02	2.805E 01	1.447E-02
4.4312 01	1.494E 01	1.00005 01	80.325E 02	* 0,305€ (32 #30277E	05 -205	1E 05	1.725E 03	3.871E 01	1.9976-02	2.767E 01	1.428E-02
4.480E 01	1,597E 01	1.034g 01	#8,408€ 02	≈0.878E ()2 a3.474E	02 =3.40	1E 02	1.784E 03	4.140E 01	2.136E#02	2.680E 01	1.363E=02
4.481E 01	1.598E 01	1.033F 0:	#8.411E 02	96.892F	12 -1.4705	A2 63.41	E na	1.786E 03	4.140E 01	2.136E+02	2.678E 01	1.382E-02
4.626E 01	1.610E 01	9.3300 04	-0 CZOC 02	-8 46¥E 4		AD - 0 77:	15 VE					
		763376 00	₩8.539E 02	#004U3E (15 m4 m 7 2 1 F	UE #4.3/	E V2	1.964E 03	4.172E 01	2.152E-02	2.420€ 01	1.249E=02
4.731E 01	1.619E 01		₩8,536E 02					2.094E 03	4.195E 01	2,164E=02	2.233E 01	1.152E-02
4.734E 01	1.6026 01	8,400Z 00	-8.538E 02	₩9.436E (D2 =4.415E	02 -5.02	E 02	2.097E 03	4.151E 01	2.141E=02	2.229E 01	1.150Ep02
4.811E 01	1.115E 01		-8.383E 02					2.194E 03	2.889E 01	1,491E=02	2.511E 01	\$043E95.1
4.879E 01	1.064E 01											
		TROOME OF	-8.058£ 02	ATSALES !	37 ACTOALE	05 43 05	IL VE	2.2786 03	2.758E 01	1.423E=02	2.758E 01	1.4236+02
4.932E 01	1.139E 01	1.139E 01	+7.754€ 02	*1.114E (03 =5:063E	02 #6.07	JE 02	2.345E 03	2,952E 01	1.523E=02	2.952E 01	1.5236-02
5 0738 01	4.575E 00	4.575E On	97.164E 02	=1.212E (3 #5.479E	02 -6.63	/E 02	5.555E 03	1.186E 01	6.110E=03	1.186E 01	6-116E=03
5.28 E 01	6.487E 00		-6.555E 02					2.789£ 03	1.681E 01	6,673E-03	1.681E 01	
5.333E 01	5.885E 00											8.673E=03
_	•		-6.394E 02					2.852E 03	1.525E 01	7.868E=03	1.525E 01	7.868E#03
5.408E 01	5.160E 00		a6,180F 05					2.948E 03	1,337E 01	6.898£#03	1.337E 01	6.898E#03
5.484E 01	4.425E 00	4.425E 00	95,995E 02	□1.431E (33 96,480E	02 =7.83	1E 02	3 046E 03	1.147E 01	5.916E=03	1.147E 01	5.916E=03
5.576E 01	3.603E 00		-5.809£ 02					3.164E 03	9.337E 00	4.817E+03	9.337E 00	
5.626E 01	3.157E 00											4.817E=03
		2012/5 00	95.417E 02	m1.40/g (13 BO + (45#	0% -0.15	E 02	3.209E 03	8.180E 00	4.220E-03	8,180E 00	4,220E=03
5.632E 01	1.875E 00	3.108E 00	-5,408E 02	D1.489E ()3 -6.754E	02 =8,13	1E 05	3.216E 03	4.859E 00	2.507£-03	8.053E 00	4-154E=03
5.646E 01	1.875E 00	2.983g On	a5.388E 02	●1.494E (3 -6.774E	02 98.16	20 9	3.234E 03	4.859E 00	2.507E=03	7.730E 00	3.988E=03
5.654E 01	2.912E 00	2.9125 04	₽5.376E 02	m1 - /1066 (3 nA 704E	02 28 17	בח ש	3 249E 03				
5.682E 01	5.662E 00	2.4426 04		- # # # 70G \		75 -U35	, V S.		7.545E 00	3.8936-03	7.545E 00	3,893E=03
			-5.340E 02					3.280E 03	6.899E 00	3,559E=03	6.899E 00	3,5 5 9E⊳03
5.704E 01	2.814E 00	2.814E 00	-5.313E 02	#1.512E (03 m6.856E	02 -6.26	1E 02	3.309E 03	7.292E 00	3.762E=03	7.292E 00	3.762E=03
5.777E 01	3.300E 00	3,300E 0n	∘5,230E 02	■1.534E (3 96.948F	02 -8-38	E 02	3.402E 03	8.551E 00	4.412E=03	8,551E 00	4.412E=03
5.879E 01	3.862E 00		-5.148E 02					3 532E 03	1.001E 01			
6.080E 01								. -		5.164E=03	1.001E 01	5.164E>03
	2.175E 00	201125 00	≈5.141E 02	-1.015E (12 #7 . E 32E	UE -0.88) # 0 %	3.790E 03	5.636E 00	2.908E=03	5.636E 00	2.908E=03
6.555E 01	1.481E 00	1.481E 00	-5.141E 02	-1.641E (03 ≈7.3 38E	02 -9.06	1E 02	3.972E U3	3.838E 00	1.980E=03	3.838E 00	1.980E=03
6.46BE 01	3.216E 00		-5.141E 02					4.289E 03	8.334E 00	4.300E=03	8.334E 00	4.300E#03
6.506E 01	4.462E 00	3.481E 04	-5.141E 02	-1.70%	7	U2 =0 %=	בת שו					-
6.510E 01	4.46ZE 00	3 E 000 0-	-48147E OF	- 1 4 1 1 2 C	/W = / 4 / / 4 L	VE -7.43	1 V G	4.357E 03	1.156E 01	5.966E+03	9.020E 00	4.654E=03
A STATE OF		SABOAR BO	-5.141E 02	MT9/045 (/> #/*3/8E	UC -46) L U Z	4.342E 03	1.156E 01	5.966E=03	9.093E 00	4.6916=03
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	XABS	PalB	P⇔OB	PDA	DUX	G=18	0⇔08	CAMALL	F-Ib/PSU	P#18/PT0	P+08/P80	P>UB/PTO
	6.530E 01	4.168E 00	3.650E 00	-5.14LE 02	#1.700E 03	-7.595E 02	9,488E 02	4.368E 63	1.080E 01	5,572E=03	9.458E 00	4.880E-03
	6.696E 01	1.720E 00					? -9. 703€ 02	4,5636 03	4.457E 00	5,299E=03	1.114E 01	5.7496-03
8	6.763E 01	1.808E 00					9.782E 02	4.665E,03	4.686E 00	2.418E+03	1.158E 01	5.976E=03
	6.840E 01	1.9105 00					9.878E 02	4.760E 03	4,949E 00	2,553E=03	8,423E 00	4.3456-03
	6.912E 01	1,601E 00					9,975E 02	4,848E 03	4,150£ 00	2,141E=03	5.468E 00	2.821E=03
	6,973E 01	1.340E 00	1.942E 00	=2.429E 02	-1.740E 03	#7.842E 02	! ■1.006E 03	4,922E 03	3.472E 00	1.791E=03	5.032E 00	2.596E=U3
	7.06BE 01	1.175E 00					1.020E 03	5.036E U3	3.044E 00	1.571E=03	4.353E 00	2.2466-03
	7.111E 01	1.100E 00					1.026E 03	5,088E 03	2.850£ 00	1.471E-03	4.149E 00	2.140E=03
	7.264E 01	1.047E 00	1.320F 00	■1.159E 02	-1.835E 03	-7.919E 02	-1.043E 03	5,273E U3	2,713E 00	1.400E=03	3.421E 00	1.765E=03
	7.354E 01	1.016E 00	3 . 100E=01	-8.136E 01	*1.845E 03	#7.936E 02	2 =1.052E 03	5.372E 03	2.635E 00	1.358E=03	8.033E-01	4.1446=04
	7.354E 01	1:016E 00	3.0556-01	-8.072E 01	■1.845E 03	₩7.936E 02	-1.052E 03	5.372E 03	2.632E 00	1,358E#Q3	7.9175-01	4.084E=04
	7.487E 01	9.700E=01	0.000				-1.068£ 03	5.424E 03	2.514E 00	1.297E=03	0.000	0.000
	7.772E 01	8.000E=01	0.000	-2,435E 01	■1.807£ 03	47.991E 02	-1.068E 03	5.523E 03	2.073E 00	1.070E=03	0.000	0.000
	8.162E 01	8,350E+01	0,000	1.058E 01	#1.870E 03	a8.050€ 0S	. ≈1.068E 03	5,628E 03	2.164E 00	1.116E=03	0.000	0.000
	8,443E 01	7.300E=01	0.000				*1.068E 03	5,682E 03	1.892E 00	9.759E=04	0.000	0.000
	8,729E 01	9.450E=01	0.000	4.818E 01	□1.8/6E 03	-8.083E 02	□1.068E 03	5.705E 03	2.449E 00	1.263E=03	0.000	0.000
	8.729E 01	9.455E=01	0.000	4.818E 01	#1.876E 03	-8.083E 02	01.068E 03	5.705E 03	2.450E 00	1.264E=03	0,000	0.000

	PERFORMANCE
ENGINE PERFORMANCE	INLET
CALCULATED THRUST	ANGLE OF ATTACK ************************************
CALCULATED THRUST COEFFICIENT	DELTA PT2
REGENERATIVE **COOLED ENGINE PERFORMANCE CALCULATED	INLET PROCESS EFFICIENCY - SUBSONIC 0.9039 KINETIC ENERGY EFFICIENCY - SUPERSONIC 0.9456
STREAM THRUST	KINETIC ENERGY EFFICIENCY = SUBSCNIC 0.8968 ENTHALPY AT PO = SUPERSONIC 24.77 (BTU/LBM) ENTHALPY AT PO = SUBSONIC 26.98 (BTU/LBM)
MOMENTUM AND FORCES	COMBUSTOR
INLET FRICTION DRAGE	FUEL-AIR RATIO
CAVITY FORCE	KINETIC ENERGY EFF1CIENCY 1.0256
STATIONS	FUEL INJECTORS
NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A 40.400 1B 41.302 1C 44.300 2A 48.777 2C 46.250 3A 54.067 3B 56.252 4 44.602

t = 167.81 sec.

202 SHEMARY REPORT

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S	p	Ŧ	ы	G A	444	ማርቪን T	SCHV	PALH	VFL	8	1/4	**	A/AC	46414	Q) r v C	PHI	ETAC
	WIND TUNNEL	1	0 5															
	0.000 748.249	3063	690.1(8)	15) 1.8	5918	28,852	2611		F 0 0	. D.7.4	0 1077/	26 020	0 0701	5117	9.999	190.1		
				01) 1.3	1989	28.851	1007	5,952	2441	1.034	0 - 1 11 / 24	23475"	V . 7 / 7 I	2111	,,,,,	* ' * 3 *		
	SPIKE TIP NS	2	0 3			50 UE4	1614											
	0.600 18.162	3063	690,1(8)	15) 1.4	9220	SE WEI	2542	0.40A	1053	2.090	0-10734	26.920	0.9791	4977	1.756	184.9		
	0.600 16.333		0 0	741 1.6	737	20.031	2002	4 3 4 11 6	1000	14 4 0 7 4			•					
	WIND TUNNEL 0.000 748.249	3063	R 11.09A	(5) 1.2	2918	28.852	2611											
	0.000 0.584	415		00) 1.	3989	28.851	1000	6.000	6000	1.834	0.10373	26,014	0.9/91	4948	9.676	190.2		
	SPIKE TIP NS	4	0 0	, ••				_										
	0 400 18 143	3063	690,1(8	15) 1,7	2916	28,851	2611								1 430	106.2		
	0.600 -16.471	2996	669.61 7	95) 1.7	2937	28,051	2584	0,391	1011	2,090	0.10373	25,014	0,9/91	HTHC	1,629	17005		
	INLET THROAT	5	0 4				3864											
	40,400 301,775	3024	678,2(8 37,0(3	04) 1.	2930	20,051	40CE	2 677	// 408	1.80%	0.94425	26.920	0.1113	4385	68.945	162.9		
	40.400 15.917		4314013	00) 1.	7201	E0 # 63 1	1022	64333	4070	11075	401-425				-			
	INLET UPNRSK 40.400 301.775	3024	678.2(8	041 1.	2930	28.651	2596											
	40.400 13.678			511	3534	28 851	1821	2.624	4778	1.893	0.85841	26.920	0.1224	4427	63.743	164.4		
	INLET DNMRSK	7	0 4	, -,														
	40,400 125,577	3024	678.21 8	04) 1.	2930	28,851	2596						4 . 55			(A) A		
	40,400 107,967			73) 1.	2961	28,851	2555	0.487	1244	1.953	0.85841	59.450	0.1224	4461	16.599	1944		
	COMBUSTOR 0	8	1 4			** **	2504											
			678.11 8 237.41 3	04) 1,	2430	20,001	£240	2 51+	11404	1.801	0.94413	26.920	1.1113	4384	68.907	162.8		
	40.410 15,936	9 91	2 21	0/) 1*	2200	20 6027	1626	6 5 3 3 1	20.0	190.0	V			•	•			
	COMBUSTOR 0 41.302 179.722	-	ABA DI B	501 1.	2972	26.508	2682											
	41.302 15.988			46) 1.	3440	26.508	2035	2,220	4516	2,062	0,45256	27.107	F.5111	0.654	60:859	157.2	0.24	007
	· · · · · · · · · · · · · · · · · · ·	10	3 2i															
	41.312 194.410	2585	686.21 8	28) 1.	3005	26.432	2656					65 . 45	. 4 4 19	#56B		107 1	n Dil	0.01
	41.312 16.024			24) 1.	3486	26.432	1992	2,266	4514	2.949	0.95333	27,197	. 110	46.54	66.576	13111	V P S. 3	0.079.4
		11	4 21		40.1	24 424	2152											
	41.377 194.018		685.9(8 282.2(4	1521 10	3011	26 441	1000	2.256	anga	2.048	0.95336	27.107	(-1110	4249	66.590	156.7	0.24	0.00
	41,377 16.254 COMBUSTOR 0	1204	5 21	1247 11	3407	ED ME 1	1775	CALSO	44/4	M K V - O	41,,,,,,							
	41,500 191.239		685.31 A	124) 1.	3012	26.419	2651											
	41.500, 17.876		295.1(4	(36) 1	3466	26.419	2018	2.190	4418	2.049	0.95367	27.107	0.1110	4231	65.485	156.1	0.24	0.00
		13	6 4															
	42,460 149,665	3027	679.76 8	371) 1.	2937	26,605	2709					24 4 19	0.4151	4.5.6.5	57.955	152.8	6.24	0.15
		2041	367.96 5	563) 1.	3267	26,606	2249	1.756	3949	2.081	0.44455	are ive	0.41121	4141	21872	12560	4 1 M 4	~ # • •
		14	7 5		547/	27 17/	2801								•			
	44.097 110.933		667.3(10	1001 1	2812	27.340	2691	1.092	2044	2-139	0,91229	27.107	0.1160	4108	41.771	151.6	0.24	0.75
		3127	8 2	27C2 44	Cott	# [# P ·· V	4 0,,								-	-		
	44,310 110,322		A65-5/10	058) 1.	.2632	27.342	2891											. ==
		3154		901) 1.	2802	27,349	2709	1,061	2875	2.139	0.91058	27,107	0.1162	4103	46°682	151.3	0.24	0.75
		16	9 3															
	44.800 109.17		661.2(10	051) 1,	2642	27.330	2884					77 167		/, O. J.	58.125	180.7	0.24	0.74
		3187		912) 1,	2792	27.336	2723	0,993	2705	∠,138	0.90695	6/11/1	04110/	4004	20.8165	4 - V = 1	0 \$ 4.4	7817
		17		0505 4	54.44	37 236	ים מכי	ı.										
	44.812 109.14	7 7146	561.1(10 515.0(ון ניכע י יונס	. 2043 . 2707	27.11	270°	2 2 0_001	5 2704	2.138	0.90694	27.107	0.1167	4083	38,113	150.6	0.24	0.74
		0 18		2 T T 3 Y (46173	E 1 4 5 3 3		·	1 - 7 "				• • • • •	•				
	46.250 102.60	9 3094	667.2(1)	0013 1	2916	23.732	289	i)										
	46.250 57.83	1 2712	527.84	864) 1	3042	23.73	272	2 0.97	2640	2.325	0.86459	27.416	· 0.(238	4064	35,477	149.0	0,63	0.19

	þ	r	н	t, p. ^ + &	21.F#1	¥ 402	~AL W	, • [5	./4	,	AZAC	wikla	r,	IIAL	Pal	ETAC
COMBUSTOR			15 8														
			667.1(1001)														
40.260			527+7(865)	1.3041	23.734	2723	0.979	5941	2,326	0.86413	27.411	r.1234	4065	35.465	144 + 5	0.63	0.19
COMBUSTOR			13 4														
47.310			657.0(1079)														
47,310			510.2(936)	1.2937	23,904	2602	0.967	2711	2.345	0.80494	27.416	0.1431	4217	33,671	153.8	C.63	n # 2 9
COMBUSTOR 47.337			14 2	1 5861	57 000	2011											
47,337			656.6(1081) 510.1(-938)				1 044	2740	2 1/14	0 00000	27 // 16	A 1777	1535	717	163 0	6 67	0 20
COMBUSTOR			15 4	196734	E3#77U	2004	W . 700	2117	C 1 D 4 C	0.00270	511416	• 1 2 2 2	4663	35,603	133.4	V . C .3	0,27
48.110			64966(1160)	1.2683	20.201	3042											
48.110	52.447	3131	487.4(1005)	1.2833	24.246	2870	0.993	2850	2.363	0.74920	27.416	0.1429	4348	33,187	158.6	0.63	0.39
COMBUSTOR	0	23	16 6		L 1 L			6020		011-720			4 D 44 4	233101	1 2 2 4 1		V#2/
48.777			660-1(1163)	1.2857	21.569	3100											
48.777	43.508			1.3021	21.571	2873	1.099	3158	2.549	0.69732	27.719	1.1552	4450	34,226	160.6	1.01	0.23
COMBUSTOR	0	24	17 2									_		•			- "
48.787			660.0(1164)	1,2856	21.572	3161											
48.787	43.397			1.3021	21.573	2874	1.101	3163	2.549	C.69641	27.719	0.1554	4453	30,234	160-6	1.01	0.23
COMBUSTOR		25				_											
49.317			656.1(1207)	1.5860	51.681	3139											
49,317	3/+267			1.2996	21,083	2878	1.193	3434	2,560	0.65131	27.719	0.1662	4558	34./63	164.4	1.01	C*59
COMBUSTOR 50.727			19 4		13 000	70.00											
50.727	77:45/	まのうと	646.6(1334)	1 2846	22.000	2044	1 242	7 4 / 5	2 501	0 15540	37 7.0	4 4 100	1. 4 n t	7		4 04	A 71
COMBUSTOR	219401	27	366.8(1066)	1.2003	KE . VI !	4704	1.503	3/42	21241	V,55504	21.114	0 - 1 130	4/70	32.279	1/240	1.01	0.30
52.827			634.5(1409)	1.2510	22.221	1207											
52.627	21.900	3600	254.6(1052)	1.2841	22.250	2935	1-476	4431	2.507	0.85496	27.719	h. 5 (79	5056	30.023	182.8	1 01	0 //2
COMBUSTOR	0	28	21 3	*****		کیر ۲ بدا		-201		01,134.0	-; ; ;	445211	2000	2010	IVERD	1.41	U g m gs
53.327			631.9(1416)	1.2498	22.246	3301						•					
53,327	20,275	2974	237.5(1041)	1.2847	22.265	2921	1.521	4442	2.609	0,4363/	27.719	1.2.80	5115	30.124	184.5	1.01	0.43
COMBUSTUR	0	29	25 4						_•-					- 1			
54.077			628.1(1437)														
54.077	18.400	2955	209,8(1032)	1.2847	22.312	2908	1,573	4575	2.012	0.41134	27,719	0.2:31	5181	29.245	186.9	1.01	0.44
COMBUSTOR			23														
54,637	71.738	\$941	624.4(1431)	1.2471	22.301	5310											
54,837 COMBUSTOR	19:200	5041	179.5(1007)	1.5006	55.252	2879	1.034	4718	5,513	0,38848	27,719	0.2702	5241	28,523	189 . 1	1.01	0.44
55,760		31	620.2(1453)	1 2017	22 167	2130											
55.760			150,9(1014)				1 - 671	4815	2.614	0.36527	27 714	7963	67.15	27 772	101 /		0 // 4
COMBUSTOR			25 5	110251		LUUL		-013	61014	01303[1	C. F. L.	V # 2 7 Q 3	2342	27,332	1 7 1 1 1	1 4 (-1	V . 40
56.262		4465	618.1(1635)	1.2041	22.849	3426											
56.262			164.2(1238)				1.545	4766	2.662	0.29413	27.719	0.3679	5478	21,783	197.4	1.01	0.62
COMBUSTOR			26 5	•				_				• • • • •	•			• • • •	
56,317	62.060	4117	617,9(1479)	1,2349	22,491	3352											
56.317	11.460	5008	97.6(1010)	1.2833	22,531	2870	1.779	5105	2.634	0.29330	27,719	0,3697	5481	23.276	197.7	1.01	0.50
COMBUSTOR			27 3														
56,457	61.851	4125	617.3(1502)	1.2343	22.501	3354											
56.457	11.364			7.5831	22.541	2871	1.752	5116	2,635	0.29119	27,719	0 3717	5449	23,152	198.6	1.61	0,50
COMBUSTOR		35			AA	2 /1											
56,53 <i>7</i> 56,537	22,210	1446	617.0(1628)	1.2098	22,032	2425					3						
COMBUSTOR	144195	3444	151+1(1217)	1.4009	55.442	3006	1 = 3 / 3	4828	6.029	0.29451	67.719	C + 3675	5495	55*048	190+≥	1.91	0.61
56,817			29 3	1 2113	שות ככ	*/1.0											
N 56.817	13.800	3464	615,9(1622) 134,4(1)99)	1.2561	22.010	4050	1.601	ARRI	J. 687	0 202/19	מוד דנ	0 74BH	6614	23 274		1 04	n 64
COPBUSTOR	0	37		4 4 5 7 1	(in # 7 * 7	2021	+ + 13 (1	403	5.40 1/	V167390	C 14 17 4		2211	22.271	40.8	1 * 0 1	h * & T
₩ 57.043			615.0(159h)	1,2165	22.753	5407											
57.043	13.079	\$279	120.7(1151)	1.265#	22.036	3005	1.654	4973	2.651	0.29303	27.719	1.3693	4522	22.647	194.5	1 - 0 4	0.58
				,								V 3 4 · 5	2066	~~•			-1 3 4- 0

ASAC MINIT ! IVAL PRI ETAD GEMAL APELL SONV LACH LEE S. 2/A " COMBUSTOP c 38 31 5 © 57.767 64.623 4132 612.2(1504) 1.234" 72.514 5355 57.767 10.770 2856 63.8(989) 1.2844 22.560 2844 1.462 5236 2.630 6.28439 27.714 0.3753 5546 23.477 200.2 1.01 0.51 COMBUSTOR 0 39 32 58.787 116.011 3409 608,8(1224) 1.2764 21.851 3148 58.787 5.925 1691 -60.57 563) 1.3337 21.034 2270 2.549 5787 2.533 0.28655 27.719 1.3777 5559 25.771 200.5 1.01 0.30 0 40 33 COMBUSTOR 52.351 4790 602.7(1763) 1.1790 23.230 3077 60.797 60.797 17.212 4024 185.1(1440) 1.2179 23.437 3224 1.418 4571 2.674 0.29652 27.719 (.4650 5547 21.465 200.) 1.41 0.76 COMBUSTOR 0 41 34 55.294 4663 598.0(1713) 1.1913 25.106 3457 62.217 62.217 16.294 3790 155.6(1346) 1.2355 23.263 3163 1.487 4705 2.664 0.30456 27.719 0.3553 5537 22.271 199.7 1.01 0.70 COMBUSTOR 0 42 35 6 47.698 5038 589.0(1861) 1.1553 23.523 3508 64.681 20.919 4551 257.3(1650) 1.1690 23.824 3332 1.223 4074 2.684 0.28868 27.719 0.3749 5519 16.277 194.1 1.01 0.92 64,681 COMBUSTOR 0 43 36 204 65.057 43.762 5118 587.4(1893) 1.1483 23.605 3518 65.057 21-162 4713 288-8(1716) 1-1554 23-915 3365 1-149 3866 2-688 0-26836 27-714 0-4032 5516 18-123 199-0 1-01 1-00 COMBUSTOR REGEN 44 37 4 45.057 43.762 5175 645.8(1918) 1.1465 23.522 3541 65.057 21.984 4796 357.5(1752) 1.1519 23.830 3395 1.118 5797 2.700 (.26838 27.719 (.8032 5582 15.835 199.9 1.01 1.00 NOZZLE AE 45 38 9 87.293 43.762 5118 487.4(1859) 1.1483 23.605 3518 87,293 1.438 3109 =577.3(1°53) 1.2533 24.447 2815 2.712 7634 2.688 G.05587 27.719 1.9371 7291 6.628 263.6 1.01 1.00 NOZZLE PO 46 39 5 87.293 43.762 5118 587.4(1859) 1.1483 23.605 3518 87.293 0.404 2376 -659.3(772) 1.2806 24.452 2487 3.421 8508 2.688 0.02287 27.719 0.7319 7820 3.024 282.1 1.61 1.00 NOZZLE AE REGEN 47 40 5 43.762 5175 645.8(1918) 1.1465 23,522 3541 87.293 87.293 1.476 3212 -534.8(1093) 1.2451 24.443 2852 2.695 7686 2.700 0.05587 27.719 1.9571 /354 6.673 265.5 1.01 1.00 NOTALE PU REGEN NO 41 87.293 43.762 5175 645.8(1918) 1.1465 23.522 3541 0.404 2449 -836.0(800) 1.2781 24.452 2523 3.409 8599 2.700 0.02242 27.719 4.8268 7908 2.996 285.3 1.01 1.00 87.293 FICTIVE COMBUSTR 67 60 65.057 301.775 5355 587.4(1988) 1.1653 23.861 3606 65.057 0.404 1502-1168.6(463) 1.3208 24.452 2008 4.668 9374 2.527 0.03986 27.719 2.7148 6357 5.807 301.5 1.01 1.00 FICTIVE POZZLE 68 61 87.293 23.157 5012 565.0(1849) 1.1438 23.546 3479 87,293 1.939 3659 -328.2(1273) 1.2024 24.370 2996 2.231 6685 2.738 0.05587 27.719 1.9371 6722 5.805 242.5 1.01 1.00

READING = 0	DOM HEREX :	= ()	11WE = 101.01;	្ត មេស្ភា ជ	SOU PI H 75	*3 * E A 2	10 74 1				,
XABS	P=18	P=CB	PDA	60 X	v#18	G⇒CB	CANALL	P-IA/PSu	P=15/PT0	P+08/PS0	P=08/PT0
6.981E=01	1.035E 00	n, unc	=4,430E=0	-	0.000	0,000	8.4/0E=02	2.565€ 00	1.3631-03	L.000	0.000
1.836E 01	1.035E 00	0.000	-3 447E C		0.000	0.000	1.6346 02	2.5658 00	1.383E-03	0.000	0.000
3.070E 01	2.190E 00	0.000	-1.652E 0		0.000	6.000	5.053E 02	5.427F 0v	2.9478#03	1 . 000	0.000
3,508E 01	3.889E 00	0.000	*3.622E (0.000	0.000	A. BOUE UZ	9.636E 00	5.1975=03	0,000	0.000
3.519E 01	3.878E 00		00 -4.302E 0		0.000	0.000	6.855E 02	9.6098 00	5.1838-03	1.474E 01	7.948E=03
3.520E 01	3.478E 00		00 -4.302E 0		0.000	0.000	6.85BE 02	9.608E 00	5.182£=03	1.465F 01	7.899E=03
3,555E 01	3.845E 00		00 m4.368E 0		0.000	0.900	7.208E 02	9.5288 00	5.139E-03	9.305E 00	9.019E=03
3.587E 01	3.870E 00		00 -4.513E U				7.530E 02	9.589E 00	5.1726-03	4.46PE 00	2.406E+03
3.606E 01	3.885£ 00		00 -4.618E 0				7.7275 02	9.627E CO	5,192t+03	6,460E 00	3.484E003
3.648E 01	4.222E 00		00 04.818E 0				8.164E 02	1.046E 01	5.643E-03	1.081E 01	5.A29E+03
3.701E 01	4.2256 00	6.576	00 -5.066F 0	201.9288	02 -1.783E	02 -1.408E 01	8.722E 02	1.047E 01	5.647E=03	1.630E 01	8.789E=03
3.733E 01	4.082E 00	7,9000	00 -5.181E C	92.0116	02 -1.817E	02 ml.937E 01	9.064E 02	1.012F 01	5,456E=03	1.958E 01	1.056E=02
3.8036 01	3.765E 00	1.327	01 -5.312E C	3041.5 ·	02 -1.8971	02 -2.992E 01	9.832E 02	9.3298 00	5.0326=03	3.288E 01	1.773E=02
3.835E 01	5.306E 00	1.569	01 -5.291E 0	3085.5m	02 =1.940E	02 =3.4625 01	1.019E 03	1.315E 01	7.091E+63	3.887E 01	2.097E=02
3.875E 01	7.266E 00		01 -5 292E 0				1.064E 03	1.800F 01	9.710E#03	3.784E 01	2.041E=02
3,882E 01	7.591E 00		01 45,293E 0				1.072€ 03	1.881E 01	1.014E=02	3.7668 01	2.031E=02
3.901E 01	8.530E 00		01 -5.289E 0				1.094E 03	2.114E 01	1.1406-02	3.860E 01	5.085E=05
3.933E 01	1.386E 01	1.6208	01 #5.338E D	2 .2.643E	02 -2.154E	05 =4.894E 01	1.130E 03	3.435E 01	1.853E=02	4.014E 01	2.1652.02
3.950E 01	1.677E 01	1.2388	01 -5.421E 0	2 -2.720E	3902.2- 20	02 -5.143E 01	1.150E 03	4.157E 01	2.2428=02	3.068E 01	1.655E=02
3.982E 01	1.727F 01	5,4008	0 45,656E 0	2 -2.873E	02 -2.314E	02 =5.590E 01	1.187E 03	4.278E 01	5.308E.05	1.338E 01	7.217E-03
4.000E 01	1.755E 01		00 -5.825E 0				1.209E 03	4.348E 01	2.345E=02	1.286F 01	6.9345.03
4.040E 01	2.085E 01	4.7278	2 00 -6.213E 0	2 -3.197E	02 #2.550E	02 =6.465E 01	1.256E 03	5.166E 01	2.787E-02	1.171F 01	6.318E=03
4.041E 01	2.093E 01		₹ 00 =6.222E 0.				1.2578 03	5,187E 01	2.798E=02	1.168E 01	6.302E#03
4.130E 01	2.829E 01					05 -1.0455 05	1.362E 03	7.010E C1	3.781E-02		4.927E+03_
4.131E 01	2.837E 01					02 -1.049# 02	1.3636 03	7.030E 01	3.792L=02	9.106E 00	4.911E#03
4.138E 01	2.891E 01					02 -1.097E 02	1.371E 03	7.163E 01	3.8645.02	8,9200 00	4.811E=03
4.150E 01	2.992E 01					02 =1.193E 02	1.306E 03	7.415E 01	3.999£=02 4.475E=02	1.444E 01 5.746E 01	7.789E=03 3.099E=02
4.246E 01	3.349E 01					02 #2.1978 02	1.501E 03	8.298E 01	7.571E-02	1.308E 02	7.0566-02
4.410E 01	5.665E 01					02 #4.356F 02	1.725E U3	1.478E 02	7.974E-02	1.319E 02	7.113E=02
4-431E 01	5,967E 01					02 #4,653F 02		1.0506 02	8.9016=02	1.343E 02	7.246E=02
4.480E 01	6,660E 01	D 4566	: 01 mc4400E 0	5 -1 -0H2E	03 mg 40/E	02 95,386E 02 02 95,405E 02		1.649E 02	8.8928=02	1.344E 02	7.249E+02
4.481E 01	6.653E 01 5.851E 01	5-7160	. 01 00 470 U	2 -1-4515	03 -4.68AE	02 97.826E 02	1.963E 03	1.450E 02	7,820E=U2	1.416E 02	7.638E+02
4.625E 01	5.846E 01	5.7175	01 07.772F 0	2 m1 . 454F	03 BA.697F	02 -7.844E 02	1.964E 03	1.4498 02	7.812E-02	1.417E 02	7.641E=02
4.731E 01	5.260E 01	9 93/1	7 01 -A. 310E 0	2 -1.7308	03 #7.5658	02 a9,735E 02		1.3036 02	7.030E-02	1.469E 02	7.9256=02
4.734E 01	5.265E 01					02 #9.783E 02		1.305E 02	7.036E-02	1.471E 02	7,9326002
4.811E 01-						02 -1-109F 03	2.194E 03	1.339E 02	7.7246002	1,2608 02	6.795E=02
4.8788 01	4.351E 01	4.3516	01 -3 430E 0	3970.50 5	03 =8.700E	02 m1.209E 03	2.277E 03	1.0788 02	5.815E-U2	1.078E 02	5.815Ep02
4.879E 01	4 340E 01	4.3408	01 -3 407E 0	2 -2.081E	03 -8.707E	02 #1.210E 03	2.278E 03	1.075E 02	5.800E=02	1.075E 02	5.800E>02
4.932E 01	3.757E 01					02 -1.280F 03		9.309E 01	5.051E=02	9.309E 01	5.021E=02
5.0738 01	3.148E 01	3.148	7 01 2.633E 9	1 -2.452E	93 -1.007E	03 -1.445E 03	S.255E 03	7,801E 01	4.2076-02	7,8019 01	4.207E=02
5.283F 01	2.190E 01	2.1908	E 01 3,2024 0	2 +2,789E	03 =1.137E	03 -1,652E 03		5.427E 01	2.927E=02	5.427E 01	2.927E=02
5.333E 01	2.0276 01	2.0276				03 -1.6968 03		5.024F 01	S.710E=02	5.024E 01	2.710E=02
5.408E 01	1 840E 01	1.849				03 =1.760E 03		4.5996 01	2.459E=05	4.559E 01	2.459E=02
5.484E 01	1.650E 01	1,650				03 -1.8235 03		4,089E 01	2.205E=02	4.089E 01	2.2056=02
5.576E 01	1.524E 01	1.5246				03 -1.8968 03		3.777E 01	2.637E=02	3.777F 01	2.0376=02
5.626E 01	1.456E 01	1.456				03 -1.9347 03		3.607E 01	1.945E=U2	3.607E 01	1.9456=02
3,632E 01	5.437E 00	1.4488	F 01 7,710E 0	2 -3,248E	03 m1.311E	03 -1.938E 03	3,216E 03	2.0915 01	1,1286+02	3.588E 01	1.9355+02
5.646E 01	8.037E 00	1.4298				03 *1.9485 03		2.091F 01	1,1285=02	3.541E 01	1.910Em02
5.654E 01	1.418E 01	1.418				03 =1.954F 03		3.514E 01	1.895E=02	3,514E 01	1,895E=02
5.682E 01	1.380E 01	1.3800				03 -1.975[04		3.420E 01	1 7085-02	3,420E 01	1.844E=02 1.748E=02
5,704E 01	1.308£ 01	1.508				03 #1,9915 03		3.2416 01	1.748E=02	3.241E 01 2.669E 01	1.4396.02
5.7778 01	1.077E 01	1+0770				03 -2.0445 03		2.669E 01	7.918t=03	1,4685 01	7.918E=03
5.879E 01	5.925E 00	5.925				03 -2.1075 03 03 -2.226F 03		4.265E 01	2.300E=02	4.265E 01	2.300E=02
6:0808 01	1.7216 01	1.7211				03 =2.319E P3	•		2.1786=02	4.C37E 01	2.178E=02
6.555E 01	1.629£ 01	1.6291	e ny weithe n	C 4111776	113 -144/46	1)3 44.3)3C 13	347155 13	440310 01	E S) O L W U E	-4031C 01	CHILLDHLAG '

	XABS	P=18	P⇔Ob .	Pna	OGX	a∾i⊧	¢=ne	CAMALI	P#TB/PSU	P#1P/PT0	P=08/P80	P=OB/PTO
N	6.468E 01	16 3560.S	2.0928 01	A.7185 02	₩4.050E 03	-1.557£ 03	-2,493F 03	4 . 7 d 9 E 6 %	5.183F 01	2.7466=02	5.183E 01	2.7966 = 02
0	6.506E 01	2.070E G1	2.162E 71	6,718E 02	#4.093E (3	-1.571t 63	a2.522E 03	4.337E 63	5,1291 01	2.766E=02	5.358E 01	2,890E=02
Ġ,	6.510E 01	2.070E 01	2.1706 01	8.718E 02	#4.098E 03	-1.573E 03	-2.525F ¢3	4,342E (3	5,129E 01	2,766£=u2	5.377F 01	2,900E=02
	6.530F 01	1.968E 01	2.207E 01	B.718E 02	#4.120E 03	■1.580E 03	#2.540E 03	4,368E U3	0.676E 01	2.630E=02	5.470E 01	2.950E=02
	6,696E 01	1-119E 01	9,320E 00	1,0458 03	-4.273F 03	-1.630E 03	-2.644E 03	4.583E 03	2.773E 01	1,0956=02	2.3098 01	1.246E=02
	6.763E 01	8.026E JO	9.045E 00	1.236E 03	322E 03	□1.644E 03	#2.678£ 03	0.665E (3	1.489£ ^1	1.0736=02	2.241E 01	1.209E-02
	6.840E 01	4.390E 00	6.906E 00	1.429E 03	-4.375F 03	-1.658E 03	42.716E 03	4.700E 03	1.0888 01	5.867E=03	1.711F 01	9.229E+03
	6,912E 01	3,453E 00	4.9052 00	1.554E 03	60 3554.44	-1.668E 03	■2.753E 03	4.848E 03	8.557E 00	4.6152#03	1.215E 01	6.555E=03
	6.973E 01	2.660E 00	4.109E 00		#4.459E 03			4.922E 03	6.591E 00	3.555£-03	1.018E 01	5.492E=03
	7.068E 01	1.913E 00	2.870E 00		#4.515E 03			5.036E 03	4.746E 00	₽.557E⇒03	7.112E 00	3.8368*03
	7.111E 01	1.575E 00	2.6562 00		•4,534E 03			5.088E 03	3.903E 00	2.105t=03	6.582E 00	3.550E=03
	7.264E 01	1.420E 00	1.895E 00		-4.590E 03			5.273£ 03	3,520€ 00	1.8985-03	4.696E 00	2.5336=03
	7.354E 01	1.329E 00	5.150E-01	1.893E 03	-4.618E 03	+1.700E 03	-2.919E 03	5.3728 03	3.294F 00	1.7776.03	1.276E 00	6.883E#04
	7.354E 01	1.329E 00	2*0835*01		₩4.619E 03			5.172E 03	3,293F 0v	1.7766=03	1.261E 00	6,801E=04
	7.487E 01	1.195E 00	0.000		#4,666E 03			5.424E 03	2.961E 00	1.5976-43	Q . 0 0 0	0.000
	7.772E 01	2,130E 00	0.000		₩4.677E 03			5.523E 03	5.278F 00	2.847E=03	0.000	0,000
	8,1628 01	1.430E 00	0.000				*2.960E 03	5,628£ 03	3,543E 00	1.911E=03	0.000	0.000
	8 443E 01	1.135E OR	0 * 0 0 0				#2.960F 03	5.602E 03	2.812E 00	1.517E=03	0.000	0.000
	8.729E 01	1,650E 00	0.000				-2.960E 03	5.705E 03	4.0846 00	2.265E=03	0.000	0.000
	8.729E 01	1.6519 00	0.000	2.126E 03	#4,714E 03	=1.754E 03	□2,960€ 05	5.705E 03	4.091E 00	2.2L7E=03	0,000	0,000

X	DORAG	CURAG	ĊF	нс
4.040E 01	1.152E 02	1.152E 02		4.383E=02
4.041E 01	1.797E=01 1.793E 01	1.154E 02		4.384E=02
4.131E 01	2.0496+01	1.333F 02		4.001F=02 4.410E=02
4.138E 01	1.252E 00	1.3478 02		4.514E=02
4,150E 01	2.334E 00	1.3718 02	2.407E=03	4.813F-02
4,246E 01	1.740E 01	1.5455 02		6.2452.05
4.410E 01	2.611E 01 3.123E 00	1.806E 02		7.952E=02 7.177E=02
4 480E 01	7,245E 00	1.9108 02		7.102E=02
4.481E 01	1.704E=01	1.911E 02		7.190Ea02
4.625E 01	2.089E 01	2.1208 05		6.613F#P2
4.626E 01	1.398E=01	2.122E 12		7.5950-02
4.731E 01	1.331E 01 3.405E=01	2.255g 02		7.519E=02 7.225E#02
4.811E 01	9.694E 00	2,3558 02		7.1128-02-
4.078E 01	8.776E 00	2.4438 02	3.259E+03	6.178E-02
4.879E 01	1.3368001	2.444E 02		6.847E-02
4.932E 01 5.073E 01	6.743E 00 1.715E 01	2.512E 02	• i i.	6.488E=02 5.826E=02
5.283E 01	2.393E 01	5.455E 05		4.560E=02
5.333E 01	5,603E 00	2.978g 02		4.216F.02
5.408E 01	8.2988 00	3.061E 02		3,953En02
5.484E 01	8,149E 00	3,143F 02		3.666F#02
5.576E 01 5.626E 01	9.530E 00 3.156E 00	3.238E 02		3.465E-02 3.158E-02
5.632E 01	4.651E=01	3.2749 02		2.5786.02
5.646E 01	1.212E 00	3,286E 12		2.641E#05
5,654E 01	7.219E=01	3.294E 02		2.687E=02
5.682E 01 5.704E 01	2.530E 00 1.942E 00	3.319E 02		2.891E=02 2.813E=02
5.777E 01	6.314E 00	3,402E 02		2.5225.02
5.8792 01	9.186E 00	3.493F 02		1.734E=02
6,0806 01	1.610E 01	3.654F 02		3.8006-02
6,222E 01	1.122E 01 2.014E 01	3,767E 02		3,054E002 3,365Ew02
6.506E 01	2.701E 00	3.995g 02		3.097E=02
6.510E 01	2.827E=V1	3.998E 02		3.143E-02
6.530E 01	1.440E 00	4.012E 02		3.130E=02
6.696E 01	1.214E 01 4.474E 00	4.134F 02		2.251E=02 2.016F=02
6.840E 01	4.675E 00	4.225E 02		1,542E=02
6.912F 01	3.720E 00	4.2626 02		1.250E=02
6.973F 01	2.755E 00	4.290E 02		1.074E=02
7.068E 01	3.661E 00	4.326g 02	• • • •	8.2906-03
7.111E 01 7.264E 01	1.449E 00 4.596E 00	4.341E 02		7.551E=03 6.248F=03
7.1548 01	1.935E	4.4068 02		3.961E=03
7.354F 01	2.568E#03	4.406€ 02	3.118₺≈03	3.950F-03
7.487E 01	8,953E=01	4.415# 02	•	4.850E-03
7,7728 01	2.2236 00	4.437E 02	•	7.503E-03
8.162E 01 8.443E 01	2.482E 00	4.462E 02		5.482£#03 4.562F#03
8.729E 01	4.501E=01	4.477E 02		6.067E#N\$
8.729E 01	0.000	4.477E 02		6.070E=05

N				
ENGINE PERFORMANCE			፤ላኒቲን	
C 10111E PE TOWN ANDE			+ ''	
CALCULATED THRUST	1600. (LBF)			0.000 (DEGREES)
MEASURED THRUST	1489, (LBF)	MASS PLIN RATTU	***********	(.979)
REYORRED COMMISSE INDIVIDE 40 \$ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2002. (LAF-SEC/LbM)		EFFICIENT	
MEASURED SPECIFIC IMPULSE.	1862. (LBF#SEC/LBF)	LINITING PRESSUR	E RECOVERY EFFICIE	* CY 0.1655
MEASURED THRUST COEFFICIENT)	UELIA MICEREPARE		0.1198 (PSI)
SCHOOLED IMMOS! COELITIES POTO 000 000 000 000 000	.*2012		ECCVERY - SLPERSCA	
		TOTAL PRESSURE A	ECOVERY - SIBSCITC	0.1678
REGENERATIVE - COOLED ENGINE PERFO	Dusher	INCET PROCESS EN	FICTERCY - SLPERSO	NIC, (.8946
	ACM MAN CE		FICIENCY - SUBSULI	
CALCULATED	438A (1083	KINETIC ETERGY E	FFICIENCY - SUPPRS	G^IC 0.9446
	6780. (LBF)	KINGIL ENGRGY F	FFICIFACY - SLBSC	1reases 3:0422
SPECIFIC IMPULSE	1659, (LBF)	ENIMALPT OF PUR	SUPERBUNIL	-0.07 (BTU/LBM)
THRUST COEFFICTENT	20/34 (COP#355/68%)	ENTHALPT AT POR	, andady if *** * * * * *	36.72 (BTU/LBM)
INDAL CAPLIFICATION SOCIETATION SOCIETATION CONTRACTOR	1,0416			
			COMBUSTOR	
MOMENTUM AND FORCES			CO" BOSICH	
TOUR TO THE PORTEO		FUEL ATO DATTO		A A3B#
INLET FRICTION DRAG	115.2 (L8F)	EDITUAL FACE BATT	.0	444444 4444
	736.S (L8F)	COMBUSTOR FEETCH	EMCY	1.000
COMBUSTOR FRICTION DRAG	284.3 (LBF)		4710	
COMBUSTOR STRUT DRAG	#6.10 (LBF)		IVENESS.	
COMBUSTOR MOMENTUM CHANGE	1131. (LBF)			.7389. 0.7779. 0.7119.
NOZZLE FRICTION DRAG	48.24 (LBF)		00 3011 200000	***************************************
NUZZLE STRUT DRAGALASAGAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA	0.00 (LBF)			
NOZZLE NOMENTUM CHANGE	1206. (LAF)		NOZZLE	
NOZZLE PRESSURF INTEGRAL	1254. (LBF)			
EXTERNAL FRICTION DRAG	46.03 (LBF)	VACUUM STREAM TH	RUST COEFFICIENT .	05 0.9219
EXTERNAL PRESSURE INTEGRAL	:1060, (LBF)	NOZZLE COEFFICIF	'NT w Cleaseesees	0.6340
TOTAL EXTERNAL DRAG	1106. (LBF)	PROCESS EFFICIEN	·CY	0.7826
TOTAL STRUT DRAGOCERPPERSONALARAGE CONTRACT	-6.10 (LBF)	KINETIC ENERGY E	FFICIENCY	0.8217
CAVITY FORCE	•1146. (LBF)			
CALCULATED LOAD CELL FORCE	#651 (LBF)			
MEASURED LOAD CELL FORCE	a763, (L8F)			
FUEL VACUUM SPECIFIC IMPULSE 0.0. 0153	6. 0119.0.			
STATIONS			FUEL VALUETAUR	
ACNITOUR.			FUEL INJECTORS	
NOMINAL CUML LEADING EDGE	34.884 (IN)	INJECTORS _	STATION	VALVE
SPIKE TRANSLATION	0.3168 (14)	14	40,400	. AC 1 C
INLET THRUST-BORGESESSESSESSESSESSESSESSESSESSESSESSESSE	40.400 (IN)	19	41.302	e
COWL LEADING EDGE	35.201 (IN)	ič	44.300	19
NUZZLE SHROUD TRAILING EDGE	73,541 (1h)	2 4	48.777	r
NOZZLE PLUG TRAILING EDGE	87.293 (IN)	ΣĆ	46.250	À
STRUT LEADING EDGE	56,457 (IN)	3A	54.067	•
STRUT TRAILING EDGE	65,05/ (IN)	38	56.252	
COMBUSTOR EXIT.	65,057 (IN)	ā T	44.802	

t = 202.01 sec.

SUMMARY REPORT

р T H GAMMA MOLWE SONV HACH VEL S A/A A/AC MEMON W IVAC PHI ETAC HIND TUNNEL 747.749 2986 666.7(792) 1.2941 28.852 2581 0.000 0000 0.390 404 -32.1(97) 1.5987 28.651 986 5.995 5913 1.827 0.10672 26.933 0.9854 5049 9.807 187.5 SPIKE TIP NS 2 Û 0.600 18.125 2986 666.7(792) 1.2940 28.851 2561 0.600 16.368 2918 646.0(772) 1.2962 28.651 2553 0.399 1019 2.065 0.10672 26.933 0.9854 4984 1.690 185.0 WIND TUNNEL 747.749 2986 666.7(792) 1.2941 28.852 2581 0.000 0.381 401 a32.7(97) 1.3987 28.851 983 6.017 5916 1.827 0.10503 20.507 0.9854 4971 9.656 187.5 0.000 SPIKE TIP NS 0.600 18,125 2986 666,7(792) 1,2940 28,851 2581 0.600 16.430 2920 646.7(773) 1.2961 25.851 2554 0.391 1000 2.083 0.10503 26.507 0.9854 4970 1.632 187.5 INLET THROAT 301,426 2948 40,400 655.2(781) 1.2953 28,851 2565 40.400 15.560 1428 283.7(353) 1.3530 28.851 1825 2.546 4647 1.885 0.94512 26.933 0.1113 4333 68.251 160.9 INLET UPNRSK 40.400 201.426 2948 655.2(781) 1.2953 28.851 2565 40.400 13.371 13/3 209.1(338) 1.3563 28.851 1791 2.638 4725 1.885 0.85920 26.953 0.1224 4374 63.089 162.4 INLET DNNRSK 40.400 124.152 2948 655.2(781) 1.2953 28.851 2565 40.400 106.764 2848 625.1(752) 1.2984 28.851 2524 0.486 1228 1.946 0.85920 26.933 0.1224 4374 16,393 162.4 COMBUSTOR 300.828 2948 40.410 655.2(781) 1.2953 28.851 2565 40.410 15.575 1429 224.0(353) 1.3529 28.851 1826 2.545 4645 1.885 0.94500 26.933 0.1113 4333 68.219 160.9 COMBUSTOR 41.314 244-906 2942 653.4(700) 1.2955 28.851 2563 41.314 17,746 1557 257.8(387) 1.3458 28.851 1900 2.342 4449 1.899 0.94709 26.933 0.1110 4229 65.488 157.0 COMBUSTOR 0 10 41.379 240,563 2942 653.3(779) 1.2955 28.851 2563 41.379 17.915 1567 260.5(390) 1.3452 28.851 1906 2.326 4433 1.900 0.94656 26.933 0.1111 4221 65.216 156.7 COMBUSTOR 41,500 233.847 2941 053.0(779) 1.2955 28.851 2562 41.500 18.275 1585 265.6(395) 1.3443 28.651 1916 2.297 4403 1.902 0.94757 26.933 0.1110 4205 64.836 156.1 COMBUSTOR 0 12 42.460 206.691 2931 42.460 19.521 1657 649.9(776) 1.2959 28.851 2558 285.0(414) 1.3406 28.851 1957 2.184 4273 1.909 0.93965 26.933 0.1119 4136 62.396 153.6 COMBUSTOR 0 13 44.099 191.553 2909 643.4(770) 1.2965 28.851 2549 44.099 19.227 1669 288.3(418) 1.3400 28.851 1963 2.147 4215 1.912 0.90643 26.953 0.1160 4100 59.379 152.2 COMBUSTOR 0 14 44.310 189.786 2906 642.5(769) 1.2966 28.851 2548 44.310 19.285 1673 289.2(418) 1.3399 28.851 1965 2.139 4205 1.913 0.90507 26.933 0.1162 4094 59.141 152.0 COMBUSTOR 0 15 44.800 184.960 2900 640.6(767) 1,2968 28,851 2546 44,800 19.466 1684 292.2(421) 1,3394 20.851 1971 2,118 4176 1.914 0.90138 26.933 0.1167 4077 58.493 151.4 COMBUSTOR 0 16 44,614 184.817 2900 640.6(767) 1.2968 28.651 2546 44.814 19:475 1684 292.3(422) 1.3393 28.851 1972 2.117 4175 1.914 0.90134 26.933 0.1167 4077 58.478 151.4 COMBUSTOR 0 17 10 4 46.260 160,516 2883 635,6(762) 1,2973 28,851 2539 46.260 16.644 1704 297.7(427) 1.3384 28.851 1982 2.074 4112 1.919 0.84901 26.933 0.1239 4040 54.256 150.0 COMBUSTOR 0 18 11 47.310 152.539 2872 632.3(759) 1.2977 28.851 2534 47.310 17.676 1707 298.5(428) 1.3383 28.651 1984 2.060 4087 1.924 0.79013 26.933 0.1331 4024 50.183 149.4

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KEADING :	0054	BLOCK	B 108 TIME	# 505°0	11 MAC	M 0.	O PT	n 747	.749	11 = 298	6.3						
	P	T	н	CAMMA	MOLHT	SANO	MALH	VEI	5	W/A	jų.	A/AC	MTYDM	Q	TUAP	0 L 7	5745
COMBUSTOR		19		g A · · · · ·	1.06.1	05111		166	J	7/4	×	AZAL	e u F i ti	G;	1446	-n1	ETAC
47.339	152.183			1.2977	28.851	2534											
47.339	17,665	1708						4085	1.924	0.78912	26,933	0.1333	4023	50.100	149.4		
COMBUSTOR		20												• •			
48.110	144.075	2864	629,8(756	1,2979	26.851	2531											
48.110	16.258	1690	293.9(423	1.3391	28,851	1975	2,076	4100	1.927	0.73623	26,933	0.1428	4027	46,906	149.5		
COMBUSTOR		21															
48,789 48,789			627.96 755														
COMBUSTOR	14.413	1021	283.4(413	1.5404	28.851	1953	2.125	4152	1,929	0.67667	26,933	0,1554	4049	43.661	150.3		
49.319	135,981	25			20 651	7674											
49.319			626.4(753 273.2(403) 1.2703) 1 1/28	28.451	6260	2 476	#20#	1 070	0 43384	24 077	0.4445		41 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
COMBUSTOR	0	23	16 5	, 1934/EG	entant.	1736	E 6 1 7 V	4604	1.730	0.03204	201733	0.1002	40/3	41,547	151.2		
50.729			622.7(750	1.2987	28.851	2521											
50.729	9.758	1482	238.0(367	1.3499	28.851	1857											
		•			,			4388	1.927	0.53936	26.933	0.1950	4160	36.778	154.5		
COMBUSTOR			17 10						• • • • • • • • • • • • • • • • • • • •				7,00	2481.0			
52,829	181,918	2819	616.56 743	1,2993	28,851	2513											
52.829	6,008	1205	165.6(295)	1,3666	28,851	1685	2,819	4750	1.907	0.44206	26,933	0.2379	4342	32.630	161.2		
COMBUSTOR		25	18 12														
53,329	272.002	2013	614.66 742	1 2995	28,851	2510								_			
53,329 COMBUSTOR	7:507	1122	145.00 274) 1,571/	50.021	1030	2.975	4847	1.898	0.42400	26,933	0.2480	4393	31,941	163.1		
54.069	52 A 22	26	19 5		36 303	20/11											
54.069	23.550	3711	626,5(1211) 401.3(1002)	1 1 2488	24,226	2041	1 (80	7751	2 710	0.0000	22 220	0 5.00		34 434			
COPAUSTOR	0	27	20 5	105000	201223	2023	11104	3321	C 4 2 7 A	0.40490	21.210	0.5654	4471	21,126	105.02	0.43	0.73
54.079			626,5(1212)	1.2440	26.206	3042											
54,079	23.577	3317	401.5(1004	1.2686	26.229	2824	1.188	1154	2.310	0.40467	27.270	0 2671	4413	21.098	145 5	0 42	A 77
COMBUSTOR	0	28	21 4					24-3		0140407	614614	, 95031	4435	£##070	TOPAS	0 9 4 3	0 1 1 2
54,830	51,114	4166	623,1(1293)	1.2272	26,509	3096											
54.839	25.312	3643	417.7(1111)				1.098	3206	2.322	0.38268	27.270	(.2782	4521	19.065	165.8	0.43	0.89
COMBUSTOR	0	29	55 505		_							-		. •	•		
55.760	44.734	4527	618.7(1347)	1.2151	26,721	3128											
55.760, COPBUSTOR	40.272	3055	424,9(1180	1.2372	26.779	2976	047	3114	2.326	0.35940	27.270	0,2962	4633	17,395	169.9	0.43	1,00
56.254	47 620	30 #543		1 1005	92 aCe	77-0											
56,254	20.780	4203	645.1(1608)	1 24/4	22,027	7361	0.01%	2077	3 600	0.20444	39 609	A N					
COMBUSTOR		31		1 10 5 140	231733	2501	0.947.3	2411	8.034	0.27314	2/.00/	0,3677	5077	13,564	183.9	0.85	0,71
56,264			645.1(1609)	1 1973	23.860	1375											
56.264	26,797	4217	468.0(1469	1.2143	23.937	3261	0.913	2977	2.599	0-29298	27.607	0.3679	5070	13,553	194 0	n a=	A 71
COMBUSTOR	v	2	25 4				- • ,	,	equ.,	**********	W.1.0-4.	402011	2011		10410	4405	4. B.L.M
56.319	43.349	4606	644,8(1624)	1,1936	23,906	3382											
56,319	25.502	4228	450.4(1472)	22122	23,995	3259	0.957	3119	2.601	11502.0	27,607	0.3690	5066	14,159	184.2	0.85	0.73
COMBUSTOR	Ç	33	26 3										-	• • •	•		
56,459	45.204	4636	644.1(1636)	1,1912	23,941	3387											
56,459 COMBUSTOR	20.5/5	4200	450.8(1486)	1.2091	24.035	3266	0.952	3110	5.605	0.29001	27,607	0.3717	5103	14.017	184.8	0,85	3.74
36,539		34			34 546	7704											
56.539	27.083	4288	643,7(1633)	1 2042	2/ 022	3300	A 012	2027	3 600	0 10734	22 102						
COMBUSTOR		35	465.4(1495)	195003	640 VEE	3613	0 4 4 E	6701	E DOU	U . K73E0	21.00/	V.3075	2115	13.612	192.5	0.85 (7.74
56,819			642.3(1654)	1.1874	23.998	3394											
56.819	27.375	4352	464.8(1519)	1.2029	24.094	3287	0.907	2980	2.602	0.29220	27.407	0-3688	61/12	17,627	186 2	V 8E 4	A 74
COMBUSTUR	0	.56	29 4							V 4 to 1 to 6 7	-, , , , , , , ,	013000	2443	13,537	10012	A B CD	1 1 1 0
57.045	44.177	4726	641.2(1669)	1.1839	24.047	3401											
57.045	27.561	4430	463.7(1537)	1.1957	24.151	3295	0.904	2980	2.602	0.29174	27,607	0.3695	5165	13,512	187-1	0.85	0.78
COMBUSTOR		37	30 4				-										
57.769	44.148	4826	637.6(1707)	1,1752	24.168	3416	_										
57.769	40,155	4527	465.3(1585)	1,1876	24,286	3317	0.886	2938	2,604	0.28722	27,607	0.3753	5227	13,114	189,3	0.85	3.84

GAMMA MOLINT SONV HACH VEL S w/A AJAC MUMTH Q IVAL PHI ETAC NO COMBUSTOR 0 38 31 4 58.789 44.309 4914 633.1(1740) 1.1674 20.279 3428 58.789 28.387 4630 459.8(1623) 1.1778 24.420 3332 0.884 2945 2.605 0.28538 27.607 0.3777 5273 13.063 191.0 0.85 0.89 COMBUSTOR. 0 39 32 2 45.381 4902 624.4(1735) 1.1686 24.288 3424 60.799 27.750 4585 434.1(1605) 1.1806 24.437 3319 0.930 3086 2.601 0.29531 27.607 0.3650 5242 14.161 189.9 0.85 0.89 60.799 CUMBURTOR 0 40 33 4 02.210 46.241 4874 618.4(1724) 1.1711 24.272 3419 26.719 4515 408.3(1577) 1.1856 24.428 3301 0.982 3243 2.598 0.30332 27.607 0.3553 5214 15.285 188.9 0.85 0.86 62.219 CONBUSTOR REGEN 41 34 21 62.219 46.241 4920 651.6(1743) 1.1685 24.236 3434 62.210 26.930 4571 441.9(1600) 1.1818 24.400 3318 0.976 3239 2.605 0.30332 27.607 0.3553 5230 15.268 189.5 0.85 0.86 NOZZLE 42 35 46.241 4874 618.4(1710) 1.1711 24.272 3419 87.295 87,295 1.179 2489 -467.4(795) 1.2839 24.633 2540 2.902 7371 2.598 0.05564 27.607 1.9371 6909 6.374 250.3 0.85 0.88 NOZZLE 43 36 87.295 46.241 4874 618.4(1710) 1.1711 24.272 3419 87.295 0.390 1935 #663.8(599) 1.3058 24.634 2258 3.547 8010 2.598 0.02575 27.607 4.1864 7291 3.205 264.1 0.85 0.88 NOZZLE AE REGEN 44 37 87,295 46.241 4920 651.6(1743) 1.1685 24.236 3434 87.295 1,198 2545 #447,0(815) 1,2818 24.633 2566 2.890 7414 2.605 0.05564 27,607 1.9371 6956 6.411 252.0 0.85 0.88 PO REGEN 45 38 NOZZLE 87.295 46.241 4920 651.6(1743) 1.1685 24.236 3434 87.295 0.390 1974 #650.6(612) 1.3041 24.634 2279 3.542 8072 2.605 0.02544 27.607 4.2365 7350 3.192 266.2 0.85 0.88 FICTIVE COMBUSTR 66 59 301.426 5252 618.4(1869) 1.1750 24.694 3525 62.219 0.390 1572-1006.2(407) 1.3319 25.085 1903 4.738 9016 2.446 0.04164 27.607 2.5886 7995 5.834 289.6 0.85 1.00 62.219 67 60 FICTIVE NOZZLE 24.013 4762 577.8(1679) 1.1669 24.255 3375 67.295 87.295 1.603 3000 =275.5(984) 1.2642 24.629 2767 2.362 6534 2.643 0.05564 27.607 1.9371 6402 5.630 231.9 0.85 0.88

	_											
XABs	PoIB	P=08	PDA	ωυ x	િન્દ્રો કો	Q=08		CAWALL	P=16/P50	F⇒IB/PT0	P#08/P80	P#Q8/PT0
•	1.040E 00	0.000	#4.416E#01	0.000	0.000	0.000	ā	2.470L=02	2.665F 00	1.391E-03	0.000	0.000
6.981E=01	1.040E 00	0.000	-3.463E 01	0.000	0.000	0.000		1.654E 02	2.565E 00	1.391t=03	0.000	0.000
1.836E 01			-1.658E 02		0.000	0.000		5.0536 02	5.625E 00	2.9356-03	0.000	0.000
3.070E 01	2.195E 00	0.000	-3.631E 02		0.000	0.000		6.804E 02	9,985E 00	5.210E-03	0.000	0.000
3.508E 01	3.896E 00	0.000			0.000	0.000		6.856E U2	00 3500.0	5.215E+03	1.475E 01	7.6986-03
3.520E 01	3.899E 00		-4.295E 02			0.000		6.858E 02	9.992E 00	5.215£=03	1.467E 01	7.654E=03
3.420E 01	3.899E 00		m4,296£ 02		0.000			7.206E 02	1.0028 01	5.2296-03	9.8278 00	5.128E=03
3.555E 01	3.910E 00		m4.366E 02		0.000	0.000		•	1.002E 01	5.229E-03	5.381E 00	2.808E=U3
3.587E 01	3.910E 00	5.100E 00	04.509E 02	a1./02F 0	2 410 (825	00000		7.531E 02	1.002E 01	5,2296-03	7.382E 00	3.8536-03
3,606E U1	3,910E 00	5.881E 00	#4.609£ 02	=1.802E 0	5 m1.005F	05 0.000		7.726E 02		5.6514-03	1.178E 01	6.146E=03
3.648E 01	4.226E 00	4.596E 00	+4.798E 02	=1.840E 0	2 91.046E	02 0.000		8.1626 02	1.0836 01			
3.701E 01	4,240E 00	6.760E 00	•5.035t 02	#2.058E 0	2 =1.904E	02 -1.536E	01 6	8.722E 02	1.067E 01	5.670t=03	1.732E 01	9.041E=03
3.733E 01	4.099E 00	8.0622 00	-5.15 2E 02	*5.146E 0	2 -1.940E	02 -2.058E	01	9.065E 02	1.050E 01	5.482E=03	2.066E 01	1.078E=02
3.803E 01	3.790E 00	1.328E 01	₩5,282£ 02	=2.342E 0	2 -2.025E	02 -3.175E C	01 9	9.831E 02	9.712E 00	5.069E=03	5.403E 01	1.776E=02
3.835E 01	5.319E 00	1.5655 01	-5.262E 02	-2.434E D	3 ⇒2.066€	02 =3.678E		1.019E 03	1.303E 01	7.113E=03	4.010E 01	2.093E=02
3.875E 01	7.243E 00	1.539E 01	-5.262E 02	#2.552E 0	3551.5* \$	02 #4.306E (01 1	1.064E 03	1.856E 01	9,6876=03	3.945E 01	2.059E=02
3.882E 01	7.573E 00	1.535E 01	₩5.262E 02	#2.573E 0	2 -2.132E	02 -4.414E	01 1	1.472E 03	1.941E 01	1.0136=02	3,934E 01	2.0536=02
3 901E 01	8.490E Q0	1.564F 0:	*5.256£ 02	-2.632E 0	2 =2.161E	02 #4.711E (01 1	1.094E U3	c,176E 01	1,135E=02	4.007E 01	5.091E=05
3.933E 01	1.382E 01	1.0112 01	\$0.3058 02	#2.733E 0	2 -2.212E	02 =5.204E	01 1	1.150E 03	3.542E 01	1,8496=02	4.129E 01	8.155E=48
3.950E 01	1.669E 01	1.346F 01	₽5.379E 02	#2.78BE 0	2 -2.241E	02 -5.466E	01 1	1.150E 03	4.276E 01	5.232E=02	3.450E 01	1.800E=02
3.982E 01	1.711E 01	A.525E 0	-5.574F 02	₩2.893E 0	2 .2.29BE	02 -5.945E	01 1	1.187E 03	4.386E 01	5.289E-02	2.185E 01	1.140E=02
4.000E 01	1.736E 01	8.431E 0	-5.704E 02	-2.954E 0	2 w2.333E	02 -6,213E	01	1.209E 03	4.448E 01	2.321E=02	2.161E 01	1.128E=02
4.040E 01	2.068E 01	8.2255 0	-6.007E 02	≈3.096E 0	2 02.413E	02 -6.830E	01 1	1.255E 63	5,299E 01	2.765E002	2.108E 01	1.100E=02
4 041E 01	2.076E 01	8.2198 0	-6-013F 02	-3-100E 0	2 -2.415E	3648.de 50	01 1	1,257E 03	5.320E 01	2.776E=02	2.106E 01	1.099E=0S
4 131E 01	2.827E 01	7.7527 0	-6-884E 02	93.574E 0	2 02.618E	02 99.5628	01 1	1,363E U3	7.243E 01	3.780E-02	1.987E 01	1.0376+02
4.138E 01	2.881E 01	7.7100 00	-4-955F 02	93.A19E 0	2 m2.674F	02 -9.852E	01	1.371E 03	7.382E 01	3.852E=02	1.976E 01	1.0326=02
4 150E 01	2.981E 01	7.8885 0	47.092F 02	93.706E 0	2 02.664E	02 =1.042E		1.386E 03	7.640E 01	3.987E-02	2.021E 01	1.055E¤V2
4.246E 01	1.147E 01	9.233# 00	07.606E 02	P4.542E 0	2 -2.916E	02 #1.627E	02 1	1.501E 03	2.941E 01	1.535E=U2	2,366E 01	1.235E=02
4.410E 01	1.497E 01	1.1535 0	-7.680F 02	#6.290F 0	2 -3.345F	02 -2.945E		1.699E 03	3.836E 01	2.002E=02	2,954E 01	1,5428002
4.431E 01	1.5426 01	1.1325 0	97.70AL 02	96.524F 0	2 95.398E	02 #3.126E		1.725E 03	3.951E 01	2,062E=02	10 3208°2	1.5146 = 02
4.480E 01	1.6468 01	1.0850	-7-786F 02	07-033E 0	2 03.519E	02 93.514E		1.784E 03	4.219E 01	2.202Eau2	2.781E 01	1.451E-02
4.481E 01	1.646E 01	1.0802.01	_7.780s 02	-7.0475 0	2 -2.5225	02 +3.525E	02	1.786E 03	4.218E 01	2.201E-02	2.777E 01	1.4492-02
4.626E 01	1.614E 01	7.000 01	=7.009F 02	BA. SHOE O	2 =3.872E	02 -4.508E		1.964E 03	4.137E 01	2.159E=02	2.419E 01	1.263E=02
4.731E 01	1.5916 01	8-42AF 02	-7-905E 02	-9.2/BE 0	2 -4.1258	02 -5.153E	ož ž	2.094E 03	4.078E 01	2.1282002	2.160E 01	1.127E-02
4.734E 01	1.574E 01	8.4002 00	67.000F 02	-9-303F A	2 a4.132F	02 -5.171E	02 2	2.097E 03	4 033E 01	2.105E=02	2.153E 01	1.1236=02
4.811E 01	1.105E 01	0.500E 0	-7-756E 02	-9-941F 0	2 -4-31AF	02 -5.623E	02 2	2 194E U3	2.632E 01	1.478E=02	2.460E 01	1.2846-02
4 879E 01	1.065E 01	1.0666.00	-7.434F 02	-1-047F 0	3 mu. 481F	02 -5.986E		2.2796 03	2.730E 01	1.425E-02	2.730E 01	1.425E=02
	1.148E 01	1 1/0F 0	-7 1285 02	mi-ONSE O	3 m/l - 608E	02 =6.245E		2.345E 03	2.942E 01	1.535E-02	2.942E 01	1.535E=02
4.932E 01		1 4 5 6 F O	-6 0006 02	-1.185¢ 0	3 -4-9/65	02 -6.900E	ož ž	2 5236 03	4.245E 01	2,2146-02	4.243E 01	2.214E-02
5.073E-01	1.656£ 01	2 0105 0	_4 A746 A2	-1 1500C 0	3 -5 4/85	02 -8.09ZE	כח	2.789E 03	5.151E 01	2.688E+02	5.151E 01	2.688E-02
5.283E 01 5.333E 01	2.010E 01 2.186E 01	2.1848 6	_ 2 E 3 G 6 0 2	-1-40AF 0	3 -5.5675	02 -8.470E		2,8536 03	5,603E 01	2.924E-02	5.603E 01	2.924E+02
		2.1666 O	-3 4415 02	-1.484E 0	3 -5-7/36	02 m9.122E	62 2	2.947E 03	6.036E 01	3.150E+02	6.036E 01	3.150E-02
5.407E 01	2.355E 01	2 - XERE 0	-3 TWOE VS	1.488E 0	3 05.745E	02 -9.131E		2,948E 03	6.042E 01	3,153E=02	6.042E 01	3.153E-02
5.408E 01	2.358E 01							3.046E U3	6.486E 01	3.385E-02	6.486E 01	3,385E=02
5.484E 01	2.531E 01		1 410/025 06	- 4 1 4 3 7 7 E V	3 0001200	02 99 8656		3.1646 03	6.732E 01	3,5136-02	6.73ZE 01	3.513E=U2
5.576E 01	2.6276 01	2.627E 0				02 -1.084E		3.208E 03	6 864E 01	3.582€=02	6.864E 01	3.5821-02
5.625E 01	2.679E 01	2.679E 0				02 91.140E		3.209E 03	6.867E 01	3.584E=02	6.867E 01	3.584E=02
5.626E 01	2,6805 01	2.680E 0				02 -1.1428		3.216E 03	0,189E 01	3.230E=02	6.082E 01	3.591E=02
5.632E 01	2,419E 01	2.685E 0				02 91,148E			6.189E 01	3.2306-02	6.919E 01	3.611E=02
5.646E 01	2,415E 01	2.700E 0				02 01,164E		3.234E 03		3.6225-02	6.940E 01	3.622t=02
5.654E 01	2.7081 01	2.708E 0				02 91.174E		3.245E 03	6,940E 01			3.661E+02
5.682E 01	2.737E 01	2.737E 0				02 -1.206E		3.2602 03	7.015E 01	3.661E002	7.015E 01	3.686E=02
5.704E 0	2,756E 01	2.756E 0				02 •1.232E		3.309£ 03	7.063E 01	3.686E=02	7.0636 01	• • • • • • • • • • • • • • • • • • • •
5.777E 01	2.815E 01	2.815E 0				02 -1.312E		3.402E 03	7.215E 01	3.7658=02	7.215E 01	3.765E>UZ
5.879E 01	2.839E 01	5.636E 0				02 -1.419E		3.532E 03	7.274E 01	3.796E-02	7.274E 01	3.796E=02
6.080E 01	2.775E 01	2.775E 0				3819°1° 20		3.790E 03	7.151E 01	3,711E-02	7.111E 01	3.711E=02
6,222E 01	2,672E 01	2.672E 0				02 +1.748E		3.972£ 03	6.847E 01	3.573E=02	6.847E 01	3.573E=02
6.46BE 01	2,158E 01	2,1586 0	1 6.430E 02	: ≠2.805E 0	3 -8.330E	02 -1, 972E	03	4.289E 03	5.5316 01	2,886E=02	5.5318 01	2.886E≠02

XABs	P=18	P=08	PDA	QQX	(I=IB	Q⇔OB	CAMALL	P=IB/PSU	P#IB/PIO	P=Ub/PS0	P#UB/PTO
6.506E 01	2.006E 01	2.080F 01	6.430E U2	₩2.854E 03	-8.468E 0	2 =2.007E 03	4.337E 03	5.141E 01	2.603t=02	5.33VE 01	2.782t+ŪZ
6.510E 01	2.006E 01	2.072E 0	6.430E UZ	-2.859E 03	*8.483E 0	2 -2.010E 03	4.342E U3	5.141E 01	2.663E=02	5.309E 01	2.771E=U2
6.530E 01	1.892E 01	2.030E 01	6.430E UZ	*2.883E 03	*8.556E 0	2 -2.028E 03	4,3688 03	4.847E 01	2,5306-02	5.202E 01	2.7156=02
,6.696E 01	9.400E 00	8.360E 00	8.017t 02	-3.053E 03	₩9.059E 0	2 -2.147E 03	4.583E U3	2.409E 01	1.257L=02	2.142E 01	1.1186-02
6.763E 01	7.064E 00	8.070E 00	9.681E 02	-3.108E 03	#9.211E 0	2 -2.187E 03	4.665E 03	1.810E 01	9.447E=03	2.068E 01	1.079E=02
6.840E 01	4.380E 00	6.574E 00	1.147E U3	#3.1/1E 03	99.354E 0	2 -2.236E 03	4.760E 03	1.122E 01	5.858E+03	1.685E 01	8.792E=43
6.912E 01	3.630E 00	5 175E 00	1.272E 03	-5.233E 03	-9.464E 0	2 -2.286E 03	4.848E 03	9.303E 00	4.8556-03	1.326E 01	6,921E=03
6.973E 01	2.995E 00	4.481E 00	1.359E 03	93.284E 03	#9.542E 0	2 =2.330E 03	4.922E 03	7.675E 00	4.005E=03	1.148E 01	5,993E=U3
7.068E 01	2.351E 00	3.400E 00	1.463E 03	●3,350E 03	₩9.645E 0	2 -2,386E 03	5.036E 03	6.025E 00	3.145E=03	8.713E 00	4.5476=03
7.111E 01	2.060£ 00	3.122E 00	1.501E 03	#3.3/5E 03	-9.684E 0	2 -2.407E 03	5.088E 03	5.279E 00	2.7556-03	8.002E 00	4.176E=03
7.264E 01	2,017E 00	2.135E 00				2 #2.470E 03	5.273E 03	5.169E 00	2.698E#03	5.471E 00	2.855E+03
7.354E Q1	1.992E 00	5 . 600 En 01	1.673E 03	-3.493E 03	-9.867€ 0	2 -2.506E 03	5.572E 03	5.105E 00	2.664E=03	1.435E 00	7.489E=04
7.354E 01	1.992E 00	5.530E=01	1.674E 03	-3.495E 03	=9.867E 0	2 .506€ 03	5.372E 03	5.105E 00	2.664E=03	1.417E 00	7,395E=04
7.487E 01	1.955E 00	0.000	1.7166 03	-3.565E 03	-9.946E 0	2 -2.570E 03	5.424E 03	5.010E 00	2.615E=03	0.000	0.000
7.772E 01	1,940E 00	0.000	1.794E 03	-3.5/8E 03	-1.008E 0	3 -2.570E 03	5.523E 03	4.971E 00	2.594E+03	0.000	0.000
8.162E 01	1,585E 00	0.000	1.869E 03	-3.592E 03	-1.022E 0	3 -2.570E 03	5,628E 03	4.062E 00	2.120E-03	0.000	0.000
8.443E 01	1.275E 00	0.000	1.901E 03	-3.604E 03	#1.034E 0	3 -2.57QE 03	5.6826 03	3.2678 00	1.705E-03	0.000	0.000
8.729E 01	1.890E 00	0.000				3 +2.570E 03	5.705E 03	4.843E 00	2.528E-03	0.000	0.000
8,729E 01	1.891E 00	0±000 t	1.939E 03	-3.625E 03	-1.055€ U	3 -2.570F 03	5.705E 03	4.847E 00	2.5296#03	6.000	0.000

X	DDRAG	CDRAG	CF	H¢
01111111111111111111111111111111111111	20110000111110000111110000011111000001111	22222222222222222222222222222222222222	33333333333333333333333333333333333333	22222222222222222222222222222222222222
6.468E 01 6.506E' 01 6.510E 01 6.530E 01	1.729E 01 2.841E 00 3.048E=01 1.531E 00			
6.696E 01 6.763E 01 6.840E 01 6.912E 01 6.973E 01	1.233E 01 4.317E 00 4.546E 00 3.727E 00 2.851E 00	4.202E 02 4.202E 02 4.207E 02 4.205E 02 4.313E 02	3.2106=03 3.1666=03 3.1406=03 3.1056=03 3.0846=03	2.058E=02 1.841E=02 1.455E=02 1.275E=02 1.135E=02
7.068E 01 7.111E 01 7.264E 01 7.354E 01 7.354E 01 7.487E 01	3.942E 00 1.617E 00 5.218E 00 2.291E 00 3.171E=03 1.166E 00	4.353E 02 4.369E 02 4.421E 02 4.444E 02	3.0906-03 3.0356-03 3.0026-03 2.9336-03 2.9326-03	9.5/06-03 8.6/66-03 7.3446-03 5.0056-03 5.0046-03
7.772E 01 8.162E 01 8.443E 01 8.729E 01 8,729E 01	2.487E 00 2.483E 00 1.128E 00 4.948E=01	4.455E 02 4.480E 02 4.505E 02 4.516E 02 4.521E 02	2.9836=03 2.9076=03 2.921c=03 2.8796=03 2.9196=03 2.9196=03	6.991E=03 6.914E=03 5.892E=03 4.962E=03 6.670E=03

		RAMJET PE	REPORMANCE		
21					
				INLET	
•	CALCULATED THRUST	. (LBF=8EC/LBM) . (LBF=8EC/LBM)	MASS FLOW RATION ADDITIVE DRAG (LIPITING PRESSOR	O,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	NEY 0-1637
	CALCULATED THRUST COEFFICIENT	7	TOTAL PRESSURE TOTAL PRESSURE INLET PROCESS (RECOVERY = SUPERSON DIMOSUS = RECOVERY REFEICIENCY = SUPERSO	NIC 0 . 1660
	REGENERATIVE COLED ENGINE PERFORMAN CALCULATED		KINETIC ENERGY	EFFICIENCY - SUBSONI EFFICIENCY - SUPERS	ONIC 0.9452
	NET THRUST	. (LBF)		# SUPERSONIC	IC, 0.8940 ******* #5.29 (BTU/LBM)
	SPECIFIC IMPULSE	. (LBF=SFC/LBM)	ENTHALPY AT PO	- SUBSONIC	30.49 (BTU/LBM)
	MOMENTUM AND FORCES			COMBUSTOR	
	INLET FRICTION DRAG	, (LBF) 8 (LBF) . (LBF) . (LBF)	EQUIVALENCE RAY COMBUSTOR EFFIC TOTAL PRESSURE COMBUSTOR EFFE (NJECTOR DISCH) VACUUM STRLAM NOZZLE COEFFIC PROCESS EFFICIE	TIG	0.851 0.879 0.00000000000000000000000000000000000
	,- 87ATIO _N S			FUEL INJECTORS	•
	SPIKE TRANSLATION	84 (IN) 86 (IN) 90 (IN) 93 (IN) 43 (IN)	INJECTORЬ 1A 1B 1G 2A	91ATIUN 40.400 41.304 44.300 48.779	VALVE
	STRUT LEADING EDGE	95 (IN) 59 (IN) 59 (IN) 19 (IN)	2 C 3 A 3 b 4	46.250 54.069 56.254 44.804	E E

t = 239.81 sec.

1-29-75

SUMMARY REPORT

				7 7	,										
РТ	м	GAMEA	MALMI	SANV	MACH	VEI	5	4/4	₩	A/AC	*(* *	n	TVAC	PHT	ETAC
NO WIND TUNNEL 1	0 5				=		-		,-	~,~~			*1~0	1 114	CINC
10.000 741.494 297	664.1(790)	1.2944	28.852	2577											
CC 0.000 0.389 40	2 432.6(97)	1.5987	20,051	984	5.999	5904	1.826	0.10665	26.942	0-9863	5042	4.785	187.2		
SPIKE TIP NS 2	U 4	•••					4 4 - 2			0,,000		.,,.,	10.84		
0,600 18,100 297	8 664.16 790	1.2943	28.851	2577											
0.600 10.346 290	9 645,46 770	1.2964	20.851	2549	0.399	1017	2.082	0.10665	26.942	0.9864	4981	1.085	184.0		
#160 TUNNEL 3	u o					• •				**,		.,,			
0.000 747.499 297	8 664.1(790)	1.2944	28.852	2577											
0.000 0.380 39	9 -33,2(96)	1.3987	26.851	981	6.020	5907	1.826	0.10506	26.540	0.9863	4969	9,644	187.2		
SPIKE TIP NS 4	υ ο	£ *		• •	•		• •	***	,,	.,	,,	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	40,33		
0.600 18.100 297	B 664.1(790;	1.2943	28,851	2577											
0.600 16.407 291	2 644.1(770)	1.2964	28.851	2550	0.392	999	2.082	0.10506	26.540	0.9865	4969	1.630	187.2		
INLET THROAT 5	0 3								- •	• • • •		••••			
40.400 296.104 292	2 647.16 773	1,2961	28,851	2555											
40.400 15.575 142	0 221.6(351)	1.3534	28.851	1820	2.535	4614	1.884	0.94463	26.942	0.1114	4308	67.740	159.9		
INLET UPNRSK 6	0 3								•			-,			
40.400 296.104 292	2 647.1(773)	1.2961	28.851	2555											
40.400 13.380 136	5 207.1(336)	1.3507	28,851	1786	2,627	4693	1.884	0.85875	26.942	0.1225	4349	62.627	161.4		
INLET DNNRSK 7	0 4							·	-						
40,400 123,282 292	2 647.1(773)	1,2961	28,851	2555											
40.400 105.933 282	2 617.2(744)	1,2993	28,851	2513	0.487	1225	1,944	0.85875	26.942	0.1225	4349	16.350	161.4		
COMBUSTOR 0 8	1 2									- •					
40,410 295,297 292	1 047.1(773)	1.2961	28.851	2554											
40.410 15.596 142	2 222.0(351)	1,3533	28.851	1821	2.533	4612	1,884	0.94451	26.942	0.1114	4307	67.698	159.9		
CUPBUSION 0 9	2 21												• •		
41.300 172.278 286		1,3000	26,532	2644											
41.300 20.165 170		1.5411	26.532	5094	2,053	4540	2.054	0.95292	27.127	0.1111	4157	62.924	153.2	0,23	0.07
COMBUSTOR 0 10	3 21														
41,310 184,167 279		1.3032	26,457	5618											
41.310 20.233 162	9 297.4(442)	1.3454	26.457	2029	5.095	4244	2.042	0.95271	27.127	0.1112	4155	62.841	153.2	0.23	0.01
EnuaD2188 0 11	4 21														
41.375 183.014 278		1.3038	26,446	5613											
41.375 20.671 163		1.3453	20.445	5035	2,075	4216	2.041	0.95415	27,127	0.1110	4142	62,511	154.7	0.23	0.00
CUMBUSTOR 0 12															
41.500 176.502 278 41.500 22.985 169		1,3057	26,449	2613											
41:500 22:985 169 CUMBUSTÖR 0 13		1.3454	20.449	2067	1,988	4109	2.044	0.95438	27.127	0.1110	4118	60,946	151.6	0.23	0.00
	5 5														
	5 649.6(907)	1,2005	20,000	2/40											
COMBUSTOR 0 14	5 418.3(680) 7 4	100100	20.000	2430	1.400	3402	5.105	0.94500	27,127	0.1121	3985	49.962	146.9	0.23	0,35
44.095 106.184 327		1 3847	37 644	2746											
44.095 66.607 294		1.2003	27.044	26.15		2000								_	
COMBUSTOR 0 15		1.2711	27.045	6045	0.0/2	5208	4.117	0.41525	27,127	0.1161	3926	32.734	144.7	0.63	0.50
44.310 106.163 324		1 3016	37 033	3744											
		1.5013	21.022	2/00	4 85.	0364									
COMBUSTOR 0 16	8 531.6(836) 9 3	114411	21.423	6046	0,035	2527	4.112	0.91094	27.127	0.1163	3455	31,695	144,6	0.23	0.48
	2 628.4(909)		34 0//4	2770											
44.800 70.929 288	- 558-7/ ADD	1.5032	24 017	2637	V 6".4	2110	3 100	0.0077			***	30	4.81		
COMBUSTUR 0 17	9 538.7(822) 10 2	4 8 6 7 4 6	E4 . 74 /	2021	V 0 0 V /	E114	60104	V . 40759	21+127	0,1167	2908	24,887	144,0	0.23	0.42
44.010 106.052 316	2 628.3(909)	1 2853	24 Q/E	277.0											
44.810 70.911 288	538.5(822)	1.20/2	24-044	7170	0.807	2124	2 100	4 00370	17 4 7 7	0 4445	200	30 400	* * * * * * * * * * * * * * * * * * * *		
	11 17	*****	F 0 1 7 4 0	2020	0 4 0 0 7	cten	E . 104	0.70/39	41.141	0.1167	3707	24.089	144 • 0	0.23	0,42
46.250 100.136 253	8 647.5(842)	1.2164	22.101	273/											
46.250 68.303 231	3 565.27 740	1.4244	22.40%	26114	0.778	203	2 6/12	V 877EF	J7 607	0 4 17 "	7004	21.30"			
	3 565.2(,760)	147524	74	2000	4.110	E030	C+344	V + 000055	c/,54/	A * 1570	2404	C1.344	141.7	0.76	0.03

IVAC PHI ETAC A / A C *UMIM 0 GAMMA MOLMT SONY MACH VEL 0 19 12 2 COPBUSTOR 100.096 2539 647.4(842) 1.5168 22.595 2724 65.285 2314 565.1(761) 1.3244 22.395 2608 0.778 2030 2.342 0.86801 27.547 0.1239 3905 27.377 141.7 0.76 0.03 46.260 46.260 0 20 13 4 COMBUSTOR 96.723 2737 636.6(911) 1.3074 22.594 2806 66,384 2504 549,9(826) 1.3152 22.594 2692 0.774 2083 2.366 0.80766 27,547 0.1332 4048 26.148 146,9 0.76 0.10 47.310 47.310 COMBUSTOR 0 21 14 2 96,690 2740 636,3(912) 1,5073 22,597 2807 66.412 25v6 549.7(827) 1.3150 22.597 2693 0.773 2082 2.367 0.80675 27.547 0.1333 4050 26,103 147.0 0.76 0.10 47.335 47.335 CUPBUSTOR 0 22 15 4 92,901 2991 628,7(1001) 1.2955 22,841 2904 62.355 2726 524.6(903) 1.3642 22.642 2783 0.800 2228 2.393 0.75257 27.547 0.1429 4190 26.053 152.1 0.76 0.19 48.110 48.110 0 23 16 COMBUSTOR 86.022 2709 650.9(1038) 1.3110 19.541 3006 49,836 2376 509,9(898) 1.3223 19.541 2827 0.939 2656 2.063 0.70443 28.092 0.1552 4293 29.075 153.3 1.34 0.10 48.775 48.775 0 24 17 2 COMBUSTOR 85.955 2713 650.6(1040) 1.3108 19.544 3008 49.717 2379 509.3(899) 1.3222 19.544 2828 0.941 2661 2.663 0.70351 28.002 0.1554 4295 29.096 153.4 1.34 0.10 48.785 48.785 0 25 18 4 COMBUSTOR 82.649 2891 646.5(1112) 1.3026 19.688 3084 49.315 472.1(939) 1.3163 19.689 2873 1.028 2954 2.687 0.65795 28.002 0.1662 4418 30.205 157.8 1.34 0.14 43,400 2483 49.315 COMBUSTOR 0 26 19 5 635,7(1246) 1,2870 19,971 3212 76.029 3220 394.5(1009) 1.3056 19.972 2944 1.180 3474 2.727 0.56075 28.002 0.1950 4667 30.277 167.4 1.34.0.22 50.725 33.300 2667 50.725 0 27 20 COMBUSTOR 70.202 3467 621.7(1348) 1.2744 20.202 3298 52.825 23.325 2711 288.1(1022) 1.3005 20.207 2945 1.387 4085 2.753 0.45961 28.002 0.2379 4977 29.178 177.7 1.34_0.28 52.825 0 28 21 COMBUSTOR 69,224 5499 618,6(1361) 1,2727 20,235 3308 21.650 2701 266.2(1017) 1.3003 20.240 2937 1.430 4199 2.757 0.44082 28.002 0.2480 5050 28.766 179.6 1.3A 0.29 53,325 53.325 0 29 22 COFBUSTOR 66,983 3579 614.2(1394) 1.2684 20,312 3333 54.075 20-191 2747 244-7(1035) 1.2975 20.319 2953 1.456 4300 2.766 0.41553 28.002 0.2631 5103 27.767 182.2 1.34 0.31 54.075 0 30 23 CUMBUSTOR 65.219 3640 609.9(1419) 1.2649 20.374 3352 18,712 2769 221,4(1043) 1,2958 20,382 2959 1,490 4409 2,772 0,39295 28,002 0,2782 51/1 26,924 184,7 1,34 0,33 54.835 54.835 0 31 24 4 COMBUSTOR 63,427 3699 604,9(1444) 1,2615 20,434 5369 55.760 17.100 2761 193.9(1046) 1.2945 20.444 2959 1.533 4535 2.778 0.36895 28.002 0.2963 5245 26.002 187.3 1.34 0.34 55.760 COMBUSTOR 0 32 25 50.510 4153 602.4(1635) 1.2318 20.851 3493 56.260 10.230 3314 199.6(1263) 1.2685 20.690 3163 1.419 4490 2.627 0.29723 28.002 0.3678 5436 20.738 194.1 1.34 0.45 50.260 0 33 26 5 COMBUSTOR 56.543 3831 602.1(1499) 1.2535 20.556 3408 56.315 12.696 2780 127.8(1043) 1.2926 20.572 2947 1.653 4872 2.798 0.29629 28.002 0.3690 5440 22.434 194.3 1.34 0.37 50.315 COMBUSTOR 0 34 27 56,392 3838 601,5(1502) 1,2530 20,565 3410 56.455 12.576 2782 124.4(1043) 1.2924 20.581 2947 1.658 4886 2.798 0.29416 28.002 0.3717 5450 22.337 194.6 1.34 0.38 56.455 U 35 28 6 COMBUSTOR 51,432 4138 601,1(1628) 1,2330 20,859 3489 15.750 3205 184.7(1243) 1.2706 20.677 3143 1.452 4565 2.824 0.29746 28.002 0.3675 5455 21.101 194.8 1.34 0.45 56.535 50.535 NO COMBUSTOR 0 36 29 3 52.135 4123 599.8(1622) 1.2341 20.828 3485 50.815 15.262 3220 171.0(1223) 1.2726 20.065 3125 1.462 4632 2.822 0.29647 2H.002 0.3688 5473 21.343 195.5 1.34 0.45 56.815 COPBUSTUR 0 37 30 53.832 4049 598.8(1591) 1.2344 20.761 3467 57.041 14.276 3083 147.6(1166) 1.2768 20.791 3070 1.547 4751 2.815 0.29602 28.002 0.3693 5486 21.859 195.9 1.34 0.43 57,041

GATMA MOLHT SONV MACH VEL S A/A AJAC MUMIM Q IVAC PHI ETAC CORBUSTOR 0 38 51 5 61.414 \$700 595.0(1468) 1.2578 20.500 5586 57.765 57.165 11.115 2586 74.2(963) 1.3001 20.519 2855 1.769 5108 2.784 0.29132 28.002 0.3753 5514 23.126 196.9 1.34 0.36 COMBUSTOR 0 39 32 7 58.785 102./65 3134 591.6(1209) 1.2899 19.482 3172 0.337 1598 044.9(577) 1.3471 19.983 2314 2.439 5644 2.684 0,26947 26,002 0.3777 5525 25.590 197.3 1.34 0.22 506785 COMBUSTOR 0 40 33 6 60.795 49,876 4428 584,4(1750) 1.2047 21,146 3549 60.795 18,637 3702 204,4(1425) 1,2463 21,225 3287 1,318 4332 2,839 0,29954 28,002 0,3650 5512 20,165 190,9 1,34 0,54 COMMUSTOR 0 41 34 4 62.215 55.047 4264 579.6(1680) 1.2235 21.000 3510 62.215 17.006 3421 166.6(1306) 1.2619 21.054 3193 1.423 4543 2.625 0.30706 20.002 0.3553 5502 21.720 196.5 1.34 0.50 COMBUSTOR 0 42 35 5 64.679 40.682 4549 568.7(1801) 1.1972 21.244 3566 21.101 3978 253.6(1542) 1.2277 21.394 3369 1.179 3971 2.848 0.29163 28.002 0.3749 5482 17.996 195.8 1.34 0.58 64.679 COMBUSTOR 0 43 36 4 45.055 42.908 4612 567.0(1828) 1.1895 21.358 3573 65.095 21,588 4131 288,3(1609) 1,2154 21,469 3410 1,095 3734 2,859 0,27112 28,002 0,4032 5479 15,732 195,7 1,34 0,61 COMBUSTUR REGEN 44 37 4 65.055 42,908 4663 602.4(1852) 1,1860 21,335 3590 65.055 23.341 4242 350.5(1659) 1.2079 21,447 3446 1.030 3550 2.666 0.27112 28.002 0.4032 5500 14.957 196.4 1.34 0.61 NOŽZLF AE 45 38 5 87.291 42.908 4612 567.0(1816) 1.1895 21.358 3573 87.291 1.244 2291 -544.9(820) 1.2969 21.540 2619 2.848 7459 2.859 0.05644 28.002 1.9371 7109 6.542 253.9 1.34 0.61 NOŻZLE PO 45 39 87.291 42.908 4612 567.0(1816) 1.1895 21.358 3573 87.291 0.389 1742 4760.1(605) 1.3207 21.541 2304 3.537 8149 2.859 0.02536 28.002 4.3112 7522 3.211 268.6 1.34 0.61 NOZZLE AE REGEN 47 40 5 87.291 42.906 4063 602.4(1852) 1.1860 21.335 3590 87.291 1.264 2343 -525.8(841) 1.2949 21,540 2646 2.836 7507 2.866 0.05644 28,002 1.9371 7160 6.584 255.7 1.34 0.61 NOZZLE PO REGEN 48 41 5 87.291 42.908 4663 602.4(1852) 1.1860 21.335 3590 57.291 0.389 1777 -746.7(619) 1.3190 21.541 2326 3.533 8216 2.866 0.02506 28.002 4.3624 7565 3.200 270.9 1.34 0.61 FICTIVE CUMBUSTR 67 60 55.055 296.104 5245 567.0(2103) 1.1879 21.945 3757 55.055 U.389 1290-1202.7(431) 1.3393 22.163 1968 4.761 9410 2.690 0.04069 28.002 2.6868 8458 5.951 302.0 1.34 1.00 FICTIVE NOZZLE 68 61 87.291 27.669 4550 542.3(1800) 1.1867 21.350 3546 57.291 . 1.537 2620 =410.1(954) 1.2649 21.540 2766 2.476 6903 2.894 0.05644 28,002 1.9371 6771 6.055 241,8 1.34 0.61

BBAX	P=18	P#OH	PDA	κυα	GPIB	ଡ≈೧୯	CANALL	P-Ib/PSU	14/8I•4	P=06/P50	P#Q8/PT0
6.981E#01	1.045E 00	0.000	-4.410E=01	0.000	0.000	0.000	2.470E#02	2.688E 00	1.3986-03	0.000	0.000
1.836E 01	1.0456 00	0.000	-5.480E 01	0.000	0,000	0.000	1.634E 02	2.6886 00	1,3986+03	0.000	0.000
3.070E 01	2.205E 00	0.000	-1.665€ UZ		0.000	0.000	5.0538 02	5.671E 00	2.950£-03	U.000	0.000
		•						9.9896 00	5.196E-03		
3.508E 01	3,8646 00	0.000	#3.638£ 02		0.000	0.000	6.804E 02			0.000	0.000
3,519E 01	3.456E UO		-4.297E UZ		0.000	0.000	6,854E 02	9.919E 00	5.159E=03	1.476E 01	7.676E=03
3,520E 01	3,855E 00	5./03E 00	•4.297£ Q∠	ប្រហ្វា	9.000	0.000	6,857E 02	9,915E 00	5.1576-03	1.467E 01	7,629L=03
3.555F 01	3.7/0E 00	3.658E 00	₩4,366£ V2	0.000	0.000	0.000	7,209E 02	4.697E 00	5,043E=03	9.409E 00	4.894E=03
3,586E 01	3.832E 00	1.852E 00	-4.508E U2	₩2.650F 02	#2.658E	00000 50	7.5296 02	9.856E 00	5.126E+03	4.694E 00	2.441E=03
3,606E 01	3.870£ 00	2.656F 00	#4.613E 02	-2.688£ B2	+2.688F	02 0.000	7,729E 02	9.954E 00	5.1/7E=03	6.830E 00	3.5536-03
3.648E 01	4.2186 00		50 4808 De				8,164E 02	1.085£ 01	5.643E-03	1 . 145E 01	5 943E+03
3.701E 01	4.210E 00					02 -1.614E 01	8,726E 02	1.083E 01	5.6.526-03	1.723E 01	8 960E=03
3,732E, 01	4.079E UU					02 =2.155E 01	9.063E V2	1.049E 01	5.4576.03	€.067E 01	1.0756=02
3.803E 01	3.785E 00					05 -3.332 01	9.834E 02	9.7358 00	5.064E=03	3.419E 01	1,7786.05
3,834E 01	5.293E U0		• • •	*-		02 =3.853E 01	1.018€ 03	1.362E 01	7.081E=03	4.022E 01	2.0926=02
5,875E 01	7.234E 00					02 44.517E 01	1,064E 03	1.861E 01	9.678£-03	3.925E 01	2.042E-p2
3,881E 01	7.545& 00	1.520E 01	-5.274E 02	≈3. 666€ 02	≈3.204£	02 =4.623E 01	1.072E 03	1.941E 01	1.009E=02	3.910E 01	2.033E>U2
3,901E 01	8.460E 00	1.557€ 01	45.268£ U2	-3.756E 02	-3.262£	02 #4.940E 01	1,094E 03	2.181£ 01	1,134E=02	4.004E 01	2.0836-02
3.932F 01	1.3/1E 01	1:616E Q1	₩5.318E 02	#3.412E Q2	43.367E	02 -5.450E 01	1.130E 03	3.525E 01	1.6336.02	4.157E.01	2.1626-02
3,950E 01	1.661E 01					02 -5.730E 01	1.150E 03	4.273E 01	2.2225.02	3.168E 01	1.6476=02
3.981E 01	1.723E 01					02 =6,225E 01	1.187E 03	4.4336 01	2.306t+02	1.389E 01	7 224E+03
4.000E 01	1.760E 01					02 -6.5118 01	1.209E 03	4.527E 01	2.355E=02	1.336E 01	6.951E-03
4.040E U1	2.344E VI						1.256E U3		3.135E=02	1.223E 01	
						02 -7.215E 01		6.038E 01			6.362E=03
4.041E 01	2.358E 01					02 =7.235E 01	1.257E 03	6.066F 01	3.155E-02	1.220E 01	6.347E=03
4.130E 01	3.657E 01					05 #1.198E 05	1,362E 03	9.405E 01	4.892E=02	9.681E 00	5.0156-03
4.131E 01	3.671E 01					05 -1.501E 05	1.363E 03	9.443E 01	4.911E=02	9.653E 00	5.021E=03
4.137E 01	3.766E VI	3.681E 00	•7.695E Q2	- 2.656€ 05	= 4.368€	02 -1.258E 02	1,3/1E 03	9,687E 01	2.078F=0S	9.469E 00	4.925E=03
4.150E Q1	3.949E 01	6.483E 00	₽7.913E 02	-5.818E 02	#4.441E	02 =1.376E 02	1,3866 03	1.016E 02	5.2836.02	1.668E 01	8.673E=03
4.246E 01	4.984E 01	2.797E 01	-9.082£ 02	=7.652E 02	-5.072E	02 -2.579E 02	1.501E 03	1.5856 05	6.6675-02	7.195E 01	3.742E002
4.409E 01	6.865E 01					02 -5.098E 02	1.699E U3	1.7666 02	9.1846=62	1.661E 02	8.618E=02
4.431E 01	7.112E 01					02 -5.438E Q2	1.725E 03	1.829E 02	9.5156-02	1.665E 02	8.659E=02
4.480E 01	7.676E 01					02 m6.251E 02	1.785E 03	1.974E 02	1.0278-01	1.674E 02	8.708E-02
4.481E 01							1,786E 03	1.9736 02	1.0265-01	1.6758 02	8.709E+02
	7.672E 01					02 -6.2686 02					
4.625E 01	7.042£ 01					02 =8.868E 02	1.963E 03	1.811E 02	9.421E-02	1.702E 02	8.854E=02
4.626E 01	7.038E 01					02 -6.887E 02	1,964E 03	1.810E 02	9.415E=02	1.703E 02	8.85SE=02
4,731E 01	6.579E 01					02 -1.088E 03	2,094E 03	1.692E 02	8,801E=02	1.723E 02	8.961E=02
4.733E 01		. 6.700E U1	#7.165E UZ	←∠. 056E 03	3620.64	02 -1.093E 03	2.097E 03	1.693E Q2	8.8006.02	1.723E 02	8.963E@02
4.811E_01	6.695E 01	5.776E 01	~5.697E 02	-2.265E 03	3500.1-	03 p1.233E 03	2,194E 03	1.722E 02	8,957E=02	1,486E 02	7.727E=02
4.877E 01	4.984E 01	4.984E 01	-4.037E 02	-2.430€ 05	-1.088E	03 -1.342E 03	2.277E 03	1.282E 02	6.667E=02	1.282E 02	6.647E=02
4.878E 01	4.972E 01	4.972E 01	04-011E 02	#2.432E 03	#1.089E	03 -1.343E 03	2.278E 03	1.279E 02	6.651E=02	1.279E 02	6.651Emg2
4.931E 01	4.340E 01					03 -1.422E 03	2.345E 03	1.116E 02	5.806E+02	1.116E 02	5.806E#02
5.072E 01	3.330E 01	3.330E 01				03 =1.616E 03	2.522E 03	8.5658 01	4.4556-02	6.565E 01	4.455E=02
5.282E 01	2.332E 01	2.332E 01				03 -1.871E 03	2.7898 03	5.499E 01	3.120E=02	5.999E 01	3.120E=02
5,332E 01	2.1656 01	2.165E 01				03 #1,926E 03	2.852E 03	5.549E 01	2.8966-02	5.569E 01	2.696£=02
5.407E 01									2.7016-02		
	2.019E 01	2.0198 01				03 -2.008E 03	2,948E 03	5.193E 01		5-193E 01	2.701E=02
5.483E 01	1.871E 01	1.871E 01				03 -2.089E 03	3,046E 03	4.813E 01	2.5038-02	4.813E 01	2.503E+02
5.576E 01	1.710E 01	1.710€ 01				03 =2.184E 03	5,164E 03	4.398E 01	2.2886=05	4.396E 01	2.2886=02
5.6268 01	1.623E 01	1.623E 01				03 42,233E 03	3,209E 03	4.174E 01	2.1/16+05	4.174E 01	2.171E=02
5.631E 01	9.26ZE 00	1.613E 01				03 =2.239E 03	3.216E 03	2.382E 01	1,2396-02	4.150E 01	2.158E=U2
5.645E 01	8.565E 00	1.5896 01	8.302£ 02	#3.813F 03	-1.561E	03 -2.252E 03	3.234£ 03	5.38SE 01	1.2596=02	4.087E 01	2.120F=05
15.653E 01	1.575E 01	1.575E 01	8.366E 02	-3.824E 03	-1.563E	03 #2.260E 03	3,245£ U3	4.051E 01	2.107E-02	4.051E 01	2.107E=02
5.681E 01	1.5266 01	1.526E 01				03 -2.287£ 03	3.280E 03	3.926E 01	2.042E-02	3.926E 01	2.0426=02
€ 5.704E 01	1.428E 01	1.428E 01				03 =2.309E 03	3.309E 03	3.672E 01	1.910E-02	3.672E 01	1.910E+02
N 5.776€ 01	1.111E 01	1.111E 01				03 -2.377E 03	3.402E 03	2.859E 01	1 487E-02	2.859E 01	1.4876-02
5.878E (1	6.337E U0	6.337E 00				03 -2.4635 03	3.532E 03	1.630t 01	8.478E+03	1.630E 01	8.478E=03
6.079E 01	1.8646 01	1.6645 01				03 -2.630E 03		4.794E 01	5 493F 05	4.794E 01	2 4936-02
							3.790£ 03				
6.221E 01	1,701E U1	1.701E 01	THEODE VE		-1 * CA 0F	03 -2.752E 03	3.972E 03	4.374E 01	2.275E=02	4.374E 01	2.2756.02

3	. XABS	P=18	P#08	PDA	GOX	G = I B	6468	CSWALL	P#18/P80	P#18/P10	P#Ub/P80	P=Q8/P10
	6.468E 01	2.110E 01	2.110E 01			03 #1.760E 0		4.2898 03	5.427E 01	2.8236+62	5.427E 01	2.8236-02
	,							• • • • •				
	6.505E 01	5.145E 01	2.173E 01			03 m1.7746 0		4.5376 03	5,517E 01	2.8706-02	5.588E 01	2.907E=02
	6.509E 01	2.145E 01	2.179E 01	9.288F 0	2 =4,786€	03 +1.775E 0	3 =3.011E 05	4.342E 03	5.517E 01	2.6706.02	5.605E 01	2,915E=02
N	0.529E 01	2.0398 41	2.212E 01	9.2886 0	2 =4,811E	03 -1.782E 03	5 =5.029E 03	4,3686 03	5.244£ 01	2.7276=02	5.691E 01	2,9608-02
<i>1</i> 27	6.695E U1	1.157E 01	9.690E DO	1.106E 0	3 =4.984E	03 -1.832E 0	3 -3.152E 03	4,583E 03	2.976E 01	1.548L=02	2.492E 01	1.296E.02
N	6.76ZE 01	8,308£ 00	9,315E 00	1,303E 0	3 -5.038E	03 -1.848E Q	5 -3.190E 05	4,665€ 43	2.137£ 01	1,1116-05	2.396E 01	1.2466-02
	6.839E 01	4.560E 00	7.116E 00	1.503E 0	3 -5,095E	03 -1.862E 0	3 -3,233E 03	4,760E U3	1.173E 01	6.100£=03	1,830E 01	9.5206-03
	6.911E 01	3,561E 00	5.0602 00	1.632E 0	3 =5.147E	03 =1.873E 0	5 -3.273E 03	4.848E 03	9,160E 00	4.764E=03	1.301E 01	6.769E#U3
	6,972E 01	2,7155 00	4,280E 00	1.7165 0	3 +5,108E	03 m1.881E 0	3 -3.307E 03	4.922E 03	6.983E 00	3,652E=03	1.101E 01	5.726E-03
	7.067E 01	2.040E 00	3.065E 00	1.810E U	3 +5.245E	03 -1.890E 0	5 ₩3,355E 03	5.0368 03	5,248E 00	2.730E-03	7.884E 00	4.100E=03
	7-11QE 01	1.735E JO	2.813E 00	1.843E 0	3 -5.208E	03 #1.893E 0	3 -3.375E 03	5.088E V3	4,463E 00	2.3216=05	7.235E 00	3.703£#03
	1.263E 01	1.8298 00	1.915E 00	1,941E 0	3 =5,351E	03 -1.903E 0	3 *3.428£ 03	5,2738 03	4.703E 00	2.4466#03	4,926E 00	2,562E+03
	7.353E 01	1.884E 00	6.500E=01	1,999E 0	3 -5,364E	03 -1.907E 0	3 =3.457E 03	5,372E 03	4.849E 00	2,520E=03	1.672E 00	8.696E=04
	7.354E 01	1.8846 00	6.444E=01	2.000£ 0	3 -5,305E	03 -1.907E 0	3 +3.457E 03	5,372E 03	4.846E 00	2.5208-03	1.657E 00	8,6205,04
	7-486E 01	1,965E 00	0.000	2,041E 0	3 -5.4216	03 -1.914E 0	3 -3,508E 03	5,424E 03	5.054E 00	2,6296=03	0.000	0.000
	7.771E 01	2.125Ē 00	0.000	2.123E 0	3 -5.433E	03 =1.925E 0	3 -3,508E 03	5,523E 03	5,466E 00	2.843E=03	0.000	0,000
	8.161E 01	1,475E 00	0.000	2.200E 0	3 -3.444E	03 =1.937E 0	3.508E 03	5,628E 03	3./94E 00	1.973E=03	0.000	0.000
	8, <u>44</u> 2E 01	1.300E 00	0.000	2,231E 0	3 +5,455E	03 -1.947E 0	3 -3.50BE 03	5,682E 03	3.344E 00	1.739E=03	0.000	0.000
	8.728E 01	1.795€ 00	0.000	2,268E 0	3 =5.472E	03 #1.965E U	\$ -3.508E 03	5,705E 03	4.617E 00	2.401E=03	0.000	0.000
	8.729E 01	1.796E 00	0 - 000	2.2685 0	3 #5.472E	03 m1.965E 0	3 -3.508E 03	5.705L G3	4.620E 00	2.403E=03	0.000	0.000

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RABJET PERFORMANCE

ENGINE PERFORMANCE			INLET	
NO MEASURED THRUST	. 6886	MASS FLUM MATIU. ACCITIVE DRAW COELIFITING PRESSURE DELTA PTZ	FFICIENT	0.9863 0.0004 0.1626 0.1181 (PSI) 0.3961 0.1649
REGENERATIVE=CODLED ENGINE PERFO CALCULATED STREAM THRUST	6820. (L8F) 1775, (L8F) 1674. (L8F#8FC/L8M)	INTET PROCESS EFF KINETIC ENERGY EF KINETIC ENERGY EF ENTHALPY AT PO	ICIENCY - SUPERSORIC. ICIENCY - SUBSORIC. FICIENCY - SUPERSORIC. SUPERSORIC	0.9055 0.9379 0.8876 =6.20 (BTU/LBM)
MOMENTUM AND FORCES			COMBUSTOR	
INLET FRICTION DRAG INLET MOMENTUM CHANGE COMBUSTOR FRICTION DRAG COMBUSTOR STRUT DRAG COMBUSTOR MOMENTUM CHANGE NOZZLE FRICTION DRAG NOZZLE STRUT DRAG NOZZLE MOMENTUM CHANGE NOZZLE PRESSURE INTEGRAL EXTERNAL FRICTION DRAG	0,77 (LBF) 1407, (LBF) =790, (LBF) =669, (LBF)	EQUIVALENCE RATIO COMBUSTOR EFFICIE TOTAL PRESENTERA COMBUSTOR DISCHARG INJECTOR DISCHARG VACUUM STRLAM THR NOZZLE COFFFICIEN PROCESS EFFICIENCE	NOZZLE UST COEFFICIENT CS. T CT.	1.340 0.608 1.449 0.7744 0.7733, 0.7602, 0.87633, 0.7602,
BNOITATA		F	UEL INJECTORS	
NOMINAL CONL LEADING EDGE	34,884 (IN)	INJECTORS	STATION	VALVE
INLET THROAT	0.3146 (IN) 40.400 (IN)	1 A 1 B	40.400 41.300	8
NOZZLE SKROUD TRAILING EDGE	134234 (IN)	1 C 2 A	44.300 48.775	D
STRUT LEADING EDGE	07.291 (IN) 56.455 (IN) 65.055 (IN) 65.055 (IN)	2 C 3A 3B 4	46,250 54,065 56,250 44,800	Ā

t = 261.41 sec.

SUPMARY REPORT

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(C)	9	Ţ	н		GANMA	hOL WT	SONV	MACH	VEL	S	v/A	₩	A/AC	MONTH	Ç	IVAC	PHI	ETAC
	WIND TUNNEL	i	ر د ن		• •		••••			•		''	-, -,		•		. ,	F 1 M G
	0.000 746.749	2981	665.2(7011	1.2943	28.852	2579											
	0.000 0.389	403	932.46	071	1.3987	28.851	985	5.997	5908	1.826	0.10655	24.906	0.0859	4030	9.784	187.3		
	SPIKE TIP NS	2	0 4	7.,	182,01	Faina*	,,,		3,00	TIOLD	0440033	201191	· # 40 3 7	3421	78704	10117		
	0.600 18.062		665.2(7011	1 2942	JR. HE.	2579											
	0.600 16.307	2913	644-51	7911	1 204%	29 921	2661	0 000	1010	3 A97	0.10655	34 904	0.0000	4070		104 7		
	WIND TUNNEL	2 2	0 0	1111	1 1 2 4 6 3	E0 + 03T	2031	0.400	1014	E.003	0+1/022	20.400	0.9024	4710	1,688	104./		
		2021	445 74	2.1.	4 3047	50 055	2070											
	0.000 0.380	400)5.266	/913	1.2743	20.002	20/7	4 - 21				6. AFA	4					
	SPIKE TIP NS	-00	-33.01	90)	1.340/	20,031	702	0,021	2411	1.020	0.10476	50.424	0.9859	4456	9,624	10/.3		
	0.600 18.062	2001	445 24	4.4.	4 3005													
					1.2942				000									
	0,600 16,374 INLET THROAT	_	042.21	172)	1.6405	50.001	2225	0.341	444	2.083	0.10476	20.454	0.9859	4956	1.626	10/.5		
		5	0 2															
	40,400 304,297			774)	1.5422	28,851	2563											
	40,400 15,403		220.8(350)	1.3536	28.851	1818	2,558	4651	1.884	0.94378	36,906	0.1113	4329	68.222	160.7		
	INLET UPNESK	5000	0 3															
	40.400 304.297			779)	1,2955	26,051	2563											
	40.400 13.237	1362	506.36	336)	1.3569	28.851	1785	2.650	4729	1.884	0.85798	26.906	0,1224	4370	63.051	162.4		
	INLET DANKSK	7	0 4															
	40.400 124.007	2941	653.2(779)	1.2955	28.851	2563											
	40,400 106,700	2842	623,2(750)	1.2986	28.851	2255	0,485	1224	1.946	0.85798	26,906	0.1224	4370	16,320	162.4		
	COMBUSTOR	8	1_ 2															
	40.410 303.772			779)	1,2955	28,651	2563											
	40,410 15,415		30.155	350)	1.3536	28,851	1819	2,557	4650	1.684	0.94366	26,906	0.1113	4328	68,193	160.9		
	COMBUSTOR 0	9	2 21										- '			-		
	41.302 188,688			833)	1,2989	26,521	2659											
	41.302 18.905		283.6(451)	1.3431	26,521	2044	2,148	4391	2.051	0.95205	27.093	0.1111	4235	64.962	156.3	0.24	0.07
		10	3 21					•					•				~	
	41.312 203.382			8:1)	1.3021	26,446	2633											
	41.312 18.944	1582	284.0(429)	1,3477	26,446	2002	2,192	4389	2.039	0.95282	27.093	0.1110	4234	64.983	156.3	0.24	0.01
		11	4 21			-							,					• • • •
	41.377 203.314		668.71	808)	1.3027	26,435	2629											
	41.377 19.199	1561	286,90	428)	1.3479	26.434	2002	2.183	4371	2.038	0.95285	27.093	0.1110	4226	64.723	156.0	0.24	0.00
		12	5 21						-		•					,-;•-		
	41.500 199.245	2819	668.3(807)	1.3028	26.433	8565											
	41.500 19.975	1604	294.10	435)	1.3467	26.433	2015	2.147	4328	2.039	0.95316	27.093	0.1110	4212	64.102	155.5	0.24	0.00
	COMBUSTOR 0	13	6 21					• -					******				••••	.,
	42.460 175.014	2807	664.6(803)	1-3032	26,433	2523											
	42.460 19.354	1637	303.91	445)	1.3451	26.432	2035	2.088	4249	2.048	0.94374	27.093	0-1121	4133	62.311	152.6	0.24	0.00
	COMBUSTOR 0	14	7 4					- •						1000			V V III -	0100
	44.097 144.927	2892	656,9(829)	1,2989	26.548	2652											
	44,097 25,979	1914	351.20	526)	1.3322	26.548	2165	1.790	3911	2.069	0.91180	27.093	0-1160	4065	55.419	150.1	0.24	0.10
	COMBUSTOR 0	15	8 3												2244.7	,5041	V 9 C. 7	411
	44.310 141.242	2909	655,81	8241	1.2981	26.569	2658											
	44.310 26.683		356.11	5271	1 3 3 0 5	26.569	2205	1.757	3873	2.073	0.91009	27.ng1	0 (142	#A5E	80 770	(110 4	A 54	
		16	9 3		44444	~~· * ~ '			, _	*****	*******	419413	41105	4013	54.770	14401	U & /C H	411
	44,800 133,861		653,1(8#41	1.2963	26.614	2670											
	44,800 28,302	2035	366.87	5411	1.3269	26.616	2244	1.685	3785	2-079	0.90647	27.00%	0 4147	0037	57 717	1/12 6	n 5e	0 16
		17	10 2	-0.7		201010	55-40	- 90-5	2,03	# E V / 7	0 8 7 7 10 4 7	E11073	041101	4023	53.313	740 10	V . F.4	U + 1 3
		2944	653.1(8 # # 3	1-2044	24.410	2670											
	44.812 28.302	2035	366-01	5441	1 1274	24.444	22/14	1.445	2727	3 090	0.90645	27 402		,, A 7 A	E 2 - 5.0"	148 -		
		18	11 "	~0 • 1	T T SEE LA	COINTO	4540	1 1003	3103	5.019	0440043	21+0A3	0 1 1 0 /	4032	53,298	140.8	V + 24	0.13
			644,5(8431	1.2074	26-711	3400											
	46.260 28.280	2131	367-01	2031	1 1337	24 742	2200	1 234	7754	7 000								
		~ · ~ ·	201946	70.43	4	50115	EE41	1.020	3163	Z 0 U Y U	0.85395	21.043	0.1239	4032	49.411	រីពន្ធ 🕏	0.24	0.23

ATHOM DAYA IVAL PHI ETAC GAMMA FULKT SUNV HACH VEL Coreustor u 19 12 4 112.016 3364 656.1(910) 1.2855 26.905 2742 47.310 28.264 2302 361.9(639) 1.5142 26.906 2365 1.572 3717 2.107 0.79457 27.093 0.1331 4094 45.901 151.1 0.24 0.39 47-310 COMBUSTOR 0 20 13 2 47.337 111,679 3171 637.9(913) 1.2852 26,913 2744 47.337 28.353 2311 362.2(6@2) 1.3138 26.914 2368 1.568 3714 2.108 0.79344 27.093 0.1333 4095 45.795 151.2 0.24 0.40 COMBUSTOR 0 21 14 48.110 104.860 3296 633.5(951) 1,2790 27.069 2783 27.444 2031 353.3(677) 1.3080 27.071 2417 1.549 3744 2.120 0.74038 27.093 0.1429 4157 43.079 153.4 0.24 0.52 48.110 COMBUSTOR 0 22 15 48,787 195,875 3252 630,0(937) 1,2810 27,030 2768 22.363 2276 316.6(629) 1.3138 27.032 2345 1.689 3959 2.116 0.68066 27.093 0.1554 4224 41.683 155.9 0.24 0.49 48.787 COMBUSTOR 0 23 16 107.238 3215 627.5(926) 1.2827 26.997 2756 49.317 49.317 19.133 2158 290.1(594) 1.3183 26.999 2289 1.795 4109 2.112 0.63659 27.093 0.1662 42/4 40.648 157.8 0.24 0.47 COMBUSTOR 0 24 17 3 50.727 102.859 3248 621.9(935) 1.2809 27.053 2765 14.887 2076 248.8(568) 1.3207 27.055 2244 1.925 4321 2.117 0.54254 27.093 0.1950 4382 36.431 161.7 0.24 0.51 50.727 COFBUSTOR 0 25 18 52.827 88.066 3433 614.2(992) 1,2713 27.290 2820 12.450 2203 217.7(604) 1.3135 27.295 2296 1.940 4454 2.137 0.44468 27.093 0.2379 4509 30.783 166.4 0.24 0.70 52.827 COMBILITOR 0 26 19 202 53.327 73.007 3742 612.3(1087) 1.2544 27.664 2904 18.092 2776 287.4(777) 1.2895 27.679 2536 1.590 4032 2.163 0.42651 27.093 0.2480 4544 26.724 167.7 0.24 1.00 53.327 COMBUSTOR 0 27 20 54.067 56.694 3734 646.6(1226) 1.2574 24,348 3096 54.067 21.355 3033 377.6(970) 1.2838 24.360 2819 1.301 3668 2.422 0.40708 27.412 0.2629 4563 25.207 166.5 0.64 0.46 COMBUSTOR 0 28 21 54.079 56,628 3738 646.5([227] 1.2571 24.352 3097 21.399 3039 378.1(972) 1.2835 24.365 2821 1.299 3665 2.422 0.40678 27.412 0.2631 4564 23.166 166.5 0.64 0.47 54.077 COMBUSTOR 0 29 22 54.837 52,748 4048 642,4(1336) 1,2372 24,700 3175 24.750 3485 413.5(1127) 1.2614 24.729 2973 1.159 3385 2.443 0.58467 27.412 0.2782 4647 20.233 169.5 0.64 0.60 54.837 COMBUSTOR 0 30 23 50,372 4328 636,7(1435) 1,2168 25,032 3234 55,760 55.760 27.266 3871 437.3(1263) 1.2383 25.085 3082 1.025 3159 2.457 0.36122 27.412 0.2963 4761 17.733 173.7 0.64 0.73 COMBUSTOR 0 31 24 4 45.244 4595 662.2(1703) 1.1961 22.698 3470 56.252 28.609 4266 484.7(1563) 1.2124 22,772 3360 0.887 2980 2.707 0.29452 27.731 0.3576 5262 13.639 189.8 1.04 0.63 56.252 0 32 25 2 COMBUSTOR 56,262 45.227 4597 662.1(1703) 1.1960 22.700 3470 56.262 28.636 4269 485.1(1564) 1.2121 22.774 3361 0.886 2976 2.707 0.29425 27.731 0.3679 5264 13,610 189,8 1,04 0,63 0 33 26 COMBUSTOR 56.317 45.107 4628 661.7(1716) 1.1932 22.734 3475 28.118 4291 477.8(1572) 1.2097 22.815 3363 0.902 3033 2.709 0.29342 27.751 0.3690 56.317 52/2 13,632 190,1 1,04 0,64 0 34 27 COMBUSTOR 56.457 44.986 4653 660.8(1726) 1.1910 22.762 3479 28,309 4326 479,6(1586) 1.2068 22.646 3370 0.893 3011 2.710 0.29132 27.731 0.3717 56,457 5290 13.631 190.8 1.04 0.65 COMBUSTOR 0 35 28 56.537 45.694 4647 660.2(1723) 1.1918 22.757 3478 56.537 29.386 4334 487.4(1990) 1.2069 22.636 3374 0.871 2940 2.708 0.29463 27.731 0.3675 5300 15.462 191.1 1.04 0.65 COMBUSTOR 0 36 29 56,817 45,456 4680 658,3(1736) 1,1889 22,/96 3484 30.150 4384 492.1(1610) 1.2030 22.877 3385 0.852 2884 2.708 0.29560 27.731 0.3688 5333 13.158 192.3 1.04 0.60 56.817 NO COMBUSTUM 0 37 30 N 57.043 46.116 4727 650.8(1755) 1.1848 22.848 3491 **~**3 57.043 30.282 4436 489,5(1630) 1.1962 22,938 3394 0.852 2893 2.709 0.29316 27,731 0.3693 5358 13,179 193.2 1.04 0.68

		P	1	н	GAMMA	MOLWT	SONV	MACH	YEL	8	W/A	27	A/AC	номін	D)	I VAC	Ph1	ETAC
	COMBUSTOR	Q																
	57.767	46,097			1.1751	22.970	3506											
00	57.767	30.705	4563	487.3(1680)	1.1862	23.078	3415	0.841	2871	2.712	0.28851	27.731	0.3753	5426	12.872	195.7	1.04	0.74
	COMBUSTOR	U	39	32 4				•	•				- 43720		104012	*		4.4
	58.787	46,529	4856	645.7(1806)	1.1729	23.010	3508											
	58.787	32.062	4612	493.8(1700)	1.1825	23.114	1425	0.805	2757	2.711	0-28667	27. 731	0.2777	ちカプス	12,282	107 5		A 7E
	COMBUSTOR	0	40	33 4					,			2, ,	V # 3	2410	121202	1,115	1104	415
	60.797	47.393	4925	634,4(1833)	1.1665	23.108	3516											
	60.797	30.675	4649	455.9(1713)	1.1763	23.244	3420	0.874	2989	2.700	0.29664	37.741	0 2450	SAKA	13,779	104 7		0 70
	COMBUSTOR		41	34 4			# 4 F A	4407	E 10 4	L 1 7 0 7	0 8 2 7 0 0 4	214121	W#3030	2000	13.//7	14012	1.04	4.14
	62,217	48.074	4948	627.1(1841)	1.1645	23.148	3518											
	62.217	28.312	4615	410.6(1697)	1.1761	21.418	3402	0.068	1201	2.707	A . ZABAR	27 741	A 4564	E 11 4 11	46 606	105 5		A 84
	COMBUSTOR	REGEN	42	35 21			J-0E	0 4 7 0 0	20,1		V 1 3 0 4 0 0	611131	A # 2 2 2 2	3414	131202	12305	1.04	0.01
	62.217	48.074	4965	641.1(1849)	1.1636	23.133	3524						۲	,				
	62.217	28.885	4646	431,6(1711)	1 1743	23.300	1412	A . 049	1210	2 710	0.30048	32 771		E #20	~~~	101		
	NOZZLE AL	E	43	36 5		231244	2-10	A442.	3230	24110	0120400	214131	0.3033	2450	12122	14242	1.04	0.61
	87.293	48.074	4948	627.1(1835)	1.1645	23.148	3518											
	87.293	1.244	2591	=536.4(871)	1.2795	23.584	2644	2.886	7630	2.707	0.05680	27 711	1 0771	7404	4 430	000 u	4 04	
	NOZZLE P	0	44	37 5		021204	,,,,,,	21000	1030	F 6 1 0 1	0403307	6/4/31	1143/1	/174	0,020	\$37.4	1.04	0.01
	87.293	48.074	4948	627.1(1835)	1.1645	21.148	151 B											
	87.293			*760.0(648)	1.3025	23.584	7240	3 E60	8771	יי מיי כ	0 03480	3 W W W W I	# =450	7444	7 044	~~	4 64	
	NOZZLE AL	REGEN	45	38 5		42,304	2240	3,300	0331		0 8 0 2 4 0 0	511131	4 4 7 0 2 0	1010	3.211	2/4+0	1.04	0.61
	87,293			641.1(1849)	1.1636	23,133	3524											
	87.293	1.252	2614	=527.6(880)	1.2786	23.584	2468	2.081	7647	2.710	A AEE80	22 224	1 0771	2010	4 4 5 7	m.a	4 54	
		REGEN	46	39 5	1,00	05,504	4492		,,,,	*****	0103307	214191	104217	(515	0,043	200.1	1.04	0.01
	87,293	48.074	4965	641.1(1809)	1-1636	23.133	1524											
	87.293	0.389	2010	-754.3(654)	1.3018	23.584	23/10	7 . KRA	8754	2.71A	0.02448	27 711	A 2069	7470	* 205	175 F		
	FICTIVE C	MBUSTR	67	60 0	.,	001004	4047	31300	0220	## LIO	040E400	2/1/31	4.3001	1037	3,205	61252	1.04	0.01
	62.217	304.297	5416	627.1(2031)	1 . 1637	23.633	2641											
	62.217	0.389	1492	01167.7(464)	1.3220	24.205	2013	4.708	9477	2.550	0.03870	27.711	3 2074	8449	E 200	#A0 4		4 00
	FICTIVE N	DZZLE	68	61 0		~~*****		4 1 7 0		41270	4402010	# () / J L	64/7/0	044/	5.700	304.0	1 = 04	1 # 0 0
	87.293	24.203		583.3(1790)	1.1600	23.124	3460											
	87.293	1.718	3146	m315.3(1088)	1.2569	23.577	7407 744C	2.122	6704	3 7R7		59 571	1 0781	4425	C 084	220 -		
	- ₩					-3-5(E-001	C 6 7 6 6	0110	E # / 3 (V 4 V 2 3 0 Y	2/1/31	1.4371	0036	5.824	134.7	2 . 04	0.41

PENDING -	Anda OFIITA	- 1/2 3	itac + sotenti	FRIA O	10 bizzi	ADSIGN II A C.	701.0				PAGE 4
XAPS	P=IR	P≖Ob	404	GOX	U⇔jp	Q#0B	CAMALL	Pw]e/FSt	1 = 15/PTO	P=0b/FS0	P=08/P10
6.981E+01	1.040E 00	0.000	=4.001E=01		n .000	0.006		2.6748 00	1.343605	0.000	0.000
1.836E 01	1.040E 00	0.000	+3.403t v1		0.000	2.000	1.6341 02	2.674F 00	1,3436=03	0.000	0.000
3.0708 01	2.205E 00	0.000	-1.66ZE U		0.000	2.000	5.753E UZ	5.6695 00	2.953t=U3	0.600	0.606
5.508F 01	1.886E 00).000	-3.635E 02		0.000	v. 000	6.404E V2	4.490F UO	5.203E=03	0.000	0.000
5.5198 01	5.917E UO	:	00 =4.296E 0		0.000	0.000	6 855E 02	1.00/F 01	5.246L=03	1.475E 01	7.6846-03
3.520E 01	3.919E UO		00 -4.297E V		0.000	0.000	6.858E 02	1.000E 01	5.2486#03	1.467E 01	7.640E#03
3.555E 01	4,015E 00		00 =4.373E 02		0.000	v.U00	7.2081 02	1.032E 61	5.377t=03	9.775E 00	5.091E=U3
3,5877 01	3,959E 00		40 -4.5201 02				7.530L U2	1.0188 01	5.3026=03	5.335£ 00	2.779E=03
5.60at 01	5.925E 00		00 -4 622E 08				7.727E VZ	1.009E 01	5.256t-03	/.401F 00	3.855E=03
5.648E 01	4.221E 00		00 94.812E 00				8.164E 02	1.085E 01	5.653t=03	1.189F 01	6.1956-03
3.701E 01	4.2256 00					02 -1.176E 01	8.722E C2	1.086E 01	5.6581#03	1.7568 01	9.149E=03
3./33E 01	4.109E 00					10 3575 14 SO	9.0646 02	1.056E 01	5.502E=03	2.095E 01	1.091E=02
3.803E 01	3.850E 00					02 -2.425E 01	9.832E 02	9.8956 00	5.156E+03	3.414E 01	1.778E=02
3.835E 01	5.402E 00					02 -2 804E 01	1.019E 03	1.389E 01	7.234L=03	4.007E 01	2.087E=02
3.875E 01	7.377E 00					02 -3 282E 01	1.064E 03	1.896E 01	9.878t=03	3.988E 01	2.077E#02
3,882E 01	7.704E 00					02 -3 361E 01	1.0/2E 03	1.981E 01	1.0326-02	3.985E 01	2.076E-02
3.901E 01	8.650E 00					02 -3.587E 01	1.094E 03	2.224E 01	1.158t=02	4.043E 01	2.1066-02
3.933E 01	1.376E 01					02 #3.956E 01	1.130E 03	3,537€ 01	1.8426-02	4.139E 01	2.156E=02
3.950E 01	1.655E 01	1.4058	01 -5.401E 02	-2.937E 0	2 -2.52ZE	02 #4.155E 01	1,150E 03	4.255E 01	2.216E=02	3.612E 01	1.881E-02
3.982E 01	1.7075 01					02 -4.513E 01	1.187E 03	4.389E 01	2.286£=02	2.648E 01	1.379E=02
4.000E 01	1.737E 01	1.023E	01 -5.682E 02	-3.104E 0	2 -2.632E	02 -4,716E 01	1,209E 03	4.467E 01	2,327£=02	2.631E 01	1.371E=02
4.040E 01	2.065E 01					02 -5.200E 01	1.256E 03	5,309E 01	2.7666.02	2,595E 01	1.351E=02
4,041E 01	2.073E 01	1.0096	0; 5.947E 02	03.253E 0	2 -2.732E	02 =5.214E 01	1,2578 03	5.330E 01	2,7766#02	2.594E 01	1.351E+02
4.130E 01	2.804E 01					02 67.972E 01	1.362E 03	7,209E 01	3,7556∞02	2.512£ 01	1.308E=02
4 - 13 E 01	2.812E 01					02 #8.020E 01	1.3636 03	7,230E 01	3.766E=02	2.511E 01	1.308E=02
4.138E 01	2.865E 01					02 =8.344E 01	1.371E 03	7.367E 01	3.837£402	2.505E 01	1.305E=02
4.150E 01	2.966E 01					02 -6.999E 01	1.386E U3	7.626E 01	3.9726.02	2.645E 01	1.378E#02
4.246E 01	2.419E 01					02 =1.579E 02	1.501E 03	6.218F 01	3.239E=07	3.733E 01	1.944E=02
4.410E 01	3.022E 01					02 03.0525 02	1.699E 03	7.770E 01	4.0476=02	5.589E 01	S.911E=02
4.431E 01	3.101g 01					02 03.256E 02	1.725E 03	7.97ZE 01	4.152E=02	5.749E 01	2.994E=02
4.480E 01	3.281E 01 3.278E 01					02 a3.759E 02	1.784E 03	8.436E 01	4.3546=02	6.116E 01	3.186E-02
4.626E 01	1. T T 1 . 1 T T T					02 03,772E 02	1,786£ 03	8.427E 01	4.389E=02	6.125E 01	3.191E=02
4,731E 01	2.541E 01					02 =5.440E 02	1.964E 03 2.094E 03	7.328E 01	3.8171=02	7.213E 01	3.757E=02
4.734E 01	2.5518 01					02 =6.731E 02	2.097E 03	6.532E 01 6.598E 01	3.402E=02	4.001E 01	4.168E=02
4.811E 01	2.840E 01					02 -7.650E 02	2.194E 03	7.301E 01	3.416E=02 3.803E=02	6.021E 01 6.810E 01	4.178E=02
4.879E 01	2.2366 01					02 =8.315E 02	2.278E 03	5 749E 01	2.9956-02	5.749E 01	3.547E#U2 2.995E#02
4.932E 01	1.913E 01					02 =8.764E 02	2.345E 03	4.919E 01	2.5626.02	4.919E 01	2.562E#02
5.073E 01	1.489E 01					02 -9.751E 02	2.522E 03	3.827E 01	1.9446-02	3.827E 01	1.994E=02
5.283E 01	1.245E 01					02 *1.106E 03	2.789E 03	3.201E 01	1.6671-02	3.201E 01	1.667E=02
5.3338 01	1.809E 01					02 01.143E 03	2.852E 03	4.651E 01	2.4236-02	4.651E 01	2.423E=02
5.407E 01	2.1368 01					60 3515.1= 50	2.947E 03	5.490E 01	2.8006-02	5.490E 01	2.860E=02
5,40gE (1	2.140E U1					02 -1.213E 03	2.948E 03	5.502E 01	5.866F=05	5.50ZE 01	2.866E=02
5.484E 01	2.475E 01					02 -1.300E 03	5.046E 03	6.363E 01	3.314E=02	6.363E 01	3.314E=02
5.576E 01	2.727E 01	2.7275				02 -1.427E 03	3.164E 03	7.010E 01	3.652E=02	7.010F 01	3.652E=02
5.625E 01	2.861E 01	2.861E				02 -1.505E 03	4.208E 03	7.355E 01	3.831E-02	7.355E 01	3.831E=02
5.626E 01	10 3498.5	2.864E		. ≈2°308E 0	3 =8.613E	02 -1.506E 03	3.209E 03	7,362E 01	3.8356-02	7.3628 01	3.835Ep02
5.632E 01	2.745E 01	2.679E	01 6.175E 02	. 02.378E 0	3 =8.628E	02 #1.515E 03	3.216E 03	7.057E 01	3.676E-02	7.401E 01	3.855E-02
5.64AE 01	2.745E 01	2.917E	01 A.364E 03	2 02.405E 0	3 P8.665E	02 -1.539E 03	3.234E 03	7.057E 01	3.676E-02	7,499E 01	3.906E=02
5.654E 01	2.939E 01	2.939g				02 m1.552E 03	3.245E 03	7.555E 01	3.9356-02	7.555E 01	3.935E=02
5.082E 01	3.015E 01	3.015E				02 -1.597F 03	3.280E 03	7.751E 01	4.0376=02	7.751E 01	4.037E=02
5.70#E 01	3.028E 01	3.028E				02 -1.634E 03	3.309E 03	7.785E 01	4.055E=02	7.785E 01	4.055E-02
5.777E 01	3.070E 01	3.070F				02 -1.748E 03	3.402E 03	7.894E 01	4.112E=02	7.894E 01	4,1126-02
5.879E 01	3.2068 01	3,2065				02 -1.898E 03	3,532E 03	8.243E 01	4.294F=05	8.243E 01	4.29#E=02
6.080E 01	3.0672 01	3.067E				02 -2.165E 03	3.790E 03	7.886E 01	4.108E-02	7.886E 01	4.108E=U2
OPERSE 01	2,831E 01	6.03]F	n1 0 4 1 4 1 F 0 5	. ******* 0	•a =1.005€	03 -2.334E 03	3.972E 03	7.279E 01	3,791E=02	7.279E 01	3.791t=02

XABS	P#18	P#08	PDA	x o o	U*IB	G≖OH	CANALL	P-IB/PS0	P=15/P10	P#08/PS0	P=08/P F0
6.46BE 01	2.270E 01	2.270E 01	8.791E 02	-3.645E 05	-1.084E	03 -2.611E 03	4.289E U3	5.837E 01	3.040L=02	5.837E 01	3.040£=02
6.506E 01	2.134E 01	2.185E 01	8.791E 02 .	-3.751E 03	-1.098E	03 -2.684E 03	4,337E 03	5.486E 01	2.85/6#02	5.61/E 01	5.926E=05
6.510E 01	2.134E 01	2.176E 01	8.791E 02 4	♥3.757E 03	≈1.099E	03 #2.658E 05	4.342E 03	5.486E 01	2.8576.02	5.593E 01	2.9138-02
6.530E 01	2.006E 01	2,130g 01	8.791£ 02 ·	-3.785E 03	≈1.107E	03 m2.678E 03	4.368E 03	5.156E 01	2,686E=02	5.476E 01	2.852E#U2
6.676E 01	9.420E 00	8.440E 00	1.044E 03	03.974E 03	■1.158E	03 =2.816E 03	4.583E 03	2.422E 01	1,261E=02	2,170E 01	1.130E=02
6,763E 01	7.184E 00	8.400E 00	1.213E 03	■4.052E 03	-1.174E	03 #2.858E 03	4.665E 03	1.847E 01	9.621E=03	2.160E 01	1.125E#02
6,840E 01	4.615E 00	6.767E 00	1.398E 03	₩4.096E 03	≈1 - 189E	03 =2.907E 03	4.760E 03	1.186E 01	6,160E-03	1.740E 01	9,062E=03
6.912E 01	3.800E 00	5.240E 00	1.5288 03	-4.156E 03	=1.201E	03 #2.956E 03	4.848E 03	9.770€ 00	5.0896-03	1.347E 01	7.017E=U3
6,973E 01	3.110E 00	4.575E 00	1.618E 03	-4.207E 03	390S.1	03 -2.9988 03	4.922E 03	7.996E 0U	4.165E=03	1.176E 01	6.127E-03
7.068E 01	2.387E 00	3.540E 00	1.724E 03	=4.277E 03	01.219E	03 =1.058t 03	5,036E 03	6.137E 00	3.197£#03	9,101E 00	4,741E=03
7.111E 01	2.060£ 00	3.2502 00	1.763E 03 4	-4.305E 03	=1.224E	03 =3.082E 03	5.088E 03	5.296E 00	2.759E403	8.357E 00	4.3538+03
7.264E 01	2.078€ 00	5.550E 00	1.876E 03 :	-4.383E 03	=1.236E	03 -3.147E 03	5.273E 03	5.343E 00	2.783E=03	5.707E 00	2,973E=03
7.354E 01	2.089E 00	7.750g=01	1.943E 03	-4.422E 03	-1.242E	03 -3.180E 03	5.372E 03	5.371E 00	2.798E=03	1.992E 00	1.038E=03
7.354E 01	2.089E UO	7.686E=01	1.944E 03	-4.423E 03	#1.243E	03 43.180E 03	5.372E 03	5.371E 00	2.798E=03	1.976E 00	1.029E=03
7.487E 01	2.105E 00	0.000	1,988E 03	-4,489E 03	-1.251E	03 ×3.239E 03	5,424E 03	5.412E 00	2.819E=03	V.000	0.000
7.7725 01	2.105E 00	0.000	2.073E 03	-4,504E 03	-1.265E	03 #3.2392 03	5,523E 03	5.412E 00	2.8196.03	0.000	0.000
8.162E 01	1.260E 00	0.000	2.144E 03	-4-518E 03	⇔1.ຂ80E	03 -3.239E 03	5.628E 03	3,239E 00	1.6675-03	0.000	0.000
8.443E 01	1.360E 00	0.000	2.174E 03	₽4.531E 03	₩1.293E	03 43. 239E 03	5.682E 03	3,496E 00	1.82!E=03	0.000	0.000
8,729E 01	1.890E 00	0.000	2.213E 03	-4.554E 03	=1.315E	03 #3.239E 03	5.705E 03	4.859E 00	2.531E-03	0.000	0.000
8.729E 01	1.891E 00	0.000	2.213E 03	#4,554E 03	•1.31SE	03 #3.239E 03	5.705E 03	4.862E 04	2,532E=03	0.000	0.000
		•		•							

x	ррнAG	CURAG	CF	11
011 011 011 011 011 011 011 011	1.165c 02 1.762c 01 1.762c 01 1.745c 01 1.216c 00 2.275c 00 1.765c 00 2.750c 01 2.655c 00 2.655c 00 2.655c 01 2.655c 01 2.655c 01 1.650c 01 1.650c 01 1.650c 01 1.650c 01 1.79c 01 2.425c 01 1.79c 01 2.425c 01 1.79c 01 2.425c 01 1.79c 00 2.425c 01 1.79c 01 2.425c 01 1.79c 01 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 1.79c 00 2.425c 01 2.79c 00 2.79c 0	1.1604E 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	33533333333333333333333333333333333333	22222222222222222222222222222222222222
	5.797E=02 3.214E=01 8.114E=01 4.665E=01	3.376E 0 3.379E 0 3.387E 0 3.392E 0	2 3.329E=03 2 3.320E=03 2 3.330E=03	
5.682E 01 5.704E 01 5.777E 01 5.879E 01 6.080E 01	1.598E 00 1.266E 00 4.025E 00 5.515E 00 1.128E 01	3.408E 0 3.421E 0 3.461E 0 3.516E 0	2 3.334E 03 2 3.335E 03	3.396E+02 3.391E=02 3.380E=02 3.339E=02 3.447E=02
6.222E 01 8.729E 01 6.468E 01 6.506E 01 6.510E 01	8.910E 00 2.519E 00 1.773E 01 2.936E 00 3.151E=01	3.715E 0 3.911E 0 4.088E 0 4.117E 0	2 3.324E=03 2 3.319E=03 2 3.350E=03 2 3.341E=03 2 3.341E=03	3,400Ew02 3,039E=02 3,406E=02 3,352E+02 3,350E=02
6.530E 01 6.696E 01 6.763E 01 6.840E 01 6.912E 01	1.584E 00 1.273E 01 4.459E 00 4.723E 00 3.868E 00	4.136E 0 4.264F 0 4.308E 0 4.355E 0	2 3.3366-03 2 3.2276-03 2 3.2106-03 2 3.1676-03 2 3.1326-03	3.304E=02 2.134E=02 1.956E=02 1.585E=02 1.349E=02
6,973E 01 7,068E 01 7,111E 01 7,264E 01	2.951E 00 4.080E 00 1.672E 00 5.403E 00	4.420E 0 4.464E 0 4.481E 0 4.535E 0	2 3.110E = 03 2 3.075E = 03 2 3.061E = 03 2 3.032E = 03	1.202E=02 9.948E=03 9.174E=03 7.627E=03
7.354E 01 7.354E 01 7.487E 01 7.772E 01 8.162E 01	2.434E 00 3.468E=03 1.256E 00 2.651E 00 2.431E 00	4.559E 0 4.572F 0 4.599E 0	2 2.975E=03 2 2.975E=03 2 3.017E=03 2 3.003E=03 2 2.917E=03	5.745E=03 5.735E=03 7.674E=03 7.634E=03 5.129E=03
8,443E 01 8,729E 01 8,729E 01	1.087E 00 5.125E=01 0.000	4.639F 0	2 2.913E=03 2 2.943E=03 2 2.943E=03	5.413E=03 6.925E=03 6.928E=03

RAMJET PERFURNANCE

N	RAMJET PERFURMANCE
ELOINE BEREUSHANGE	INLET
CALCULATED THRUST	MASS FLOW RAILU
CALCILATED THRUST CUEFFICIENT 0.6347 MEASURFU THRUST CUEFFICIENT 0.7491 REGENEPATIVE-COOLED ENGINE PERFURFANCE	OFLTA PTZ
CALCULATED	INLET PROCESS EFFICIENCY - SUBSCRIC 0.9050 KINFTIC ENERGY EFFICIENCY - SUPERSURIC 0.9450
SINEAM INDUST	KINETIC ENERGY EFFICIFNCY = SUBSCNIC 0,8934 ENTHALPY AT PO = SUPERSONIC = 06.10 (ETU/LBY) SEC/LBM) ENTHALPY AT PO = SUBSONIC
MUMENTUM AND FORCES	Curbustgr
INLET FRICTION DRAG	COMBUSTOR EFFICIENCY
BUDITATS	FUEL INJECTORS
NOMINAL COML LEADING EDGE 54.884 (IN) SPIKE TRANSLATION	INJECTORS STATION VALVE
INLET IMPUATABLE SECRET	1A 40.400 1B 41.302 B 1C 44.300 2A 48.777
STRUT LEAUING EDGE	2C 46.250 3A 54.067 E 3B 56.252 E 4 44.802

t = 293.81 sec.

1-29-フェ

SUMMARY REPORT

T GAMPA MOLNT SONY MACH VEL S NIND TUNNEL */A AZAC MUNTA IVAC PHI ETAC 1 0 5 0.000 747.249 2902 659.4(785) 1.2949 26.852 2571 0.000 0.386 399 =33,4(96) 1.3987 28,651 980 6.007 5888 1,624 0.10656 26,947 0.9873 5029 9.751 186.6 SPIKE TIP NS ٠, 18,050 2962 659.4(785) 1.2948 28,851 2571 0.600 0.600 10.306 2894 | 638.9(765) 1.2969 28.851 2543 0.398 1013 2.081 0.10656 26.947 0.9873 49/2 1.678 184.5 WIND TUNNEL 747.249 2962 659.4(785) 1.2949 28.652 2571 0.000 0.000 0.379 396 033,9(95) 1.3986 28.851 977 6.027 5890 1.824 0.10507 26,570 0.9873 4960 9,618 186.7 SPIKE TIP NS 18,050 2962 659,4(785) 1,2948 28,851 2571 0.600 16.361 2896 639.66 766) 1.2968 28.851 2544 0.392 996 2.081 0.10507 26.570 0.9873 0.600 4960 1.627 186.7 INLET THROAT 40.400 506,013 2912 644,1(770) 1,2965 28,851 2650 40.406 15.225 1394 214,8(344) 1.3550 28,851 1804 2.569 4635 1.880 0.94482 26,947 0.1114 4316 68.058 160.2 INLET UPNASK 306.013 2912 644.1(770) 1.2965 28.851 2850 40.400 40.400 13.085 1540 200,5(350) 1.3582 28,851 1771 2.660 4711 1,880 0,85893 26,947 0.1225 4357 62.890 161.7 INLET ONNRSK 40.400 123.609 2912 644.1(770) 1.2965 28.851 2550 40.400 106.393 2813 614,6(742) 1,2995 28,851 2510 0,485 1216 1,943 0,85893 26,947 0,1225 4357 16,236 161.7 COMBUSTOR 0 40.410 305.431 2911 644.1(770) 1.2965 26.651 2550 40.410 15.238 1395 215.0(344) 1.3549 28.651 1805 2.567 4634 1.881 0.94470 26.947 0.1114 4316 68.028 160.1 COMBUSTOR 41.300 181.326 2875 662.0(830) 1.3000 26.319 2657 41.300 20.396 1696 292.5(463) 1.3419 26.319 2070 2.077 4300 2.064 0.95378 27.152 0.1111 4210 63.742 155.0 0.26 0.07 COMBUSTOR 0 10 3 21 195.665 2797 662.0(806) 1,3035 26,237 2629 41.310 20.447 1007 293.0(439) 1.3467 20.237 2025 2.122 4297 2.051 0.95357 27.152 0.1112 4209 63.678 155.0 0.26 0.01 41.310 COMBUSTOR 0 11 4 21 41.375 195,709 2785 661,7(802) 1,3041 26,225 2624 41.375 20.783 1605 296.2(439) 1.3469 26.225 2025 2.112 4276 2.049 0.95501 27.152 0.1110 4200 63.465 154.7 0.26 0.00 COMBUSION 41,500 , 185,140 2814 661,0(811) 1,3027 26,258 2635 41.500 22,541 1683 309.0(461) 1.3429 26,258 2069 2.029 4197 2.056 0.95523 27,152 0.1110 4183 62,304 154.0 0.26 0.03 COMBUSTOR 0 13 42,460 137,484 3083 654,4(893) 1,2902 20,564 2728 31.824 2189 368.1(611) 1.3199 26.565 2325 1.628 3785 2.101 0.94585 27.152 0.1121 4108 55.635 151.3 0.26 0.26 42.460 COMBUSTOR 0 14 44.095 110.537 3608 639.9(1055) 1.2639 27.206 2887 44.095 57.112 3135 477.9(900) 1.2804 27.212 2708 1.051 2847 2.146 0.91334 27.152 0.1161 4100 40.406 151.0 0.26 0.74 COMBUSTOR 0 15 44.310 109,989 3610 637,8(1055) 1,2637 27,215 2887 58.661 3157 482.7(907) 1.2795 27.221 2716 1.026 2786 2.146 0.91175 27.152 0.1163 4098 39.477 150.9 0.26 0.75 44.310 COMBUSTOR 0 16 44.800 109,244 3588 632,7(1048) 1,2646 27,206 2879 44.800 62.189 3181 493.6(915) 1.2788 21.211 2726 0.968 2639 2.145 0.90820 27.152 0.1167 4086 37.242 150.5 0.26 0.74 COMBUSTOR 0 17 10 0 44.810 109.228 3587 632.6(1048) 1,2646 27,206 2879 44.810 62.166 3181 493.5(915) 1.2789 27.211 2726 0.968 2639 2.145 0.90821 27.152 0.1167 4086 37.247 150.5 0.26 0.74 COMMUSTOR 0 18 11 8 46.250 102.967 3081 647.0(1003) 1.2916 23.594 2896 46.250 58.797 2709 510.5(B69) 1.3039 23.595 2728 0.958 2613 2.530 0.86595 27.465 0.1238 4095 35.164 149.1 0.65 0.21

	WENDTHO .	0004	06.0	n ett 11. c .	- F43 0.				, , - , ,		,, - 2,700								•
		P	Ţ	н	GAMPA	MULHT	SONV	44Ch	VFL	S	W/A	**	A/AC	MOFIM	ω	IVAÇ	PHI	£TAC	
	COMBUSTOR			12 2															
				646.9(1003)															
	46,260			510,4(869)	1,3038	53.240	2129	0.958	2613	4,536	0.86542	27.465	0.1239	4046	35,148	144.1	0.65	0.51	
	COMBUSTOR		20		. 2000	45.	1030												
	47.310			635.2(1084)					2700	3 354	0 50524	37 nas	6 (33)	4274	74 001	15/1	0 45	0 31	
	47.310 COMBUSTOR		21	458.5(942)	1.2732	231031	2000	0.900	2144	6.320	V 9 Q V 2 E 4	€1.403	V 0 1 3 3 E	4634	35.903	13441	V 5 Q D	A # 3 1	
	47.335			634.9(1086)	1 2798	23.860	2076												
	47.335			488,5(943)					2707	2.356	0.80434	27-465	0.4333	4236	33.632	154.2	0.65	0.31	
	COLEUSTOR		2.5		114.56	£ 3 \$ 40 £	EP4V	4 1 1 0 2	.,.,	44084	0000454	H . I . G .	C = 1 4 4 4	4650	351032	A 7" # 4	0,00	****	
	48.110			626.8(1164)	1.2662	24.110	3046												
	48,110			472.3(1016)					2781	2.374	0.7503c	27.465	0.1429	4363	32 427	158.9	0.65	0.40	
	COMBUSTOR		43		••													• •	
	48.775			641.8(1165)	1.2867	21.320	3105												
	48.775	44.264	2736	446.0(973)	1.3026	21.327	2882	1.086	3130	2.569	0.69899	27.786	0.1552	4463	34.001	160.6	1.06	0.23	
	COMBUSTOR			17 2															
	48.785			641.7(1166)															
	48.785			445.3(973)	1,3026	21.329	2883	1.068	3135	2.509	0.269900	27,786	0.1554	4465	34.009	160.7	1.406	0.23	
	COMBUSTOF		25			54	* 4												
	49,315			637,3(1213)				1 175	3100	2 602	4 - 5 7 6 7	29 904	0 1443	4673	9.0.00			A 34	
	49 _m 315 COMBUSTOR		56	406,5(988)	1 - 4 7 7 4	211400	2014	191/3	3375	2000	0 . 0 3 # 0 /	#1#(QD	0.100Z	42/6	34.480	10410	7 . 70	V.CQ.	
	50.725			626.8(1339)	1 3435	24 76/	1262												
				_340.8(1070)				1260	8748	2.412	0.55603	27.786	0.4950	4815	32.364	173_2	1 - 04	n 74	
	COMBUSTOR		~~~~		100011	C + 8 / 1.G	E117	* 9 5 7 7	3173	In 2 M A G		#11100	V \$ 1 7 3.0	4017	261204	11523	* * * * *	V 8.5 V.	
	52.825			613.4(1414)	1.2522	21.977	\$305												
	52.825	22,012	2979	237.5(1056)	1.2848	21.993	2941	1.474	4337	2.628	0.45606	27.786	0.2379	5086	30,736	183.1	1.06	0.42	
	CUMBUSTOR		28		V • • • • •										,			-•	
_	53.325			610.5(1421)	1.2511	21.999	3309												
♀ .	53.325	20.337	2948.	214.6(1043)	1.2856	22.017	2926	1.521	4451	2.630	0.45742	27,786	0.2480	5136	30.257	184.5	1.06	0.42	
2	CUMBUSTOR	0	29	22 4														-	
£	54.075			606.4(1438)															
ORIGIN	54.075			168.2(1040)	1.2049	22.073	5919	1,567	4575	2.634	0.41233	27.786	0.2631	5203	29,313	187.2	1.06	0.44	
<u>'</u>	COMBUSTOR		30																
	54.835			602-4(1444)				4 4 5 5	// M O O	5 / TI				~ ~	** ***				
d	54.835			159.5(1022)	1.5001	26.040	20 A.T.	1.025	4708	4.032	0.30995	C/+/00	0.5/8%	2502	28.529	104.4	1 . 0.6	Q. 45.	
\mathbb{R}	COMBUSTOR 55.760'		31		. 2/12/1	22 1/11	7770												
5	55.760			597.9(1466) 135.7(1028)				1.450	#800	3. A//A	0 34410	27 786	X 00 A	6120	21 741	101 b	1 04	0 04	
GE	COMBUSTOR			25 5	116043	221101	2077	1 1007	4007	4 9 9 9 9	n # 20010	212100	V & & 7 0 J	3267	51.361	14110	1 = 60	V = 40	
	56.260	50.190	4456	595.6(1650)	1.2083	22-617	3440												
5	56.260			102.8(1255)					4760	2.684	0.29494	27.786	0.3678	5503	21.820	198.1	1.06	0.61	
	COMBUSTUR	Ų	33	26 5									- 4004 / 4				* * * -	2000	
	56.315			595.4(1511)	1.2352	195.55	3366												
	56.315	11.605						1,770	5107	2,656	0.29401	27.786	0.3690	5507	23,333	198.2	1.46	0.50	
	COMBUSTOR		34															•	
	56.455			594.8(1515)	1.2346	22,270	3367												
	56.455	11.506			1.2828	22.310	2885	1.774	5118	2.657	0.29189	27.786	0,3717	5515	23.216	198.5	1.06	0,50	
	COMBUSTOR	0	35	28 9															
	56,535	20.202	445/	594.5(1643)	1.4100	£6.000	5437	4 645	4650	3 (0 -	0.30041				n=				
Ø	56.535 5 COMBUSTOR	14+505		129.4(1232)	1.4586	EC. 071	2005	לפר , ו	4024	C*P91	U.49516	27.786	0.3675	2250	25.158	198.7	1.06	0,61	
	COMBUSTOR		36		1 211/	53. LB.	2/11/2												
C.	56.815			595.3(1636) 117.2(1213)					ARR 1	2.670	0.20/10	27.744	ስ. ፕሬይል	5616	22.316	100.7	1.04	A 4A	
	COPEUSTOR	(1	3703	30 11	416207		2400	14714	4001	₩ . ₩ . 7	A # W 14 T A	SE FE FUN	ハキンむむひ	950	22.315	Y 2 2 8 73	AAVD	". D V	
	57.041	57.800	4357	592.3(1611)	1.2107	22.522	3421												
	57.041	13,258	3281	98,3(1164)	1 2651	22.597	3022	1.645	4972	2.674	0.29310	27.786	0.3693	5548	22.695	199-7	1.06	0.58	
	_		_	*													~ = -		

GAMIA MULTI SONV MACH VEL 8 4/4 AZAC MINUM IVAC PHI ETAC COMMUSTUR 0 36 31 5 64,452 4123 589,3(1518) 1.2342 22,292 3369 57.765 57.765 10.920 2860 40.7(1001) 1.2843 22.532 2860 1.832 5239 2.653 0.28908 27.786 0.3753 5574 23.53/ 200.6 1.06 0.51 COMBUSTOR 0 39 32 7 58.785 112.805 3416 585.8(1241) 1,2755 21.625 3165 56.785 6.112 1722 -82.4(581) 1.5368 21,629 2301 2.514 5/83 2.558 0.28724 27,786 0.3777 5585 25.613 201.0 1.06 0.31 COMBUSTOR 0 40 33 6 53.278 4711 579.4(1751) 1.1857 22.921 3481 60.795 60.795 16,650 3893 147,3(1404) 1,2278 23.09/ 3208 1,450 4650 2,692 0,29723 27,786 0,3650 5572 21,479 200,5 1,06 0,72 COMBUSTOR 0 41 34 4 55.181 4657 574.5(1729) 1.1909 22.876 3472 62.215 62.215 16.594 3800 134.8(1367) 1.2347 23.031 3182 1.474 4691 2.687 0.30529 27.786 0.3553 5561 22.255 200.1 1.06 0.70 COMBUSTOR 0 42 35 5 64.679 47.992 4991 564,7(1863) 1.1578 23.246 3516 64.679 20.759 4488 227.3(1644) 1.1735 23.532 3336 1.232 4109 2.706 0.28938 2/.786 0.3749 5542 18.479 199.5 1.06 0.88 COMBUSTOR 0 43 36 5 65.055 43.940 5082 563.0(1900) 1.1500 23.339 3529 65.055 21.122 4669 260.9(1718) 1.1583 23.637 3373 1.153 3888 2.713 0.26903 27.786 0.4032 5539 16.255 199.4 1.06 0.97 COPBUSTOR REGEN 44 37 43,940 5136 616,9(1924) 1,1481 23,265 3550 65.055 65.055 21,971 4750 326.2(1754) 1.1546 23.562 3402 1,121 3814 2.723 0.26903 27,786 0.4032 5563 15.947 200.2 1.06 0.97 NOZZLE AL 45 38 87.291 43.940 5082 563.0(1870) 1.1500 23.339 3529 87.291 1.412 3005 +606.0(1025) 1.2622 24.082 2798 2,733 7648 2.713 0.05600 27,786 1,9371 7306 6.657 262.9 1.06 0,97 NOZZLE PO 46 39 5 87.291 43.940 5082 \$63.0(1870) 1,1500 23.339 3529 87.291 0.386 2275 0886.9(745) 1,2851 24.083 2457 3.467 8518 2.713 0.02255 27.786 4.8107 7832 2.985 281.9 1.06 0.97 NOZZLE AE REGEN 47 40 87.291 43.940 5136 616.9(1924) 1.1481 23.265 3550 87.291 1.448 3101 -567.6(1063) 1.2584 24.081 2838 2.712 7699 2.723 0.05600 27.786 1.9371 7367 6.700 265.1 1.06 0.97 NOZZLE PO REGEN 48 41 87.291 43,940 5136 616,9(1924) 1,1481 23,265 3550 87.291 9.386 3340 -862,6(769) 1.2828 24.083 2489 3.457 8604 2.723 9.02214 27.786 4.8988 7916 2.961 284.9 1.06 0.97 FICTIVE COMBUSTR 67 60 65.055 306,013 5341 563,0(2006) 1,1666 23,611 3622 05.055 0.386 1425-1188₄3(444) 1,3264 24,08<u>3 1975</u> 4,740 9361 2,546 0,03958 27,786 2,7412 _ 8356 5,757 300,7 1,06 1,00 FICTIVE NOZZLE 68 61 87.291 25.255 4986 536.7(1860) 1.1461 23.300 3492 87.291 _ 1.840 3499 #398:4(1224) 1.2276 24:058 2980 2:296 6841 2:755 0:05600 27:786 1:9371 6821 5:954 245:5 1:06 0:97

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	XABS	Peib	P=06	PDA		BOX		u≠ [A		9.0 mQ		CAHALL	P=18/PE0	₽#18/PT0	P=OB/PSO	P=OB/PTO
	6.981E=01	1.0258 00		=4.397	F=01			0,000		0.000			2.653E 00	1.3722-03	0.000	0.000
	1.836E 01	1.0258 00		e3.414		0.000		0.000		0,000		1.6346 02	2.653E 00	1.372E-03	0.000	0.000
	3.070E 01	2.205E 00		e1.651				0.000		0.000		5.0535 02	5.7068 00	2.9516=03	0.000	0.000
	3.508E 01	3.890E 00		03.626				0,000		0.000		6.804E 62	1.007E 01	5.206£#03	0.000	0.000
	3.519E 01	3.924E 00		00 -4.286				0.000		0.000		6.8546 02	1.015E 01	5.251E-03	1.475E 01	7.6286-03
	3.520E 01	3.925E 00		00 64.282				0.000		0.000		6,857E 02	1.01pE 01	5.2536-03	1.46/E 01	7.586E=03
	3.555E 01	4.030E 00						0.000		0.000		7 209E 02	1.043E 01	5.3936-03	9.834E 00	5.085E=03
	3.586E 01	3.928E 00					0.2		0.2	0.000		7.529E 02	1.017E 01	5.257E-03	5.499E 00	2.844E=03
	3.606E 01	3.865E 00		00 -4.606						0.000		7.729E 02	1.000E 01	5.1726-03	7.549E 00	3.904E+03
	3.648E 01	4.212E 00		00 -4.792						0.000		8.164E 02	1.090E 01	5.6376-03	1.196E 01	6.185E=03
	3.701E 01	4°550F 00		00 05.027							40	8.726E 02	1.092E 01	5.647E-03	1.753E 01	9.063E-03
	3.732F 01	4.1018 00		00 -5.141								9.063E V2	1.061F 01	5.488£=03	2.083E 01	1.0/76-02
	3.803E 01	3.835E 00		01 -5.276								9.834E 02	9.925£ 00	5.132E=03	3.436E 01	1.7778=02
	3.834E 01	5.392E 00		01 -5.259								1,018E 03	1.395E 01	7.215E-03	4.040E 01	2.089E=02
	3.875E 01	7.395E 00										1.064E 03	1-914E 01	9.896E-03	4.004E 01	2.071E=02
	3.881E 01	7.715E 00		01 -5.266								1.072E 03	1.997E 01	1.0326-02	3.998E 01	2.068E=02
	3.901E 01	8.680E UO		01 -5.269								1.094E 03	2.246E 01	1.162E-02	4.058E 01	2.098E = 02
	3.932E 01	1.378E_01		015.316								1 110E 03	3.551E 01	1.8366.02	4.154E 01	2.1485-02
	3.950E 01	1.652E 01		01 -5.387								1.150E 03	4.277E 01	2.211E=02	3.589E 01	1.856E=02
	3.981E 01	1.713E 01		00 09.540								1.1675 03	4.434E 01	2.293E#02	2.575E 01	1.332E>02
	4.000E 01	1.749E 01		00 -5.676								1,209£ 03	4.526E 01	2,341E+02	2,556E 01	1.323E-02
	4.040E 01	2.176E 01		00 -5.961								1.256E 03	5.630E 01	5°615Fe05	2.523E 01	1.305E=02
	4.041E 01	.2.166E 01		00 =5.968								1.257E 03	5.658E 01	2.9265=02	2.522E 01	1.304E-02
	4.130E 01	3.135E 01		00 -6.854								1.362E 03	8.114E 01	4.1968-02	2.4436 01.	1.2636>02
	4.131E 01	3.146E 01		00 -6.845								1.363E 03	8.1426 01	4.210E=U2	2.442E 01	1.263E=02
	4.137E 01	3.215E 01		00 06.942								1.3718 03	8.321E 01	4.3036 = 02	2,4368 01	1.200E+02
	4-150E 01	3.349E 01		01 97.089								1.3868 03	8.666E 01	4.4816-02	3 - 000E 01	1.552E-02
	4.246E 01	3.532E 01		01 =7.672								1,5016 03	9 142E 01	4.727E=02	7.330E 01	3.790E-02
	4.409E 01	5.741E 01		01 07.494								1.6998 03	1.486E 02	7.683E=02	1.470E 02	7.603E=02
	4.431E 01	6.032E 01		01 -7.484						*5.214E		1.725E 03	1.561E 02	8.072E=02	1.475E 02	7.6296-02
	4.480E 01	6.694E 01		01 =7.539								1.785E 03	1.732E 02	8.958E#02	1.487E 02	7.687E=02
	4.481E 01	6,688E 01		01 =7.536								1.7866 03	1.731E 02	8.9506.02	1.487E 02	7.688E#UZ
	4.6258 01	5.886E 01		01 -6.707								1.963E 03	1.583E 02	7.8775-02	1.920E 02.	
	4.626E 01	5.880E 01		01 -6-699								1.904E 03	1.522E 02	7.870E=02	1.520E 02	7.861E-02
	4,731E 01	5.296E 01		01 -5.19								2.094E 03	1.370E 02	7.087E-02	1.544E 02	7.986E-02
	4./33E 01	5.309E 01		01 -5.16								2.097E 03	1.374E 02	7.1056-02	1.545E 02	7.9895-02
	4.811E 01	5.730E 01	_ *	01 -3.797								2.194E 03	1.485E 02	7.668E=02	1.330E 02	6.877E=02
	4.877E 01	4,4268 01		01 -2.319								2.2/7E 03	1.1468 02	5.924E-02	1.146E 02	5.924E=02
	4.878E 01	4.416E 01	-	01 #2.292								2.275E 03	1.143E 02	5.909E-02	1.143E Q2	5.9095-02
	4.931F 01	3.847E 01		01 -1.150								2.345E 03	9.957E 01	5.149E002	9.957E 01	5.149E=02
	5.072E 01	3.169E 01				₩2.871E						2.522£ 03	8 201E 01	4.2415.02	6.2018 01	4.2416-02
	5.282E 01	2.201E 01				□3.243E						2.789E 03	9.697E 01	2.9406.02	5.097E 01	2.9466-02
	5.332E 01	2.034E 01				35362E						2.852E 03	5.663E 01	2.7226=02	5.263E 01	2.7228-02
	5.407E 01	1,858E 01	1.858g			□3.436E						2.948E 03	4,809E 01	2.487E=02	4.8092 01	2.4876002
	5.483E 01	1.680E 01				-3.546E				-2.099E		3.046E 03	4,346E 01	2.248E0U2	4.346E 01	2.248E=02
	5.576E 01	1.549E 01	1.549E			35,6/28						3.164E 03	4.008E 01	2.0726-02	4.008E 01	2.072E=02
	5.626E 01	1.478E 01	1.478E			₩5.735E						3.209E 03	3.824E 01	1.977E=02	3.824E 01	1.9778-02
	5.631E 01	8,512E 00	1.470E			₽3.741E						3,2168 03	2.203E 01	1.1396.02	3.804E 01	1,9676-02
	5.645E 01	8.5126 00	1.4500			≈3.758E						3 234E 03	2.203E 01	1.139E+02	3.752E 01	1.940E=02
	5.653E 01	1.439E 01	1.439E			-3,768E						3,245E 03	3.723E 01	1,925E-02	3.723E 01	1.9256002
	5.681E 01	1.399€ 01	1.399F			-3.801E						3.280E 03	3.620E 01	1.8726.02	3,620E 01	1.872E-02
,	5.704E 01	1.326E 01	1.326E			#3.847E						3,309E 03	3.431E 01	1.774E002	5.451E 01	1.7746=02
1	5.770E Q1	1.092E 01				-5.910E						3,402£ 03	2,826£ 01	1.0616-02	2.826E 01	1.4616-02
	5,878E 01	6,112 <u>t</u> 00	6.112E	9.95	16 UZ	#4.00bE	0.5	#1,580E	93	-2,428E	03	3,512E U3	1,5828 01	8,180E-03	1.582E 01	8.1804-03
	6.079E 01	1.665E 01		01 9,98	£ 02	-4.166E	03	-1.617E	0.5	42.569E	03	3.790E 03	4.509E 01	5°558E 05	4,309E 01	2,2286=02
	6.551E 01	1.659E 01	1.6598	01 9.98	r 02	## \$ 2 2 E	03	#1.045E	03	=2.677E	03	3.472E 03	4.294E 01	2.221E=02	4.294E 01	2,2216=02

XABS	L MTR	P#Ud	PDA	СVХ	ъ⇒ <u>լ</u> ∺	C=OE	CAFALL	P#1H/PSU	019/8149	P=06/PS0	P=UB/P10
6.468E 01	2.076E 01	2.076E 01	9.961E 02	#4.545E 03	-1.716E 03	-2.876E 03	4 2898 63	5.3726 01	2.778t=02	5.372E 01	2.778E=02
6.505E 01	2.085£ v1	2+139E 01	9,981€ 02	-4.642E 03	■1.730E 03	42.912E 05	4.337E US	5.396E 01	2.790E-02	5.537E 01	2.863E=02
6,509E 01	5.082E 01	2.146E 01	9.981E 02	74.647E 03	#1.731E 03	#2.915E 03	4.342E 03	5.596E 01	2.790E=02	5.554E 01	2.872E=02
0.529E 01	1.982E 01	2.180E 01				W2.932E 03	4.368E 03	5.129E 01	2.652E#02	5.642E 01	2.917L=02
6.695E 01	1.127£ 01	9.250E 00	1.171E 03	=4.840E 03	≈1.790E 03	*3.050E 03	4.583E 03	2.917E 01	1.508E=02	2.394E 01	1.238E=02
6.762E 01	8,199E 00	9,135F 00	1,363£ V3	-4.894E 03	-1.806E 03	-3.088E 03	4.605E 03	2.122E 01	1.0975+02	2.364E 01	1.2425=02
6.839E 01	4.670E 00	6,952E 00	1.561E 03	#4.953E 03	#1.821E 01	-3.132E 03	4.760E 03	1.209E 01	6.250E=03	1.799E 01	9.303E-03
6.911E 01	3.658E 00	4.910E 00	1.690E 03	-5.009E 03	#1.833E 03	-3.176E 03	4.848E 03	4.466E 00	4.895E=03	1.271E 01	6.571E=03
6.972E 01	2,800E 00	4,187E 00	1.773E 03	+5.055E 03	#1.840E 03	-3.215E 03	4.922E 03	7.246E 00	3.747E=03	1.083E 01	5.603E=03
7.067E 01	1.974E 00	3.060E 00	1.867E 03	-5.120E 03	-1.850E 03	#3.271E 03	5.036E U3	5.108E 00	2.642E=03	7.919E 00	4.095E=03
7.110E 01	1.6006 00	2.802E 00				-3.294E 03	5.08BE 03	4.141E 00	2.141E=03	7.2528 00	3.750E=03
7.263E 01	1.822E 00	1.885E 00	1.995E 03	*5,215E 03	-1.863E 03	"3.353E 03	5.273E 03	4.715E 00	2.438E=03	4.878E 00	2.523E+03
7.353E 01	1.952E 00	7.650E-01				-3.3818 03	5.372E 03	5.052E 00	2.613E=03	1.980E 00	1.0246=03
7.354E 01	1.953E 00	7.600E=01	2,0566 03	₩5,249E 03	-1.808E 03	-3.381E 03	5.372£ 03	5.054E 00	2.613E-03	1.967E 00	1.017E=03
7.486E 01	2.1458 00	0.000	2.099E 03	●5.306E 03	-1.875E 03	#3.431E 03	5.424E 03	5.551E 00	2.871E=03	0.000	0.000
7.771E 01	2.110E 00	0,000	2.184E 03	-5.319E 03	-1 .888E 03	#3.431E 03	5.523E 03	5.4618 00	2.824E-03	0.000	0.000
8.161E 01	1.450E 00	0.000	2,2608 03	*5.334E 03	-1.903E 03	-3.431E 03	5.628E 03	3.753E 00	1.940E=03	0.000	0.000
8.442E 01	1.380E 00	0.000	2,292£ 03	#5.348E 03	#1.917E 03	-3.431E 03	5.682E 03	3.571E 00	1.8476-03	0.000	0.000
8,728E 01	1.745E 00	0.000	2.329E 03	-5.371E 03	-1.940E 03	-3.431E 03	9.705E 03	4.516E 00	2.335E-03	0.000	0.000
8.729E 01	1.746E 00	0,000	2.329E 03	95.3/1E 03	₩1,940E 03	#3.431E 03	5.705E 03	4.518E 00	2.336E=03	0.000	0.000

NO APRIOR = 729 B/sec

say GNOT = 300 8 tulser

ANOT = 0 8 tulser

¥	UNKAG	Lipas	ſF	~ (
4.040F 61	1.1//E 02 1.739E=01	1.177E #2 1.174F Z	2.1646+05 2.165c=03	50+3965*+
4.130E U1	1.7026 UI	1 1515 12	2.8012#03	4.71148-16
4.1315 14	1.9556*01	1.555E Ja	さいないと=v3	5.2246=42
4.1376 01	1.1916 00	1.365E 02	2.3946-03	5.365E-02
4.150E 01	2.255E 00	1.554E 02	2.405t = 0.5 2.510E= 0.3	5.64/F#02 6.710E#02
4,409E 01	2.532£ v1	1.0076 02	2.8186-03	1,906E=02
4.451E 01	5.067E 00	1.838E 05	3,0596=03	1.256E#02
4,480E 01	7.037E 00	1.900E 02	5.076E+03	7.231E-02
4.451E 01 4.625E 01	1.3586=01 2.053E 01	2.115E 02	3.0736 03 3.337t 03	/.238E=02 6.652E=02
4.626E 01	1.381E=01	2.116E 02	2.9628-03	7.640E=02
4.731E 01	1:3196 01	2.248E U2	2.905E+03	7.5/3E=02
4.733E 01 4.811E 01	3.138E=01 9.592E 00	2.251E 02	3,0176+03	7.2678-02
4.811E 01 4.877E 01	9.592E 00	2.547E 02	2.981t=u3 3.266E=Q3	7.1/0E+02 0.220E#02
4.878E 01	1.326E=01	2.435E 02	2.959E=05	6.9296-05
4.931E 01	6.669E 00	5.205E 05	2.8996#03	0.594E#02
5.072E 01 5.282E 01	1.705E 01 2.392E 01	2.672E 02	2.8456*03	5.887E#02
5.332E 01	5.604E 00	2.911E 02	2.848E=03 2.921E=03	4.615£=02 4.262E=02
5.407E 01	8.301E 00	3.050E 02	2.8966+03	4.013E-02
5.483E 01	6-143E 00	3.132E 02	2.867£-U3	5.750E=02
5.576E 01 5.626E 01	9.557E 00 3.154E 00	3.227E 02	2.865E+03	3.522E=02
5,631E 01	4.665E=01	3.259E 02	2.839E=03 3.026t=v3	3.208E#Q2 2.619E#02
5.645E 01	1.215E 00	3.276E 02	2.8506.03	2.753E=02
5.653E 01	7-220E=01	3.283E U2	3.372E003	2.74UE=02
5,681E 01 5,704E 01	2.530E 00	3.308E 02	3.0116=03 2.989E=03	2.938E+02 2.859E+02
5.776E 01	6.333E 00	3.391E 02	2.9266.03	2.565E=02
5.878E 01	9,212E 00	3.483E 02	2.787E=03	1.707E=02
6.079E 01	-1.625E 01	3.646E 02	2.5426-03	3./64E=02
6.221E 01 6.468E 01	1.125E 01 2.013E 01	3.758E 02	3.105E+03 3.146E+03	3.138E+02 3.385E+02
6.5058 01	2.7.9E UO	3.9876 02	3.343E=03	3.157E-02
6.509E 01	2.836E=01	3.969E 02	3.455E=03	5-1/7E-02
6.529E 01	1.445 00	4.004E 02	3,453£003	5.163E=02
6.695E V1	1.216E 01 4.480E 00	4.125E 02	3.390E=03 3.378E=03	2.274E+02 2.054E+02
0.839E 01	4.704E 00	4.217E 02	3.3426-03	1.5646.02
6.911E 01	3.751E 00	4.255E 02	3.3036*03	1.200E=02
6.972E U1	2.780£ 00 3.722£ 00	4.283F 02	3.273±#03	1.1046.02
7.067F 01 7.110E 01	3.722£ UO 1.479£ 00	4.335E 02	3.219E=03	ნ.651E∞03 1.822E∞03
7.263E 01	4.786E 00	4.3826 02	3.170E-03	6.858E+03
7.353E 01	2.239E 00	4.405E 02	3.125tev3	5.408E=03
7.354E 01 7.486E 01	3.294E*03	4.405E 02	3.125±+03 3.177±+03	5.401E=03
7.771E 01	5.603F 00	4.443E 02	3.159E=U3	/.6<3E=03 7.409E=03
8.161F 01	2.476E UO	4.468E 02	1. 0886=u3	5.590E=03
8.728E 0.	1.119E 06	4.479E 02	3.067E=03	5.364E=05
8.728E 0. 8.729E 01	0.000 0.000	4.484E 72	3.004±=03	6.305E-03
		4 7 7 7 7 G VE	28004540	~ = ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~

RAMJET PERFORMANCE

ENGINE PERFORMANCE	INLET
CALCULATED THRUST	ANGLE OF ATTACK
REGENERATIVE DECOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	INLET PROCESS EFFICIENCY = SUPERSONIC 0.8962 INLET PROCESS EFFICIENCY = SUBSONIC 0.9057 KINETIC ENERGY EFFICIENCY = SUPERSONIC 0.9415 KINETIC ENERGY EFFICIENCY = SUBSONIC 0.8897 ENTHALPY AT PO = SUPERSONIC 88.09 (BTU/LBM) ENTHALPY AT PO = SUBSONIC 27.76 (BTU/LBM)
MOMENTUM AND FORCES	CU#bUSTOR
INLET FRICTION DRAG	FUELWAIR RATIO
STATIONS	FUEL INJECTORS
NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A 40,400 1B 41,300 B 1C 44,300 2A 46,775 D 2C 46,250 A 3A 54,065 3B 56,250 4 44,800

t = 164.03 sec.

REALING # 0065 BLOCK = 00 TIME # 164.035 -4CH 6.0 P1 # 749.749 T1 # 5054.6
RAMJET PERFORMANCE

••					-,										
2 4				5 ()	W M A	RY	REF	ORT							
ko p r		CANAL A		COLU				4.4						F5	
MIND TUNNEL 1	и 0 5	11 A T F A	nulri	PONY	MALM	V F L	5	w/A	4	14/4	мГчуч	L	IVAL	РИТ	ETAC
0.000 749.749 3035		1.2926	28.852	2600											
0.000 0.399 414	-29.6(100)				5.908	5964	1.831	0.10730	26.953	0.9807	5097	9.945	189.1		
SHIKE ILD HP 5	0 3	-			- •					- • /	• • • •				
0.600 18.075 3034		1.2925	20.851	5600											
0.600 16.256 2962		1.2948	20.851	2571	0.407	1047	5.088	0.10736	26,953	0.9807	4961	1.746	184.1		
WING TUNNEL 3	0 0														
0.000 749.749 3035 0.000 0.380 409	70 04 00/)	1.2925	28.852	2600	4 A1L	6070			34 A.M						
SPIKE TIP NS 4	#30.9(98) 0 ∪	1.3400	20+021	447	0.013	597 0	1.031	0.103//	20.007	0.9807	4955	4.658	184.5		
0.600 18.075 3034		1.2925	28.851	2600											
0.000 16.390 2968					0.391	1006	2.088	0-10377	26-067	0.9807	4933	1.623	189.2		
INLET THRUAT 5	0 4	• • -				,,,,	-,,	****		24,700,		,	,		
40,400 \$00,243 2999		1,2938	28,851	2586											
40.400 15.930 1467	235,9(363)	1.3507	28.851	1848	2,530	4674	1.891	0.94777	26,953	0.1110	4369	65.847	162.1		
INLET UPNHSK 6	0 3														
40.400 300.243 2999 40.400 13.687 1410		1.2938	28.851	2586	2 () (49E /									
INLET DANKSK 7	218.9(348)	1.3500	50 * 031	1014	C+0C1	4/54	1.041	0.00101	50.423	0.1221	4411	63.657	103.6		
40.400 125.405 2999		1.2937	28.881	2586											
40.400 107.781 2897	639.8(766)	1.2769	28.851	2545	0.487	1240	1.951	0.86161	26.953	0-1221	4411	16,609	163.6		
COMEUSTOR O B	1 4				- •		••••	• • • • • • •		- • • •		*****			
40.410 249.522 2999		1,2938	28,851	5296											
40.410 15.949 1468	, _ , _ ,	1.3507	28,851	1849	2,527	4672	1.891	0.94765	26.953	0.1110	4368	66.809	162.1		
COMBUSTOR 0 9 41,324 236,453 2990	2 4	1 2046	20 054	วยอรั											
	667.9(794) 273.9(403)	1.3427	28.851	1034	2 296	111110	1 004	A 95009)	0 1100	11705	FE E41	462.6		
COMBUSTOR 0 10	3 4	110451	201027	1,134	E # E 70	4440	1.700	0.45000	20,733	0.1100	4643	02,201	121.0		
41.389 232.013 2990		1.2940	28.851	2582											
41,389 18.734 1627	276.9(406)	1.3421	28 851	1940	2.274	4422	1.907	0.95049	26.953	0.1107	4236	65.324	157.2		
COMBUSTOR 0 11	4 3														
41.500 226.001 2988															
41.500 19.078 1646 COMBUSTOR 0 12		1.3412	28.851	1951	2.251	4391	1.909	0.95023	26,955	0.1107	4220	64.047	156.6		
COMBUSTOR 0 12 42,460 197,700 2975	5 5	()D/E	20 464	3674											
42.460 20.511 1726		1-3374	58 82 4 E0 10 5 1	1994	2.427	4242	1 017	0.90130	34 057	A 4114	4 4 4 4	43 041	164 4		
COMBUSTOR 0 13	6 4	1133/4	201021	4	E 4 7 80 1	4646	18711	4 4 7 4 1 3 4	201733	0.1110	4141	62.061	125.0		
44,109 185,032 2948	655,1(781)	1.2953	28.851	2565											
44.109 20.034 1727	303.9(433)	1.3374	28.851	1995	2,101	4192	1.919	0.90796	26.953	0.1159	4106	59.148	152.4		
COMBUSTOR 0 14	7 4									•	-	+ -1	••		
44.310 183.950 2944		1.2954	28.851	2564											
44.310 20.050 1728 COMBUSTOR 0 15	304-1(433)	1.3373	28.851	1995	2.047	4185	1.919	U.90674	26,953	0,1161	4101	58,966	156.8		
44,800 180,514 2936		1 2957	124 20	2541											
	305.5(435)	1.3371	24.851	1008	2.085	4162	1.010	0 00727	74 OF 7	A 4166	/. n a a	E# #21			
COMBUSTOR 0 16	9 4	.,		. , , ,	~ • • • • •	4,46	4 8 7 1 7	0,70323	20,733	0.1105	4000	DOTALI	15111		
44,824 180,334 2936		1,2957	28,851	2560											
44.824 20.150 1733	305.6(435)	1.3371	28.851	1998	2,082	4161	1.919	0.90323	26.953	0.1165	4087	56.402	151.0		
COMPOSION 0 17	19 4														
46.260 164.950 2915	707 74 (171)	1,2963	28,851	2552					<u>.</u>				_		
46,260 19.274 1759 COMBUSTOR 0 18	307.2(436)	1"3200	20.001	2001	£,055	4113	1,923	0.85116	26,953	0.1236	4056	54.401	150.5		
47.310 151.682 2901		1.2968	28.851	25.114											
47.310 17.983 1735	306.2(436)	1.3370	28.851	2000	2.047	4093	1_028	U. 791A7	24-057	0.1420	BOAT	50.344	1 1 1 2 4		
			1			3	20,50	481.1701	20,733	V41367	-041	~ V • 3 C 3	44797		

				. • •	, -, -						, ,	.,	. , .						•
		P	Ŧ	н		GAMMA	MOLPIT	SONV	масн	VFI	9	W/A	н	A/AC	MUMTM	a	IVAC	PHT	FTAC
	COMBUSTOR	. 0		12 4		U (1, 1, 7, 1)	,		*****	14 =	•		.,	-,	. •	-			2170
				640.6(7471	1.2968	28.851	2546											
	47.349								2.048	4094	1.928	0.78634	26.953	0 - 1 3 3 5	0001	50.155	1/19.0		
	COMBUSTOR			13 5	3-7			•				**!***			404.	244122	44,44		
				637.96	7441	1 2071	28.851	2542											
	48.110								2.065	4107	1.010	0.73779	26 053	0 4/126	4040	47.089	460 0		
	COMBUSTOR		21		7347	1 1 2 2 7 7	504031	1701	-1052	4.07	18730	9413117	206725	V 1 1 4 5 U	4044	H / \$ 007	12010		
	48.799	_		635,5(7421	1 2073	28 851	25.40											
	48.799								2 116	A 4 6 4	1.073	0.67715	24 05 1	0 1660	11044	// T 786	160 0		
	COMBUSTOR	. 4,5,74	22	15 3	4177	1 4 3 3 7 0	501021	1700	E . 110	4101	18736	4.01112	20.773	V = 1 3 34	4080	43.785	130.4		
	49.329		2877	633.9(7401	1 2075	DA 851	2634			,								
	49.329									// 24.7	1 037	0.63330	74 067	0 1445	0000	n e nico			
	COMBUSTOR			16 5	40.7	142411	FÖLOST	1243	E . 100	4613	1 4 7 3 3	0.03330	40.733	0.1002	4070	41.459	19101		
	50.739	126 81/		629.9(7071	1 2070	20 86.	3674											
	50.739								2 260	4700	. 07	0 51014	74 06 7	A 405A		74 113	467 7		
	COMBUSTOR	101717		17 4	380)	145455	50,021	1743	6.604	#3va	1.730	0.53974	20.733	0.1750	4125	36.132	123.0		
					7-21	1 2007	28 854	2527											
	52.839			625,00					2 260	"""			24 257	A 3750		20 000	3 m () ()		
					3611	1 . 3470	501021	1021	6.704	4400	1 4 4 1	0.44238	604423	0.23/4	41/2	#U.244	154*6		
	COMBUSTOR			18 4	7-11	. 3004	20 054	25.00											
	53,339	1131,02	2044	623,9(751)	1.2400	20.051	6563									. = = -		
	53.339	/ 1505			266)	1,3510	20.051	1845	2,377	4426	1.942	0.42430	20.955	0.2480	4184	29.184	155.2		
	COMBUSTOR		26		7.05			****											
0	54.089	111.005	502A	622.50	744)	1.2787	26,051	2521											
OF E	54.089	01001			354)	1.325	50.021	1959	2.434	4459	1.942	0.39996	26.953	0.2631	4200	27,716	155.8		
	COMBUSTOR		27																
벋	54,849	109,057	2835	621.10	748)	1.2989	28,851	2519											
z	54.849	6,371			348)	1.3540	\$8*82T	1814	2.472	4485	1.943	0.57822	26,953	0.2782	4211	26,364	156.3		
A	COMBUSTOR		28																
	55.760			619,60															
H	55.760	5.664			343)	1.3553	28.851	1801	2,504	4509	1.945	0.35545	26.953	0.2961	4222	24,908	156.6		
A	COMBUSTOR	. 0	29	22 4													-		
Ġ.	56.274	92,242	5959	618,9(746)	1,2991	26,851	2916											
邑	56.274	4.492	1341	200.7(330)	1.3582	28.851	1772	2.582	4574	1.954	0.28610	26.953	0.3678	4255	20.538	157.9		
	COMBUSTOR	. 0	30	33 5					-										
7	56,324	45,151	2827	618.9(746)	1.2791	28,851	2516											
	56.329	4.473	1340	200.5(330)	1,3563	28.851	1771	2.584	4576	1.954	0,28524	26,953	0.3689	4256	20.283	157.9		
	COMBUSTOR	0	31	24 5			-												
	56,469	91.786	2827	618.7(746)	1,2991	28,851	2516											
	56.469	4.430	1337	199.8(329)	1,3584	28.851	1769	2,588	4578	1.955	0.28314	26,953	0,3717	4257	20.145	157.9		
	COMBUSTOR	0	32	25 4															
	56.549	93,011	5859	618,6(745)	1,2991	28,851	2515											
	56,549	4.474	1336	199.5(329)	1.3585	28.851	1768	2,590	4580	1.954	0.28636	26,953	0,3675	4258	20.380	156.0		
	COMBUSTOR	0	53	26 4					-										
	56,829	93.223	2825	618.3(745)	1.2991	28,851	2515											
	56.829	4.441	1332	198.4(328)	1.3587	28.851	1766	2.595	4583	1.953	0.28536	26.953	0.3688	4259	20.327	158.0		
	COMBUSTOR	0	34	27 4					• •		• • • • •								
	57.055	93.433	2824	618.06	745)	1.2992	28.851	2515											
	57.095	4.421	1329	197.76	327)	1.3509	28.851	1764	2.600	4586	1.953	0.28483	26.953	0.3695	4260	20.300	158.1		
	COMBUSTOR	0	35	28 3		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	,,					*********	204,03	0,50,5	7000	,			
	57,779			617.1(7041	1 2997	28,851	2513											
	57 779	4.313	1320	195.27	3251	1 3595	28.851	1758	2.615	4595	1.051	0.28041	26.957	0.3753	4260	20.024	158 2		
	COMBUSTOR		36		-6-1	* * * * * . ~					4 2 7 0 2	2150041	44417	013133	4504	E V # V E 4	12015		
	58,799			616,1(7/131	ממסכו	28.851	2512					•						
	58.799	4.257	1312	197.71	3531	1 3400	28.45	175/	7-4-8	4600	1.052	0.27862	26 067	በ 3777	11245	10 614			
, C	COMBUSTOR	7,671	37	30 5	ز دے د	* # 4 3 7 7	"0001	1134	- 90-4	-000	11772	V . E / OOZ	60.773	V#3/1/	4603	19.916	12005		
	60.809			614.4(7/11	1.2004	2H_H51	2610											
-	60.809	7,460	17.55	194.74	3-51	1.3500	24.45	1740	3.401	2577	1 051	0 36623	34 567	A 9250	4564	34 544	45.7 *		
	- A B A M A	40427	4-55	1 2 2 4 1 [26.7	1	20.001	1100	E POAT	42//	1 . 421	0.28832	40 A A D D	0.3050	4651	20.508	15/07		

87.305

GAMPA MOLWT SONV MACH VEL S A/AC MOMIM Q IVAC PHI ETAC A/A N COMBUSTOR 0 38 31 5 95.195 2809 613.4(740) 1.2997 28.851 2508 62.229 62,229 4.627 1330 198.0(327) 1.3588 28.851 1765 2.583 4559 1.950 0.29613 26.953 0.3553 4241 20.983 157.3 COMBUSTOR 0 39 32 87.445 2803 611.5(738) 1.2999 28.851 2506 64.693 64.693 4.460 1344 201.5(331) 1.3580 25.851 1773 2.554 4529 1.955 0.28070 26.953 0.3749 4223 19.759 156.7 COMBUSTOR 0 40 33 65.069 80,942 2802 611,1(738) 1,2999 28,851 2505 65.069 4.155 1345 201.9(331) 1.3579 28.851 1774 2.550 4525 1.961 0.26096 26.953 0.4032 4220 18.352 156.6 NOZZLE 41 34 3 80.942 2802 611.1(738) 1.2999 28.851 2505 87.305 67.305 0.378 696 38.7(168) 1.3946 28.851 1293 4.138 5352 1.960 0.05432 26.953 1.9371 4671 4.519 173.3 NOZZLE 42 55 80,942 2802 611,1(738) 1,2999 28,851 2505 87,305 87.305 0.399 707 41.2(171) 1.3942 28.851 1303 4.098 5340 1.961 0.08631 26.953 1.8686 4665 4.674 175.1 FICTIVE COMBUSTR 62 55 65.069 300.243 2801 611.1(738) 1.2999 26.851 2505 0.399 487 -12.0(117) 1.3991 28.851 1083 5.154 5584 1.870 0.08549 26.953 1.2309 4804 7.419 178.2 65.069 FICTIVE NOZZLE 63 56 242,556 2775 603.2(730) 1,3007 26.851 2494 67.305

0.226 434 -24.7(105) 1.3990 28.651 1023 5.47/ 5606 1.882 0.05432 26.953 1.9371 4808 4.732 178.4

XABS	P⇔IB	P#08	PDA	QOX	u=18	G⇔O⊟		CAWALL	Pals/PSU	F=18/PTO	P=08/P50	P#08/P10
_	•									-		
6.981E#01	1.050E 00	0,000	#4.408E=01	0.000	0.000	0.000			2.630E 00	1 . 400E . 03	0.000	0.000
1.836E 01	1.050E 00	0.000	#3.496E 01	0.000	0.000	0.000		1.634E 02	2.630E 00	1.400E=03	0,000	0.000
3.070E 01	2.170E 00	0.000	-1.655E 02	0.000	0.000	0.000		5.053E 02	5.436E 00	2.894E=03	0.000	0.000
					0.000			6.804E 02	9.720E 00	5.175E=03	0.000	0.000
3.508E 01	3.880E 00	0.000	₩3.615E 02			0.000						
3.521E 01	3.899E 00	5.885E 0	o =4.299E 02	0.000	0.000	0.000		6,860E U2	9.767E 00	5.200E=03	1.474E 01	7.849E=03
3.521t 01	3.900E 00	5.851F 0	0 94.299E 02	0.000	0.000	0.000		6.863E 02	9.769E 00	5.201E=03	1.466E 01	7.803E=03
3.555E 01	3.950E 00		0 -4.365E 02	*	0.000	0.000		7,201E 02	9.895E 00	5.268L-03	9.836E 00	5.237E-03
										5.191E-03		
3.588E 01	3.892E 00		0 -4.515E 05					7.535E 02	9.750E 00	-	5.135E 00	2.734E=03
3,606E 01	3.860E Q0	2.785E 0	0 #4.606E 02	-1.400E	02 =1.400E	02 0.000		7.721E 02	9 670£ 00	5.148E=03	6.978E 00	3,715E=03
3.648E 01	4.201E 00	4.4902 0	o =4.796E 02	-1.434F	02 -1-4346	00000 50		8.157E 02	1.052E 01	5.603E#03	1.125E 01	5.9886-03
3.7018 01	4.165E 00		n -5.032E 02				01	8 718E 02	1.043E 01	5.5556-03	1.664E 01	8.857E=03
												1.0642-02
3.734E 01	4.0526 00		0 -5.150E 02					9.070E 02	1.015E 01	5.405E=03	1.998E 01	
3.803E 01	3,815E 00	1.326g 0	1 -5.279E 02	●1.920E	02 #1.574E	02 =3.457E	01	9,825E 02	9.557E 00	5.0886.03	3.322E 01	1,769E=42
3.836E 01	5,357E 00	1.577E 0	1 -5.298E 02	⊕2.015E	02 =1.613E	02 #4.026E	01	1.019E 03	1.3428 01	7,145E=03	3.952E 01	2.104E#02
3.875# 01	7.191E 00		1 -5.256E 02				01	1.063E 03	1.801E 01	9.5918-03	3.842E 01	2.046E=02
3.88%E 01								1.072E 03	1.894E 01	1.008E=02	10 3058 ct	2.0346+02
	7.5608 00		1 -5.257E 02									- "
3,901E 01	8,410E 00	1,2216 0	1 05.250E 02	54 1 C 4 J F	05 #1*151F	02 43,1450	O.T.	1,093E 03	3.107E 01	1.1226-05	3.885E 01	2.0685-02
3.934E 01	1.378E 01	1.597E 0	1 -5.3028 02	≈2.3/7E	990er# 50	02 º5.705E	01	1,1316 03	3,452E 01	1.830E=02	4.0032 01	2.1316-02
3,950E 01	1.641E 01		1 -5.3748 02				01	1,150E 03	4.111E 01	2.1695-02	3.077E 01	1.638E=02
3.981E 01	1.702E 01		0 -5.620£ 02					1 108E 03	4.263E 01	2.270E=02	1.190E 01	6.335E-03
												6.129É=03
4.000E 01	1.733E 01		0 05.779E 02				01	1.208E 03	4.342E 01	2.3126-02	1.151E 01	
4.040E 01	-2.03ZE 01	4.835E 0	0 ¤6°110E 0S	9256,5°	02 -2-1746	02 07,483E	01	1.259E 03	5.091E 01	2.710E-02	1.061E 01	5.6486.03
4.04 E 01	- 2.040E 01	4.225F 0	0 06.179E 02	9856.5	02 w2.178E	02 07.300E	01	1.256E 03	5.109E 01	2,720£*02	1.059E 01	5.6366003
4.132E 01	2.7228 01		0 97.236E 02					1.364E 03	6.819E 01	3.6316.02	8.519E 00	4.5366.03
								1.372E 03	6.941E 01	3.695E-02	8.372E 00	4.458E+U3
4,139E 01	2.771E 01		0 -7.318E 02									
4.150E 01	2.854E 01		0 =7.460E 02					1.385E 03	7.149E 01	3.806E-02	9,369E 00	4.988E=03
4.246E 01	1.046E 01	7.174E 0	0 -8.070E 02	₽4.872E	02 =3.163E	02 #1.709E	02	1.500E 03	2.621E 01	1.3956-02	1.79/E 01	9.568E¤U3
4.411E 01	1.480E 01	1.307E 0	1 08.123E 02	97.088E	02 #4.020Ë	02 93.068E	02	1.700E 03	3.706E 01	1.973E=02	3.275E 01	1.743E0UZ
4.43 E 01	1.532E 01		1 -8.136E 02					1.724E 03	3.839E 01	2.044E=02	3,201E 01	1.704E-02
								1 784E 03	4.162E 01	2.216E=02	3.0222 01	1.609E=02
4.480E 01	1.661E 01		1 =8.189E 02						•			
4.4822 01	1.660E 01		1 =8.193E 02				02	1.787£ 03	4.160E 01	2.215E#02	3.014E 01	1.605E=02
4.626E 01	1.611E 01	9.937E 0	0 =8.258E 02	∞9.747E	02 ×5.042E	02 =4.704E	02	1.963E 03	4.U37E 01	2.149E=02	2.489E 01	1.3256-02
4.73 E 01	1.576E 01		0 -8.238E 02				02	2.093E 03	3.947E 01	S0=3S01.S	2,106E 01	50=3151,1
4.735E 01	1.852g 01							2.098E 03	3.888E 01	2.070E-02	2.092E 01	1.1146-02
			0 ×8.229E 02									
4.81 iE 01	1.090E 01		0 -8.088F 05					2.193E 03	2.731E 01	1.454E-02	2.375E 01	1.265E002
4,880E 01	1.0508 01	1.050E 0	1 97.7638 02	#1,235E	03 66:097E	02 00.255%	02	2,2/9E 03	5°031E 01	1,4016=02	2.631E 01	1,401E=02
4.933E 01	1.129E 01	1.129F 0	1 a7.462E 02	∞1.280E	03 -6.2978	02 ¤6°209E	02	2.346E 03	2.829E 01	1.5066002	2.829E 01	1.506E=02
5.074E 01	4.6126 00		0 =6.874E 02					2.523E 03	1.155E 01	6.152E-03	1.155E 01	6.1526=03
								2.789E 03	1.635E 01	8.703E=03	1.635E 01	8.703E=03
5.284E 01	6.525£ 00		0 =6.261E 02									
5.334F 01	6.025E 00		\$0 38PO.0¤ 0					2.853E 03	1.509E 01	0.036E-03	1.5098 01	8.036E003
5,409E 01	5,031E 00	5,0818 0	0 92,8836 02	91.588E	03 = 7.781E	02 =8.099E	02	2.949E 03	1.2738 01	6.777E=03	10273E 01	6.777E=U3
5.485E 01	0.125E 00	4.125F D	0 05,700E 02	01.625E	03 #7.967F	02 08.282E	02	3.046E 03	1.033E 01	5.5026.03	1.0338 01	5,5026003
5.576E 01	3.469E 00		0 .5.531E 02					3.164E 03	8.691E 00	4.627E=03	8.691E 00	4.627E-03
5.627E 01	3.099E 00		0 m5.175E 02					3.209E 03	7.764E 00	4,134E003	7.764E 00	4.134E=03
5,633E 01	1,650E 00	3.060E 0	0 #5.166E 02	=1.005E	03 -8.275E	02 ×8.575E	02	3,216E 03	4.133E 00	2.2016.03	7.665E 00	4.081E=03
5.647E 01	1.650E 00	2.959E 0	0 -5.147E 02	□1.640E	05 =8.297E	02 m8.599E	0.5	3.234E 03	4.133E 00	2.2012=03	7.413E 00	3.9476=03
5.055E 01	2.902E 00		0 +5.135E 02					3.244E 03	7.269E 00	3.870E=93	7.269E 00	3.870E=03
5.6832 01	2.700E 00		0 =5.099E 02					3.200E 03	6.764E 00	3.601E=03	6.764E 00	3.601E=03
5.705E 01	2,925£ 00		0 -5.071E 02					3,309E 03	7.327E 00	3.901E-03	7.327E 00	3.9016-03
5.778E 01	3.645E 00	3.6455 0	0 #4.485£ 05	=1.751E	03 -8,476E	02 -8.834E	05	3.402E 03	9,131E 00	4.8625#03	9.131E 00	4.8626-03
5.880E 01	3.562E 00	3.562F 0	0 #4.899E 02	-1.760E	03 -8.5852	02 -9.020E	92	3.532E 03	8.924E 00	4.752E=03	8.924E 00	4.752E=03
6.081E 01	1.575E 00		0 -4,893E 02					3,790E 03	3.945E 00	2.101E-03	3,945E 00	2-101E=03
										1.6512003	3.100E 00	1.651E=03
6.223E 01	1.237E 00		0 -4.893E 02					3,9726 03	3.100E 00			
6.469E 01	2.588E 00		0 =4°847E 05					4.289E 03	4.482£ 00	3.451E=03	6-485E 00	3.451E-03
6.507E 01	4.275E UO	2.794E 0	0 =4.8935 02	-1.843E	03 09.086E	02 99.846E	0.2	4.3378 03	1.0718 01	5.702E 03	6.996E 00	3.726E0U3
6.511E 01	4.2/5E 00	2.815F 0	0 -4.893E 02	≈1.894E	03 .9. U90E	02 -9.851E	02	4 342E 03	1.071E 01	5.702k-03	1.053E 00	3.755E=03
	· - ·	 ·										

XABS	P#18	P≠DH	P04	Q Q X	6=1 8	9+08	CAMALL	P#IB/PSU	F=18/P10	P#05/P\$0	P#08/P10
6.531E 01	4.078E 00	5.925E 00	=4.893£ 0.	2 -1.899E 03	-9.110E 0	2 =9.877E 02	4.36BE U3	1.0218 01	5.439t=03	7.127E 00	3.9016-03
6.697E U1	2.440E 00	5.360E 00	-4.070E 0	2 +1.955E 03	-9.251E 0	2 -1.008E 03	4.503E 03	6.112E 00	3.254£#U3	1.343E U1	7.149E=03
6.764E 01	1.970E 00	4.4025 00	-3.755E 02	2 =1.946E 03	-9.294E 0	2 -1.017E 03	4.665E 03	4,935k OU	2.6281-03	1.103E 01	5.872E=03
6.841E 01	1.430E 00	3,192E 00	■5.034E U	> =1.901E 03	#9.338E U	2 =1.027E 03	4.760E U3	3.5826 00	1.907E=03	7.496E 00	4.2576-03
6.913£ 01	1.787E 00	2.060E 00	-2.499E 07	2 -1.976E 03	-9.372E 0	د0 38E 0ء1= 2	4.848E 03	4.4775 00	2.384E=03	5.16QE 00	2.748E#03
6.974E 01	5,0405 00	2.109E 00	-2.040E 0	2 -1, 989€ 03	#9.396E 0	2 =1.049E 03	4 9226 03	5.236£ 0U	2.7886-03	5.283E 00	2.813E=03
7,069E 01	1.415E 00	2.185E 00	-1.441E 0	2 +2.009E 03	-9.430E 0	2 -1.066E 03	5.036E U3	3.546E 00	1.868t=03	5.474E 00	2.914F=03
7.112E U1	1.110E 00	1.973E 00	-1.210E 0	2 =2.017E 03	-9.443E 0	2 -1.073E 03	5.008E 03	€./d1E 00	1.4606=03	4.943E 00	2,6328=03
7.265E 01	9.187E=01	1.220E 00	-6.028£ 0	1 =c.041E 03	-9.486E 0	2 +1.093t 03	5.273E 03	2,302E 00	1.2c5t+03	3.056E 00	1.6276=03
7.280E 01	9,000E=01	1.217E 00	#5.572€ 0:	1 -2.043E 03	-9.489E 0	2 -1.094E 03	5.290E 03	2.25SE 00	1.200E=03	3.050E 00	1.6248=03
7.355F 01	8.766E=01	1.205E 00	-1,866£ 0:	I -2.054E 03	#9.508E 0	2 -1.103E 03	5.374E 03	2.196E 00	1.169E=03	3.019E QO	1.607E=03
7.355E 01	A.764E=01	1.205F 00	=1.638E 0:	1 =2.054E 03	•9.508E 0	≥ #1.103E 03	5.375E 03	2.196E OU	1.169E=03	3.018£ 00	1.607E#03
7.4888 01	6.350E=01	0.000	1,698£ U	3 *2.0/6E 03	9.538E 0	2 =1.122E 03	5.426E U3	2.092E 00	1.114E=03	0.000	0.000
7.773E 01	8.400 <u>L</u> #01	0.000	3.519E 0	1 -2.082E 03	9.594£ 0.	2 -1.122E 03	5.525E 03	2.104E 00	1.120E=03	0.000	0.000
8.163E 01	1.250£ 00	0.000	7.986E 0	l ⇔∠.055€ 03	5 -9.657E 0	2 *1.122E 03	5.630E U3	3.131F 00	1.667E=U5	0.000	0.000
8 444E 01	1.045€ 00	0.000	1.054E 0	2 #2.094E 03	-9.718E 0	2 -1.122E 03	5.684E U3	2.618E 00	1.394E=03	0.000	0.000
8.730E 01	1,230E 00	0.000	1.3288 0	2 -2.105E 03	9-831E 0	2 -1.122E 03	5.707E 03	3.081E 00	1.641E=03	0.000	0.000
8.736E 01	1.230E 00	0.000	1.328E 0	2 •2•105E 03	5 #9.831E 0	2 -1.122E 03	5.707E 03	3.082E 00	1.641E=03	0.000	0.000

" Caration	_	0000 OFOCK	m on like	m 10m 10m	. 40.1
x		UDRAG	CURAG	ÇF	нс
•		y unting	CONNE	Ų.	****
4.01105	01	1.152E 02	1.1528 02	2.219t=03	4.4098-02
4 0416		1.804E=01	1.154E 02	2.220E#03	4.409E=02
4 132E		1.659E 01	1,320€ 02	2.349E=03	4.7618.02
4.1398		1.192E 00	1.332F 02	2.358E=03	4.787E=02
4.1508		2.040E 00	1.352E 02	2.374E=03	4.829E-02
4,2468		1.755E 01	1.528E 02	2.439E#03	4.9588-02
4.4116		2.956E 01	1.823F 02	2.449E+03	4.804E=02
4.4316		3.534E 00	1.859E 02	2.453E=03	4.805E=02
4.480		8.629€ 00	1.945E 02	2.064E#03	4.804E=02
4.4826		4.181E=01	1.949E 02	2.464E+03	4.8106.02
4,6266		2.464€ 01	2.195F 02	2.486E=03	4.5/2t=02
4.7316		1.697E 01	2.365E 72	2.492t+03	4.2625.05
4 7356		5.986E=01	2.371E 02	2.491E=03	4.242E=02
4 8115		1.148E 01	2.486E 02	2.484E-03	5.951E=02
4.8868		9.677E 00	2.5836 02	2.457E=03	3.572E=02
4,9338		6.925E 00	2.652E 02	2.430E=03	3.2416-05
5.074		1.656E 01	2.817F 02	2.377E+03	2.720E=02
5.2848		2.075E 01	3.025E 02	2.319E=03	2.154E=02
5.334E		4.375E 00	3.069E 02	2.302E+03	2.046E=02
5.4098		6.246E 00	5.131E 0>	2.2804-03	1.905E=02
5.4856		5.982E 00	3.191E 02	2.263E=03	1.752E-02
5.5768		6.770E 00	3.259E 02	2.247E=03	1.6586-02
5.6275		2.309E 00	5.282E 02	2.198E+03	1.298E-02
5 6336		3.145E-01	3.285E 02	2.197E-03	1.293E=02
5.647E		7.890E=01		2.195E=03	1.282E#02
5.6556	01	4.547E=01	3.293E 02 3.297E 02	2.189E=03	1.243E-05
5.6838	01	1.567E 00	3.313E 02	2,1835=03	1.254E002
5.705E	0.1	1.277E 00	3.3266 05	2.178E-03	1.2/8E=02
5.7788	01	4.057E 90	3.367E 02	2.167E=03	1,25ÏE#02
5.880E	01	5.644E 00	3.423E 02	2.157E+03	1.2366.02
6.0818	01	1.125E 01	3.536E 02	2.160E=03	1.261E=02
6.2238	0.	8,164E 00	3.617E 02	2.160E+03	1.3176-02
6.4698	01	1.401E 01	3.757E 02 3.778E 02	2.191Em03	1.269Em02
6.5078	01	5.050E 00	3.778E 02	2.217E#03	1.195E=02
0,5116	01	2.003E#01	3.780E 02	2.209E=03	1.0726-02
6.53[8		9.5446=01	3.789E 02	2.2065-03	1.0615-05
6,6978		8.252E 00	3,872E 02	2.218E-03	1.1466-02
6.7648		3.031E 00	3.902E 02	2.179E#03	9.8345=03
6.8418		2.990E 00	3.932E 02	2.117E-03	7.699E=03
6,9138		2.352E 00	3.955F 02	2.081E=03	6.682E=03
6.9746		1.915E 00	3.974E 02	2,094E-03	7.135E-03
7.0698		2.894E 00	4.003E 02	2.0636-03	6.332E=03
7.1126		1.188E 00	4.015E 02	2.0356 - 03	5.6225-03
7.2658		3,547£ 00	4.051E 02	1.970E=03	4.2418=03
7.280		2.903E=01	4.054E 02	1.968E=03	4.2076-03
7.3558		1.409E 00	4.0686 02	1.962E=03	4.146E=03
7.3558		2.6836+03	4.068E 02	1.962E=03	4.145E=03
7.4888		7.969E=01	4.076E 02	1.9218=03	3.4418-03
7.7738		1.392E 00	4.0908 02	1.911E-03	3.487E=03
8.1636		1.711E 00	4.107E 02	1.964E#03	4.698E=03
8.4448		9,481E=01	4.116E 02	1.925E=03	4.0/45=03
8.7306		3,901E=01	4.1208 02	1.943E=03	4,5966+03
₹ 8.730E	01	0.000	4.120E 02	1.943E=03	4.597E=03
47					
~7					

RAMJET PFRFURMANCE

S		HANGET FI	H. GRANGE			
Z R	ENGINE PERFORMANCE			INLET		
	MEASURED IHRUST	3. (LBF) 7. (LBF) 4. (LBF=SEC/LBM) 7. (LBF=SEC/LBM) 51	HASS FLOW RATIO: ADDITIVE DRAG CO LIMITING PRESSUR DELTA PT2 TOTAL PRESSURE R TOTAL PRESSURE R	DEFFICIENT E RECOVERY EFFICIE RECOVERY - SUPERSON RECOVERY - SUBSONIC FICIENCY - SUPERSON	0.9807 0.0009 NCY 0.1649 0.1199 IC 0.4005 0.1673	
	NET THRUST). (LBF)). (LBF)). (LBF=SEC/LBM)	INTELLET PROCESS EF KINETIC ENERGY E KINETIC ENERGY E ENTHALPY AT PO =	FIGIENCY - SUPSONI FFICIENCY - SUPERSONI FFICIENCY - SUBSONI SUPERSONIC	C.s.c 0.9042 ONIC 0.9455 ICares 0.8946	
	•	• •				
	INLET MOMENTUM CHANGE COMBUSTOR FRICTION DRAG COMBUSTOR STRUT DRAG COMBUSTOR MOMENTUM CHANGE NOZZLE FRICTION DRAG NOZZLE STRUT DRAG NOZZLE MOMENTUM CHANGE NOZZLE MOMENTUM CHANGE EXTERNAL FRICTION DRAG EXTERNAL PRESSURE INTEGRAL	2. (LBF) 6. (LBF)	EDUIVALENCE RATI COMBUSTOR EFFICI TOTAL PRESSURE R COMBUSTOR EFFECT INJECTOR DISCHAR VACUUM STREAM TH NOZZLE COEFFICIE PROCESS EFFICIE	ENCY	0.000 0.000 0.2696 0.6800 0.6800	
	STATIONS			FUEL INJECTORS		
	SPIKE TRANSLATION	884 (IN) 286 (IN) 400 (IN) 21.5 (IN) 55.5 (IN) 305 (IN) 469 (IN) 069 (IN)	INJECTORS 18 10 2A 2C 3A 3B 4	91ATION 40.400 41.314 44.300 48.789 46.250 54.079 56.264 44.814	VALVE	

t = 174.83 sec.

2

46.240

PAGE 1 ろー 3 - 2厂 IVAC PHI ETAC

SUVMARY REPORT Ü GAMMA MOLY SUNV MACH VEL S W/A AJAC 10414 6 WINC TUNNEL 0 5 1 - 0.000 745.999 3021 677.2(803) 1.2931 28.852 2594 0.495 411 -30.3(99) 1.3988 28.851 996 5.976 5950 1.830 0.10666 26.866 0.9834 5066 9.862 188.6 SPIKE TIP NS 18.087 3021 677.2(803) 1.2929 28.851 2594 0.600 16.305 2950 655.8(782) 1.2951 26.651 2566 0.403 1034 2.086 0.10666 26.866 0.9834 4970 1.713 185.0 0.600 WIND TUNNEL 0.000 745,999 3021 677.2(803) 1.2931 28.852 2594 0.000 0.381 407 -31.3(98) 1.3988 28.851 991 6.010 5954 1.830 0.10413 26.229 0.9834 4950 9.635 188.7 SPIKE TIP NS 0.600 18.087 3021 677.2(803) 1.2929 28.851 2594 0.600 16,400 2954 657.0(783) 1.2950 28.851 2568 0.391 1005 2.086 0.10413 26.229 0.9834 4950 1.626 188.7 INLET THRUAT 289,451 2992 668,6(794) 1,2940 28,651 2583 40.400 40.400 16.049 1480 237.4(367) 1.3500 28.851 1856 2.503 4645 1.893 0.94040 26.866 0.1115 4337 67.883 161.4 INLET UPNASK 0 3 40.400 289.451 2992 668.6(794) 1.2940 28.851 2583 40.400 13,783 1423 222.2(3g2) 1.3533 28.851 1821 2.595 4726 1.893 0.85491 26.866 0.1227 4380 62.791 163.0 INLET DNNRSK 123.844 2992 668.6(794) 1.2939 28,851 2583 **40.400** 40,400 106,283 2890 637.6(764) 1,2971 28,851 2542 0,490 1245 1,951 0,85491 26,866 0,1227 4380 16,541 163.0 0 8 COMBUSTOR 1 21 245.750 2951 669.3(813) 1.2962 27.708 2620 40.410 40.410 12.523 1422 218.6(366) 1.3544 27.708 1859 2.555 4749 1.966 0.94332 26.953 0.1116 4336 69.617 160.9 0.11 0.07 COMBUSTOR 2 21 41.292 184,165 2883 671,7(824) 1,2999 26,577 2648 41.292 15.744 1580 271.2(426) 1.3473 26.577 1995 2.243 4477 2.046 0.94854 27.044 0.1113 4212 65.993 155.7 0.23 0.04 COMBUSTOR 0 10 3 21 41.302 192.536 2843 671.7(812) 1.3018 26.534 2633 41.302 15.781 1537 271.7(414) 1.3499 26.534 1972 2.269 4474 2.039 0.94884 27.044 0.1113 4210 65.472 155.7 0.23 0.01 CONSUSTOR 0 11 4 21 191.024-2836 671.5(810) 1.3021 26.528 2631 41.367 41.367 16.018 1542 275.0(416) 1.3497 26.528 1975 2.255 4454 2.039 0.94885 27.044 0.1113 4201 65.681 155.3 0.23 0.00 COMBUSTOR 0 12 5 21 41.500 186.294 2834 671.1(809) 1.3022 26.527 2630 41.500 16.859 1572 283.8(424) 1.3482 26.527 1993 2.209 4402 2.040 0.94995 27.044 0.1111 4180 64,991 154.6 0.23 0.00 COMBUSTOR 0 13 6 21 42.460 147.089 2823 667.6(806) 1.3025 26.527 2625 42.460 12.524 1540 274.8(415) 1.3498 26.526 1974 2.246 4434 2.057 0.94103 27.044 0.1122 4087 64.636 151.1 0.23 0.00 COMBUSTOR 0 14 7 21 44.087 138.413 2851 659.6(814) 1.3008 26.582 2634 44.087 19.458 1772 325.7(482) 1.3383 26.582 2106 1.941 4088 2.064 0.90928 27.044 0.1161 4015 57.761 148.4 0.23 0.05 COMBUSTOR 0 15 8 21 142,661 2802 658,4(799) 1,3030 26,535 2616 44.310 44.310 20.394 1745 332.1(475) 1.3399 26.535 2093 1.930 4041 2.057 0.90723 27.044 0.1164 4004 56.967 148.1 0.23 0.01 COMBUSTOR 0 16 9 21 44.800 140.553 2787 655,7(794) 1.3036 26,528 2609 44.800 22.450 1784 345.8(487) 1.3384 26.528 2116 1.861 3938 2.056 0.90342 27.044 0.1169 3982 55.285 147.2 0.23 0.00 COMBUSTOR 0 17 10 21 44.802 140.659 2786 655.7(794) 1.3037 26.527 2609 44.802 22.451 1783 345.8(486) 1.3384 26.527 2115 1.862 3938 2.056 0.90372 27.044 0.1168 3982 55.302 147.2 0.23 0.00 COMPUSTOR 0 18 11 3 46.260 135.866 2765 648.1(787) 1.3043 26.550 2600

22,971 1795 308,4(490) 1.33/9 26,530 2121 1.826 3872 2.056 0.85095 27,040 0.1201 3985 51,210 147,4 0,23 0.00

MUMIN 0 IVAL PRI ETAC GAMMA MULMI SONV MACH VEL S AZAC COMBUSTOR 0 19 12 4 47,310 122,904 2935 643.0(838) 1.2963 26.727 2660 23.305 1975 342.9(501) 1.3288 26.727 2210 1.754 3875 2.078 0.79196 27.044 0.1333 4054 #1.687 144.9 0.23 0.17 47.310 COMBUSTOR 0 20 13 3 47.327 121,862 2948 642,9(842) 1,2957 26,742 2665 23,495 1993 343.8(546) 1.3280 26,742 2218 1.744 3869 2.080 0.70932 27.644 0.1338 4057 4/.455 150.0 0.23 0.19 47.327 COMBUSTOR 0 21 14 48.110 106,033 3192 639,2(916) 1,2842 27,021 2746 25,839 2306 355,7(638) 1.3138 27,023 2361 1.595 3766 2.107 0.73801 27,044 0.1431 4112 43.194 154.1 0.23 0.42 48.110 0 22 15 COMBUSTOR 118,564 2980 636,1(852) 1,2939 26,799 26/5 48.777 18.278 1909 301.6(521) 1.3306 26.799 2171 1.865 4091 2.084 0.67944 27.044 0.1554 4166 43.200 154.1 0.23 0.23 48.777 COMBUSTOR . 0 23 16 49.307 131,427 2850 633.7(8(2) 1,2998 26,666 2628 14.304 1662 268,0(449) 1.3424 26.666 2039 2.097 4277 2.065 0.63544 27.044 0.1662 4204 42.239 155.5 0.23 0.12 49.307 COMBUSTOR 0 24 17 21 50.717 148.317 2719 628.0(772) 1,3055 26.548 2578 8.831 1345 212.8(359) 1.3605 26.547 1851 2.462 4558 2.044 0.54157 27.044 0.1950 4272 38.361 158.0 0.23 0.04 50.717 0 25 18 COMBUSTOR 52.817 106.952 2947 621.3(841) 1.2948 26.812 2660 9.262 1631 215.8(439) 1.3425 26.812 2015 2.236 4505 2.087 0.44388 27.044 0.2379 4351 31.075 160.9 0.23 0.25 52.817 COMBUSTOR 0 26 19 134.970 2763 620.0(785) 1.3032 26.620 2593 53.317 7.005 1323 184.8(352) 1.3611 26.620 1834 2.545 4667 2.055 0.42573 27.044 0.2480 4368 30.875 161.5 0.23 0.08 53.317 0 27 20 COMBUSTOR 54.067 126.747 2795 618.1(795) 1.3017 26.660 2605 0.692 1347 179.8(359) 1.5593 26.660 1848 2.554 4683 2.062 0.40131 27.044 0.2631 4388 29.208 162.2 0.23 0.12 54,067 COMBUSTOR 0 28 21 54.827 120,201 2822 616,3(803) 1,3004 26,694 2614 6.375 1364 174.5(363) 1.3580 26.694 1858 2.531 4702 2.068 0.37950 27.044 0.2782 4407 27.733 162.9 0.23 0.14 54.827 COMBUSTOR 0 , 56 55 55.760 113.027 2853 614.4(812) 1.2989 26.734 2625 55.760 6.039 1386 168.6(369) 1.3565 26.734 1870 2.526 4723 2.075 0.35614 27.044 0.2965 4429 26.142 163.8 0.23 0.18 COMBUSTOR 0 30 23 56.252 75,619 3067 613,5(877) 1,2889 26,969 2700 5,862 1663 178.6(446) 1,3394 26,970 2026 2,302 4665 2,121 0,28696 27,044 0,3679 4474 20,003 165.4 0,23 0,38 56.252 COMBUSTOR 0 31 24 56.307 125.318 2733 613.4(776) 1.3043 26.610 2581 3.859 1135 135.5(300) 1.3723 26.610 1706 2.866 4890 2.057 0.28620 27.044 0.3689 4475 21.750 165.5 0.23 0.07 56.307 COMBUSTOR 0 32 25 56.447 124,498 2737 613,1(777) 1,3041 26,615 2582 56.447 3.834 1137 134,7(301) 1.3722 26,615 1707 2.866 4893 2.058 0.28410 27.044 0.3717 4478 21.603 165.6 0.23 0.08 COMBUSTOR 0 33 26 21 44.096 3707 613.0(1072) 1.2547 27.711 2889 56.527 56.527 5.763 2373 174.6(650) 1.3038 27.727 2355 1.989 4684 2.191 0.28733 27.044 0.3675 4480 20.915 165.6 0.23 1.00 COMBUSTOR 0 34 27 21 56,807 44.125 3705 612.5(1072) 1.2548 27.711 2888 56.807 5,662 2362 171.1(646) 1.3041 27.727 2350 2.000 4700 2.191 0.28648 27.044 0.3686 4485 20.923 165.8 0.23 1.00 COMBUSTOR 0 35 28 21 57.033 44.011 3704 612.2(1072) 1.2546 27.711 2888 57.033 5.539 2351 167.6(643) 1.3045 27.727 2345 2.011 4716 2.191 0.28579 27.044 0.3695 4489 20.947 160.0 0.23 1.00 COMBUSTOR 0 36 29 21 57.757 45.156 3701 611.1(1071) 1.2549 27.711 2887 5.145 2319 157.9(633) 1.3057 27.727 2330 2.044 4762 2.192 0.28135 27.044 0.3753 4497 20.022 166.3 0.23 1.00 57.757 **POLONBARTOR** 0 37 30 21 U158,777 39,356 3697 609.8(1069) 1,2548 27,711 2885 58.777 4,012 2233 131.6(607) 1,3088 27.727 2289 2.137 4892 2.199 0.27956 27.044 0.3777 4500 21,253 166.4 0.23 1.00

GAMMA MOLWT SONV MACH YEL 5 A/A A/AC 9 M1 MOH IVAC PHI ETAC COMBUSTOR 0 38 31 21 CT 60.787 21.613 3689 608.1(1067) 1.2529 27.708 2880 €0 60.787 1.537 2046 75.5(551) 1.3157 27.727 2197 2.349 5162 2.241 0.28929 27.044 0.3650 4463 23.204 165.8 0.23 1.00 COMBUSTOR 0 39 32 21 42.207 37.099 3689 607.1(1067) 1.2549 27.711 2882 62.207 3.581 2199 121.3(597) 1.3100 27.727 2273 2.169 4930 2.202 0.29713 27.044 0.3555 4470 22.767 165.3 0.23 1.00 COMBUSTOR 0 40 53 21 64.671 45,909 3682 604,2(1064) 1.2559 27.712 2880 64.671 8.756 2570 235.6(710) 1.2969 27.727 2445 1.757 4295 2.186 0.28165 27.044 0.3744 4451 16.799 164.6 0.23 1.00 COMBUSTUR 0 41 34 200 65.047 42.714 3680 603.7(1064) 1.2558 27.712 2880 10.173 2702 277.2(751) 1.2923 27.727 2502 1.615 4042 2.191 0.26184 27.044 0.4032 4448 16.448 164.5 0.23 1.00 65.047 COMBUSTOR REGEN 42 35 3 65.047 42,714 3864 670.1(1124) 1.2472 27.702 2941 65.047 9.903 2838 320.6(794) 1.2875 27.726 2560 1.634 4182 2.209 0.26184 27.044 0.4032 4538 17.017 161.8 0.23 1.00 NOZZLE AE 43 36 87.283 42.714 3680 603.7(1057) 1.2558 27.712 2880 87.283 0.731 1431 -102.6(373) 1.3451 27.727 1858 3.200 5945 2.191 0.05451 27.044 1.9371 5360 5.036 198.2 0.23 1.00 NOZZLE PO 44 37 87.283 42.714 3680 603.7(1057) 1.2558 27.712 2880 87.283 0.395 1219 *161.1(315) 1.3582 27.727 1723 3.590 6186 2.191 0.03595 27.044 2.9374 5497 3.456 203.3 0.23 1.00 NOZZLE AE REGEN 45 38 87.283 42.714 3864 670.1(1124) 1.2472 27.702 2941 0.770 1544 -70.9(405) 1.3386 27.727 1925 3.163 6089 2.209 0.05451 27.044 1.9371 5501 5.158 203.4 0.23 1.00 87.283 NOZZLE PO REGEN 46 39 87.283 42.714 3864 670.1(1124) 1.2472 27.702 2941 87.283 0.395 1300 -138,9(337) 1.3531 27.727 1776 3.582 6362 2.209 0.03466 27.044 3.0461 5656 3.427 209.1 0.23 1.00 FICTIVE COMBUSTR 66 59 289,451 3687 603,7(1066) 1,2601 27,719 2887 65.047 0.395 724 -291.7(184) 1.3861 27.727 1341 4.990 6694 2.054 0.06550 27.044 1.6119 5789 6.814 214.1 0.23 1.00 65.047 FICTIVE NOZZLE 67 60 87.283 24.115 3655 595.6(1056) 1.2550 27.710 2869 87.283 0.974 1763 -8.1(468) 1.3274 27.727 2048 2.685 5496 2.230 0.05451 27.044 1.9371 5103 4.656 188.7 0.23 1.00

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_	XABB		PwIB	P=06 `	PDA	X00	Q=1B	0=08	CAWALL	P=18/PS0	P#IB/PTO	P#08/P\$0	P#QB/P40-
2	6.509E	01	1.080E 01	9.630E 0n	-2.181E 02	#2.126E 03	#1.965E 0	3 -1.061E 03	4.342E 03	2.735E 01	1,448E=02	2.439E 01	1.291L=02
11	6.529E		1.02ZE 01					3 -1.067E 03	4.368E 03	2.587E 01	1.369E=02	2.545E 01	1.347E=02
	6.695E		5.360E 00					3 =1.101E 03	4.583E 03	1.358E 01	7.185E=03	9.675E 00	5.121E+03
	6.762E		3.543E 00					3 -1.110E 03	4.665E 03	8 974E 00	4 749E = 03	9.061E 00	4.796E=03
	6.839E		1.455E 00	2.809# 00				3 -1.120E 03	4.760E 03	3.685E 00	1.9506=03	7.114E 00	3.765E+03
	6.911E		1.815E 00	2.090E 00				3 #1.130E 03	4.848E 03	4.597E 00	2.433E-03	5.293E 00	2.802E-03
	6.972E		2.120E 00	2.207E 00				3 -1.140F 03	4.922E 03	5.369E 00	2.842E=03	5.591E 00	2.959E=03
	7.0675		1.4455 00						5.036E 03	3.661E 00	1.937E-03	6.053E 00	3.204E=03
				2.390E 00				3 =1.159E 03					
	7 . 1 . 1 O.E.		1.140E QO	2.134E 00				3 -1.169E 03	5,088E 03	2.887E 00	1.5286=03	5.406E 00	2.861E=03
	7.2635	01	9.8976001	1.225E 00	2.727E 02	#2.245E 03	=1+100E 0	3 -1,192E 03	5.273E 03	2.507E 00	1.327E=03	3.1032 00	1,642E=03
	7.278E	01	9.750E#04	1.555E 00	2.7758 02	-2.294E 03	-1.100E 0	3 -1.1932 03	5.290E 03	2.469E 00	1-3076-03	3.094E 00	1.6385=03
	7.353E	01	9.371E=01	1.205E 00	3.154E 02	#2.304E 03	1.102E 0	3 -1.202E 03	5.374E 03	2.374E 00	1.2562-03	3.052E 00	1.6152+03
	7.353E		9.369E=01	1.205E 00				3 =1.202E 03	5.375E 03	2.373E 00	1.256E=03	3.0528 00	1.615E=03
	7.486E		8.700E-01	0.000				3 -1.221E 03	5.427E 03	2.203E 00	1.166E=03	0.000	0.000
	7.771E		8.600E-01	0.000				3 -1.221E 03	5.525E 03	2.178E 00	1.153E-03	0.000	0.000
	0.161E		1.275E 00	0.000				3 -1.221E 03	5.630E 03	3.229E 00	1.709E=03	0.000	0.000
	8 4425		1.055E 00	0.000				3 -1.221E 03	5,684E 03	2.672E 00	1.414E=03	0.000	0.000
	8.728E		1.315E 00	0.000				3 -1.221E 03	5.707E 03	.3.331E 00	1.7636=03	0.000-	0.000
	8,728E	01	1.316E 00	0.000	4.715E 02	° ∞2.342E 01	1 =1.121E 0	3 =1.221E 03	5.707E 03	3.332E 00	1.763E=03	0.000	0.000

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RAMJET PERFURMANCE-

RAMJET PERFURMANCE-												
			INLET									
MEASURED SPECIFIC IMPULSE	LBF) MA LBF=8EC/LBM) AD	NGLE OF ATTACK	· · · · · · · · · · · · · · · · · · ·	DEGREES)								
CALCULATED THRUST COEFFICIENT	υΕ Το Το	LTA PT2		PSI)								
REGENERATIVE-COOLED ENGINE PERFORMANCE CALCULATED	IN KT	VLET PROCESS EFFICIENCY = : INETIC ENERGY EFFICIENCY =	SUBSONIC 0.9035 SUPERSONIC 0.9465									
STREAM THRUST	LBF) FN	INETIC ENERGY EFFICIENCY = ITHALPY AT PO = SUPERSONIC	*1.05 (BTU/LBM)								
. MOMENTUM AND FORCES		co	PBUSTOR									
INLET FRICTION DRAG	LOF) LOF) LOF) LOF) LOF) LOF) LOF) LOF)	JELWAIR RATIO	0.226 1.000 1.000 0.1476 0.7985 ENTS 0.8414. 0.7284.									
TOTAL EXTERNAL DRAG	LBF) PR LBF) KI LBF)	ROCEBS EFFICIENCY	0 . 5167									
Ć												
BROITATE		PUEL INJECT	DAS									
NOMINAL COWL LEADING EDGE	(IN) (IN) (IN) (IN)	#JECTORS STATION 1A 40.400 1B 41.292- 1C 44.300 2A 48.767 2C 46.250 3A 54.057 3B 56.242 4 44.792	B A B									

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SUMMARY REPORT

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20	WIND TUNNEL	۳,	H 0 5	GAMMA	HOLWT	SONV	HACH	VEL	8	H/A	M	A/AC	МТЧОМ	Q	IVAC	PHI	ETAC
	0.000 745.499 0.000 0.402 SPIKE TIP NS	3062 421 2	689.8(815) =28.1(101)				5.952	5993	1.834	0.10694	26,840	0.9799	5101	9,960	190.0	•	
	0.600 18.062 0.600 16.236 0.600 TUNNEL	3062	689.8(815) 667,5(793)	1.2916	26.851 28.851	2611 2582	0,408	1054	2,091	0.10694	26.840	0.9799	4955	1.752	184.6		
	0.000 745.499 0.000 0.382 8PIKE TIP N8	414	687,8(815) -29,5(100) 0 0	1,3989	28,851	999	6.003	5999	1.834	0.10317	25.895	0,9799	4925	9.619	190.2		
	0.600 18.062 0.600 16.380 INLET THROAT	2995 ₁ 5	689.8(815) 669.4(795) 0 4	1,2937	28.851	2584	0.391	1010	2.091	0.10317	25.895	0.9799	4924	1.620	190.2		
	40,400 304,417 40,400 15,632 INLET UPNRSK	1460 6	673.7(799) 232.2(361) 0 3	1.3511	28.851	1844	2.549	4701	1.891	0.93949	26,840	0.1115	4368	68,630	162.7		
	40,400 304,417 40,400 13,436 INLET DNNR87 40,400 124,872	1404 ?	673.7(799) 217.2(347) 0 4 673.7(799)	1.3944	59*921	1810	2.640	4779	1.891	0.85409	26.840	0.1227	4409	63,437	164.3		
	40.400 -107.442 COMBUSTOR 0 40.410 255.929	80 62 .	643.1(769) 1 21 675.1(820)	1 32966	20.851	2549	0.486	1238	1.952	0.85409	26,840	0.1227	4409	164434	1,54 +3		
	40.410 12.525 CDMBUSTOR 0 41.292 189.294	1416	210.7(365) 2 21 670.1(031)	1-3548	27.690	1857		4789	1.969	0.94258	56 . 935	0.1116	4367	70,155	162.1	0.12	07
	41,302 198,507	10 2854	270.1(426) 3 21 678.0(819)	1.3477	56.418 56.403	1997	2,262				-		4243	66,563	197.0	0.24	0.04
	41.302 15.717 COMBUSTOR 0 41.367 197.012 41.367 15.950	11 2847	270,6(414) 4 21 677,8(817)	1,3019	25.411	2642	, ,,		æ					66,541	-	77	
	COMBUSTOR 0 41.500 192.182 41.500 16.847	12 2845	273.9(415) 5 21 677.4(816) 283.1(424)	1.3020	26.410	2641							_	\$6.523			
	COMBUSTOR 0 42.460 155.650 42.460 13.361	13 2832	6 21 673,2(812) 278,3(419)	1.3024	26,410	2635	,							64.967	•	•	ي م
	COMBUSTOR 0 44,087 149,367 44,087 23,185	1789	7 21 663,9(806) 345,9(490)	1.3028	26,420	2626								56.333	, -	·	·
	44.310 148.041 44.310 24.279		8 21 662,4(802) 353,3(495) 9 3	1.3034	26,411 26,411	2521 2521	1.845	3933	190.5	0.90669	27.028	0.1164	4028	1 55,419	149.0	0.24	0.00
	44.800 136.384 44.600 26.680	2855 1928	659.1(818) 369.3(531) 10 2	1.3007	26,480 26,480	2640 2196	1.734	3808	2.072	0.90288	27,028	0,1169	3997	53.426	147.9	0.24	0.06
	44.802 136.427 44.802 26.681 COMBUSTOR 0	2854 1927 18	659.1(818) 369.3(531) 11 13	1.3322	26.479	2196	1.734	3608	2.07 <u>2</u>	0.90318	27.028	0,1168	3997	53,443	147.9	0.24	0.06
	46.250 119.473 46.250 27.110		651.4(807) 384.9(542)	1.3094	24.834 24.833	2647 2232	1.657	3652	2.164	0.85562	27,172	0.1240	3945	48.559	145.2	0.42	0.01

AZAC MUMIM Q IVAC PHI ETAC GAMMA MOLMT SONV MACH VEL S COMBUSTOR 0 19 12 2 119,349 2674 651,4(808) 1,3094 24,835 2647 46.260 27.113 1861 384.9(543) 1.3377 24.635 2232 1.656 3651 2.164 0.65499 27.172 0.1241 3946 40.517 145.2 0.42 0.01 COMBUSTOR 0 20 13 47.310 108.008 2796 643.7(846) 1.3036 24.976 2693 27,424 2010 363.6(588) 1,3304 24,476 2307 1,564 3608 2,183 0,79573 27,172 0,1333 5963 44,612 146,6 0,42 0,09 47.310 COMBUSTOR 0 21 14 107,526 2803 47.327 643.6(849) 1.3032 24.984 2696 27.465 2019 383.7(591) 1.3300 24.984 2311 1.560 3606 2.185 0.79307 27.172 0.1356 3986 44.439 146.7 0.42 0.09 47.327 COMBUSTOR 0 22 15 99,963 2915 638,1(884) 1.2979 25,111 2737 48,110 27.069 2137 378.6(627) 1.3241 25.111 2367 1.522 3603 2.200 0.74152 27.1/2 0.1431 4035 41.522 146.5 0.42 0.16 48.110 COMBUSTOR 0 23 16 48.767 96.549 2758 637.7(873) 1.3058 23.804 2742 25.483 1958 361.6(599) 1.3335 23.804 2335 1.592 3717 2.273 0.68671 27.298 0.1552 4087 39.662 149.7 0.58 0.09 48.767 COMBUSTOR 0 24 17 48.777 95.460 2759 637,6(874) 1,3057 23.806 2743 361.4(599) 1.3334 23.806 2336 1.592 3718 2.273 0.68582 27.298 0.1554 4088 39.624 149.7 0.58 0.09 48,777 23.455 1959 COMBUSTOR 0 25 18 49.307 92.220 2826 634.4(896) 1.3025 25.877 2769 49.307 21.958 2001 348.4(6;3) 1.3310 23.878 2355 1.606 3782 2.283 0.64141 27.298 0.1662 4144 37.704 151.8 0.58 0.12. COMBUSTOR 0 26 19 81.748 3018 626.6(960) 1.2934 24.082 2839 50.717 19.237 2145 320.7(658) 1.3231 24.082 2421 1.616 3912 2.309 0.54665 27.298 0.1950 4280 33.232 156.6 0.58 0.21 50.717 COMBUSTOR o 27 20 52.817 79.032 3042 617.0(968) 1.2919 24.132 2846 13.462 2000 253.7(609) 1.3279 24.132 2339 1.823 4264 2.313 0.44805 27.298 0.2379 4438 29.686 162.6 0.58 0.23 52.617 COMBUSTOR 0 28 21 2 53.317 79.177 3032 615.1(964) 1.2924 24.127 2842 12.382 1951 239.1(592) 1.3299 24.127 2312 1.876 4337 2.312 0.42973 27.298 0.2480 4466 28.966 163.6 0.58 0.23 53.317 COMBUSTOR 0 29 22 3 54.067 77.290 3053 612.2(972) 1.2913 24.155 2849 11.410 1939 224.6(588) 1.3300 24.156 2304 1.911 8404 2.315 0.40508 27.298 0.2631 4505 27.724 165.0 0.58 0.24 54.067 COMBUSTOR 0 30 23 3 76.372 3058 609.6(973) 1.2909 24.167 2850 54.827 10.425 1905 209.1(577) 1.3312 20.166 2284 1.900 4476 2.316 0.3830/ 27.298 0.2782 4541 26.649 166.3 0.58 0.25 54.827 COMBUSTOR 0 31 24 3 55.740 73.839 3088 606.6(983) 1.2894 24.204 2860 55.760 9.647 1906 195.7(576) 1,3308 24.205 2283 1.987 4535 2.321 0.35949 27.298 0.2965 4580 25.333 167.8 0.58 0.26 0 32 25 5 COMBUSTOR 56,252 54,649 3419 605,1(1095) 1,2728 24,544 2969 9.238 2284 198.8(698) 1.3124 24.548 2464 1.830 4509 2.369 0.28966 27.298 0.3679 4696 20.298 172.0 0.58 0.40 56.252 COMBUSTOR 0 33 26 56.307 64,234 3192 605.0(1018) 1.2843 24.312 2895 7,540 1929 163,9(583) 1,3266 24,314 2289 2,052 4698 2,340 0,28889 27,298 0,3689 4699 21,093 172,1 0,58 0,31 56.307 COMBUSTOR 0 34 27 3 56,447 63,933 3197 604,6(1020) 1,2841 24,318 2897 162.4(583) 1.3284 24.320 2290 2.054 4704 2.341 0.28677 27.298 0.3717 4703 20.965 172.3 0.58 0.31 36.447 7.481 1931 COMBUSTOR 0 35 28 56.527 56.043 3400 604.4(1089) 1.2738 24.526 2963 56.527 9,008 2242 191,1(684) 1,3141 24,530 2444 1.861 4548 2.365 0.29003 27.298 0.3675 4707 20,499 172,4 0.58 0.39 COMMUSTOR 0 36 29 56,807 57.116 3384 605.7(1083) 1.2746 24.511 2958 56,807 8.775 2206 184.1(672) 1.3157 24.515 2426 1.809 4582 2.363 0.2891/ 27.298 0.3686 4716 20.592 172.8 0.58 0.39 NO COMBUSTOR 0 37 30 57.047 3395 603.1(1087) 1.2740 24.524 2961 CT 57,033 € 57,033 6,775 2215 182.4(675) 1.3152 24,529 2430 1.80d 4588 2.365 U.28848 27.298 U.3695 4723 20.569 173.0 0.58 0.39

RAMMA MOLET SONV MACH VEL S AZAC MUMIP Q IVAC PHI FTAC 0 38 31 4 NO COMBUSTOR O 57.757 55.942 3437 601.3(1101) 1.2718 24.573 2974 C 57.757 6.775 2258 179.3(689) 1.3130 24.578 2449 1.876 4595 2.367 0.28400 27.298 0.3753 4742 20.280 173.7 0.58 0.41 COMBUSION. 0 39, 32 / 58.7777 102.077 2850 599.0(903) 1.3002 23.994 2771 58.777 4.800 1334 89.00 3951 1.3607 23.994 1940 2.605 5052 2.274 0.28219 27.298 0.3777 4751 22.155 174.0 0.58 0.17 COMBUSTOR 0 40 33 6 604.7/8/7 40.328; 3890 594.5(1257) 1.2449 25.080 3098 12.825 2978, 246.4(929) 1.2813 25.105 2749 1.518 4173 2.406 0.29201 27.298 0.3650 4740 18.936 175.6 0.58 0.62 60.787 COMBUSTOR 0 44 34 5 62.207 42.485, 4302 590.7(1400) 1.2152 25.564 3189 18.881; 3707 336,7(1181) 1.2438 25.630 2991 1.187 3551 2.428 0.29993 27.298 0.3553 4731 16.551 173.3 0.58 0.82 62.207 COFBUSTOR 0 42 55 4 64.671 40.930 4177 583.4(1356) 1.2240 25.439 3161 64 674 16.156 3496 305.4(1107) 1.2555 25.491 2926 1.275 3/29 2.425 0.28430 27.298 0.3749 4/16 10.477 174./ 0.58 0.77 COMBUSTOR 0 43 36 3 65.047 37.966 4180 582.2(1357) 1.2230 25.446 3160 , 15.126 3507 306.5(1111) 1.2547 25.500 2929 1.268 3714 2.431 0.26430 27.298 0.4032 4713 15.254 172./ 0.58 0.77 65.047 COMBUSTOR REGEN 44 37 3 65.047 37.966 4369 670.2(1427) 1.2114 25.407 3218 65.047 16.732 3767 409.9(1205) 1.2413 25.484 3020 1.195 3608 2.452 0.26430 27.298 0.4032 4790 14.821 175.5 0.58 0.77 NOZZŁE AE 45 38 S 87.283 37.966 4180 582.2(1339) 1.2230 25.446 3160 0.978 1903 -258.0(558) 1.3165 25.514 2209 2.935 6484 2.431 0.05502 27.298 1.9371 5986 5.544 219.3 0.58 0.77 87.283 NOZZLE PU 46 39 5 37,966 4160 582.2(1339) 1,2230 25,446 3160 8/.283 87.28% 0.402 1529 -376.4(440) 1.3349 25.514 1995 3.472 6926 2.431 0.03005 27.298 3.5467 6241 3.234 228.6 0.58 0.77 NOZZLE AE REGEN 47º 40 87.283 37.966 4369 670.2(1427) 1.2114 25.407 3218 87.283 1.031 2052 -209.2(607) 1.3102 25.514 2289 2.898 6633 2.452 0.05502 27.298 1.9371 6140 5.672 224.9 0.58 0.77 NOZZLF PU REGEN 48 41 5 87.283 37.966 4369 670.2(1427) 1.2114 25,407 3218 0.402 1633 -343.9(472) 1.3292 25.514 2657 3.463 7123 2.452 0.02894 27.298 3.6831 6423 3.203 235.3 0.58 0.77 87.282 FICTIVE COMBUSTR 68 61 0 304,417 4662 582,2(1532) 1,2100 26,040 3289 0.402 1073 -715.0(298) 1.3574 26.150 1664 4.842 8057 2.281 0.05107 27.298 2.0868 7051 6.395 258.3 0.58 1.00 FICTIVE MOZZLE 69 62 87.283 26,477 4130 563,1(1338) 1.2227 25,446 3141 87.283 1.161 2129 #183.6(633) 1.3071 25,514 2329 2,625 6112 2.455 0.05502 27.298 1.9371 5762 5.226 211.1 0.58 0.77

XABS	P⇒I#	P≈08	AGS	60 x	Ma15	0=08	CAMALL	P#15/P80	F=18/PT0	P=06/PS0	F=08/610
6.981E-01	1.055E 00	0.000	=4.406E=U1	0.000	0.000	0.000	2.4/0t=02	2.625E UU	1.415E#03	0.000	0.000
1.8368 01	1.055E 00	0.000	#3.513E 01	0.000	0.000	0.000	1.6346 02	2,6250 00	1 .415E=03	0.000	0.000
3.070E 01	2,185E 00	0.000	#1.665E UZ	0.000	0.000	0.000	5.0538 02	5.437F 00	2,931E+03	0.000	0.000
3.508E 01	3.889£ 00	0.000	•3.633E 02	0.000	0.000	0.000	6°804ĕ 05	9,676E 00	5.21ot=03	0.000	0.000
3.5185 01	3.906E 00		0 -4.3046 05	0.000	0.000	v.000	6.850E 02	9.718E 00	5.2396-03	1.473E 01	7.942E=03
3.519E 01	3.907E 00		0 +4.304E 02	0.000	0.000	0.000	6.853E 02	9.7216 OU	5.240E=03	1.465E 01	7.895E=03
3.555E 01	3.9656 00		0 -4.376E 02	0.000	0.000	1.000	1.213E 02	9,0658 00	5.319L=03	9.4998 00	5.1216#03
3.5868 01	3.932E 00		0 -4.517E 02				7.5456 02	9.783E 00	5.2/4E=03	5.101E 00	2.750E=U3
3.606E 01	3.910E 00		0 -4.6246 02				7.733E 02	9.7298 00	5.245E=03	7.152F 00	3.856E=03
3.048E 01	4.205E 00 4.185E 00		0 -4.815£ 02				8.169E 02	1.047E 01	5.642E=03	1.139E 01	6.142E=03
3.732E 01	4.071E 00					02 =1.647E 01	8,730E 02	1.0418 01	5.614E=03	1.674E 01	9,027E=03
3.803E 01	3.805E 00					02 *2.1825 01	9.059E 02 9.83A£ 02	1.0135 01	5.460E=03	1.984E 01	1 070E#02
3.8348 01	5.291E 00		1 +3,2662 02			02 =3.396E 01 02 =3.914E 01	1,0186 03	9.467E 00 1.316E 01	5.104E=03 7.097E=03	3.350E 01 3.43/E 01	1,806E=0Z 2.123E=0Z
3.875E 01	7.291E 00					02 -4.606E 01	1.065E 03	1.8146 01	9.700£=03	5.634E 01	2.0675-02
3.881E 01	7.565E 00					02 -4.701E 01	1.071E 03	1.883E 01	1.0156-02	3.6196 01	2.0598-02
3.901E 01	8.550E 00					02 -5.039E 01	1.094E 03	2.127E 01	1,147E-02	3.887E 01	2.096E-02
3.932E 01	1.365€ 01					02 -5.547E 01	1.130E 03	3.395E 01	1.830L=02	3.990E 01	2.151E=02
3.950E 01	1.669E 01					02 -5.848E 01	1.151E 03	4.152E 01	2.238E-02	2.945E 01	1.588E-02
3.981E 01	1.719E 01					02 =6.343E 01	1.187E 03	4.277E 01	2.306E=02	1.194E 01	6.439E=03
4.000E 01	1.751E 01					02 +6.649E 01	1.209E 03	4.356E 01	2.348E-02	1.147E 01	6.181E=03
4.040E 01	2.077E 01					02 -7.320E 01	1.256E U3	5.167E 01	2.786E=02	1.048E 01	5.647E=03
4.041E 01	2.085E 01	4.200E 0	0 #6.225E 02	#4.311E 0	2 -3.577E	02 =7.338E 01	1.257E 03	5.188E 01	2.797E=02	1.045E 01	5.634E#03
4.129E 01	2.804E 01					05 a1.058E 05	1.362E 03	6.977E 01	3.761E=02	8.268E 00	4.457E=U3
4-130E 01	5.815E 01					02 -1.034E 02	1.363E 03	6.497E 01	3.772E=02	8.243E 00	U.44E=03
4.137E 01	2.865E 01					05 #1.099E 05	1.371E U3	7.129E 01	3.843L=02	8.083E 00	4.357E=03
4.150E 01	2.9746 01					02 -1.137E 02	1.386E 03	7.399E 01	3.9891-02	9.843E 00	5.307E=03
4.246E 01	1.766E 01					02 =1.788E 02	1.501E 03	4.395E 01	2.369E-02	2.254E 01	1.2156-02
4.409E 01 4.431E 01	2.866E 01					02 -3.159E 02	1,698E 03	7,132E 01	3.845E-02	4.406E 01	2,375E=02
4.480E 01	3.017E 01 3.349E 01					02 =3.358E 02	1.725E 03	7.508E 01	4.047E=02	4.574E 01	2.466E=02
4.480E 01	3.348E 01	1.9845 0	1 074070E VE	#1.009E 0	2 -4.278E	02 =3.824E 02 02 =3.826E 02	1.785E 03 1.765E 03	8.332E 01 8.331E 01	4.445F=05	4.945E 01	2.666E#UZ
4.625E 01	2 994E 01					02 -5.345E 02	1.963E 03	7.450E 01	4.016E=02	4.946E 01 6.041E 01	2.666E#02 3.257E#02
4.626E 01	2.992E 01					02 -5.357E 02	1.9646 03	7.444E 01	4.013E=02	6.048E 01	3.261E=02
4.731E 01	2.735E 01		-8.636E 02				2.095E 03	6.805E 01	3.669E-02	6.842E 01	3.6896-02
4.733E 01	2.738E 01					02 -6.544E 02	2.097E 03	6.813E 01	3.673E-02	6 855E 01	3.696E=02
4.811E 01	2.880E 01	2.534F 0	-8.004E 02	-1.659E 0	9.203E	02 -7.383E 02	2,194E 03	7.166E 01	3.863E=02	6.305E 01	3.399E=02
4.877E 01	2.348E 01	2.348E 0	-7.256E 02	■1.775E 0	9.721E	02 -8.032E 02	2.277£ 03	5.843E 01	3.150E=02	5.843E 01	3.150E-02
4.878E 01	2.346E 01					02 #8.042E 02	2.278E 03	5.836E 01	3.146E=Q2	5.836E 01	3.146E=02
4.931E 01	5.195E 01					03 -8.529E 02	2.344E 03	5.464E 01	2.945E=02	5.464E 01	2.945E=02
5.0728 01	1.924E 01					03 =9.651E 02	2.555E 03	4.787E 01	2.580E-02	4.787E 01	2.580E+U2
5.282E 01	1.346E 01					03 =1.0928 03	2.788E 03	3.350£ 01	1 806E-02	3.350E 01	1.8064-02
5.332E 01 5.407E 01	1.238E 01					03 -1.1186 03	2.852£ 03	3.081E 01	1.6616-02	3.081E 01	1.6615-02
5.483F 01	1.141E 01 1.042E 01					03 -1.154E 03	2.9486 03	2.839E 01	1.531E=02	2.839E 01	1.531E+UZ
5.576E 01	9.647E 00					03 #1.189E 03	3.045E 03	2.594E 01	1.398E=02	2 594E 01	1.398E=02
5.625E 01	9.238E 00	7.244 P 0	0 -11 1/19E 01	PERGETE OF	0 0 1 0 3 4 3 5	03 =1.228E 03 03 =1.248E 03	3.165E 03	2.400E 01	1.2946=02	2.400E 01	1.2946-02
5.6318 01	5.887E 00					03 =1.250E 03	3,209E 03	2.298E 01	1.259L=02 7.897L=03	2.298E 01	1,239E=02
5.645E 01	5.8672 00					03 -1.255E 03	3.2346 03	1.465E 01	7.897E=03	2.287E 01 2.258E 01	1,233E=02 1,217E=02
5.653E 01	9.008E 00					03 =1,258E 03	3,245E 03	2.2416 01	1.2085.03	2.241E 01	1.2085=02
5.681E 01	8.775E 00	8.775F 0	0 -1.768E 01	-2.703E 0	-1.434E	03 =1.269F 03	3.280E 03	2.183E 01	1.1776-02	2.183E 01	1.17E=02
5.703E 01	8.775E 00	8.775E 0	9-146E 00	-2.719E 0	-1.441E	03 -1.277F 03	3.309E 03	2.183E 01	1.1776-02	2.183E 01	1.1776=02
5.776E 01	8.775E 00	8.775F 0				03 -1.305E 03	3.402E 03	2,183E 01	1.1776-02	2.183E 01	1.177E#02
5.878E 01	4.800E 00	4.890E 0				03 -1.339E 03	3.532E U3	1.194E 01	6.439L=03	1.194E 01	6.439E=U3
6.079E 01	1.282E 01	1.585E 0	3.242E 01	-2.954E 0:	-1.537E	03 -1.422E 05	3.790E 03	3.191E 01	1.7206-02	3.191E 01	1.7206-02
6.2216 01	1.888E 01	1.889E 0	1 3.2426 01	-3.057E 0.	*1.559E	03 #1.4986 03	3.972E 03	4.698E 01	2.533E=02	4.698E 01	2.533E=02

_ XABs	P=18	P=08	PDA	Gox	C= * 0	N=08	MARLE	D 74/4000	D 151.000A	0 0 100	
		•			C+18		CAWALL	b⇔IR\b80	P=18/PT0	P#0#/PSQ	P=08/P]0
. N 6.467E 01	1.616E 01	1.616E 01	3.242E 01		-1.6166	03 =1.640E 03	4.2895 03	4.020E 01	2.1676-02	4.0c0E 01	2.167E+02
C76.505E 01	1.451E U1	1.574E 01	3.2426 01	-3.240E 03	#1.626E	03 -1.664E 03	4.337E 03	3.611E 01	1.947E-02	3.916E 01	2.111E=U2
№6.509E 01	1.451E 01	1.570E 01	3.242E 01	#3.293E 03	≈1.627E	03 -1.666E 03	4.342E 03	3.611E 01	1.947E-02	3.905E 01	2.105E=02
6.529E 01	1.393E 01	1.547E 01	3.242E 01	-5.310E 03	₩1.633E	03 -1.678E 03	4.368E 03	3.467E 01	1.869E=02	3.850E 01	2.0766-02
6,695E 01	9.140E 00	7.680E 90	1.611E 02	#3.429E 03	-1.669E	03 -1.760E 03	4.583E 03	2.274E 01	1.226E-02	1.911E 01	1.0306-02
6.762E 01	6.088E 00	7.7328 00	3.161E 02	₩3.408E 03	#1.680E	03 -1.788E 03	4.665E 03	1.515E 01	8.166E-03	1.924E 01	1.037Epu2
6.839E 01	2,5806 00	6.155E 00	4.677E 02	*3.513E 03	-1.691E	03 m1.822E 03	4.760E 03	6.419E 00	3.461E=03	1.531E 01	8.256E>03
6.911E 01	2.42BE 00	4.6802 00	5.659E 02	#3.559E 03	-1.6995	03 -1.860E 03	4.848E 03	6.042E 00	3.257E=03	1.164E 01	6.278E=03
6,972E 01	2.300E 00	3.788E 00	6.356F 02	#3.597F 03	-1.7055	03 +1.892E 03	4.922E 03	5.723E 00	3.085E=03	9.426E 0U	•
7.067E 01	1.897E 00	2.400E 00	7.1686 02	-3.648F 01	7125	03 =1.926E 03	5.036E 03	4.721E 00	2.545E=03		5.082E=03
7.110E 01	1.715E 00	00 3862°2	7.460F 02	03.651E 03	-1.7155	03 =1.936E 03	5.088E 03			5,972£ 00	3.219£#03
7.263E 01	1.191E 00	1.935E 00	8 3086 05	-3 FOTE VA	W14/135	03 -1.4365 03		4.267E 00	2,300E=03	5.718E 00	3.0826.03
7.278E 01	1.140E 00		9 7505 05	*31070E U3	010/248	03 -1.973E 03	5.273E 03	2.964E 00	1,598E=03	4,815E QQ	2.596E+U3
		1.819E 00	5.354F 05	₩3.700E 03	#1.724E	03 -1.976E 03	5.290E 03	2.836E 00	1.529E=03	4,526E 00	2.440E+03
7.353E 01	1.198E 00	1 - 240E 00	8.833E 05	-3.724E 03	-1.728E	03 -1.997E 03	5.374£ 03	2.980E 00	1.607E=03	3.085E 00	1.6638-03
7.353E 01	1.198E 00	1.237E 00	8.837E U2	•3.725E 03	=1.728E	03 -1.997E 03	5.375E 03	2.981E 00	1.607E-03	3.078E 00	1.6596-03
7.486E 01	1.300E 00	0.000	9.1206 02	=\$.712E 03	=1.733E	03 =2.039E 03	5.427E 03	3.235E 00	1.744E-03	0.000	0.000
7+771E 01	1.630E 00	0.000	9.706E 02	₩3.782E 03	-1.742E	03 -2.039E 03	5.525E 03	4.056E 00	2.186E=03	0.000	0.000
8.1618 01	1.410E 00	0.000	1.036E 03	43.791E 03	-1.751E	03 =2.039E 03	5.630E 03	3.508E 00	1.891E=03	0.000	0.000
8.442E 01	1.470E 00	0.000	1.068E 03	-3.798E 03	#1.759E	03 +2.039E 03	5.684E 03	3.650E 0v	1.972L=03	0.000	0.000
8.728E 01	3.100E 00	0.000	1.123E 03	-3.812E 03	=1.772E	03 =2.039E 03	5.707E 03	7.713E 00	4.158£-03	0.000	0.000
8.728E 01	3.103E 00	0.000	1.123F 03	-3.812F 03	7777	03 -2.039E 03	5.707E 03	7.7228 00	4.163E=03	0.000	0.000

				• •	• - •
	X	DDRAG	CORAG	ÇF	нс
	4.040E 01 4.041E 01 4.129E 01 4.130E 01 4.137E 01 4.137E 01 4.137E 01	1.156E U2 1.919E=01 1.827E 01 1.974E=01 1.2513E 00 1.828E 01	1.156E 02 1.158E 02 1.340E 02 1.342E 02 1.355E 02 1.350E 02	2.205£=05 2.479E=03 2.645E=03 2.425E=03 2.408E=03 2.470E=03	4.344E=02 3.5/7E=02 4.154E=02 4.420E=02 4.655E=02 3.845E=02
	4.409E 01 4.431E 01 4.480E 01 4.480E 01 4.625E 01 4.626E 01 4.731E 01	2.981E 01 3.830E 00 8.287E 00 3.404E-02 2.466E 01 1.663E-01 1.576E 01	1.861E 02 1.899E 02 1.982E 02 1.982E 02 2.229E 02 2.230E 02 2,388F 02	2.521E=03 2.538E=03 2.554E=03 2.554E=03 2.609E=03 2.590E=03	5.428E*02 5.548E*02 5.819E*02 5.819E*02 5.352E*02 5.854E*02 5.809E*02
	4.733E 01 4.811E 01 4.877E 01 4.878E 01 4.931E 01 5.282E 01 5.332E 01	2.501E=01 1.120E 01 9.276E 00 1.382E=01 6.815E 00 1.6182E 01 4.880E 00	2.390E 02 2.593E 02 2.597E 02 2.665E 02 2.665E 02 2.648E 02 3.097E 02	2.661E-03 2.663E-03 2.669E-03 2.669E-03 2.669E-03 2.608E-03 2.608E-03 2.615E-03	5.634E=02 5.523E=02 4.716E=02 5.085E=02 4.8345E=02 3.283E=02 3.067E=02
	5.407E 01 5.407E 01 5.576E 01 5.625E 01 5.631E 01 5.645E 01	7.055E 00 6.817E 00 7.977E 00 2.567E 00 3.804E=01 9.813E=01 6.017E=01	3.167E 02 3.235E 02 3.315E 02 3.341E 02 3.345E 02 3.354E 02	2.581E=03 2.570E=03 2.570E=03 2.517E=03 2.570E=03 2.550E=03 3.121E=03	2.691E=02 2.692E=02 2.532E=02 2.532E=02 1.914E=02 1.987E=02
	5.681E 01 5.703E 01 5.776E 01 5.878E 01 6.079E 01 6.221E 01 6.467E 01	2.127E 00 1.588E 00 5.041E 00 7.368E 00 1.340E 01 8.764E 00 1.614E 01	3.382E 02 3.398E 02 3.448E 02 3.522E 02 3.656E 02 3.743E 02 3.905E 02	2.684E w 03 2.668E + 03 2.661E + 03 2.661E + 03 2.652E w 03 2.405E w 03 3.017E = 03 3.166E = 03	2.122E.02 2.124E.02 2.121E.02 1.391E.02 2.955E.02 2.924E.02 2.528E.02
	6.505E.01 6.509E.01 6.529E.01 6.695E.01 6.762E.01 6.639E.01	2.420£ 00 2.501£=01 1.266£ 00 1.031£ 01 3.654£ 00 3.745£ 00 2.993£ 00	3.929E 02 3.931E 02 3.944E 02 4.047E 02 4.121E 02 4.151E 02	3.159E=03 3.227E=03 3.222E=03 3.106E=03 3.070E=03 2.989E=03 2.952E=03	2,418E=02 2,448E=02 2,441E=02 1,825E=02 1,617E=02 1,194E=02 1,034E=02
	6.972E 01 7.067E 01 7.110E 01 7.263E 01 7.278E 01 7.353E 01 7.353E 01	2.301E 00 3.119E 00 1.259E 00 4.066E 00 3.463E=01 1.574E 00 2.834E=03	4:174E 02 4:205E 02 4:218E 02 4:259E 02 4:262E 02 4:278E 02 4:278E 02	2.930£=03 2.880£=03 2.868£=03 2.824£=03 2.814E=03 2.780£=03 2.780£=03	9,206E=03 7.202E=03 6.843E=03 5.607E=03 4,607E=03 4.603E=03
1	7.486E 01 7.771E 01 8.161E 01 8.442E 01 8.728E 01 8.728E 01	9.250E=01 1.911E 00 2.080E 00 1.042E 00 5.506E=01 0.000	4.287E 02 4.306E 02 4.327E 02 4.337F 02 4.343E 02 4.343E 02	2.7846=03 2.8056=03 2.7646=03 2.7586=03 2.8626=03 2.8626=03	4.909E=03 5.792E=03 5.157E=03 5.296E=03 9.154E=03 9.141E=03

RAMJET PERFORMANCE

22		RAMJET (PERFORMANCE			
7.0	* ENGINE PERFORMANCE			INLET		
MEASURED TH CALCULATED MEASURED SF CALCULATED	THRUST RUST PECIFIC IMPULSE PECIFIC IMPULSE THRUST COEFFICIENT HRUST COEFFICIENT	0.2575	MASS FLOW RAT ADDITIVE DRAG LIMITING PRES DELTA PTZ TOTAL PRESSUR	CK	0.9799 0.0010 0.1652 0.186 0.4083	
NET THRUST. SPECIFIC IN		5909. (LBF) 804. (LBF) 1757. (LBF)8FC/LBM)	INLET PROCESS INLET PROCESS KINETIC ENERG KINETIC ENERG ENTHALPY AT P	EFFICIENCY - SUPERSONI EFFICIENCY - SUBSONIC. Y EFFICIENCY - SUBSONIC Y EFFICIENCY - SUBSONIC O - SUPERSONIC	U 0.8973 0.9049 IC 0.9404 0.8887 1.33	(BTU/LBM)
				COMBUSTUR		
INLET MOMEN COMBUSTOR F COMBUSTOR F COMBUSTOR F NOZZLE FRIC NOZZLE STRI NOZZLE PRES EXTERNAL PF EXTERNAL PF TOTAL STRUT CAVITY FORC CALCULATE MEASURED LO	MOMENTUM AND FORCES FION DRAG	277.3 (LBF) =1.80 (LBF) 345. (LBF) =0.00 (LBF) 1049. (LBF) 0.00 (LBF) 0.00 (LBF) =1.80 (LBF) =1.80 (LBF) =1.601. (LBF) =1.601. (LBF)	EQUIVALENCE R COMBUSTOR EFF TOTAL PRESSUR COMBUSTOR EFF INJECTOR DISC VACUUM STREAM NOZZLE COEFFI PROCESS EFFIC	O	0.581 0.770 0.1247 0.6984 431. 0,7415.	
í	- STATIONS			FUEL INJECTORS		
SPIKE TRANS INLET THROA COWL LEADIN NOZZLE PLUC STRUT LEADI STRUT LEADI	AL LEADING EDGE AT NG EDGE DUD TRAILING EDGE G TRAILING EDGE ING EDGE LING EDGE EXIT	34.884 (IN) 0,3069 (IN) 40,400 (IN) 15.191 (IN) 73.531 (IN) 87.283 (IN) 56.447 (IN) 65.047 (IN)	INJECTORS 1A 1B 1C 2A 2C 3A 3H 4	STATION 40,400 41,292 44,300 48,767 46,250 54,057 56,242 44,792	VALVE B D E	

Reading 65

t = 196.43 sec.

S SUMMARY REPORT Ö Ö PORTH G IVAC PHI ETAC T Н GAMMA MOUNT SONV MACH VEL S A/AC WIND TUNNEL 0 5 1 689,1(814) 1.2919 28,852 2610 0.000 746.749 3060 0.402 420 =28.2(101) 1.3989 28.651 1006 5.954 5991 1.834 0.10710 26.885 0.9801 5107 9.971 190.0 0.000 SPIKE TIP NS > 0.600 18,062 3060 689,1(8,4) 1,2917 28,851 2610 666.9(793) 1,2940 28,651 2581 0.404 1055 2.090 0.10710 26.885 0.9801 4957 1.757 184.4 0.400 16.232 2987 WIND TUNNEL 0.000 746.749 3060 689.1(8:4) 1.2919 28.852 2610 w29.7(100) 1.3989 28.851 999 6.005 5997 1.834 0.10321 25.910 0.9801 4926 9.620 190.1 0.000 0.381 414 SPIKE TIP NS 18.062 3060 689.1(814) 1.2917 28.851 2610 0.60n 668,7(794) 1,2938 28.851 2583 0.391 1010 2.090 0.10321 25.910 0.9801 4925 1.620 190.1 16.381 2993 0.600 INLET THROAT 40.400 318,846 2990 667,9(794) 1.2940 28,851 2582 15.155 1421 221,7(351) 1,3534 20.851 1820 2,596 4725 1.886 0.94106 26.885 0.1115 4382 69,108 163.0 40.400 INLET UPNRSK 40 40 n 318,846 2990 667,9(794) 1,2940 28,851 2582 13.035 1366 207.3(337) 1.3567 28.851 1767 2.687 4801 1.886 0.85551 26.885 0.1227 4422 63.835 164.5 40.400 INLET DNNRSK 40,400 125,387 2990 668.0(794) 1.2940 28.851 2582 40.400 108,127 2891 638,00 764) 1,2971 28,851 2542 0,462 1225 1,950 0,85551 26,885 0,1227 4422 16,289 164,5 COMBUSTOR 15 1 40.410 270.468 2950 670.3(815) 1.2963 27.612 2624 14.212 1433 221.3(370) 1.3539 27.612 1869 2.536 4740 1.965 0.94426 26.980 0.1116 4381 69.553 162.4 0.12 0.07 40.410 COMBUSTOR 2 21 204,560 2879 673.2(827) 1.3002 26.435 2653 41.292 41.292 17.254 1572 269,8(426) 1,3479 26.435 1996 2,252 4494 2.046 0.94964 27.075 0.1113 4274 66.329 157.9 0.24 0.04 COMBUSTOR 0 10 214.518 2837 673.1(814) 1.3022 26.391 2638 41.302 17.286 1527 269.9(413) 1.3507 26.390 1971 2.274 4492 2.039 0.94994 27.075 0.1113 4273 66.313 157.8 0.24 0.01 41.302 COMBUSTOR 0 11 4 21 213-160 2830 672-9(812) 1.3025 26-384 2635 41.367 17.513 1530 272.86 414) 1.3506 26.384 1973 2.267 4474 2.038 0.94998 27.075 0.1113 4264 66.050 157.5 0.24 0.00 41.367 COMBUSTOR 0 12 5 21 206.376 2827 672,3(811) 1.3026 26.383 2634 41.500 41.500 18,801 1566 283,5(425) 1,3487 26,383 1995 2,211 4410 2,040 0,95105 27,075 0,1111 4247 65,185 156,8 0,24 0,00 COMBUSTOR 0 13 6 21 156.629 3009 667.0(866) 1.2940 26.593 2698 42.460 42.460 19.054 1816 293.5(496) 1.3351 26.693 2129 2.030 4323 2.077 0.94211 27.075 0.1122 4185 63.293 154.6 0.24 0.17 COMBUSTOR 0 14 44.087 122,499 3472 654,5(1007) 1,2714 27,151 2843 44.087 38,751 2640 396,0(757) 1,2978 27,155 2528 1,425 3596 2,124 0,41034 27,075 0,1161 4179 50,879 154,3 0,24 0,62 COMBUSTOR 0 15 44.310 120.317 3507 652.4(1018) 1.2696 27.199 2853 44.310 40.202 2755 402.5(777) 1.2951 27.203 2554 1.385 3536 2.127 0.90828 27.075 0.1164 4174 49.910 154.2 0.24 0.66 COMBUSTOR 0 16 44.800 116.165 3562 647.2(1035) 1.2665 27.280 2867 44.800 43.390 2875 416,9(814) 1.2901 27.286 2600 1.306 3394 2.131 0.90446 27.075 0.1169 4155 47.707 153.5 0.24 0.72 COMBUSTOR 0 17 10 44.802 116.194 3561 647.1(1035) 1.2666 27.280 2867 44.802 43.387 2874 416.9(813) 1.2901 27.286 2599 1.306 3394 2.131 0.90476 27.075 0.1168 4155 47.725 153.5 0.24 0.72 COMBUSTOR 0 18 11 6 46,250 107,237 3124 648,6(987) 1,2892 24,377 2866 46.250 41.490 2510 451,3(774) 1.3096 24.578 2589 1.274 3298 2.279 0.86612 27.315 0.1240 4117 44.081 150.7 0.55 0.23

GAMMA MOLWE SONV MALH VEL S MOMIN Q W/A A/AC IVAC PHI ETAC COMBUSTOR 0 19 12 2 107.170 3125 648.5(987) 1.2892 24.379 2866 46.26n 46.260 41.477 2511 431.1(774) 1.3096 24.380 2589 1.274 3298 2.279 0.85949 27.315 0.1241 4118 44.050 150.6 0.55 0.23 COMBUSTOR 0 20 13 47.310 100.745 3245 635.4(1027) 1.2830 24.536 2904 47-310 40,101 2633 416,7(813) 1,3035 24,537 2637 1,254 3308 2,291 0,79991 27,315 0,1333 4178 41,118 152,9 0,55 0,30 COMBUSTOR 0 21 14 47.327 100.477 3253 635.2(1030) 1.2826 24.545 2907 47.327 40.085 2642 416.5(816) 1.3030 24.547 2641 1.255 3308 2.292 0.79724 27.315 0.1338 4182 40.985 153.1 0.55 0.31 COMBUSTOR 0 22 15 48.110 95.919 3362 625.9(1066) 1.2770 24.682 2941 48.110 37.596 2727 397.0(843) 1.2985 24.685 2670 1.267 3384 2.302 0.74542 27.315 0.1431 4251 39.207 155.6 0.55 0.36 COMBUSTOR 0 23 16 48.767 91.615 3067 630.6(1046) 1.2924 22.494 2960 48.767 32.318 2406 379.7(799) 1.3145 22.495 2644 1.340 3543 2.437 0.69286 27.542 0.1552 4318 38.151 156.8 0.83 0.21 COMBUSTOR 0 24 17 48.777 91.545 3069 630.5(1047) 1.2923 22.496 2960 48.777 32.276 2407 379.3(799) 1.3145 22.497 2644 1.341 3545 2.437 0.69196 27.542 0.1554 4319 38.121 156.8 0.83 0.21 COMBUSTOR 81 25 0 87.954 3169 625.3(1083) 1.2874 22.600 2996 49.307 49.307 30.037 2474 359.8(822) 1.3107 22.602 2671 1.365 3645 2.448 0.64715 27.542 0.1662 4398 36.656 159.7 0.83 0.24 COMBUSTOR 0 26 19 50.717 77.715 3519 613.0(1211) 1.2697 22.963 3110 50.717 27.806 2807 332.60 939) 1.2944 22.968 2805 1.336 3746 2.483 0.55155 27.542 0.1950 4595 32.109 166.8 0.83.0.36 COMBUSTOR 0 27 597.7(1276) 1.2594 23.179 3161 52.817 72.354 3699 52.817 19.950 2800 240.3(932) 1.2917 23.190 2785 1.518 4229 2.499 0.45206 27.542 0.2379 4835 29.706 175.6 0.83 0.43 COMBUSTOR 0 28 53.317 70.451 3762 594.5(1299) 1,2557 23,250 3179 19.155 2847 228.3(948) 1.2892 23.264 2801 1.528 4280 2.504 0.43358 27.542 0.2480 4881 28.840 177.2 0.83 0.45 53.317 COMBUSTOR 55 65 0 69.046 3800 589.9(1313) 1.2534 23.300 3188 54,067 17.426 2833 202,4(942) 1.2890 23,315 2790 1.578 4403 2.508 0.40871 27,542 0.2631 4944 27,968 179.5 0.83 0.47 54.067 COMBUSTOR 0 30 23 68,445 3807 585,5(1315) 1,2528 23,318 3189 54.827 54.827 15.675 2778 174.3(921) 1.2906 23.334 2764 1.641 4536 2.508 0.38650 27.542 0.2782 5000 27.246 181.5 0.83 0.48 COMBUSTOR 0 31 24 3 55.760 / 67.240 3831 580.6(1324) 1.2512 23.354 3194 55.760 14-137 2746 147-1(908) 1.2913 23.372 2746 1.696 4658 2.510 0.36270 27.542 0.2965 5061 26.254 183.7 0.83 0.49 COMBUSTOR 0 32 25 5 52.223 4240 578.3(1476) 1.2228 23.793 3292 56.252 50,252 13.327 3248 152,9(1089) 1.2666 23.853 2928 1.576 4614 2.551 0.29225 27.542 0.3679 5206 20.954 189.0 0.83 0.64 COMBUSTOR 0 33 26 5 56.307 61.961 3851 578.1(1331) 1.2496 23,381 3199 50.307 10.106 2609 84.6(857) 1.2956 23.401 2680 1.854 4969 2.518 0.29148 27.542 0.3689 5209 22.510 189.1 0.83 0.50 COMBUSTOR 0 34 27 56.447 61.877 3854 577.5(1332) 1.2494 23.386 3200 56.447 9.990 2606 81.4(896) 1.2956 23,406 2678 1.861 4983 2.518 0.28933 27.542 0.3717 5216 22,404 189.4 0.83 0.50 0 35 28 COMBUSTOR 56.527 53.567 4208 577.2(1464) 1.2253 23.761 3285 56.527 12.874 3176 138.8(1062) 1.2699 23.817 2901 1.614 4683 2.547 0.29262 27.542 0.3675 5221 21.298 189.6 0.83 0.62 COMBUSTOR 0 36 29 56.807 54.690 4178 576.0(1453) 1.2276 23.731 3278 56,807 12,412 3108 125,7(1037) 1,2730 23,783 2876 1,650 4747 2,544 0.29176 27,542 0,3686 5235 21,522 190,1 0,83 0,61 COMBUSTOR 0 37 30 55.986 4136 575.1(1437) 1.2306 23.689 3268 57.033 57.033 11.929 3027 112,9(1007) 1.2766 23.734 2845 1.690 4809 2.540 0.29106 27.542 0.3695 5245 21.751 190,4 0.83 0.60

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GAMMA MOLHT SONV MACH VEL 8 AZAC MOMTM D #/A IVAC PHI ETAC' NO COMBUSTOR 0 38 31 # O 57,757 60,417 3988 572.2(1582) 1.2008 23.539 3233 CC 57.757 10.380 2758 74.4(909) 1.2883 23.569 2738 1.825 4991 2.526 0.28654 27.542 0.3753 5270 22.224 191.3 0.83 0.55 COMBUSTOR 0 39 32 8 58.777 113.265 3247 568,9(1109) 1,2821 22,808 3013 5.475 1575 -46.6(499) 1.3442 22.810 2148 2.583 5550 2.426 0.28472 27.542 0.3777 5280 24.556 191.7 0.83 0.31 58.777 COMBUSTOR 0 40 33 7 60.787 48.680 4681 563.4(1640) 1.1866 24.321 3370 17.137 3949 196.6(1348) 1.2234 24.488 3132 1.368 4284 2.569 0.29462 27.542 0.3650 5269 19.614 191.3 0.83 0.83 60,787 0 41 34 COMBUSTOR 62.207 51.768 4521 559,1(1580) 1.2007 24.152 3343 62.207 15,825 3665 161,3(1241) 1,2426 24,271 3054 1,461 4462 2,559 0.30261 27,542 0.3553 5260 20,982 191,0 0.83 0.76 COMBUSTOR 0 42 35 5 64.671 45.291 4833 550.5(1697) 1.1717 24.527 3388 64.671 19.405 4275 239,1(1471) 1.1972 24.741 3207 1.231 3947 2.576 0.28684 27.542 0.3749 5242 17.595 190.3 0.83 0.92 COMBUSTOR 0 43 36 4 65.047 41.473 4918 548,9(1729) 1.1625 24,627 3397 65.047 19.801 4459 270.6(1541) 1.1802 24.865 3244 1.151 3732 2.582 0.26667 27.542 0.4032 5240 15.466 190.2 0.83 0.98 COMBUSTOR REGEN 44 37 5 65.047 41.473 5055 660.9(1787) 1.1557 24.481 3445 65.047 23.023 4705 428.9(1642) 1.1653 24.711 3321 1.026 3408 2.605 0.26667 27.542 0.4032 5295 14.122 192.3 0.83 0.98 NOZZLE AE 45 38 5 41.473 4918 548.9(1674) 1.1625 24.627 3397 87.283 1.263 2686 =507.0(858) 1.2731 25.091 2603 2.793 7269 2.582 0.05551 27.542 1.9371 6849 6.271 248,7 0.83 0.98 87.283 NOZZLE PU 46 39 87.283 41.473 4918 548.9(1674) 1.1625 24.627 3397 87.283 0.402 2085 =722.4(643) 1.2957 25.092 2313 3.448 7976 2.582 0.02498 27.542 4.3039 7271 3.097 264.0 0.83 0.98 NOZZLE AE REGEN 47 40 87.283 41.473 5055 660.9(1787) 1.1557 24.481 3445 1.334 2865 =432.6(931) 1.2654 25.089 2690 2.750 7397 2.605 0.05551 27.542 1.9371 6994 6.581 253.9 0.83 0.98 87.283 NOZZLE PO REGEN 48 41 87.281 41.473 5055 660.9(1787) 1.1597 24.481 3445 87.283 0.402 2223 -674.1(691) 1.2901 25.092 2384 3.429 8173 2.605 0.02401 27.542 4.4785 7458 3.050 270.8 0.83 0.98 FICTIVE COMBUSTR 68 61 65.047 318.846 5123 548,9(1807) 1,1823 24,859 3481 0.402 1288=1007.0(379) 1.3377 25.155 1845 4.782 8824 2.418 0.04485 27.542 2.3974 7800 6.151 283.2 0.83 1.00 65.047 FICTIVE NUZZLE 69 62 0 87.283 26,621 4840 522,0(1698) 1,1396 24,612 3367 1.552 3039 +373.8(988) 1.2590 25.087 2754 2.432 6695 2.613 0.05551 27.542 1.9371 6502 5.776 236.1 0.83 0.98 87,283

XABs	Biwq	P#OB	PDA	K O G	હ=1 1	Q∞08	CAMALL	P#18/PS0	P#18/PT0	P=U6/P80	P#08/P10
6,981E=01	1.060E 00	0.000	#4.406E=01		0.000	0.000		2.636E 00	1.4196=03	0.000	0,000
1 83 E 01	1.060E 00	0.000	-3.529E 01	0.000	0.000	0.000	1.6346 02	2.636E 00	1 #419E#03	0.000	0.000
3.070E 01	2.195E 00	0.000	-1.672E U2	0.000	0.000	0.000	5.053E U2	5.458E 00	2.939E=03	0.000	0.000
3.508E 01	3.896E 00	0.000	-3.646E 02	0.000	0.000	0.000	6.804E 02	9.6886 00	5.218£=03	0.000	0.000
3.518E 01	3.919E 00	5.9238 00			0.000	0.000	6.850E 02	9.745E 00	5.249E-03	1.473E 01	7,9326+03
3,519E 01	3.921E 00		-4.318E V2		0.000	0.000	6.853E 02	9.749E 00	5.2506-03	1.465E 01	7.888E=03
3.555E 01	4.000E 00		+4.389t 02		0.000	0.000	7.2138 02	9,946E 00 9,856E 00	5.357E=03 5.308E=03	9.765E 00 5.594E 00	5.259E=03
3.586E 01	3.964E 00		, -4.527£ 02 , -4.632£ 02				7.525E 02 7.733E 02	9.796E 00	5.2768=03	7.575E 00	4.080E=03
3.606E 01 3.648E 01	3.940E 00 4.207E 00		-4.817E 02				8.169L 02	1.046E 01	5.6346=03	1.167E 01	6.285E+03
3.701E 01	4.220E 00		-5.052E 02				8.730E 02	1 0495 01	5.6512-03	1.684E 01	9.068E#03
3.732E 01	4-106E 00					2.484E 01	9.059E 02	1.021E 01	5.498E=03	1.983E 01	1.068E-02
3.803E 01	3.840E 00					-3.862E 01	9.838E 02	9.548E 00	5.142E=03	3.330E 01	1.7946=02
3.834E 01	5.453E 00					44.449E 01	1.018E 03	1.356E 01	7.302E=03	3.910E 01	2.106E=02
3.875E 01	7.624E 00	1.540g 0	-5.298E 02	#4.724E 02	-4.201E 02	2 -5.233E 01	1.065E 03	1.896E 01	1.0211=05	3.858E 01	5.065E=05
3.881E 01	7.923E 00	1.535E 0	-5.301E 02	■4.753E 02	! =4.219E 08	2 45.340E 01	1.071E 03	1.970E 01	1.061E=02	3.817E 01	2.056E=02
3,901E 01	8,990E 00					2 =5.723E 01	1.094E 03	2.235E 01	1.5046-05	3.690E 01	2.095E=02
3.932E 01	1-4015 01					-6,297E 01	1.130E 03	3.485E 01	1,8776=02	4.000E 01	2.1546=02
3.950E 01	1.701E 01					2 =6,637E 01	1.1518 03	4.230E 01	2.278E+02	3.267E 01 2.039E 01	1.760E=02 1.098E=02
3.981E 01	1.737E 01					2 =7,195E 01	1.187E 03	4.319E 01	2.356E=02	1.9908 01	1.0726.02
4.000€ 01	1.759E 01					9 a7.541E 01	1.256£ 03	5.162E 01	2.7806-02	1.888E 01	1.0176-02
4.040E 01 4.041E 01	2.075E 01					2 -8,299E 01 2 -8,319E 01	1.257E 03	5.1828 01	2 7916-02	1.885E 01	1.0156+02
4.129E 01	2.7835 01					01.173E 02	1.362E 03	6 9195 01	3.7466#02	1.661E 01	8.947E=03
4.130E 01	2.791E 01	6-071F 00	#7.020E 02	-6.513E 0	-5.334E 0	-1.179E 02	1.363E 03	6,938E 01	3.7376-02	1.659E 01	8.934E=03
4.137E 01	2.842E 01					-1.217E 02	1.371E 03	7.067E 01	3.806t-02	1.642E 01	8.8456-03
4.150E 01	2.947E 01					20 300E 02	1.386E 03	7.329E 01	3.947E=02	5.051E 01	1.0886=02
4.246E 01	1.901E 01					2.059E 02	1.501E 03	4.727E 01	2.5466-02	4.748E 01	2.5576=02
4.409E 01	3.982E 01					2 03.6336 02	1.698E 03	9.900E 01	5.332E-02	9.370E 01	5,046E=02
4.431E 01	4.267E 01					3,870E 02	1.725E 03	1.061E 02	3.714E=02	9-382E 01	5.053E+02
4.4805 01	4.8946 01	3.784E 0	=7.580E 02	#1.355E 03	=9.047E Q2	2 =4.501E 02	1.785E 03	1.217E 02	6.553E=02 6.553E=02	9.409E 01	5.068L=02
4.480E 01	4.893E 01		-7.584E 02				1.963E 03	1.114E 02	5043500.0	9.489E 01	5.110E-02
4.625E 01 4.626E 01	4.482E 01					5 =6,937E 02 5 =6,956E 02	1 964E 03	1.114E 02	5.998E=02	9.489E 01	5.111E=0Z
4.731E 01	4.181E 01					8.975E 02	2.095E 03	1.039E 02	5.598L=02	9.5478 01	5.142E-02
4.733E 01	4.177E 01					50 3800.Pm	2.097E 03	1.039€ 02	5.5946-02	9.548E 01	5,1426-02
4.811E 01	4.010E 01					-1.042E 03	2.194E 03	9.970E 01	5,3706-02	8.725E 01	4.6998-02
4.877E 01	3.232E 01					5 -1.146E 03	2.277E 03	8.036E 01	4,328E=02	8.036E 01	4.328E=02
4.878E 01	3.228E 01	3.558E 0	-4.662E 02	-2.646E 03	-1.499E 0	5 -1.147E 03	2.278E 03	8.025E 01	4.3226-02	8.025E 01	4.322E-02
4.93 E 01	3.004E 01					5 -1.220E 03	2.344E 03	7.469E 01	4.02ZE=02	7.469E 01	4.0226-02
5.072E 01	2.781E 01	2.781E 01				3 -1.391E 03	2.522E 03	6.914E 01	3.724E=02	6.914E 01	3.724E=02
5,282E'01	1.995E 01	1.995E 0				5 = 1 - 598E 03	2.788E 03	4.960E 01	2.672Em02	4,4605 01	2.6728=02
5.332E 01	1.915E 01	1.915g 0				3 -1.641E 03	2.852E 03 2.948E 03	4.763E 01 4.333E 01	2.565E=02 2.334E=02	4.763E 01 4.333E 01	2.565t+U2 2.334E+U2
5.407E 01 5.483E 01	1.743E 01 1.567E 01	1.7438 0				3 #1.704E 03	3.045E 03	3.897E 01	2.0996=02	3.897E 01	2.0995=02
5.576E 01	1.414E 01	1.567E 0:				3 =1.764E 03 5 =1.833E 03	3.165E 03	3,515E 01	1.8936=02	3.515E 01	1.893E=02
5.625E 01	1.333E 01	1.3336 0				5 +1.868E 03	3 2096 03	3.314E 01	1.7656-02	3.314E 01	1.7858#02
5.631E 01	6.975E 00	1,5248 0				1 -1.871E 03	3.216E 03	1.7348 01	9.340E=03	3.291E 01	1.773E+02
5.645E 01	6.975E 00	1.301E 0				3 -1.881E 03	5.234E 03	1.734E 01	9.340E=03	3.234E 01	1.742E=02
5.653E 01	1.287€ 01	1.287E 0				3 #1.886E 03	3.245E 03	3.201E 01	1.724E=02	3.201E 01	1.7246=02
5.681E 01	1.2418 01	1.241E 0				5 =1.905E 05	3.280E 03	3.086E 01	1.665F-05	3.086E 01	1.6626#02
5.703E 01	1.193E 01	1.193E 0				1.920E 03	3.3095 03	2.966E 01	1.597E=02	2.966E 01	1.597E=U2
5.776E 01	1.038E 01	1.038E 0				3 -1 969E 03	3.402E 03	2.581E Q1	1.390km02	2.581E 01	1,3908=02,
5.878E 01	5.475E 00	5.475E 0				3 #2.026E 03	3,5328 03	1.3616 01	7.3326#03	1.3618 01	7,3326=03
6.079E 01	1.7148 01	1.714E 0				3 =2.134E 03	3.790E 03	4.261E 01	2.295E-02 2.119E-02	4.261E 01 3.935E 01	2.2955-02
6.221E 01	1.582E 01	1,5826 0	7 34410E 08	-4101AF A	7 4643466 U.	3 -2.219E 03	4871EE V3	3.935E 01	# # Y 7 7 E O E.	711756 01	2.119E=02

•	•											
	XABS	P=IB	Р⇒ОВ	PDA	80x	ਨ≈IB	0=08	CANALL	P=18/PS0	P#18/P10	P#OB/PS0	P#08/P10
Ö	6.467E 01	1.940E 01	1.940E 01	5.970t 02	. #4.850E 0	3 =2.476E C	3 -2,374E 03	4.289£ 03	4.825E 01	2.5996-02	4.625E 01	2.599E#Û2
7	6.505E 01	1.965E 01	1.995E 01	5.970E 02	-4.892E 0	3 -2.493E (3 -2.400E 03	4.337E 03	4.886E 01	2.631E#02	4.961E 01	2.6/26.02
0	6.5098 01	1.965E 01	2.001E 01				3 -2.403E 03	4.342E 03	4 886E 01	2.631E=02	4.975E 01	5.680F=05
	6.529E 01	1.867E 01	2.030E 01	5.970E 02	-4.919E 0	3 -2.503E C	3 -2.416E 03	4.368E 03	4 643E 01	2.5006-02	5.047E 01	2.718E=02
	6.49gE 01	1.056E 01	9.640E 00				3 =2.518E 03	4.5838 03	2.626E 01	1.414E-02	2-397E 01	1.291E=02
	6.762E 01	7.457E 00	9.157E 00				3 =2.555E 03	4.665E 03	1.854E 01	9.985E=03	2.277E 01	1.226E#02
	6.839E 01	3.890E 00	6.960E 00				3 -2.601E 03	4.760E 03	9.672E 00	5.209E=03	1.731E 01	9.320E=03
	6,911E 01	3.362E 00	4.905E 00				3 =2,651E 03	4.848E 03	8.360E 00	4.502E-03	1.220E 01	6.568E=U3
	6.972E 01	2.915E 00	3.970E 00	1.337E 03	-5.512E 0	3 -2.618E	3 =2.694E 03	4.922E 03	7.248E 00	3.904E=03	9.872E 00	5.317E=03
	7.067E 01	2.127E 00	2.515E 00				3 =2.746E 03	5.036E 03	5.288E 00	2.8488-03	6.253E 00	3.368E-03
	7-110E 01	1.770E 00	2.366E 00				3 #2.765E 03	5.088E 03	4.401E 00	2.370E-03	5.882E 00	3.168E=03
	7.263E 01	1.547E 00	1.835E 00				3 -2.818E 03	5.273E 03	3.846E 00	2.071E-03	4.563E 00	2.457E=43
	7.278E 01	1.525E 00	1.756E 00				3 -2.822E 03	5.290E 03	3.792E 00	2.042L=03	4.366E 00	2.351E-03
	7.353E 01	1.464E 00	1.360E 00				3 -2.847E 03	5.374E 03	3.639E 00	1 960E 03	3.382E 00	1.821E=03
	7.353E 01	1.463E 00	1.358E 00				3 -2.847E 03	5.375E 03	3.639E 00	1 9606 03	3.376E 00	1.818E=03
	7.486E 01	1.355E 00	0.000				3 42.899E 03	5.427E 03	3.369E 00	1.815E-03	0.000	0,000
	7.771E 01	2.600E UO	0.000				3 -2,8998 03	5.525E 03	6.465E 00	3.482E=03	0.000	0.000
	8.16 E 01	1.840E 00	0.000				3 -2.899E 03	5.630E 03	4.575E 00	2.464E=03	0.000	0.000
	8.442E 01	1.500E 00	0.000	1.8505 03	-5-605F 0	4 -2.707F	3 -2.899E 03	5.684E 03	3.730E 00	2.009E=03	0.000	0.000
	8.728E 01	3.145E 00	0.000	1.9065 03	-5.6.3E 0	3 -2.7348 6	3 =2.899E 03	5.707E 03	7.820E 00	4.212E.03	0.000	0.000
	8.728E 01	3.148E 00	0.000	1.9065 01		2 -0-1375 (3 42.899E 03	5.707E 03	7.828E 00			-
			4 + 4 ~ A	4 8 7 V V III V II	,	3 -51/335 (13 9610776 V3	3810(203	/ * OEGE UV	4.216E=03	0.000	0.000

	KENDING	₽.	ands brack	E AD LIME	= 190,435	MACH 6.0
	X		DORAG	CDRAG	CF	HÇ
	4.040E 4.041E	01 01	1.185E 02 1.897E=01	1.185E 02 1.187E 02	2.172E=G3 2.462E=O3	4.267E+08
		01		1.3678 02	2.607E=03	4.468E=02
		01		1.3686 02	2.387E=03	4.774E#02
	4.137E	01		1.381E 02	2.359E=03	4.852E-02
	4.150E 4.246E	01		1.405E 02	2.373E=03	5.0826404
	4.409E	01	2.823E 01	1.581E 02 1.864E 02	2.623E=03	5.028E=02 7.225E=02
	4.431E	01		1.901E 02	2.879E-03	6.701E=02
	4.480E	01	8,436E 00	1.986E 02	2.901E=03	6.817E=08
	4.480E	01		1.986E 02	2.901E=03	6.817E=02
	4.625E	01	2.490E 01	2.235E 02	3,1986=03	6,155Ee02
	4.626E 4.731E	oi	1.667E 01	2.237E 02 2.403E 02	3,198E=03 2.816E=03	6.155E=02 6.739E=02
	4.733E	01	2.463E=01	2.406E 02	2.8166-03	6.739E=02
	4.811E	01	1.110E 01	2.517E 02	2.860E-03	6.321E=02
		0 1		2.612E 02	3.124E-03	5.465E+02
	4,878E 4,931E	01	1.421E+01	2.6135 02	2.827E=03 2.789E=03	6.035E-02
	5.072E	οi	6.979E 00 1.695E 01	2.853E 02	2.765E=03	5.792E=02 5.3/0E=02
		0i	10 3562.S	3.0828 02	2.805E-03	4.1962002
	5.332E	01	5.308E 00	3.135E 02	2.886E-03	3,947E=02
		01	7.850€ 00	3.214E 02	2.883E=03	3.662E-02
		01	7.733E 00 9.165E 00	3.291E 02 3.383E 02	2.870E=03 2.843E=03	3.419E=02
	5.6258	01	2,963E 00	3.383E 02 3.412E 02	2.808E=03	3.185E=02 2.886E=02
		01	4.425E-01	3.417E 02	2.973E-03	2.307E=02
ORIGINAL' PAGE IS OF POOR QUALITY	5.645E	01	1-146E 00	3.428E 02	2.769E-03	2.425E=02
0.0	5.053E	01	5.8146.01	3.435E 02	3.324E-03	2.432E=02
	5.681E 5.703E	01	2.397E 00 1.834E 00	3.459E 02	2.952E=03	d.633E+02
P(5.776E	ŏi	1,834E 00 5,909E 00	3.477E 02 3.536E 02	2.926E=03 2.877E=03	2.565E=02
26	5.078E	01	8,648£ 00	3.6238 02	2.780E=03	1.877E=02
A A	6.079E	01	1.519E 01	3.775E 02	2.552E-03	3,637E#08
ا تا	9.551E	01	1.053E 01	3.880E 02	3.142E=03	2.848E=02
P.	6.467E ~6.505E'	01	1.915E 01 2.575E 00	4.071E 02 4.097E 02	3.139E=03 3.319E=03	3.0415=02
A.A.	6.509E	01	2.680E=01	4.097E 02 4.100E 02	3.434E=03	2.870E+02 2.910E+02
记 思	6,529E	οi		4.113E 02	3.430E=03	2.844E+02
13 13	0.0955	01	1.151E 01	4.229E 02	3.3285.03	2.130E=02
7	6.762E	01	4.232E 00	4.471E 02	3.300E=03	1.894E=02
	6,839E 6,911E	01	4.405E 00 3.522E 00	4.315E 02 4.350É 02	3.239E=03	1.436E=02
	6.972E	01	2.6526 00	4.377E 02	3.174E=03	1.0446.02
	7.067E	01	3,526E 00	4.412E 02	3.1236=03	7.835E=03
	7.110E	01	1.385E 00	4.426E 02	3.1076=03	7.168E=03
	7.263E	01		4.471E 02	3.0758-03	6.1672=03
	/•278E 7•353E	01	3.893E=01 1.806E 00	4.474E 02 4.492E 02	3.070E=03	6.025E#03
	7.353E	01	3.300E=03	4.492E 02 4.492E 02	3.046E=03	5.308E=03 5.304E=03
	7.486E	01	1.042E 00	4-503£ 02	3.033E=03	5.108E=03
	7.7718	01	2.393€ 00	4.527E 02	3.103£m03	8.415E-03
4	8.161E	01	2.758E 00	4.5548 02	3.036E=03	6.461E+03
271	8,442E 8,728E	01	1.209E 00 5.936E-01	4.567E 02 4.572E 02	2.9966=03	5.5098#05
71	8.728E	01	0,000	4.572E 02 4.572E 02	3.081E=03 3.081E=03	9,512E=03 9,52UE=03
	<i>3</i> –	-				

RAMJET PERFORMANCE

<i>1</i> 2		MANUEL PERF	UNNANCE			
72	ENGINE PERFORMANCE			INLET		
MEASU CALCU MEASU	LATED THRUST	(LBF) (LBF=SEC/LBM)	MASS FLOW RATIO ADDITIVE DRAG COLF LIMITING PRESSURE	FICIENT	0.9801 0.0010 0.1656	
MEASU	LATED THRUST COEFFICIENT	F	TOTAL PRESSURE REC TOTAL PRESSURE REC INLET PROCESS EFFI	OVERY - SUPERSONIC OVERY - SUBSONIC CIENCY - SUPERSONIC CIENCY - SUPERSONIC	0.4270 0.1679 0.9033	(PSI)
STREA	CALCULATED 6639		KINETIC ENERGY EFF	ICIENCY - SUPERSONIC	0.9368	
NET T SPECI	HRUST a a segres a se	(LHF)	ENTHALPY AT PO . S	ICIENCY - SUBSONIC UPERSONIC URSONIC	-4.00	(BTU/LBM)
THRUS	T COEFFICIENT.				-	·
	MOHENTUM AND FORCES			COMBUSTOR		
COMBU COMBU COMBU NOZZL NOZZL	FRICTION DRAG	(LBF) (LBF) (LBF) (LBF) (LBF) (LBF)	EQUIVALENCE RATIO, COMBUSTOR EFFICIEN TOTAL PRESSURE RAT COMBUSTOR EFFECTIV	CY	0.833 0.983 0.1301 0.8452	0.8116+ 0.7073
NOZZL NOZZL EXTER TOTAL TOTAL CAVIT GALCL MEASL	E MOMENTUM CHANGE E PRESSURE INTEGRAL NAL FRICTION DRAG NAL PRESSURE INTEGRAL EXTERNAL DRAG STRUT DRAG Y FORCE 1293 ULATED LOAD CELL FORCE 1262 1209 1209 1209 11175	(LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF)	NOZZLE COEFFICIENT PROCESS EFFICIENCY	NOZZLE ST COEFFICIENT = CS = CT	0.8667 0.8793	
	, SMOITATS		FU	EL INJECTORS		
SPIKE INLET COWL NGZZL NGZZL STRUT	TRANSLATION	4 (IN) 9 (IN) 0 (IN) 1 (IN) 1 (IN) 5 (IN) 7 (IN) 7 (IN)	INJECTORS 1A 1B 1C 2A 2C 3A 3B	8TATION VA 40.400 41.292 44.300 48.767 46.250 54.057 56.242 44.792	LVE A B C E	

Reading 65

t = 201.83 sec.

PAGE 1

SHMMARY REPURT

GAMMA MOLAT SONV MACH VEL 5 AZAC MUNTH V / A IVAL POI ETAC WIND TUNNEL 746.499 3022 677.7(803) 1.2930 28.852 2595 0.000 0.395 412 -30.2(99) 1.3968 26.851 996 5.975 5952 1.830 0.10674 26.883 0.0833 5073 9.673 188.7 SPIRE TIP NS 0.60n 18.037 3022 677.7(803) 1.2929 28.651 2595 0:600 10.243 2951 650.1(782) 1.2951 25.651 2566 0.405 1039 2.087 0.10674 26.803 0.9635 4959 1.723 164.5 WIND TUNNEL 146.499 3022 677.7(803) 1.2930 26.652 2595 0.000 0.380 407 -31.3(98) 1.3968 28.651 990 6.014 5956 1.830 0.10380 26.142 0.9833 4935 9.608 188.8 0.000 SPIKE TIP AS 0,600 18.037 3022 677,7(803) 1,2929 26,651 2595 0.600 16,354 2956 65/.5(783) 1.2950 28.851 2568 0.391 1095 2.087 0.10380 26,142 0.9833 4935 1.621 188.8 INLET THROAT 316.074 2955 65/.3(783) 1.2951 28.651 2568 40.400 15.057 1402 216.9(346) 1.3545 28.851 1809 2.595 4695 1.883 0.94100 26.883 0.1115 4353 68.653 161.9 40.400 INLET UPNESK 40.400 \$16,074 2955 657,3(783) 1,2951 28,851 2568 12.948 1348 202.6(332) 1.3578 28.851 1776 2.666 4770 1.883 0.85546 26.883 0.1227 4393 63.416 163.4 INLET DNNRSK 124.541 2955 657.3(783) 1.2951 28.851 2568 40.400 40.400 107.367 2857 627.66 754) 1.2982 28.851 2528 0.482 1219 1.947 0.85546 26.883 0.1227 4343 16.207 163.4 COMBUSTOR 0 8 268,717 2917 659,8(806) 1,2974 21,594 2611 40.410 40.410 15.187 1441 223.6(372) 1.3534 27.593 1875 2.492 4672 1.963 0.94425 26.979 0.1116 4352 66.564 161.5 0.12 0.07 COMBUSTOR 0 9 2 21 206,899 2847 662,9(817) 1,3013 26,421 2640 41.292 41.292 18.566 1577 271.1(428) 1.3477 26.420 2000 2.214 4428 2.043 0.94963 27.075 0.1113 4255 65.344 157.2 0.24 0.04 COMBUSTON 0 10 3 21 216,780 2804 662,9(804) 1,3032 26,376 2625 41.302 41.302 18.605 1532 271.5(415) 1.3504 26.376 1975 2.241 4425 2.035 0.94992 27.075 0.1113 4254 65.328 157.1 0.24 0.01 COMBUSTOR 4 21 0 11 41.367 215,586 2797 662.6(802) 1.3035 26,370 2622 41.367 18.854 1535 274.4(416) 1.3503 26.370 1977 2.250 4407 2.035 0.94993 27.075 0.1113 4246 65.065 156.8 0.24 0.00 CUMBUSTOR 0 12 41.500 - 208.781 2803 662.0(803) 1.3032 26.378 2624 41.500 20.292 1501 285.5(429) 1.34/9 26.377 2004 2.100 4341 2.038 0.45103 27.075 0.1111 4230 64.153 156.2 0.24 0.01 COMBUSTOR 0 13 42.460 174.052 2895 656.3(R31) 1.2968 26.493 2656 23.631 1787 311.0(489) 1.3372 26.493 2118 1.905 4157 2.060 0.94210 27.075 0.1122 4177 60.856 154.3 0.24 0.10 42.460 COMBUSTOR 0 14 44.087 116.898 3657 643.0(1065) 1.2615 27.393 2894 44.087 45,582 2989 416.6(848) 1.2848 27.461 2639 1.275 3566 2.135 0.91032 27.075 0.1161 4168 47.620 154.7 0.24 0.82 COMBUSTOR 0 15 44.310 115.288 3701 640.9(1078) 1.2590 27.453 2905 44.310 47.815 3070 425.6(874) 1.2813 27.463 2669 1.230 3282 2.138 0.90827 27.075 0.1164 4107 40.320 154.6 0.24 0.86 COMBUSTOR 0 16 44.800 112.738 3770 635.3(1099) 1.2551 27.555 2922 44.800 52.718 3210 444.2(919) 1.2750 27.566 2719 1.137 3093 2.141 0.90405 27.075 0.1169 4181 43.469 154.4 0.24 0.94 COMBUSTOR . 0 17 10 44.802 112.770 3769 635.3(1099) 1.2551 27.554 2921 44.802 52.723 3215 444,1(918) 1.2751 27.565 2719 1.157 3093 2.141 0.90475 27.0/5 0.1168 4160 43.483 154.4 0.24 0.94 COMBUSTUR 0 18 11 6 46.250 105.857 3299 642.0(1079) 1.2812 23.799 2972 46.250 50.671 2809 482.2(923) 1.2556 23.00) 2766 1.018 2856 2.552 0.86283 27.401 0.1240 4215 38.021 153.6 0.66 0.29

	READING =	0065	BLOCK	# 102	TIPE	# 201,8	33 MAÇ	н 6.4) PT :	746	499	T] # 302	2.4							ş
		р	T	н		GAMMA	MOLWT	รถพง	MACH	VEL	8	W/A	w	A/AC	MTMOM	O	TVAP	Dut	ETAC	
	COMBUSTOR		19			O MINIT	(IIOE III)	00117	7" 4 W 7 *	* C C	Ģ	77.8	"	A/FC	mur (n	· ·	ITAL	LUT	GIAL	
		105.827	3302	642.7((1080)	1.2811	23.802	2972												
	46.250	56.698	2872	482.16	924)	1.2955	23.804	2787	1.017	2835	2.352	0.86220	27,401	0,1241	4216	37,985	153.9	0.66	0,29	
	COMBUSTOR	0	50	13 4															-	
	47.310	102.723	3600	628.2(1183)	1.2658	24.142	3063												
	47 x 310				(1038)	1.2797	24.147	2402	0.951	2762	2.372	0.80243	27.401	0,1335	4386	34.443	100-1	0.06	0.42	
	COMBUSTOR 4/.327		15 (628.0(11081	1 3451	5/1 155	3067												
	47.327	59.674	3217	476.01	1042)	1.2790	24.160	2910	0.948	2758	2.373	0.79975	27.401	0-1338	4343	34.276	160.4	0.66	0.4%	
	COMBUSTOR		22		11-4-1		,,,		••••	-,		••••	818403	0,1250	4375	241610	10412	V, 00	7145	
	48.110	99,166	5894	617.81	12871	1.2493	24.482	3143												
	48.110	50.564	3473	450.1((1130)	1.2653	24.495	2987	0.970	2897	2.390	0.74776	27.401	0.1431	4540	33,664	165.7	0.66	0.55	
	COMBUSTOR	04 04 0	23																	
	48,767 48,767	73,000 #5.866	3350	626,8((1292)	1,2693	21,777	2515	1 007	* 20 7	2 500	0 (0107	37 864	0 4550	0464	9 F				
	COMBUSTOR	-24000	24	17 2	1084)	145011	c1110c	2445	1.071	2503	£.500	0.69692	¢1.104	0.1352	4651	12.201	101.44	1.04	0.35	
	46.777			620.7(12031	1.2691	21.779	3213												
	48.777	45.732	3947	410.40	1084)	1.2870	21.784	2992	1.100	3290	2.580	\$00000	27.700	0.1554	4653	35,587	168.0	1.04	0.33	
	COMBUSTOR	0	25	18 4					• "	-							*-,**	• • • •		
	49.307	91.830	3648	621.1(1326)	1,2645	21,871	3238												
	49,307	3/.067	3013	353.7((1064)	1.2868	21.879	2968	1.535	3658	2.587	0.65095	27.704	0.1662	4761	37,007	171.9	1.04	0.36	
	COMBUSTOR 50.717	84.518	26 2948	607.9(40025	1 2072	22 (80	1720											•	
	50.717	30.806	3205	285.41	11281	1.2754	22.208	3025	1.328	4017	2-611	0.55478	27.704	0.1960	4997	34.420	180.0	1 - 0#	0 . AB	
ح.	COMBUSTOR	0	27	20 4	111317		507000	****	* • • • •	- • • •		00304.0	61414-	011730	7,,,	348067	10044	1104	OFMS	
\\$	50.717 COMBUSTOR	78.594	4141	591.36	1526)	1.2331	22.438	3372												
20.4	€52,817	22,275	3232	180,00	1144)	1.2707	22.477	3014	1.505	4537	2.626	0.45471	27.704	0.2379	5263	32.058	190.0	1.04	0,52	
CONT. SON CONTROL OF	YCOMBUSTOR	70 22	28																	
\$\\\	53.317	20.273	1176	587.86	1554)	146330	22.43/	2307	1 647	1491	3 49E	0 67617	97 9A4		E	74 (07				
20 62	COMBUSTOR	CANTIE	29	22 4	11121	196133	661413	5704	10001	40/4	51043	0.43613	C IA	0.2460	2212	31,682	14110	1+04	n • DR	
10 4	54.067	76.791		582.7(1539)	1.2303	22.495	3379												
AT AU	54.067	10.585	3160	123.7(1114)	1.2725	22.539	2978	1,609	4793	2.629	0.41111	27,704	0.2631	5379	30,620	194.2	1.04	0.54	
13 KB	COMBUSTOR	0	30	23 3														,	-	
AY.	74.047 54.650	75,857 16,875		240.01	1540}	1,2290	52.522	3381	1 667	#020		A 700E4	79 80"		r 420					
⊘ ,	COMBUSTOR	0.00012	31		109/3	1+6130	ESEDIA	E120	1.000	4450	# * D D V	0.38876	61.104	0.2702	2453	29.727	140.3	1.04	0.55	
	55.760	74.322			15881	1.2265	22.567	3387												
	55.760	15.320			1087)	1.2736	55.650	2945	1.712	5042	2.633	0,36483	27.704	0.2965	5504	28,584	198.7	1.04	0.56	
	COMBUSTOR		32	25 5	• • •			_	•									***		
	56.252	57.785			1729)	1,1898	23,023	3467												
	56,252 COMBUSTOR	14.500			1316)	1.2397	23.194	3133	1,592	4988	2.672	0.29396	27,704	0,3679	5662	22.789	204.4	1.04	0.72	
	56.307	68.780	33 4258		. 5 . 7 .	. 2540	22 587	1700												
	56.307	10.954			1055)	1.2788	22.587	2875	1.A70	537A	2.640	0.29319	27.704	0.2489	5444	3/ 5/13	20/1 5	1 0/1	A 67	
	COMBUSTOR			27 3			241044	2417		20,0	210-0	V 12 73 1 7	E1 # / 0=	0 1 3 0 0 9	3000	24.502	COMED	1.04	0 4 5 7	
	56.447	68.656	4263	569.30	1565)	1.2245	22.593	3389												
	56.447	10.837	2943	- ali.5(1025)	1.2787	22.651	2874	1.876	5391	2.640	0.29103	27.704	0.3717	5674	24,382	8.405	1.04	0.57	
	COMBUSTOR 56.527	Q	35	28 21														- '	•	
	56.527	50.683 14,042			1707)	1.1494	23.490	1277	1 650	E066	3 - an	0 30474	34 466	0 7/7/	1.435				4 4 8 8	
	COMBUSTOR			59 51	1240)	181070	E31710	3603	11220	7000	E . 000	0.29434	21.104	V.50/5	2019	e3.145	205.0	1.04	1 * Q Ø	
	56.807	50.809	5126	\$67.60	19081	1.1500	23.492	3532												
8	56.807	13.575	4373	43.00	1580)	1.1707	23.990	3257	1.573	5124	2,688	0.29347	27.704	0.3686	5693	23,368	205.5	1.04	1.00	
27	COFOUSIUR			30 2i	_									-				·	- # - T	
ပၢ	5/.033	50.678	5125	566.6(1908)	1.1500	23.495	3532								_				
	67.033	12,951	4345	≤0 + 1 (1264)	1.1721	24.004	3248	1*901	2501	6.080	0.29276	27.704	0.3695	5704	23.662	205.9	1.04	1.00	

GAMMA MOLMT SONV MACH VEL S A/F A/AC MIMOM IVAC PHI ETAC NO CUMBUSTOR 0 38 51 21 ~ 57,757 49,223 5118 503,5(1905) 1,1494 23,494 3529 ආ 57,757 10.950 4258 -25.7(1532) 1.1764 24.042 3219 1.687 5429 2.690 0.28822 27.704 0.3755 5728 24.319 206.7 1.04 1.00 COMBUSTOR 0 39 32 21 38.652 5083 559.8(1891) 1.1479 23.465 3516 58.777 58.777 5.775 4007 w162.2(1426) 1.1895 24.122 3134 1.918 6011 2.709.0.28639 27.704 0.3777 5734 26.752 207.0 1.04 1.00 COMBUSTOR 0 40 33 21 60.787 53,235 5118 553,6(1904) 1,1509 23,518 3529 16.462 4444 84.0(1611) 1.1686 23,963 3262 1.4/7 4848 2.081 0.29635 27.704 0.3650 5713 22.525 206.2 1.04 1.00 60.787 COMBUSTOR 0 41 34 21 62,207 54,123 5115 549,0(1903) 1,1512 25,526 3528 16.406 4427 72.6(1604) 1.1697 23.974 3277 1.490 4883 2.679 0.30439 27.704 0.3553 62.207 5697 23.097 205.7 1.04 1.00 COMBUSTOR 0 42 35 200 64.671 51.107 5098 539.5(1896) 1.1510 23.531 3521 64.671 19.121 4535 142.9(1650) 1.1647 23.913 3310 1.344 4455 2.682 0.28852 27.704 0.3749 5672 19,474 204.7 1.04 1.00 COMBUSTOR 0 43 36 200 55.047 47,330 5087 537,8(1891) 1,1504 23,523 3517 65.047 20,099 4600 189,9(1678) 1.1614 25,865 3336 1.251 4172 2.688 9.26825 27,704 0.4032 5668 17,391 204.6 1.04 1.00 COMBUSTOR REGEN 44 57 3 65.047 47.330 5188 639.2(1937) 1,1471 23,383 3557 65.047 18.252 4658 244.0(1704) 1.1565 23.791 3358 1.325 4447 2.708 0.26823 27.704 0.4032 5714 18.536 200.3 1.04 1.00 NOZZLE AE 45 38 5 87.283 47.330 5087 537.8(1834) 1.1504 23.523 3517 87,283 1.341 2905 -650.9(981) 1.2653 24.235 2746 2.808 7712 2.688 0.05584 27,704 1.9371 7306 6.692 263./ 1.04 1.00 NOZZLE 46 39 5 87.283 47.330 5087 537.8(1834) 1.1504 23.523 3517 0.395 2231 +907.0(725) 1.2862 24.236 2426 3,504 6503 2.686 0,02363 27,704 4,5776 7785 3.122 281.0 1.04 1.00 87.283 NOZZLE AE REGEN 47 40 S 87.283 47.330 5188 639.2(1937) 1.1471 23.383 3557 87.263 1.406 3084 \$580.3(1051) 1.2593 24.234 2823 2,766 7812 2.708 0.05584 27.704 1.9371 7424 6.779 268.0 1.04 1.00 NOZZLE PO REGEN 48 41 87.283 47.330 5188 634.2(1937) 1.1471 23.383 3557 87.283 0.395 2353 =861.7(770) 1.2819 24.236 2488 3.484 8666 2.708 0.02283 27.704 4.7368 7942 3.075 286.7 1.04 1.00 FICTIVE COMBUSTR 68 61 65.047 316.074 5307 537.8(1981) 1.1677 23,759 3601 65.047 0.395 1415-1194.1(438) 1.3267 24.236 1962 4.744 9309 2.528 0.04080 27.704 2.6508 8284 5.903 299.0 1.04 1.00 FICTIVE NUZZLE 69 62 0 31.448 5006 508.2(1857) 1.1480 23.509 3486 87.283 87.283 1.612 3242 -516.4(1114) 1.2523 24.231 2886 2.461 7160 2.717 0.05584 27.704 1.9371 6965 6.213 251.4 1.04 1.00

XABS	Р⇒ІВ	P#08	PDA	QQX	umtā	0-00	Can At I	P= 18/P80	P=18/PT0	a-nv 1050	0-40 40 10
6.981E=01	1.065E 00	0,000	=4.397E=01	0.000	0.000 UPIB	0#08 0.000	CAMALL 2.470E=02	2.694E 00	1.427E=03	P#05/P50 0.000	P=Q8/PI0 0.000
1.836E 01	1.065E 00	0.000	-3.545E 01	0.000	0.000	0.000	1.634E 02	2.694E 00	1.427E-03	0.000	0.000
3,070E 01	2.200E 00	0.000	-1.678E UZ	0.000	0.000	0.000	5.053E 02	5.564E 00	2.947E=03	0.000	0.000
3.508E 01	3.90ZE 00	0.000	#3.655E 02		0.000	0.000	6.804E 02	9.869E 00	5.227E+03	0.000	0.000
3.518E 01	3.926E QD	5.825E 00	-4.318E 02	0.000	0.000	0.000	6,850E 02	4.93UE 00	5.259E-03	1.473E 01	7.803E#03
3.519E 01	3.927E 00		64.318E 02		0.000	0.000	6.853E 02	9.933E 00	5.261E+03	1.466E 01	7.764Epu3
3.555E 01	4.010E 00		-4.389€ 02		0.000	0.000	7.213E UZ	1.014E 01	5.372E=03	1.030E 01	5.456E-03
3.586E 01	3.974E 00				02 -3.6155		7,525E U2	1.005E 01	5.323E-03	6,576E 00	3,4834-03
3.606E 01 3.648E 01	3.950E 00 4.207E UU				02 =3.657E		7,733E 02	9.991E 00	5.291E=03	8.476E 00	4.489E+03
3.701E 01	4.235E 00				02 =3.747E	02 0.000 02 =1.051E 01	8,169E 02 8,730E 02	1.064E 01 1.071E 01	5.635E=03 5.673E=03	1.241E 01 1.736E 01	6.570E=03 9.196E=03
3.732E 01	4.118E 00					02 =1.392E 01	9,059E U2	1 041E 01	5.516E-03	2.023E 01	1.072E=02
3.801E 01	3.845E 00					02 -2 157E 01	9,838E 02	9.725E 00	5.151E-03	3.385£ 01	1.793E-02
3.834E 01	5.512E 00					02 -2.480E 01	1 018E 03	1.394E 01	7.384E=03	3.971E 01	2.103E-02
3,875E 01	7.757E 00					02 -2.910E 01	1,065E 03	1 962E 01	1.0398-02	3.899E 01	2.065E-02
3.881E 01	8.065E 00	1.537E 01	~5.280£ 0≥	-4.633E	02 =4.336E	02 =2.969E 01	1,071E 03	2.040E 01	1.081E=02	3.889E 01	2.060E=U2
3.901E 01	9.170E 00					02 -3.178E 01	1.094E 03	2.319E 01	1.2286-05	3.963E 01	2.099E-02
3,932E 01	1.41BE 01					02 #3.490E 01	1.130E 03	3.587E 01	1.9002-02	4.075E 01	2.158E#02
3.950E 01 3.981E 01	1.717E 01 1.747E 01					02 #3,674E 01	1,151E 03	4.344E 01	2.301E=02	3.464E 01	1.8356#02
4.000E 01	1.766E 01					02 =3.975E 01 02 =4.161E 01	1,187E 03	4.419E 01 4.466E 01	2.340E=02 2.365E=02	2,441E 01 2.422E 01	1.293E=02 1.283E=02
4.040E 01	2.088E 01					02 =4.609E 01	1.256E 03	5.281E 01	2.7976-02	2.382E 01	1.2426=02
4.041E 01	2.096E 01					02 #4.622E 01	1,257E 03	5.301E 01	2.8086-02	2.381E 01	1.261E=02
4.129E 01	2.800E 01	9.071E 00	#6.828E 02	=6.276€	02 =5.494E	02 #7,821E 01	1,362E 03	7,097E 01	3.759E=02	2.294E 01	1.2156=02
4.130E 01	2.814E 01					02 -7.881E 01	1,363E 03	7.118E 01	3.7706-02	2.293E 01	1.2156=02
₩ 137E 01	2.867E 01					02 #8.280E 01	1,371E 03	7.250E 01	3.840E=02	2.287E 01	1.211E#02
~ 25 150E 01	2.974E 01					02 =9.160E 01	1.386E 03	7.521E 01	3,9846-02	2.744E 01	1.453E=02
0 64.246E 01 4.409E 01	2.340E 01					02 =1.757E 02	1.501E 03	5.919E 01	3.1356=02	6.035E 01	3.196E=02
4.431E 01 4.431E 01 4.480E 01	4.525E 01					02 =3.448E 02 02 =3.695E 02	1.498E 03	1.144E 02 1.220E 02	6.0618.02	1.1618 02	6.151E#02
A 4.480E 01	5.482E 01					02 -4. 381E 02	1.785E 03	1.387E 02	6.463E#02 7.344E#02	1.198E 02 1.280E 02	6.348E=02 6.780E=02
2 4.480E 01	5.482E 01					02 =4.384E 02	1.785E 03	1.387E 02	7.344E=02	1.280E 02	6.781E=02
4.625E 01	5.318E 01	6.016E 01	*5.895E 02	-1.897E	03 m1.182E	03 97.154E 02	1.963E 03	1,345E 02	7.124E-02	1.522E 02	8.059E=02
4.480E 01 4.480E 01 4.625E 01 4.625E 01 4.733E 01 4.733E 01 4.811E,01	5.317E 01	6.023g 01	#5.877E 02	-1.901€	03 #1.183E	03 #7.176E 02	1.964E 03	1.345E 02	7.123E=02	1.523E 02	8.0686=02
4.731E 01	5.198E DI					03 =9,514E 02	2.095E 03	1.315E 02	6.963E#02	1.69BE 02	8,994E=02
4.733E 01	5.210E 01					03 -9.5516 02	2.097E 03	1.318E 02	6.979E=02	1.701E 02	9.009E=02
4.811E-01 4.877E 01	5.750E 01 4.588E 01					03 =1.119E 03	2.194E 03	1.454E 02	7.703E#02	1.407E 02	7.4526-02
4.878E 01	4.573E 01					03 =1.238E 03 03 =1.239E 03	2,277E 03. 2,278E 03	1.160E 02 1.157E 02	6.146E#02 6.126E#02	1,160E 02	6.1465-02
4.931E 01	3.787E 01					03 ~1.323E 03	2.3448 03	9.578E 01	5.073E-02	1.157E 02 9.578E 01	6,126E=02 5,073E=02
5.072E 01	3.081E 01	3.081E 01	2.881E 02	353E.E	03 =1.807E	03 -1.515E 03	2 522E 03	7 792E 01	4 127E-02	7 792E 01	4.127E-02
5.282E 01	2.227E 01	2.227E 01	5.804E 02	43.781E	03 -2.032E	03 -1.749E 03	2.788E 03	5.634E 01	2.984E+02	5.634E 01	2.984E-02
5.332E 01	2.027E 01	2.027E 01	6.3576 02	-3.877E	03 #2.080E	03 #1.798E 03	2.852E 03	5.127E 01	2.716E-02	5.127E 01	2.716E-02
5.407E 01	1.858E 01	1.858E 01				03 #1.870E 03	2.948E 03	4,701E 01	2.490E=02	4.701E 01	2.4905-02
5.483E 01	1.6878 01	1.687E 01				03 -1.940E 03	3.045E 03	4,268E 01	5.201E-05	4.26BE 01	5.56!E=05
5.576E 01 5.625E 01	1.532E 01 1.450E 01	1.532E 01				03 =2.0198 03	3.165E 03	3.875E 01	2,0526-02	3.875E 01	2.0526=02
5.631E 01	7.500E 00	1.441E 01				03 =2. 058E 03	3.209E 03	3.667E 01	1.942E=02 1.005E=02	3,667E 01	1,9425=02
5.645E 01	7.500E 00	1.417E 01				03 -2.073E 03	3,234E 03	1.897E 01	1.005E-02	3,644£ 01 3,585£ 01	1,930E=02 1.899E=02
5.6538 01	1.404E 01	1.404E 01				03 =2.079E 03	3.2456 03	3.552E 01	1.8816-02	3.552E 01	1.881E=02
5.681E 01	1.357E 01	1.357E 01				03 -2.101E 03	3,280£ 03	3.433E 01	1.818E=02	3.433E 01	1.818E=V2
5.703E 01	1.295E 01	1.295E 01	1.066E 03	P4 = 454E	03 m2.346E	03 =2.118E 03	3,309E 03	3,276E 01	1.735E=02	3.276E 01	1.735E-02
5.776E 01	1.095E 01	1.0958 01	1.098E 03	=4.551E	03 #2,376E	03 -2.174E 03	3,402E 03	2.770E 01	1.467E=02	2.770E 01	1.4676=02
5,878E 01	5.775E 00	5.775E 00				03 *2,240E 05	3,532E 03	1.461E 01	7.736E-03	1.461E 01	7.736E+03
6-2215 01	1.646E Q1	1.646E 01	1.1205 03	94.063E	03 -2.458E	03 =2.3658 03	3.790E 03	4.1646 01	2.2056-02		2.2056#02
7 0,2215 01	1.641E 01	. sowie of	TOTERS 03	+ 7 3 C C	A3 45441F	03 *2.461E 03	3.7/25 05	APTOOF OT	E # 1 AGE # 05	4.150E 01	2.198E+U2

	SBAX	PwlB	₽₩OB	PDA	(e u x	n=I4	Ø₩UB	CANALL	P#15/P50	F#18/P10 *	P=Od/PSO	P#UB/P10
15	6,467E 01	1.9128 01	1.912F 01	1.1208 03	-5.210E 03	-2.582E	03 -2.534E 03	4.2696 03	4,6366 01	2.561E+02	4.8_6F 01	2.561E=02
72	6.505E 01	2.060£ 01	1.9548 01	1,1206 03	=5.265E 03	42.600F	03 =2.063E 03	4.5574 05	5.2268 01	2.708E=02	4.941E 01	2.6174#02
Ç.	6.5098 01	5.066F 01	1,958E 01	1.120t 03	-5.208F 03	-2.602E	03 ≈2.666t 03	4.542E 03	5,226E 01	2.768E+02	4.4528 01	2.623E=02
	6.529E 01	1.964E U1	1.980E 01	1.120£ 03	*5.293E 03	-2.611E	03 -2.681E 03	4.3086 03	4.9688 01	2.631E=U2	5.008E 01	2.652L=U7
	6,695E 01	1.116E 01	9.740E 00				03 #2.195E 03	4.5836 63	2.823E 01	1.4951-02	2.464E 01	1.305E+02
	6.162F 01	7.817E 00	9.367E 00	1.480E 03	-5.533E 03	-2.697E	03 -2.837E 03	4.665E 03	1.977E 01	1.047E-02	2.369E 01	1.2558=02
	6.839F 01	3.975E 00	7.123E 00	1.672E 03	-5.604E 03	=2.715E	03 =2.890E 03	4.760E 03	1.005E 01	5.3256=03	1.802E 01	9.542E+03
	6.911F 01	3.447E 00	5.025E 00	1.796E 03	≈5.6/5E 03	-2.72FE	03 -2.948E 03	4.848E 03	8./19E 00	4.6186-03	1.271E 01	h.731E=03
	6.972E 01	3.000E 00	4.137E 00	1.879E 03	-5.734E 03	+2.737E	03 -2.997E 03	4.955F 03	7.588E 00	4.019E=03	1.0461 01	5,542L#03
	7.067E 01	2.177E 00	2.755E 00	1,974E 03	-5.804E 03	-2.747E	03 +3.057E 03	5.036E 03	5.507E 00	2.917L=03	6.968F 00	3.6916-03
	7.110E 01	1.8056 00	2.565E 00				03 -3.078E 03	5.088E 03	4.565E 00	2.4182-03	6.48BE 00	3.436E=03
	7.263E 01	1.4866 00	1.890E 00	2.0986 03	=5.898E 03	-2./61E	03 -3.137E 03	5.273L 03	3.759E 00	1.991E=03	4.780E 00	2.5326-03
	7.278E 01	1.455E 00	1.807E 00				03 -3.142E 03	5,290L U3	3.680E 00	1.9496-03	4.570£ 00	2.420E=03
	7.353E 01	1.437E 00	1.390E 00				03 =3.169E 03	5,374E 03	3.634E 00	1.9256#63	3.516E 00	1.862E=03
	7.3535 01	1.437E 00	1.3886 00				03 +3,169F 03	5.375E 03	3.634E 00	1.925E=03	3.510E 00	1.859E=03
	7.4868 01	1.4058 00	0.000				03 +3.226E 03	5.427E 03	3.554E 00	1.882£=03	0.000	0.000
	7.771E 01	2.725E 00	0.000				03 #3.226E 03	5.525E 03	6.892£ UU	3.650E=03	0.000	0.000
	8.161E 01	1.900E 00	0.000				03 -3.2266 03	5.630E 03	4.B06E 00	2,545£⇒03	0.000	0.000
	8.442E 01	1.530E 00	0.000				03 #3.22¢E 03	5.684E 03	3.870E 00	2.0506#03	0.000	0.000
	8.728F 01	3.410E 00	0.000				03 =3,226E 03	5,707E 03	8,625E 00	4.568£=03	0.000	0.000
	8.728E 01	3.414E 00	0.000	2.469E 03	-6.082E 03	~2.856E	03 +3.226F 03	5.707E 03	8.635E 00	4.573E+03	0.000	0.000

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01010101010101010101010101010101010101	0111.7765EE 00111.	22222222222222222222222222222222222222	20000000000000000000000000000000000000	22222222222222222222222222222222222222
76,079E 01 6,221E 01 6,467E 01	2.116E 01 1.353E 01 2.231E 01	3.890E 02 4.025E 02 4.248E 02	3.275E=03 3.264E=03	3.067E=02 3.069E=02

279

T3LMAR C3	PERFURMANCE
ENGINE BEST CHAVCE	INTEL
CALCULATED THRUST	ANGLE OF ATTACK
REGENERATIVE COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	INLET PROCESS EFFICIENCY - SUPERSONIC, 0.4026 INLET PROCESS EFFICIENCY - SUBSONIC 0.4963 XINETIC ENERGY EFFICIENCY - SUPERSONIC 0.49373 KINETIC ENERGY EFFICIENCY - SUBSONIC 0.6842 ENTHALPY AT PO - SUPERSONIC 46.14 (BTU/LBM) ENTHALPY AT PO - SUBSONIC 31.42 (BTU/LBM)
MARKET AND TORRES	COMBUSTOR
INLET FRICTION DRAG	FUEL-AIR RAYIU
STATIONS	FUEL INJECTORS
NOFINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A 40.400 A 1B 41.292 B 1C 44.300 2A 48.767 C 2C 46.250 E 5A 54.057 3B 56.242 4 40.792

Reading 65

t = 218.03 sec.

8 3 Ţ 41404 GAMPA MOLHT SONY MACH VEL 8 +/4 A/AC IVAC PHI ETAC WINC TUNNEL 1 0 5 0.000 745.999 3054 687.4(813) 1.2920 28.852 2698 0.401 419 =28.5(101) 1.3969 28.651 1005 5.957 5985 1.834 0.10693 26.857 0.9806 5097 9,446 189.6 SPIKE TIP NS 18.012 3054 687.4(813) 1.2918 28.851 2608 0.600 0.600 16.186 2981 665.2(791) 1.2941 28.851 2578 0.409 1055 2.090 0.10693 26.857 0.9806 4946 1.753 184.1 WIND TUNNEL 0.000 745.999 3054 687.4(813) 1.2920 28.852 2608 0.000 0.380 412 -30.0(99) 1.3988 28.851 997 6.009 5992 1.854 0.10303 25.877 0.9806 4914 9.595 189.9 SPIKE TIP NS ш 0 0 18.012 3054 687.4(813) 1.2918 28.851 2608 0.600 0.600 16.335 2987 667.1(793) 1.2940 28.851 2581 0.391 1009 2.090 0.10303 25.877 0.9806 4914 1.616 189.9 INLET THROAT 318,819 2991 668,1(794) 1,2940 28,851 2582 40.400 40.400 15.134 1421 221.6(351) 1.3534 28.851 1820 2.597 4726 1.886 0.94010 26.857 0.1115 4378 69.053 163.0 INLET UPNRSK 318.819 2991 668.1(794) 1.2940 28.851 2582 40.400 40.400 13.016 1365 207.2(337) 1.3567 28.851 1787 2.688 4802 1.886 0.85464 26.857 0.1227 4418 63.784 164.5 INLET DNNKSR 40,400 125,283 2991 668,1(794) 1,2940 28,851 2582 40,400 108.041 2891 638.1(765) 1.2971 28.851 2542 0.482 1225 1.950 0.85464 26.857 0.1227 4418 16.271 164.5 COMBUSTOR 0 8 1 21 40.410 265.692 2945 670.9(819) 1.2967 2/,428 2631 40.410 15.167 1461 228.5(380) 1.3525 27.427 1892 2,486 4705 1.977 0.94382 26.967 0.1116 4377 69.012 162.3 0.14 0.07 COMBUSTOR 2 21 41.292 203.735 2867 673,9(830) 1,3009 26,192 2661 41.292 18.867 1601 279.6(439) 1.3467 26.192 2023 2.195 4442 2.060 0.94941 27.069 0.1113 4275 65.535 157.9 0.27 0.04 COMBUSTOR 0 10 3 21 41,302 213,864 2821 673,8(816) 1,3030 26,146 2644 41,302 18.909 1553 280.0(425) 1.3496 26.145 1997 2.223 4439 2.052 0.94971 27.069 0.1113 4274 65.515 157.9 0.27 0.01 COMBUSTOR 0 11 4 21 41.367 212.673 2814 673.5(814) 1.3034 26,139 2641 41.367 19.181 1557 283.1(426) 1.3495 26.139 1999 2.211 4420 2.051 0.94972 27.069 0.1113 4265 65.233 157.6 0.27 0.00 COMBUSTOP 0 12 41,500 204,757 2824 672,8(817) 1,3028 26,152 2645 41.500 20.873 1614 295.86 443) 1.3465 26.152 2032 2.157 4343 2.055 0.95082 27.069 0.1111 4248 64.179 156.9 0.27 0.01 COMBUSTOR 0 13 42.460 147.854 3104 666.8(903) 1.2897 26,467 2742 42,460 29.559 2128 355.5(594) 1.3224 26.468 2299 1.722 3959 2.103 0.94189 27.069 0.1122 4180 57.447 154.4 0.27 0.25 COMEUSTOR 0 14 44.087 113.469 3734 653.4(1098) 1.2578 27.226 2929 53,102 3102 462.0(917) 1.2776 27.236 2724 1.136 3094 2.157 0.91012 27.069 0.1161 4183 45.763 154.5 0.27 0.80 44.087 COMBUSTOR 0 15 44.310 112.813 3752 651.3(1103) 1.2568 27.255 2933 44.310 54.741 3224 467.6(930) 1.2757 27.265 2739 1.107 3031 2.158 0.90806 27.009 0.1164 4182 42.777 154.5 0.27 0.82 COPBUSTOR 0 16 44,800 111.672 3770 646.0(1109) 1.2556 27.294 2936 44.800 58.342 3293 479.3(952) 1.2729 27.304 2762 1.046 2888 2.159 0.90424 27.069 0.1169 4176 40.587 154.3 0.27 0.85 COMBUSTOR 0 17 10 44.802 111.697 3769 646.0(1108) 1.2556 27.293 2936 44.802 58.340 3292 479.2(951) 1,2729 27.303 2762 1.046 2888 2.159 0.90455 27.069 0.1168 4176 40.604 154.3 0.27 0.85 COMBUSTOR 0 18 11 6 46.250 105.653 3278 653.2(1075) 1.2826 23.682 2971 46,250 56.968 2853 494.5(921) 1.2968 23.683 2787 1.011 2618 2.357 0.86226 27.303 0.1240 4208 37.760 153.7 0.67 0.27

OF POOR QUALITY

GAMMA MULMI SONV MACH VEL S A/AC MOTIF Q IVAL PHI ETAC n/A COMBUSTOR 0 19 12 2 46,260 105,621 3281 653,1(1076) 1,2825 23,685 2972 50.959 2856 494.3(922) 1.2967 25.086 2788 1.011 2819 2.357 0.86163 27.383 0.1241 4209 3/.741 153.7 0.67 0.27 46.260 COMBUSTOR 0 20 13 47,310 102.004 3553 639.6(1171) 1.2686 23.993 3056 47,310 55,964 3121 473,9(10;2) 1,2836 23,998 2881 1,000 2880 2,377 0,80191 27,383 0,1333 4362 35.686 159.3 0.67 0.39 COMBUSTOR 0 21 14 47.327 101.821 3565 639.4(1175) 1.2679 24.006 3060 47.327 56.040 5134 474.0(1017) 1.2830 24.011 2885 0.997 2877 2.378 0.79925 27.383 0.1338 4368 35,730 159.5 0.67 0.39 COMBUSTOR 0 22 15 48.110 98.206 3811 629.9(1261) 1.2545 24.287 3128 48.110 53.929 3365 454.1(1096) 1.2709 24.298 2958 1.002 2966 2.394 0./4727 27.383 0.1431 4500 34.439 164.5 0.67 0.50 COFBUSTOR 0 23 16 48.767 93.092 3482 638.5(1261) 1.2735 21.706 5187 48.767 44.389 2958 420.5(1050) 1.2914 21.710 2958 1.116 3302 2.574 0.69616 27.674 0.1552 4605 35.725 166.4 1.03 0.30 COMBUSTOR 0 24 17 48.777 93.039 3485 638.4(1262) 1.2734 21.708 3188 48.777 44.269 2959 419.7(1050) 1.2914 21.712 2958 1.118 3508 2.574 0.69526 27.674 0.1554 4607 35.741 166.5 1.03 0,30 COMBUSTOR 0 25 18 49.307 90.646 3587 633,2(1301) 1.2680 21.814 3220 49.307 37.879 2966 373.4(1051) 1.2896 21.820 2952 1.221 3606 2.583 0.65024 27.674 0.1662 4714 30.437 170.3 1.03 0.33 COMBUSTOR 0 26 19 50.717 83.341 3892 621,1(1420) 1.2508 22.130 3307 50.717 30.881 3164 307.4(1122) 1.2781 22.147 3013 1.315 3962 2.608 0.55418 27.674 0.1950 4950 34.118 178.9 1.03 0.43 COMBUSTOR 0 27 20 52.817 77.457 4108 605.8(1504) 1.2368 22.378 3360 52,817 22.275 3192 203.4(1128) 1.2733 22.411 3003 1.495 4488 2.624 0.45421 27.674 0.2379 5217 31.676 188.5 1.03 0.50 COMBUSTOR 0 59 51 53.317 77.705 4087 602.6(1495) 1.2381 22.364 3354 53.317 20.082 3100 172.4(1092) 1.2769 22.396 2964 1.565 4639 2.623 0.43565 27.674 0.2480 5266 31.410 190.3 1.03 0.50 COMBUSTOR 0 29 22 54.067 75.842 4137 597.9(1515) 1.2346 22.425 3365 54.067 18.471 3107 146.6(1093) 1.2757 22.463 2962 1.604 4752 2.627 0.41066 27.674 0.2631 5352 30.327 194.7 1.03 0.51 COMBUSTOR 0 30 23 54,827 74.731 4160 593.5(1523) 1.2329 22.458 3369 54,827 16:837 3077 118:8(1080) 1:2763 22:499 2946 1:655 4874 2:629 0:58834 27:674 0:2782 5392 29:414 194:8 1:03 0:52 COMBUSTOR 0 31 24 55,760 73.152 4194 588,6(1537) 1,2303 22.504 3376 55,760 90.2(1072) 1.2762 22.550 2934 1.702 4994 2.631 0.36443 27.674 0.2965 5457 28.283 197.2 1.03 0.54 15.300 3059 COMBUSTOR 0 32 25 56,252 56.772 4621 586.3(1705) 1.1949 22.953 3458 56.252 14.489 3639 100.0(1294) 1.2440 23.100 3121 1.580 4933 2.671 0.29364 27.674 0.3679 5608 22.511 202.7 1.03 0.69 COMBUSTOR 0 33 26 56,307 68,305 4178 586,0(1530) 1.2307 22.495 3371 56.307 10.762 2863 15.6(995) 1.2832 22.541 2847 1.877 5342 2.636 0.29287 27.674 0.3689 5612 24.316 202.8 1.03 0.53 COMBUSTOR 0 34 27 56.447 68.186 4183 585.4(1532) 1.2304 22.501 3372 56:447 10.647 2862 12.1(994) 1.2832 22.548 2846 1.882 5356 2.637 0.29071 27.674 0.3717 8620 24.197 203.1 1.03 0.94 COMBUSTOR 0 35 28 21 56.527 48,957 5138 585,0(1912) 1,1491 23,490 3535 56,527 14.036 4431 84.7(1604) 1.1666 23.979 3274 1.528 5004 2.692 0.29402 27.674 0.3675 5625 22.864 203.3 1.03 1.00 COMBUSTOR 0 36 29 21 49.046 5137 583.6(1911) 1.1491 23.492 3535 56,807 56.807 15.575 4410 70.7(1595) 1.1676 23.991 3267 1.551 5067 2.691 0.29315 27.674 0.3686 5640 23.085 201.8 1.00 NO COMBUSTOR 0 37 30 21 ∞ 57.03₃ 48.883 5136 582.9(1911) 1.1491 23.493 3534 ω 57.033 12.951 4383 54.0(1583) 1.1668 24.005 3257 1.579 5144 2.691 0.29245 27.674 0.3695 5650 23.380 204.2 1.03 1.00

T GAMMA MOLKT SÖNY MACH VEL S A MIMUH DAVA 4/4 IVAC PHI ETAC NO COMBUSTOR 0 38 31 21 CC 57.757 47,358 5128 579,911908) 1,1490 23,493 3531 57.757 10.950 4299 2.9(1547) 1.1726 24.044 3228 1.664 5374 2.693 0.28791 2/.674 0.3/53 5674 24.043 205.0 1.03 1.00 COMBUSTOR 0 39 32 21 58.777 37.663 5095 576.5(1894) 1.1471 23.465 3519 6.000 4067 m126.4(1449) 1.1831 24.126 3149 1.883 5931 2.712 0.28697 27.674 0.3777 5662 26.367 205.3 1.03 1.00 58.777 COMEUSTOR 0 40 33 21 60.787 51.426 5130 570.6(1908) 1.1500 23.517 3532 60.787 10.050 4406 103.1(1619) 1.1663 23.970 3267 1.4/1 4637 2.685 0.29603 27.674 0.3650 5661 22.251 204.5 1.03 1.00 COMBUSTOR 0 41 34 21 62.207 52.338 5128 566.3(1907) 1.1503 23.525 3531 98.7(1616) 1.1669 23.975 3286 1.472 4837 2.682 0.30405 27.674 0.3555 5645 22.856 204.0 1.03 1.00 62.207 16.312 4461 COMBUSTOR U 42 35 21 64.671 49.639 5112 557.4(1900) 1.1502 23.530 3525 64.671 19.102 4569 170.2(1663) 1.1623 23.910 3323 1.325 4401 2.685 0.28621 27.674 0.3749 5620 14.715 203.1 1.03 1.00 0 43 36 200 COMBUSTOR 65.047 46.079 5101 555,8(1895) 1.1496 23.522 3520 65.047 20.133 4634 217.8(1691) 1,1593 23.860 3346 1.229 4112 2.691 0.26794 27.674 0.4032 5616 17.123 203.0 1.03 1.00 COMBUSTOR REGEN 44 37 3 46.079 5187 645.9(1935) 1.1467 23.399 3555 65.047 65.047 19-112 4700 277-5(1721) 1-1548 23-783 3369 1-271 4282 2-708 0-26794 27-674 0-4032 5657 17-830 204-4 1-03 1-00 NOZZLE AE 45 38 87.283 46.079 5101 555.8(1846) 1.1496 23.522 3520 87.283 1.369 2967 -627.8(1004) 1.2632 24.271 2771 2.778 7696 2.691 0.05578 27.674 1.9371 7299 0.671 263.7 1.03 1.00 NOZZLE PU 46 39 87.283 46.079 5101 555.8(1846) 1.1496 23.522 3520 87.283 0.401 2279 -890.5(741) 1.2844 24.272 2448 3.475 8507 2.691 0.02550 27.6/4 4.5974 7759 3.107 281.5 1.03 1.00 NOZZLE AE REGEN 47 40 87.283 46,079 5187 643.9(1935) 1.1467 23,399 3555 87.283 1:426 3124 ~565,8(1065) 1,2574 24,269 2837 2,742 7760 2,708 0,05578 27,674 1,9371 7399 6,743 267,4 1,03 1,00 NOZZLE PO REGEN 48 41 5 46.079 5187 643.9(1935) 1.1467 23.399 3555 87.283 87.283 0.401 2386 -850.5(781) 1.2807 24.272 2502 3.457 8648 2.706 0.02281 27.674 4.7359 7924 3.066 286.3 1.03 1.00 FICTIVE COMBUSTR 68 61 65.047 318,819 5330 555,8(1988) 1,1669 23,769 3607 65 047 0.401 1454-1188.1(444) 1.3254 24.272 1973 4.734 9342 2.528 0.04100 27.674 2.6352 6305 5.952 300.1 1.03 1.00 FICTIVE NOZZLE 69 62 87.283 29.703.5020 531.3(1861) 1.1467 23,496 3490 87.283 1.678 3348 =473.5(1155) 1.2445 24.262 2922 2.427 7091 2.723 0.05578 27.674 1.9371 6931 6,146 250.5 1.03 1.00

1,496 01 1,476 02 03 03 03 03 03 03 03	XABS	P=18	P=0s	PDA	QUX	L = 1 B	e ≈ D €	CAMALL	P=IH/PSU	010.4016	P#08/PS0	L-(.0.4016
1.0760 01 1.0700 00 0.000				-		b=18 0-000				P=18/P10		F=08/P10
\$1.000 0 1, 1.000 0 1,	-							, ,				
5.5186 01 3,9926 07 0,000			•									
3.5186 01 3.9186 03 5.9086 03 4.7256 02 0.0000 0.0000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00								•				
3.595 0 3.4960 0 5.876 0 0 -4.326 0 2 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.	· .			•				- · · · · · · · · · · · · · · · · · · ·				
3.5986 01 3.7986 00 3.7936 0 4.4350 02 -3.2276 0 0 0.2776 0 0 0.2776 0 0 0.000												
3.59.66 01 3.90.66 00 3.00.66 00 4.2756 00 -4.5356 02 -3.1036 02 -3.1036 02 0.00.00 7.5556 02 9.0325 00 5.20.60.00 3.00.60.03 3.00.60 01 4.2035 00 4.7035 00 -4.6356 02 -3.20.60 02 -3.20.60 02 0.00.00 6.10.00 0 5.10.00 01 5.6356 03 1.00.60 01 9.00.00 1.00	3.5556 01	4.010E 00										
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3.736 01 4.6976 00 5.0026 00 5.1026 02 -3.0956 02 -3.0956 02 -3.0026 01 9.0026 02 1.0226 01 5.4026 03 3.0036 01 1.97076 02 3.0036 01 1.5006 01 -5.2026 02 -3.0946 02 1.0226 01 1.0226 01 5.4026 03 3.0946 01 1.97076 02 3.0956 02 -3.0946 02 1.0226 01	3,648E 01	4,203E 00	4.745E 0	9.823€ 02	#3.249E 02	=3.299E 0	00000	8,169E 02	1.049E 01	5.634E=03	1.184E 01	6.361E=03
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3.635 01 5,3816 00 1.576 01 -5,286 02 -4,026 02 -3,096 02 -3,096 01 1.055 03 1.3016 01 7.215 03 3,016 01 2.105 03 3.675 01 7.215 03 3.586 03 3.355 01 2.006 02 3.6875 01 7.7345 00 1.5376 01 -5,286 02 -4,2246 02 -3,805 02 -4,360 01 1.0516 03 1.930 01 1.0576 02 3.6246 01 2.056 02 3.695 03 1.536 01 1.536 01 1.50												
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3,9010 01 8,7500 00 1,5000 01 5,000 01 5,2880 02 -4,3600 02 -3,031 02 -4,710 01 1,0920 03 2,1880 01 1,1715 02 3,8940 01 2,14850 02 1,3315 01 1,0020 01 1,3075 03 1,4015 01 1,3010 03 3,4015 01 1,3010 03 3,4015 01 1,3010 03 3,4015 01 1,2405 02 4,4000 02 1,7715 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 02 -5,0020 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 02 -5,0020 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 02 -5,0020 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 01 1,7715 01 0,7205 00 -5,6146 02 -4,0020 02 -4,0020 01 1,205 03 8,0020 01 1,205 03 8,0020 01 1,7715 01 0,7020 02 -5,0020 01 1,205 03 8,0020 0												
3.935 01 1.337E 01 1.692E 01 -5.348E 02 -4.546E 02 -3.00E 02 -5.221E 01 1.310E 03 3.40E 01 1.595E-02 3.397E 01 1.309E-02 3.95E 01 1.595E 01 1.595E-02 3.95E 01 1.595E 01 1.595E-02 3.95E 01 1.595E 01 1.595E-02 3.95E 01 1.595E 01 1		,									· · · · · · · ·	
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4,006 01 1,772E 01 9,028E 00 -5,746E 02 -4,746E 02 -4,301E 02 -6,226E 01 1,206E 03 5,298E 01 2,235E-02 2,250E 01 1,210E-02 4,041E 01 2,131E 01 9,028E 00 -6,049E 02 -8,198E 02 -4,508E 02 -4,508E 02 -4,508E 02 1,258E-02 2,258E 01 2,210E-02 4,041E 01 2,131E 01 9,028E 00 -6,049E 02 -8,202E 02 -4,508E 02 1,258E 03 7,246E 01 3,848E-02 2,258E 01 1,210E-02 4,131E 01 2,949E 01 8,091E 00 -6,049E 02 -8,0												
# 4,001E 01 2:131E 01 9,028E 00 +0.02E 02 =5:199E 02 -4:500E 02 =5:090E 01 1.255E 03 5.295E 01 2:858E-02 2:252E 01 1:210E-02 4:192E 01 2:910E 01 9,028E 00 +0.091E 02 =5:022E 02 =4:509E 01 1.08E 03 7.246E 01 3.893E-02 2:150E 01 1:66E-02 4:130E 01 2:913E 01 8:091E 02 =6:091E 02 =5:000E 02 =1:002E 02 1:501E 03 7.246E 01 3.893E-02 2:150E 01 1:66E-02 4:130E 01 2:913E 01 8:091E 02 =6:091E 02 =5:000E 02 =1:002E 02 1:501E 03 7.246E 01 3.893E-02 2:150E 01 1:66E-02 4:150E 01 3.080E 01 1:08E 01 7:171E 02 =6:377E 02 =5:131E 03 7.410E 01 3.881E-02 2:150E 01 1:66E-02 4:150E 01 3.080E 01 1:08E 01 7:171E 02 =6:377E 02 =5:131E 02 1:30EE 03 7.410E 01 3.881E-02 2:150E 01 1:66E-02 4:26E 01 3.080E 01 7:530E 02 =6:050E 02 =5:631E 02 2:1501E 03 8.047E 01 4:371E 02 2:150E 01 1:62E-02 4:400E 01 5:235E 01 2:687E 01 7:530E 02 =5:631E 02 =2:02E 02 1:501E 03 8.047E 01 4:325E-02 6:700E 01 3.640E 02 1:501E 03 8.047E 01 4:325E-02 6:700E 01 3.640E 02 7:350E-02 4:400E 01 5:235E 01 7:350E 02 1:22E 03 7:350E-02 4:400E 01 5:235E 01 7:350E 02 1:22E 03 7:350E-02 4:400E 01 5:235E 01 7:350E 02 1:22E 03 7:350E-02 4:400E 01 5:235E 01 7:350E 02 1:22E 03 7:350E-02 4:400E 01 5:568E 01 7:350E 02 1:22E 03 7:350E-02 4:400E 01 5:568E 01 7:300E 02 1:350E 02 1:501E 03 1:350E 02 7:350E-02 4:400E 01 5:400E 01 5:568E 01 7:290E 02 1:350E 03 1:350E 02 1:750E 03												
# 4,09E 01 2,131E 01 9,025E 00 = 6,09E 02 *5,202E 02 = 4,509E 02 = 6,09E 02 1,257E 03 5,317E 01 2,555E 02 2,252E 01 1,210E 02 4,130E 01 2,904E 01 1,656=02 4,130E 01 2,904E 01 1,656=02 4,130E 01 2,904E 01 1,656=02 4,130E 01 2,904E 01 1,656=02 4,130E 01 2,907E 01 1,656=02 4,130E 01 2,907E 01 1,656=02 4,130E 01 2,907E 01 1,656=02 4,130E 01 2,907E 01 1,656=02 4,130E 01 2,907E 01 1,656=02 4,130E 01 3,086E 01 1,086E 01 7,117E 02 6,377E 02 5,130E 02 1,140E 02 3,31E 03 7,40E 01 3,50E=02 2,165E 01 1,65E=02 4,246E 01 3,228E 01 1,230E 02 1,230E 02 8,506E 02 5,50E 02												
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4.15E 01 3,08E 01 1.08E 01075E 02 -0.191E 02 -0.191E 02 -1.140E 02 1.316E 03 7.41UE 01 3.88E-U2 2.105E 01 1.162E-U2 4.26E 01 3.08E 01 1.08E 01 -1.17E 02 -0.37TE 02 -0.134E 02 -2.20E 02 1.50E 03 8.44TE 01 4.325.02 6.704E 01 3.649E.02 4.40E 01 5.22E 01 5.36E 01 5.36E 01 7.34E 02 -0.06E 02 -5.63E 02 -2.20E 02 1.50E 03 8.44TE 01 4.325.02 6.704E 01 3.649E.02 4.40E 01 5.22E 01 5.36E 01 7.34E 02 -1.22E 03 -7.61E 02 -4.25E 02 1.72E 03 1.30E 02 7.371E.02 1.36E 02 7.33E.02 4.40E 01 5.22E 01 5.36E 01 7.34E 02 -1.22E 03 -7.92E 02 -4.25E 02 1.72E 03 1.37E 02 7.371E.02 1.36E 02 7.36E.02 4.40E 01 6.10E 01 5.56E 01 -7.28E 02 -1.56E 03 -7.92E 02 -4.25E 02 1.72E 03 1.37E 02 7.371E.02 1.36E 02 7.36E.02 4.40E 01 6.10E 01 5.56E 01 -7.28E 02 -1.56E 03 -7.92E 02 -4.68E 02 1.78E 03 1.52E 02 8.17F.02 1.38F 02 7.403E.02 4.40E 01 6.10E 01 5.56E 01 -7.28E 02 -1.56E 03 -7.68E 02 -1.78E 03 1.52E 02 8.17F.02 1.38F 02 7.403E.02 4.62E 01 5.47EE 01 5.49EE 01 -6.23E 02 -1.56E 03 -1.65E 03 1.52E 02 8.17F.02 1.38F 02 7.403E.02 4.62E 01 5.47EE 01 5.49EE 01 -6.23E 02 -1.56E 03 -1.65E 02 1.76E 02 1.78E 03 1.52E 02 8.17F.02 1.38F 02 7.403E.02 4.62E 01 5.47EE 01 5.49EE 01 5.49EE 01 -6.23E 02 -1.56E 03 -1.65E 03 -7.68E 02 1.78E 03 1.56E 03 7.33E.02 8.17F.02 1.38F 02 7.403E.02 4.62E 01 5.47EE 01 5.56E 01 5.47EE 01 5.56E 03 5.47EE 01 5.	4.130E 01		8,691E 0	-6.901E 02	■6.104E 02	0 3510 2	2 -1 092E 02					
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4.449E 01		3,225E 01	2.687E 0	€ 50 30£ 02 ·	□8.036E 02	=5.634E 0	20 3202 02					
4.486			5.396E 0	1 -7.344E 02	#1,165E 03	-7.612E 0	2 44.J38E 02	1.698E 03	1.304E 02		1.3466 02	7.2334=02
4.486E 01 5.478E 01 5.918E 01 -6.286E 02 -1.368E 03 -8.696E 02 -1.768E 02 1.768E 03 1.522E 02 8.178E 02 7.483E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 7.493E 02 1.366E 02 7.337E 00 1.366E 02 7.337E 02 1.308E 02 7.								1.125E 03		7.371E=02	1.360E 02	7.305E+V2
4.625E 01 5.478E 01 5.498E 01 6.284E 02 -1.851E 03 -1.083E 03 -7.02E 02 1.964E 02 7.337E-02 1.477E 02 7.932E-02 4.731E 01 5.032E 01 6.173E 01 -4.577E 02 -2.245E 03 -1.233E 03 -7.702E 02 2.095E 03 1.253E 02 6.747E-02 1.540E 02 8.272E-02 4.733E-01 5.033E 01 6.173E 01 -4.577E 02 -2.245E 03 -1.233E 03 -9.981E 02 2.095E 03 1.253E 02 6.747E-02 1.540E 02 8.272E-02 4.733E-01 5.033E 01 6.173E 01 -4.509E 02 -2.245E 03 -1.233E 03 -9.981E 02 2.095E 03 1.253E 02 6.747E-02 1.540E 02 8.272E-02 4.817E-03 1.350E 01 6.173E 01 -4.509E 02 -2.245E 03 -1.233E 03 -9.981E 02 2.095E 03 1.253E 02 6.747E-02 1.540E 02 8.272E-02 4.817E-03 1.500E 02 -2.490E 03 -1.418E 03 -1.267E 03 2.194E 03 1.356E 02 6.747E-02 1.540E 02 7.012E-02 4.817E-03 1.500E 02 1.500E 02 7.012E-02 4.817E-03 1.500E 03 1.356E 02 7.012E-02 4.817E-03 1.500E 03 1.500E 03 1.500E 02 1.500E 02 7.012E-02 4.817E-03 1.500E 03 1.500												
4.731E 01 5.033E 01 0.175E 01 0.4.577E 02 0.2.265E 03 0.2.23E 03 0.995E 02 1.946E 03 1.366E 02 7.337E=02 1.540E 02 8.272E=02 4.733E 01 5.033E 01 0.4.577E 02 0.2.265E 03 0.2.23E 03 0.995E 02 2.995E 03 1.253E 02 6.737E=02 1.540E 02 8.272E=02 4.811E 01 5.033E 01 0.4.577E 02 0.2.265E 03 0.2.23E 03 0.995E 03 1.256E 02 6.737E=02 1.540E 02 3.75E=02 4.877E=02 4.												7. 7. 7. 7. 2
4.731E 01 5.02E 01 6.171E 01 -4.577E 02 =2.25E 03 =1.23E 03 =9.94E 02 2.097E 03 1.25E 02 6.73EE02 1.540E 02 8.272E-02 4.811E 01 5.033E 01 6.175E 01 =4.507E 02 =2.251E 03 =1.23E 03 =9.94E 02 2.097E 03 1.256E 02 7.446E-02 1.541E 02 8.272E-02 4.877E-01 4.439E 03 4.208E 03 4.208E												
4.733E 01 5.033E 01 6.175E 01 =4.509E 02 =2.231E 03 =1.233E 03 =9.981E 02 2.097E 03 1.258E 02 7.446E=02 1.303E 02 7.012E=02 4.811E 01 5.555E 01 5.231F 01 =3.088E 02 =2.490E 03 =1.438E 03 =1.54E 03 2.277E 03 1.308E 02 7.446E=02 1.303E 02 7.012E=02 4.878E 01 4.439E 01 =1.579E 02 =2.688E 03 =1.420E 03 =1.267E 03 2.277E 03 1.108E 02 5.934E=02 1.108E 02 5.934E=02 4.931E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 3.788E 01 2.097E 02 =3.688E 03 =1.420E 03 =1.528E 03 2.278E 03 1.108E 02 5.934E=02 5.078E=02 5.072E 02 5.072E=02 5.072E=02 5.073E=02 5.072E=02 5.		' ' ' - ' - ' - ' - ' - ' -										,
4.811E 01 5.555E 01 4.439E 01 4.439E 01 4.439E 01 4.439E 02 22.666E 03 41.436E 03 41.54E 03 2.77E 03 1.108E 02 5.950E=02 1.108E 02 5.950E=02 4.439E 01 4.439E 01 4.439E 01 4.439E 01 4.439E 01 4.439E 01 4.439E 01 4.439E 01 4.439E 01 4.439E 01 4.439E 01 4.443E 01 4.439E 01 4.439E 01 5.786E 02 3.169E 03 4.269E 03 2.786E 03 2.786E 03 2.786E 03 3.786E 01 3.786E 01 3.786E 01 3.786E 01 3.786E 01 4.443E 01 4.443E 03 41.446E												
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4.931E 01 3.788E 01 3.888E 01 4.443E 01 =2.831E 03 =1.483E 03 =1.347E 03 2.344E 03 7.706E 01 4.140E=02 7.706E 01 4.140E=02 7.706E 01 3.088E 01 2.097E 02 =3.107E 03 =1.480E 03 =1.528E 03 7.706E 01 4.140E=02 7.706E=02 7.706E 01 4.140E=02 7.706E=02 7.706E 01 4.140E=02 7.706E=02								•				
5.072E 01 3.088E 01 3.088E 01 2.07E 02 #3.107E 03 #1.640E 03 #1.528E 03 7.706E 01 4.140E=02 7.706E 01 4.140E=02 5.02E 01 2.27E 01 2.27E 01 2.08E 02 #3.589E 03 #1.840E 03 #1.749E 03 2.788E 03 5.558E 01 2.986E=02 5.558E 01 2.986E=02 5.558E 01 2.986E=02 5.558E 01 2.986E=02 5.558E 01 2.986E=02 5.01E=02 5.01E=02												T. F. C. C.
5.282E 01	5.072E 01	3.088E 01										
5.432E 01 2.008E 01 2.008E 01 1.847E 01 5.574E 02 *3.678E 03 *1.882E 03 *1.776E 03 2.852E 03 2.948E 03 4.609E 01 2.476E=02 4.609E 01 2.476E=02 5.601E 01 2.692E=02 5.407E 01 1.847E 01 1.847E 01 1.847E 01 1.847E 01 1.847E 01 1.847E 01 1.847E 01 1.840E 03 *1.941E 03 *1.940E 03 2.948E 03 4.609E 01 2.476E=02 4.609E 01 2.476E=02 5.576E 01 1.530E 01 1.530E 01 7.756E 02 *3.005E 03 *2.056E 03 3.045E 03	5.282E 01	2,227E 01	2.227E U									
5.407E 01 1.847E 01 1.847E 01 6.320E 02 =3.807E 03 =1.941E 03 =1.866E 03 2.948E 03 4.009E 01 2.476E=02 4.009E 01 2.476E=02 5.483E 01 1.684E 01 1.684E 01 1.684E 01 1.684E 01 1.684E 01 1.684E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.530E 01 1.449E 01 1.530E 01 1.449E 01 1.449E 01 1.449E 01 1.449E 01 1.449E 01 1.440E 01 1.4			2.008E 7	5,574E 02	⇒3.6/8€ 03	-1.882E 0	3 #1.796E 03				- · · · · · · · · · · · · · · · · · · ·	
5.483E 01 1.684E 01 1.684E 01 1.684E 01 7.005E 02 =3.928E 03 =1.995E 03 =1.935E 03 3.045E 03 4.201E 01 2.257E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 2.051E=02 3.818E 01 1.942E=02 3.818E 01 1.942E=02 3.818E 01 1.942E=02 3.818E 01 1.942E=02 3.818E 01 1.942E=02 3.818E 01 1.942E=02 3.818E 01 1.942E=02 3.818E 01 1.942E=02 3.818E 01 1.942E=02 3.818E 01 1.882E=02 3.818E 01 1.882E=02 3.818E 01 1.882E=02 3.818E 01 1.820E=02 3.818E 01 1.8			1.847€ 0	6.320E 02	-3.807E 03	=1.941E Q	3 -1,866E 03	2.94BE 03	4.609E 01		4.609E 01	2.476E=02
5.625E 01 1.449E 01 1.449E 01 9.303E 02 =4.150E 03 =2.082E 03 =2.047E 03 3.616E 01 1.942E=02 3.616E 01 1.942E=02 5.631E 01 7.125E 00 1.440E 01 9.344E 02 =4.136F 03 =2.085E 03 =2.051E 03 3.216E 03 1.778E 01 9.551E=03 3.535E 01 1.899E=02 5.645E 01 7.125E 00 1.417F 01 9.437E 02 =4.154E 03 =2.092E 03 =2.062E 03 3.234E 03 1.778E 01 9.551E=03 3.535E 01 1.899E=02 5.653E 01 1.404E 01 1.404E 01 9.493E 02 =4.163E 03 =2.092E 03 =2.062E 03 3.245E 03 3.503E 01 1.882E=02 3.503E 01 1.882E=02 5.681F 01 1.357E 01 1.357E 01 9.674E 02 =4.163E 03 =2.108E 03 =2.062E 03 3.280E 03 3.387E 01 1.820E=02 3.387E 01 1.820E=02 5.773E 01 1.295E 01 1.295E 01 9.803E 02 =4.225E 03 =2.117E 03 =2.106E 03 3.309E 03 3.232E 01 1.736E=02 3.232E 01 1.736E=02 5.773E 01 1.095E 01 1.095E 01 1.013E 03 =4.205E 03 =2.117E 03 =2.160E 03 3.402E 03 3.232E 01 1.736E=02 2.732E 01 1.408E=02 5.878E 01 6.000E 00 6.000E 00 1.032E 03 =4.400E 03 =2.224E 03 3.599E 03 1.497E 01 4.608E=02 2.732E 01 1.408E=02 6.079E 01 1.605E 01 1.605E 01 1.035E 03 =4.400E 03 =2.224E 03 3.5790E 03 4.005E 01 2.151E=02 4.005F 01 2.151E=02								3.045E 03	4.201E 01		4.201F 01	2.257E=02
5.631E 01 7.125E 00 1.440E 01 9.344E 02 -4.136F 03 =2.05E 03 3.05E 03 1.778E 01 9.551E=03 3.535E 01 1.899E=02 5.645E 01 7.125E 00 1.417F 01 9.437E 02 =4.154E 03 =2.072E 03 =2.062E 03 3.234E 03 1.778E 01 9.551E=03 3.535E 01 1.899E=02 5.653E 01 1.404E 01 1.404E 01 9.493E 02 =4.154E 03 =2.062E 03 3.245E 03 3.503E 01 1.862E=02 3.503E 01 1.882E=02 5.681F 01 1.357E 01 1.357E 01 1.357E 01 9.674E 02 =4.197E 03 =2.108E 03 =2.068E 03 3.280E 03 3.387E 01 1.820E=02 3.387E 01 1.820E=02 5.703E 01 1.295E 01 1.295E 01 1.295E 01 9.803E 02 =4.225E 03 =2.108E 03 =2.106E 03 3.309E 03 3.232E 01 1.736E=02 3.232E 01 1.736E=02 5.776E 01 1.095E 01 1.095E 01 1.013E 03 =4.305E 03 =2.145F 03 =2.160E 03 3.402E 03 3.232E 01 1.408E=02 2.732E 01 1.408E=02 3.678E 01 6.000E 00 6.000E 00 1.032E 03 =4.400E 03 =2.145F 03 =2.160E 03 3.552E 03 1.497E 01 4.603E=03 1.497E 01 8.043E=03 6.079E 01 1.605E 01 1.605E 01 1.035E 03 =4.502E 03 =2.344E 03 3.790E 03 4.005E 01 2.151E=02 4.005F 01 2.151E=02	· · · · · · ·										3.818E 01	2.051E=U2
5.645E 01 7.125E 00 1.417F 01 9.437E 02 *4.154E 03 *2.092E 03 *2.068E 03 3.234E 03 1.778E 01 9.551E=03 3.535E 01 1.899E=02 5.653E 01 1.404E 01 1.404E 01 9.493E 02 *4.103E 03 *2.098E 03 *2.068E 03 3.245E 03 3.503E 01 1.862E=02 3.503E 01 1.882E=02 5.681F 01 1.357E 01 1.408E=02 3.232E 01 1.736E=02 3.232E 01 1.736E=02 3.232E 01 1.736E=02 3.232E 01 1.736E=02 3.232E 01 1.408E=02 5.678E 01 6.000E 00 6.000E 00 1.032E 03 *4.400F 03 *2.176E 03 *2.244E 03 3.502E 03 1.497E 01 1.408E=02 1.497E 01 1.408E=02 6.079E 01 1.605E 01 1.605E 01 1.035E 03 *4.400F 03 *2.344E 03 3.790E 03 4.005F 01 2.151E=02 4.005F 01 2.151E=02												
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5.681f 01 1.3576 01 1.3576 01 9.6746 02 =4.1976 03 =2.1086 03 =2.0896 03 3.2806 03 3.3876 01 1.8206=02 3.3876 01 1.8206=02 3.287036 01 1.2956 01 1.2956 01 9.8036 02 =4.2256 03 =2.1176 03 =2.1086 03 3.3096 03 3.2326 01 1.7366=02 3.2326 01 1.7366=02 3.2326 01 1.7366=02 3.2326 01 1.7366=02 3.2326 01 1.7366=02 3.2326 01 1.7366=02 3.2326 01 1.7366=02 3.2326 01 1.46086=02 3.2326 01 1.4006=02 2.7326 01 1.4006=02 2.7326 01 1.4006=02 2.7326 01 1.4006=02 3.2326 01 1.4006=02 2.7326 01 1.4006=02 3.2326 01 1.4006=02 2.7326 01 1.4006=02 3.2326 01 1.4006=02 2.7326 01 1.4006=02 3.2326 01 1.4006=02 2.7326 01 1.4006=	_ · _ - _ ·									•		
5.703E 01 1.295E 01 1.295E 01 9.803E 02 =4.223E 03 =2.117E 03 =2.106E 03 3.309E 03 3.232E 01 1.736E=02 3.232E 01 1.736E=02 5.776E 01 1.095E 01 1.095E 01 1.013E 03 =4.305E 03 =2.149F 03 =2.160E 03 3.402E 03 2.732E 01 1.466E=02 2.732E 01 1.468E=02 5.878E 01 6.000E 00 6.000E 00 1.032E 03 =4.400F 03 =2.176E 03 =2.224E 03 3.552E 03 1.497E 01 8.043E=03 1.497E 01 8.043E=03 6.079E 01 1.605E 01 1.035E 03 =4.502E 03 =2.218E 03 =2.344E 03 3.790E 03 4.005E 01 2.151E=02 4.005F 01 2.151E=02												
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6-079E 01 1.605E 01 1.605E 01 1.035E 03 -4.502E 03 -2.218E 03 -2.344E 03 3.790E 03 4.005E 01 2.151E-02 4.005F 01 2.151E-02												
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XABS	P=18	P#0B	AMS	ФUХ	u⇔IB	₩OB	CAMALL	P-IU/FSU	P-18/PT0	P#Ub/FS0	P=08/P10
0 6.467E 01	1.910E 01	1.910E 01	1.035E 03	-4.929F 03	-2.327E 0	3 -2.6031 03	4.2098 03	4.767F 01	2.501t=02	4.747E 01	2.501E=Ú2
9 6.505E 01	2.074E 01	1.953E 01	1.035t u3	-4.975E 03	-2.342E 0	3 -2.631E 03	4.337E 03	5.175E 01	2.760E=02	4.875E 01	7.618E=U2
6.509F 01	2.074E 01	1.957F 01	1.0358 03	#4.9/7E 03	-2.544E 0	3 -2.634E 03	4.342E 03	5.175E 01	2.780b=02	4.884E 01	2.6246=02
6.529E 01	1.909E U1	1.480E 01	1.035E 03	=5.00UE 05	-2.352L U	3 -2.644E 03	4.36BE 03	4,9136 01	2.639t#02	4.941E 01	2.6546+02
6.695E 01	1.098E 01	9.660E 00	1.201E 03	*5.163E 03	-2.408E 0	3 -2.755E 03	4.583E 03	2.740E 01	1.472L=02	2.410F 01	1.2958-02
6.762E 01	7.678E 00	9.307E 00	1.392E 03	-5.217E 03	-2.425E 0	3 =2.793E 03	0.665E 03	1.916E 01	1.0298-02	2.323E 01	1.24BE=U2
6.839E 01	3.885E 00	7.105E 00	1.582E 03	-5.2/9E 03	-2.440E 0	3 -2.839E 03	4.760£ 03	9.694E 00	5.208E=03	1.773E 01	9.5246-03
6.911E 01	3.460E 00	5.045E 00	1.705E 03	₩5.342E 03	₩2.451E 0	3 #2.890E 03	4.8486 03	8.634E 00	4.638E=03	1.259E 01	6.763E=03
6.972E 01	3.100E 00	4.095E 00	1.789E 03	-5.392E 03	-2.459E 0	3 =2.935E 03	4.4528 03	1.735E 00	4.155E=03	1.022E 01	5.489E+03
7.067E 01	2.126E 00	2.61BE 00	1.883E U3	-5.449E 03	#2.467E 0	3 -2.981E 03	5.036E 03	5,305E 00	2.8506-03	6.525E 00	3.505E=03
7.110E 01		00 3054.5				3 -2.998E 03	5.088E 03	4.205E 00	2.2591-03	6.054E 00	3.252E=03
7.263E 01	1.485E 00	1.755E 00	2.001E 03	-5.524E 03	₩2.480E 0	3 -3.044E 03	5.273E 03	3.705E 00	1.9908=03	4.379E 00	2.3536=03
7.278E 01	1.465E UO	1.719E 00	2:008E 03	-5.529E 03	-2.480E 0	3 -3.048E 03	5.290t 03	3.656E 00	1.9646#03	4.290E 00	2.305E+03
7.353E 01	1.633E 00	1.540E 00	2.062E 03	-5.555E 03	-2.484E 0	3 -3.071E 03	5.374E 03	4.074E 00	2.1896-03	3.843E 00	2.064E=03
7,353E 01		1.539E 00				3 -3.071E 03	5.375E U3	4.076E 00	2.1906-03	3.840E 00	2.0636-03
7.486E 01	1.930E 00	0.000	2.103E 03	-5.607E 03	#2.490E 0	3 =3.117E 03	5.427E 03	4 816E 00	2.5876#03	0.000	0.000
7,771E 01	2.730E 00	0.000				3 =3.117E 03	5.525E 03	6.812E 00	3.660E=03	0.000	0.000
8.161E 01	2.125E 00	0.000	2.300E 03	-5.628E 03	#2.511E 0	3 =3.117E 03	5.630E 03	5.303E 00	2.849E=03	0.000	0.000
8.442E 01	1.570E 00	0.000				3 =3.117£ 03	5.684E 03	3.918E 0u	2.105E=03	0.000	0.000
8.728E 01	3.465E UO	0.000				3 -3.117E 03	5.707E 03	8.646E 00	4.645E=03	0.000	0.000
8.728E 01	3.469E 00	0.000				3 -3.117E 03	5.707E 03	8.656E 00	4.650E#03	0.000	0.000

x	DORAG	CURAG	CF	нс
01101111111111111111111111111111111111	001 1000 001 1000 001 1000 001 1000 001 000 001 000 001 000 001 00	22222222222222222222222222222222222222	22222233333333333333333333333333333333	22222222222222222222222222222222222222
6.695E 01 6.762E 01 6.839E 01	1.283E 01 4.605E 00 4.747E 00	4.491E 02 4.437E 02 4.484F 02	3.377E=03 3.361E=03 3.315E=03	2.304E=02 2.044E=02 1.530E=02
7.263E 01 7.278E 01 7.353E 01 7.353E 01 7.486E 01 7.771E 01 8.442E 01 8.728E 01	4.573E 00 3.944E=01 1.921E 00 3.675E>03 1.250E 00 2.779E 00 5.033E 00 1.331E 00 0.466E=01	4.671E 022 4.671E 022 4.671E 022 4.671E 022 4.671E 022 4.742F 022 4.752E 022 4.752E 022	3-129E=03 3-121E=03 3-121E=03 3-139E=03 3-170E=03 3-117E=03 3-063E=03 3-166E=03	0.1935=03 0.195=03 0.004E=03 0.004E=03 7.042E=03 7.402E=03 5.920E=03 1.008E=02

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RAMJET PERFORMANCE

N		RAPUFI PERFO	1 PERFURGACE						
288	ENGINE PERFORMANCE			INLET					
	MEASURED SPECIFIC IMPULSE. 1995.	• •	MASS FLOW RATIO ADDITIVE DRAG COLFILIPITING PRESSUPE I	e	. 0.9806 . 0.0009 . 0.1656				
	CALCULATED THRUST COEFFICIENT		TOTAL PRESSURE RECI TOTAL PRESSURE RECI INLET PROCESS EFFI	CVERY = SUPERSCRIC DVERY = SUBSORIC CIENCY = SUPERSORIC CIENCY = SUPERSORIC	. 0.4274 . 0.1679 . 0.7025	(F8I)			
	CALCULATED			ICIENCY - SUPERSUNIC.					
	STREAM THRUST 7026.	(LBF)		ICIENCY - SUBSCRIC					
	NET THRUST	(LBF=8EC/LBM)		UPERSONIC					
	MOMENTUM AND FORCES			COMBUSTOR					
	, , , , , , , , , , , , , , , , , , , ,								
	INLET FRICTION DRAG	• •		• • • • • • • • • • • • • • • • • • • •					
	COMBUSTOR FRICTION DRAG			CY					
	COMBUSTOR STRUT DRAGARERS 10-91	(L8F)	COMBUSTOR EFFECTIVE	ENESS	. 0.8685				
	COMMUSTOR MOMENTUM CHANGE		INJECTOR DISCHARGE	COEFFICIENTS 0,8361	0.7074.	0.7952: 0.7054			
	NOZZLE STRUT DRAG	(LBF)	-						
	NOZZLE MOMENTUM CHANGE			NOZZLE					
	NOZZLE PRESSURE INTEGRALA		DIELOW OTHERW TUNG	o- 00511151517	0.0004				
		(LBF) (LBF)		ST CUEPFICIENT = CS					
	TOTAL EXTERNAL DRAGERER RESERVED BY STATE OF STA	· ·	PROCESS EFFICIENCY		0.8693				
	TOTAL STRUT DRAG	(LBF)	KINETIC ENERGY FFF	ICIENCY	. 0,8866				
		7.67 =119.44							
	, 8TATIONS		Ftil	EL INJECTOR8					
	NOMINAL COME LEADING EDGE 34.884	LITHI	INJECTORS	STATION	ALVE				
	SPIKE TRANSLATION		IA	40.400	ALVE				
	INLET THRUATALORS SACRES SACRES SACRES SACRES 40,400		18	41.292	B				
	COWL LEADING EDGE		1 C 2 A	44,300					
	NOZZLE PLUG THAILING EDGE		5C	48.767 46.250	D E				
	STRUT LEADING EDGE	(ÎN)	3 A	54,057	•				
	STRUT TRAILING EDGE		36	56.242					
	COMBUSTOR EXITATE STATE OF STA	((ц	44,792					

t = 235.13 sec.

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⊋	P	T	Ħ	(GAMMA	MOLAT	SUNV	MACH	νFI	5	A/A	W	A/AC	HIMUM	¢	IVAL	PHI	ETAC
	WIND TUNNEL	1	0 5	`						•				• • • •	•		•	.
	0.000 /46.249	3033	681.0(8	063 1	.2927	28,852	2599											
	0.000 0.397	414	-29.6(1	100) 1	3989	28.851	999	5,969	5963	1.831	0.10679	26.870	0,9624	5080	9,896	184.1		
	SPIKE TIP NS	2	0 3	-														
	0.000 18.000		681.0(8															
	0,600 10,192	2961	659.2(7	(85) 1	.2948	20,051	2571	0.407	1046	830.5	0.10679	56.870	0.9824	4948	1,736	184.1		
	WIND TUNNEL	3	0_0															
	0.000 746.249																	
	0.000 0.379	409	#30.9 (98) 1	.3988	28,851	995	6,015	5969	1.831	0.10336	26,008	0.9824	4920	9.588	169.5		
	SPIKE TIP NS	1027	0 0	1.6. 4	1000	74 LE4	15.00											
	0.600 14.000		681,0(8					A 1201	1004	2 484	0 10774	34 868	0 0024	46.00	1.616	.00 5		
	INLET THROAT	2,01	660,867	יו ניפי	16740	E0.031	2513	0.371	TOUR	2.400	0.10220	501110	0,9024	4920	1.010	104.5		
	40.400 314.567	2971	662.01 7	1081 1	2046	28 AC	257/											
	40.400 15.165	_	220.3(3					2.587	4701	1.885	0.94053	26.870	0.1115	4360	68.718	162.2		
	INLET UPNESK	6	0 3	., .,	1000	40,000	1	44241	~, ~,		441-055	Coldin	011115	4200	001110	40616		
	40.400 314.567		662.0(7	788) 1.	.2945	28.851	2574											
	40.400 13.040	1360	205.8(3					2.679	4778	1.885	0.85503	26.870	0.1227	4400	63,483	163.7		
	INLET DNNRSK	7	0 4	• • • • •	•		-						• • • • • • • • • • • • • • • • • • • •			•		
	40.400 124.723	2971	662.0(7															
	40.400 107.496	2871	632.10 7	759) 1	,2977	28,851	2534	0,483	1223	1.948	0.85503	26.870	0.1227	4400	16.255	163.7		
	COMBUSTOR 0	8	1 21	_														
	40.410 253.570		665.7(8															
	40.410 15.189 COMBUSTOR 0	1464	228,6(3	5843 1	* 7250	27.176	1403	2.457	4677	1.992	0.94497	27.000	0.1116	4359	68,682	161.4	0.17	0.07
	COMBUSTOR 0 41.292 207.484	•	2 21	2.21	3017	24 422	2644											
	41.292 18.686		274.7(4					2.212	4430	2.047	A - 0/19/11	27.060	0 1113	//260	65,361	187.4	0.35	n n %
	_	10	3 21	.5.1 1.	.3400	201355	2003	48545	4420	2007	1177771	611007	0 1 1 1 1 2	4200	024201	12114	0 8 5 3	0 6 0 3
	41.302 215.266		666,9(8	1 (868	.3032	26.287	2631											
	41,302 16,726							2.233	4427	2.041	0.94970	27.069	0.1113	4259	65.344	15/.3	0.25	0.00
		11	4 21		****		-	_ • - •	- •			• • • •					- •	
	41,367 213,704	2803	666,6(8	306) 1	.3035	185.65	2629											
	41.367 18.983	1544						5.550	4409	2.041	0.94971	27.069	0.1113	4251	65.074	157.0	0,25	0.00
	.	12	5 3	•														
	41.500 207.006		666.0(8													_		
	41.500 20.501			434) 1	3475	56.588	5014	2.155	4339	5.044	0.95082	27,069	0.1111	4234	64.116	150.4	0,25	0.01
		13.	6 3		*^^0	24 750	54.07											
	42.460 181.870 42.460 22.571							2 017	4362	2 // E G	0.94188	27 040	A 4433	#1 B B	44 694	156 7	A 3E	۸ ۸ ۲
		14	7 6	*/** *	• 3 4 0 0	201334	2005	E . U . I	4207	2.030	0.94100	6/1007	4.1155	4100	61.581	13441	0.23	U . U D
	44.087 117.069		649.0(10	0.991 1	. 2582	27.368	291A											
	44.087 47.103							1.253	3348	2.145	0.91011	27.069	0.1161	4218	47.360	155.8	0.25	n . 84
		15	6 3					••					*****		.,,,,,,,		****	
	44.310 115.576	3771	647.0(11	103) 1.	.2556	27,429	2929											
	44.310 49.506	3155						1.206	3259	2.147	0.90806	27.069	0.1164	4218	45.993	155.8	0.25	0.88
		16	9 4											-				-
	44.800 113.256																	
	44,800 54,783		455.3(9	7//8) 1	,2713	27.539	2753	1.111	3057	2.150	0.90424	27.069	0.1169	4212	42.965	155.6	0.25	0.96
	-	17																
	44,802 113,281	5035	642.1(11	125) 1	2518	27.525	2945		***									_ _ .
	44.802 54.786 COMBUSTOR 0	18	455.2(9	440) 1	. 2/14	.538</td <td>2752</td> <td>1.111</td> <td>2028</td> <td>4.150</td> <td>0.90454</td> <td>27.069</td> <td>0.1168</td> <td>4212</td> <td>42,980</td> <td>155.0</td> <td>0.25</td> <td>0.96</td>	2752	1.111	2028	4.150	0.90454	27.069	0.1168	4212	42,980	155.0	0.25	0.96
	46.250 106.721			0.00	27110	27.465	2007											
			488,7(9					1.015	3856	9.754	n BADEA	27 701	0 4280	4364	78 303	166 4	n 44	A 7.0
				. 4 - 7	9 14 7 3 3	F2#00#	6407	* * 0 * ~	2020	0	A * A A E 2 A	61.0371	0 . 1 5 4 0	4640	38.505	12241	A # 00	0 # D 0

AZAC MOPTE W IVAC PHI ETAC GAPMA MOLKT SONV MACH VEL S h/A COMEUSTOR 0 19 12 2 46.260 106.690 3355 651.0(1100) 1.2788 23.005 2994 57.387 2923 488.0(943) 1.2933 23.607 2810 1.014 2850 2.358 0.8618/ 27.391 0.1241 4250 36.170 155.2 0.66 0.31 40.200 0 20 13 COMBUSTOR 47.310 103.502 3660 638.1(1266) 1.2630 24.140 3085 59.260 3251 479.7(1056) 1.2775 24.155 2924 0.965 2815 2.379 0.60213 27.391 0.1333 4421 35.096 161.4 0.66 0.43 47.310 COMBUSTUR 0 21 14 3 47.327 103.337 3672 637.9(1211) 1.2623 24.162 3088 59,365 3265 480.0(1061) 1.2768 24.169 2929 0.960 2812 2.380 0.79945 27.391 0.1338 4428 34.931 161.6 0.66 0.44 47.527 COMBUSTOR 0 22 15 4 48.110 99.906 3956 629.0(1310) 1.2462 24.488 3164 55.906 3518 453.1(1147) 1.2630 24.504 3003 0.988 2967 2.397 0.74748 27.391 0.1431 4574 34.460 167.0 0.66 0.56 48.110 COMBUSTOR 0 23 15 6 48,767 94.764 3595 638.8(1308) 1.2678 21,756 3227 45.064 3060 413.5(1091) 1.2865 21.762 2999 1.120 3359 2.585 0.69667 27.694 0.1552 4683 30.372 169.1 1.04 0.33 48.767 0 24 17 COMBUSTOR 48,777 94.715 3598 638.7(1309) 1.2677 21.758 3228 412.2(1091) 1.2865 21.764 2999 1.123 3366 2.585 0.69577 27.694 0.1554 4665 36,400 169.2 1.04 0.33 48.777 44.910 3060 COMBUSTOR u 25 18 49.307 93.153 3658 633.8(1332) 1.2644 21.825 3246 49.307 36,762 2992 353,0(1062) 1.2878 21.853 2962 1.265 3748 2.590 0.65071 27.694 0.1662 4791 37.902 173.0 1.04 0.35 COMBUSTUR 0 26 19 5 84.723 3999 621.9(1465) 1.2446 22.179 3340 50.717 50.717 COMBUSTOR 0 27 20 52.817 78,973 4209 607.0(1547) 1,2305 22,422 3389 22,500 3280 191,8(1164) 1,2666 22,465 3035 1,502 4556 2,633 0,45455 27,694 0,2379 5294 32,198 191,2 1,04 0,53 52.817 COMBUSTOR 0 28 21 53,317 79,601 4173 603,9(1533) 1,2328 22,393 3380 20.112 3164 158.0(1118) 1.2734 22.433 2988 1.581 4724 2.630 0.43597 27.694 0.2480 5344 32.005 193.0 1.04 0.52 53.317 COMBUSTOR 0 29 22 77,927 4214 599,4(1549) 1,2298 22,445 3388 54,067 18.411 3158 130.7(1114) 1.2728 22.491 2981 1.625 4843 2.634 0.41096 27.694 0.2631 5409 30.930 195.5 1.04 0.53 54.067 COMBUSTOR 0 30 23 3 77.091 4226 595,1(1953) 1,2288 22,466 3390 54,827 16.687 3110 101.1(1095) 1.2742 22.515 2958 1.681 4972 2.634 0.38862 27.694 0.2782 5469 30.027 197.5 1.04 0.54 54.827 COMBUSTOR 0 31 24 55,760 74.959 4276 590.3(1573) 1.2251 22.528 3400 75.7(1098) 1.2729 22.584 2957 1.716 5075 2.639 0.36470 27.694 0.2965 5533 28.762 199.6 1.04 0.56 55.760 15.344 3120 COMBUSTOR 0 32 25 58.040 4718 588,1(1748) 1.1870 22,994 3480 56.252 86,7(1337) 1.2366 23:180 3151 1.590 5009 2:678 0:29386 27:694 0:3679 5691 22:875 205:5 1:04 0:72 56.252 14,636 3742 COMBUSTOR 0 33 26 69.128 4295 56.307 987,9(1580) 1.2229 22,553 3403 4.0(1040) 1.2776 22.016 2891 1.809 5405 2.646 0.29308 27.694 0.3689 5695 24.618 205.6 1.04 0.57 56.307 11.029 2976 COMBUSTUR 0 34 27 56.447 66,925 4302 587.3(1583) 1.2224 22,562 3404 0.9(1040) 1.2774 22.626 2892 1.873 5417 2.647 0.29093 27.694 0.3717 5703 24.490 205.9 1.04 0.57 56.447 10.928 2979 COMBUSTOR 0 35 28 21 56.527 51,319 5149 586.9(1921) 1.1494 23.438 3543 72,5(1602) 1.1684 23.935 3275 1.549 5074 2.693 0.29424 27.694 0.3675 5706 23.200 206.1 1.04 1.00 56.527 14.241 4419 COMBUSTOR 0 36 29 21 51.501 5148 585,8(1921) 1,1495 23,440 3543 56.807 N 56,807 13.837 4399 59.7(1594) 1.1695 23.944 3268 1.570 5131 2.693 0.29337 27.694 0.3686 5723 23.393 206.6 1.04 1.00 COYBUSTOR 0 37 30 21 57,033 51.386 5147 584.9(1920) 1.1495 23.441 3542 57.033 13.183 4371 42.1(1582) 1.1708 23.958 3259 1.599 5212 2.693 0.29266 27.694 0.3695 5733 23.703 207.0 1.04 1.00

GAMPA MOLWT SONV MACH VEL S M/A M a TINUM DAVA IVAL PHI ETAC NO COMMUNIOR 0 36 31 21 CO 57,757 49.929 5140 582,0(1917) 1.1493 23.441 3540 № 57.757 11.085 4261 -11.9(1543) 1.1753 23.998 3229 1.669 5452 2.695 0.28612 27.694 0.3753 5758 24.410 207.9 1.04 1.60 COFBUSTOR 0 39 32 21 58.777 39.503 5106 578.7(1903) 1.1074 23.413 3527 58.777 5.887 4030 -149.4(1438) 1.1685 24.080 3145 1.919 6036 2.714 0.28628 27.694 0.3/77 5765 26.854 206.2 1.04 1.00 COMBUSTOR 0 40 53 21 60.787 55.927 5141 573.0(1917) 1.1503 23.464 3540 00.787 17,175 4486 111,1(1031) 1,1667 23,407 3299 1,457 4808 2,687 0,29675 27,694 0,3650 5744 22,135 cV/a4 1,04 1,00 COMBUSTOR 0 41 34 21 62.207 54.664 5138 568.8(1916) 1.1506 23.472 3539 62.207 16.219 4440 81.0(1611) 1.1690 23.934 3284 1.505 4940 2.685 0.50428 27.694 0.3553 5729 25.362 206.9 1.04 1.00 COPBUSTOR 0 42 35 200 64.671 51.619 5122 560.1(1909) 1.1504 23.475 3533 64,671 19.444 4565 163.2(1665) 1.1633 23.861 3326 1.340 4457 2.688 0.28842 27.694 0.3749 5703 19.976 205.9 1.04 1.00 COMBUSTOR 0 43 36 200 65.047 47.777 5111 558.6(1904) 1.1497 23.467 3528 20.262 4625 207.6(1691) 1.1602 23.815 3347 1.252 4190 2.694 0.26813 27.694 0.4032 5700 17.462 205.8 1.04 1.00 65,047 COMBUSTOR REGEN 44 37 65.047 47.777 5186 637.2(1939) 1.1472 23.358 3559 17,978 4644 232.0(1700) 1.1572 23.774 3353 1.343 4502 2.709 0.26613 27.694 0.4032 5732 18,762 207.0 1.04 1.00 65.047 NOZZLE AE 45 38 5 87,283 47.777 5111 558.6(1860) 1.1497 23.467 3528 1.346 2926 -641.5(990) 1.2648 24.196 2757 2.810 7749 2.694 0.05582 27.694 1.9371 7338 6.722 265.0 1.04 1.00 87.283 NOZZLE PO 87,283 47.777 5111 556,6(1860) 1.1497 23.467 3528 0.397 2246 -899.7(732) 1.2857 24.197 2437 3.505 8542 2.694 0.02363 27.694 4.5763 7818 3.137 282.3 1.04 1.00 87.283 MOZZLE AE REGEN 47 40 87.283 47.777 5188 637.2(1939) 1.1472 23.358 3559 87.283 1.395 3064 4567.0(1044) 1.2603 24.195 2817 2.779 7827 2.709 0.05582 27.694 1.9371 7429 6.789 268.5 1.04 1.00 NOZZLE PO REGEN 48 41 5 87,683 47.777 5188 637.2(1939) 1.1472 23.358 3559 87,283 0.397 2343 -864.7(767) 1.2624 24.197 2484 3.489 8669 2.709 0.02301 27.694 4.6986 7940 3.100 286.7 1.04 1.00 FICTIVE COMBUSTR 68 61 314.567 5335 558,6(1995) 1,1668 23,707 3613 65.047 0.397 1431-1188.0(444) 1.3257 24.197 1974 4.735 9349 2.535 0.04065 27.694 2.6615 8318 5.902 300.3 1.04 1.00 65.047 FICTIVE NUZZLE 0 56 96 87.283 32.142 5035 534.0(1872) 1.1472 23.446 3500 87.283 1.611 3262 #507.0(1123) 1.2518 24.192 2897 2.492 7217 2.723 0.05582 27.694 1.9371 7012 6.261 253.2 1.04 1.00

ACADING # C	אטיים פוניי	- 137 [1]	hr = 532*133	писл о		40.547	- 3(13363				FAUL 4
XABS	₽⊎IB	P=0e	PDA	QOX	81=W	G=08		CAMALL	P=18/PSu	P=18/P10	P=UB/PS0	P+0B/P10
6.941E+01	1.070E 00	0.000	₩#.389£₩01	0.000	0.000	0.000		2.470E=02	2.6946 00	1.434E=03	0.000	0.000
1.836F 01	1.070E 00	0.000	-3.562E 01	0.000	0.000	0.000		1.63/E 02	2.6941 00	1.434E=03	0.000	0.000
3.070E 01	5.210E 00	U . 000	-1.686E 02		0.000	U.000		5.053E U2	5.565F 0v	2,961E=03	0.000	0.000
3,508£ 01	3.896E 00	0.000	-3,664£ 02		0.000	0.000		6.804E 02	9.811F 00	5.221E=03	0.000	0.000
3.518E 01	3.919E 00		0 =4.329E 02		0.000	0.000		6.850E 02	9.869E 00	5.252t=03	1.474E U1	7.843E-03
3.519E 01	3.921E 00		0 =4.329E V2		0.000	0.000		6.8535 02	9.672E 00	5.254E=03	1.466E 01	7.8006+03
3,555E 01	4.000E 00		0 =4.4036 02		0.000	0.000		7.213E C2	1.007F 01	5.3t0L=03	4.608E 00	5.2206-03
3.586E 41	3.961E 00		0 =4.541E 02					7.525E 02	9.9741 00	5,308=03	5.666E 00	3.015E-03
5.606E 01	3.935E 00		0 -4.645E 02					7.733E 02	9.9085 00	5.2/3t=03	7.719E 00	4.108E=03
3.648E 01	4.189E 00		0 =4.829E 02					8.169E 02	1.0556 01	5.614E=03	1.197E 01	6.368E+U3
3,701F 01	4.200E 00		0 =5.058£ 02				0.1	8,730E 02	1.058E 01	5.6286.403	1.732E 01	9.2206.03
3.732E 01	4.10>E 00		0 m5.164L 02					9.059E 02	1.034E 01	5.501E=03	2.043E 01	1.087E-U2
3.803E 01	3.885E 00		1 -5.301E 02					9.838E 02	9.782E 00	5.206E+03	3.374E 01	1.7966-02
3.834E 01	5.427E 00		1 -5.286L 02					1.018E U3	1.367E 01	7.2736-03	3.947E 01	2.1016-02
3.875E 01	7.503E 00		1 -5.2986 02					1.065E 03	1.889E 01	1.005L=02	3.864E 01	2.056E=02
3.881E 01	7.789E 00		-5.301E 02					1.071E 03	1.9618 01	1.0446-02	3.853E 01	2.050E=02
3.90 E 01	8.810E 00		1 -5.302E 02					1.094E 03	2.218E 01	1.1811-02	3.920E 01	2 086E-02
3.932E 01	1.399E 01		-5.360E 02					1.130E 03	3,5228 01	1.8746-02	4.023E 01	2 141E=02
3,950E 01	1.707E 01		1 -5 444E 02					1.151E 03	4.300E 01	2.2886-02	3.413E 01	1 816E=02
3.981E 01	1.746E 01		0 -5.633E 02					1.187E 03	4.397E 01	2.340E=02	2.392E 01	1.2736=02
4.000E 01	1.770E 01		0 -5.762E 02					1,209E 03	4.458E 01	2.3726-02	2.373E 01	1 2636=02
4.040E 01	2,1038 01		0 =6.050E 02					1.256E 03	5.296E 01	2.818E=02	2.333E 01	1.242E=02
4.041E 01	2.112E 01		0 -6.056E Q2					1.257E 03	5.317E 01	2.8306-02	2.332E 01	1.2416-02
4.1298 01	2.846E 01		0 -6.867E 02					1.362E 03	7.16SE 01	3,8136-02	2.245E 01	1.1956-02
4.130E 01	2.854E 01		0 -6.877E 02					1.363E 03	7.186E 01	3.824E-02	2.244E 01	1.194E=02
4.137E 01	2.908E 01		0 =6.946E 02					1,371E 63	7.322E 01	3.897E=02	2.238E 01	1.1916-02
4.150E 01	3.019E 01		1 =7.085£ 02					1.386E 03	7.601E 01	4.045E+02	2.723E 01	1.449E+02
4.2462 01	2.044E 01		1 .7.373E 02					1.501E 03	5.146E 01	2.739E-02	6.221E 01	3.310E-02
4,409E 01	4.596E 01		-6.806E 02					1.698E 03	1.157E 02	6.159E=02	1.215E 02	6.465E002
4.431E 01	4.946E 01	4.955E 0	1 -6.774E 02	-1.128E 0	3 -7.703E	02 -3.5746	0.2	1.725E 03	1.2456 02	6.628E-02	1.248E 02	6.640E=02
4.480E 01	5.715E 01		-6.749E 02					1.785E 03	1.439E 02	7.658t=02	1.320E 02	7.0246-02
4.480E 01	5.715E 01	5.243E 0	1 #6.752E 02	₩1.262E C	3 -8.4425	02 *4.178	0.2	1.785E 03	1.439E 02	7.658£=02	1.320E 02	7.025E=02
4,625E 01	5.384E 01	6.090E 0	1 -5.649E 02	-1.723E (3 -1.0646	03 =6.592	0.2	1,963E 03	1.356E 02	7.2156=02	1.533E 02	8.161E=02
4.626E 01	5.382E 01	6.096E 0	1 -5.631£ 02	#1.727E (3 -1.0656	03 -6,6116	0.2	1.964E 03	1.355E 02	7.212E=02	1.535E 02	8,169E=U2
4.731E 01	5.142E 01		1 =3.775£ 02					2,095E 03	1.295E 02	6,890£-02	1.690E 02	8,992E+02
4.733E 01	5.15\$E 01		1 -3.702E 02					2.097£ 03	1.298E 05	6,905£=02	1.692E 02	9.005E=02
4.811E 01	5.665E 01	5.516E 0;	1 -5.133F 05					2.194E 03	1.426E 02	7.5912-02	1.389E 02	7.3926>02
4.877E 01	4,506E 01	4.506E 0				03 =1.1148		2.277E 03	1,135E 02	6.0396=02	1.135E 02	6.039E=02
4.878E 01	4,491E 01		1 =5.669E 01					2.278E 03	1,131E 02	6.018E=02	1.131E 02	6.018E=02
4.931E 01	3.676E 01	3.676E 0				03 -1.1898		2.344E 03	9.257E 01	4.926E=02	9.657E 01	4.926E=02
5.072E 01	3.133E 01	3.133E 0				. 03 -1.3591		2.522E 03	7.889E 01	4.1986=05	7.889E 01	4.198E=02
5.2828 01	2.250g 01	2,250g 0				03 -1.5686		2.788E 03	5.666E 01	3.015E=02	5.666E 01	3.015E=02
5.332E 01	2.011E 01	2.011E 0				03 -1.612		2.8528 03	5.064E 01	2,6956-02	5.064E 01	2,695E>02
5.407E 01	1.841E 01	1.841E 0				03 -1.6778		2.948E 03	4.636E 01	2.467E-02	4,636E 01	2.467E=02
5,483E 01	1.669E 01	1.669E 0				03 =1.740		3.045E 03	4.202E 01	5.536E=05	4.202E 01	5.536E=05
5,5765 01	1.534E 01	1.534E 0	•			03 =1.8116		3.165E 03	3.864E 01	2.0566-02	3.864E 01	S.029E=05
5,625E 01	1.464E 01	1 . 464E 0				1.846 - د٥		3.209E 03	3,685E 01	1.961E=02	3.685E 01	1.961E=02
5.631E 01	7.500E 00	1.4568 0				03 =1.850		3.2166 03	1,889E 01	1.0056=02	3.6665 01	1.951E=02
5.6458 01	7.500E 00	1.436E 0				03 =1.8598		3.234E 03	1.889E 01	1.0056-02	3.615E 01	1.924E=02
5.653E 01 5.681E 01	1.424E 01	1.424E 0	•			03 -1.865		3.245E 03	3.586E 01	1.908E=02	3.586E 01	1,908E=02
	1,3845 01	1,384F 0	•			: 03 =1.884€		5.280E 03	3,484E 01	1.8546-02	3.484E 01	1.854E=02
5.703E 01	1,3188 01	1,318E 0				03 =1.9008		3.309E 03	3.319E 01	1.767E-02	3.319E 01	1.767E=02
	1.108E 01	1,108E 0				03 =1.9516		3,402E 03	2.791E 01	1,4851-02	2.791E 01	1.4855-02
5.878E 01	5.887E 00	5.887E 0				03 -2.0116		3.532E 03	1,482E 01	7.8896=03	1.482E 01	7.889E=03
6.079E 01	1.717E 01	1.7175 0				03 -2.1256		3.790£ 03	4.325E 01	2.302E=02	4.325E 01	2.302E=02
6,221E 01	1 1 4 4 5 5 5 7 1	1.655E 0	1 1.1405 02	-41433E (12 #2.6428	: v3 =2.2138	. 0.5	3.9726 03	4.084E 01	2.1756=02	4.084E 01	2.1736.02

			-									
	XABS	_ P≖IB	P=08	PDA	A O D	6=1B	₽÷⊍B	CAHALL	P=16/PSC	P=18/P[0	P=OB/PSO	Pm08/P10
I	0.467E 01	1.944E U1	1.9446 01	1.1448 03	-4.696E 03	-2.324E 03	-2.373E 03	4.2098 03	4.896E 01	2.6u6t = 02	4.836E 01	2.606E=Û2
4	0.505E 01	2.059E 01	1.994E 01				-2.400E 03	4.337E 03	5.184E 01	2.7596=02	5.020E 01	2.6716-02
i,C		2.059E 01	1.999E 01				-2.402E 03	4.342E 03	5.184E 01	2.7596=02	5.033E 01	2.678E+02
	6.529E 01	1.956E 01	2 025E 01				-2.416E 03	4.3686 03	4.926E 01	5.655F=05	5.099E 01	2.714E002
	6.695E 01	1.106E 01	9 400E 00				+2.519E 03	4.583E U3	2.785E 01	1.482E-02	2.367E 01	1.260E-02
	6.762E 01	7.705E 00	9.315E 00				-2.556E 03	4.665E 03	1.940E 01	1.033E=02	2.346E 01	1.2486=02
	6.839E 01	3.850E 00	7.098E 00				=2.691E 03	4.760E U3	9.694E 00	5.1596.03	1.787E 01	9.5126=03
	6.911E 01	3.501£ 00	5.025E 00				3 =2.651E 03	4.84RE 03	8.515E 00	4.691E=03	1.265E 01	6.734E=03
		3.205E 00								4.295E=03	1.016E 01	5.405E=03
	6.972E 01		4.034E 00				6 -2.692E 03	4.922£ U3	8.070E 00			
	7.067E 01	2.1386 00	2.490E 00				5 =2.739E 03	5,036E 03	5.383E 00	2.865E=03	6.270E 00	3.337E=03
	7.110E 01	1.655E 00	2.335E 00				-2.755E 03	5.088E 03	4.167E 00	2,218t=03	5.880E 00	3.129E=03
	7.263E 01	1.5238 00	1.785E 00				\$ =2.802E 03	5,273£ 03	3.835E 00	2.0416-03	4.495E 00	2.392E-03
	7.278E 01	1.510E 00	1.768E 00				\$ -2. 806E 03	5,290£ 03	3.802E 00	2,023E-03	4.451E 00	2,369E=03
	7.353E 01	1.645E 00	1.6802 00	2.173E U3	■5.316E 03	i ≈2.487£ v]	\$ =2.828E 03	5.374E U3	4.1438 00	2.205=03	4,230E 00	2,251E-03
	7.353E 01	1.646E 00	1.6802 00	2.176E 03	₩5.316E 03	3 ≈2•487£ 03	5 =2,826E 03	5.375E 43	4.144E 00	2.206E-03	4.229E 00	2,251E=03
	7.486E 01	1.885€ 00	0.000	5.213E 03	*5.369E 03	-2.494E 01	5 ₩2 ,875E 03	5.447E 03	4.746E 00	2.526E=03	0.000	0.000
	7.771E 01	2.730E 00	0.000	2.305E 03	⇒5.380E 03	3 =2.505E 03	5 =2.875E 03	5.525E 03	6.874E 00	3.658E=03	0.000	0.000
	8.14jE 01	2.035E 00	0.000	2.407E 03	-5.392E 01	5 -2.517E 03	3 02.875E 03	5.630E 03	5.124E 00	2.727E=03	0.000	0.000
	8.442E 01	1.575E 00	0.000				3 -2.875E 03	5.684E 03	3.966E 00	2.111E=03	0.000	0.000
	8.728E 01	3.520£ 00	0.000				-2.875E 03	5.707E 03	8.863E 00	4.717E=03	0.000	0.000
	8.728E 01	3.524E 00	0.000				-2.875E 03	5.707E 03	8.874E 00	4.722E=03	0.000	0.000

4.040E 01 1.193E 02 1.193E 02 2.172E=03 4.263E=02 4.129E 01 1.787E 01 1.373E 02 2.558E=03 4.679E=02 4.130E 01 1.887E=01 1.375E 02 2.557E=03 5.196E=02 4.137E 01 1.195E 00 1.387E 02 2.377E=03 5.196E=02 4.2426 00 1.724E 01 1.584E 02 2.377E=03 5.196E=02 4.2426 00 1.724E 01 1.851E 02 2.377E=03 5.654E=02 4.406E 01 2.674E 01 1.851E 02 2.5883E=03 6.191E=02 4.406E 01 3.536E 00 1.887E 02 3.038E=03 7.243E=02 4.486E 01 3.536E 00 1.887E 02 3.038E=03 7.243E=02 4.486E 01 3.536E=01 1.967E 02 3.038E=03 7.243E=02 4.486E 01 3.536E=01 2.197E 02 3.038E=03 7.243E=02 4.486E 01 3.536E=01 2.197E 02 3.038E=03 7.243E=02 4.625F 01 2.300E 01 2.197E 02 3.038E=03 7.243E=02 4.626E 01 1.586E=01 2.197E 02 3.038E=03 7.483E=02 4.631E 01 1.497E 01 2.399E 02 3.038E=03 7.483E=02 4.631E 01 1.497E 01 2.548E 02 3.063E=03 7.483E=02 4.631E 01 1.497E 01 2.548E 02 3.084E=03 7.483E=02 4.677E 01 9.196E 00 4.547E 02 3.284E=03 7.483E=02 4.677E 01 9.196E 00 4.547E 02 3.284E=03 7.493E=02 4.677E 01 1.437E=01 2.548E 02 3.084E=03 7.493E=02 5.328E 01 7.571E 00 2.881E=03 3.794E=03 5.328E 01 7.571E 00 3.495E 02 3.084E=03 7.493E=02 5.407E 01 1.877E 01 2.810E 02 2.889E=03 7.072E=02 5.407E 01 1.877E 01 3.405E 02 2.997E=03 4.695E=02 5.407E 01 1.675E 01 3.405E 02 2.997E=03 4.695E=02 5.407E 01 1.675E 01 3.405E 02 2.997E=03 4.697E=02 5.407E 01 1.877E 01 3.405E 02 2.997E=03 4.697E=02 5.407E 01 1.675E 01 3.405E 02 3.331E=03 3.75RE=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.75RE=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.250E=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.274E=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.250E=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.250E=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.250E=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.250E=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.250E=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.250E=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.250E=02 5.653E 01 7.513E=01 3.405E 02 3.331E=03 3.250E=02 5.653E 01 3.309E 00 3.436E 02 3.331E=03 3.250E=02 5.653E 01 3.309E 00 3.436E 02 3.331E=03 3.250E=02 5.653	X	UDRAG	CDRAG	CF	HC
##130E 01 1.887E=01 1.375E 02 2.377E=03 5.009E=02 4.150F 01 1.15E 01 1.387E 02 2.377E=03 5.140E=02 4.25E 00 1.412E 02 2.377E=03 5.140E=02 4.26E 01 1.724E 01 1.584E 02 2.377E=03 5.140E=02 4.406E 01 2.674E 01 1.584E 02 2.377E=03 5.140E=02 4.406E 01 3.550E 00 1.887E 02 3.009E=03 7.122E=02 4.480E 01 8.043E 00 1.887E 02 3.009E=03 7.122E=02 4.480E 01 8.043E 00 1.967E 02 3.038E=03 7.2243E=02 4.406E 01 1.588E=01 2.197E 02 3.333E=03 6.859E=02 4.625F 01 2.300E 01 2.197E 02 3.333E=03 6.859E=02 4.731E 01 1.99E 01 2.349E 02 3.038E=03 7.463E=02 4.733E 01 1.588E=01 2.197E 02 3.333E=03 6.859E=02 4.733E 01 1.588E=01 2.399E 02 3.038E=03 7.463E=02 4.733E 01 1.035E 01 2.349E 02 3.038E=03 7.463E=02 4.61E 01 1.035E 01 2.349E 02 3.038E=03 7.463E=02 4.675E=02 4.675E=02 4.675E=02 3.284E=03 6.859E=02 4.675E=02	4.041E 01	3.919E=01	1.195E 02	2.558E=03	4.0/9E=02
4.150	4.130E 01	1.887E=01	1.375E 02	2.378E=03	5.069E-02
##409E 01	4-1508 01	2.4268 00	1.4128 02	2.373t=03	5.4U5E=02
4.480E 01	4.409E 01	2.674E 01	1.851E 05	2.583E=03	8.191E#02
4.626E 01 1.588E=01 2.199E 02 3.333E=03 7.833E=02 4.733E 01 2.25E=01 2.351E 02 3.083E=03 7.833E=02 4.733E 01 2.25E=01 2.351E 02 3.083E=03 7.833E=02 4.733E 01 1.437E=01 2.351E 02 3.034E=03 7.837E=02 4.817E=01 1.35E 01 2.455E 02 3.034E=03 7.837E=02 4.877E 01 9.196E 00 2.547E 02 3.284E=03 6.547E=02 4.578E 01 1.437E=01 2.548E 02 2.947E=03 6.548E=02 5.072E 01 1.877E=01 2.810E 02 2.881E=03 5.932E=02 5.282E 01 2.572E 01 3.047E 02 2.8898E=03 4.293E=02 5.322E 01 2.572E 01 3.047E 02 2.8898E=03 4.293E=02 5.322E 01 2.572E 01 3.047E 02 2.897E=03 4.293E=02 5.322E 01 2.572E 01 3.047E 02 2.8878E=03 4.293E=02 5.322E 01 2.572E 01 3.405E 02 2.972E=03 4.293E=02 5.322E 01 2.572E 01 3.405E 02 2.972E=03 4.293E=02 5.576E 01 1.025E 01 3.405E 02 2.8874E=03 3.572E=02 5.576E 01 1.025E 01 3.405E 02 2.8874E=03 3.572E=02 5.576E 01 1.025E 01 3.405E 02 2.8874E=03 3.572E=02 5.576E 01 1.025E 01 3.405E 02 2.8874E=03 3.572E=02 5.576E 01 1.025E 01 3.405E 02 3.8321E=03 2.696E=02 5.576E 01 1.025E 01 3.405E 02 3.8321E=03 2.696E=02 5.653E 01 7.513E=01 3.443E 02 3.8321E=03 2.696E=02 5.653E 01 7.513E=01 3.443E 02 3.8321E=03 2.706E=02 5.653E 01 7.513E=01 3.405E 02 3.8321E=03 2.706E=02 5.653E 01 7.372E 00 3.517E 02 3.3308E=03 2.706E=02 5.706E 01 1.226E 01 3.700E 02 3.3331E=03 3.137E=03 5.137E=03 5.706E 01 1.226E 01 1.226E 01 4.046E 02 3.2377E=03 3.137E=03 5.13			1.967E 02		7.245E-02
4.811E 01 1.035E 01 2.455E 02 3.063E=03 7.463E=02 4.871E 02 3.034E=03 7.371E=02 4.877E 01 1.035E 01 2.455E 02 3.034E=03 7.072E=02 4.978E	4.626E 01	1.588E=01	2.199E 02	3.333E=03	6.859E=02
4.877E 01 9.196E 00 2.547E 02 3.284E=03 7.072E=02 4.878E 01 1.437E=01 2.548E 02 3.020E=03 7.072E=02 5.072E 01 1.877E 01 2.622E 02 2.949E=03 6.544E=02 5.282E 01 2.572E 01 3.067E 02 2.898E=03 4.693E=02 5.282E 01 2.572E 01 3.067E 02 2.898E=03 4.693E=02 5.332E 01 6.004E 00 3.272E 02 2.972E=03 4.221E=02 5.407E 01 8.891E 00 3.210E 02 2.972E=03 4.221E=02 5.407E 01 8.891E 00 3.210E 02 2.972E=03 3.550E=02 5.407E 01 1.025E 01 3.405E 02 2.898E=03 3.550E=02 5.631E 01 4.967E=01 3.405E 02 2.897E=03 3.550E=02 5.631E 01 7.513E=01 3.405E 02 3.806E=03 2.690E=02 5.631E 01 7.513E=01 3.465E 02 3.836E=03 2.690E=02 5.631E 01 7.513E=01 3.463E 02 3.338E=03 2.704E=02 5.631E 01 7.513E=01 3.463E 02 3.338E=03 2.704E=02 5.681E 01 7.372E 00 3.5491E 02 3.339E=03 2.4466=02 5.681E 01 7.372E 00 3.513E 02 3.339E=03 2.4466=02 5.681E 01 7.372E 00 3.567E 02 3.339E=03 2.4466=02 5.676E 01 1.125E 01 3.700E 02 3.339E=03 2.4466=02 5.676E 01 1.356E 01 4.046E 02 3.224E=03 3.226E=02 6.221E 01 1.356E 01 4.271E 02 3.227E=03 3.226E=02 6.509E 01 1.321E 01 4.304E 02 3.226E=03 3.226E=02 6.509E 01 1.321E 01 4.304E 02 3.226E=03 3.226E=02 6.509E 01 1.321E 01 4.304E 02 3.226E=03 3.226E=02 6.509E 01 1.321E 01 4.300E 02 3.337E=03 3.226E=02 6.509E 01 1.321E 01 4.300E 02 3.337E=03 3.226E=02 6.509E 01 1.321E 01 4.300E 02 3.337E=03 3.226E=02 6.509E 01 1.321E 01 4.300E 02 3.226E=03 4.536E=02 6.509E 01 1.321E 01 4.300E 02 3.226E=03 4.536E=02 6.509E 01 1.321E 01 4.300E 02 3.226E=03 7.536E=02 7.676ZE 01 4.694E 00 4.507E 02 3.226E=03 7.536E=02 7.676ZE 01 4.694E 00 4.695E 02 3.137E=03 6.246E=02 7.263E 01 4.696E 00 4.507E 02 3.137E=03 6.246E=02 7.278E 01 7.339E 00 4.606E 02 3.102E=03 6.249E=03 7.278E 01 7.339E 00 4.606E 02 3.102E=03 6.249E=03 7.278E 01 7.339E 00 4.606E 02 3.102E=03 6.249E=03 7.278E 01 7.339E 00 4.606E 02 3.102E=03 6.249E=03 7.264E=03 3.269E=03 6.249E=03 6.2	4.733E 01	2.252E-01	2.351E 02	3.083E=03	7,463E=02
4.931E 01 7.371E 00 2.622E 02 2.949E=03 6.544E=02 5.072E 01 1.877E 01 2.810E 02 2.881E=03 5.932E=02 5.282E 01 2.572E 01 3.067E 02 2.898E=03 4.693E=02 5.483E 01 6.004E 00 3.216E 02 2.972E=03 4.693E=02 5.483E 01 8.891E 00 3.216E 02 2.972E=03 4.692E=02 5.483E 01 8.671E 00 3.216E 02 2.972E=03 3.752E=02 5.576E 01 1.025E 01 3.405E 02 2.874E=03 3.211E=02 5.625E 01 3.309E 00 3.443E 02 2.874E=03 3.211E=02 5.631E 01 4.967E=01 3.443E 02 3.064E=03 2.699E=02 5.631E 01 4.967E=01 3.443E 02 3.031E=03 2.699E=02 5.631E 01 4.967E=01 3.443E 02 3.313E=03 2.699E=02 5.653E 01 7.513E=01 3.463E 02 3.313E=03 2.774E=02 5.653E 01 7.513E=01 3.463E 02 3.313E=03 2.774E=02 5.653E 01 7.513E=01 3.463E 02 3.321E=03 2.699E=02 5.676E 01 1.275TE 00 3.5491E 02 3.313E=03 2.774E=02 5.703E 01 2.248E 00 3.513E 02 3.3309E=03 1.555E=02 5.776E 01 1.255E 01 3.700E 02 3.2408E=03 1.555E=02 6.776E 01 1.355E 01 4.046E 02 3.277E=03 3.137E=02 6.221E 01 1.355E 01 4.046E 02 3.277E=03 3.137E=02 6.509E 01 1.312E=01 4.304E 02 3.317E=03 3.256E=02 6.509E 01 1.312E=01 4.304E 02 3.317E=03 3.256E=02 6.509E 01 1.619E 00 4.301E 02 3.376E=03 3.256E=02 6.509E 01 1.619E 00 4.304E 02 3.317E=03 3.256E=02 6.728E 01 4.608E 00 4.517E 02 3.287E=03 1.284E=02 6.728E 01 4.608E 00 4.713E 02 3.137E=03 6.329E=03 7.263E 01 4.608E=00 4.713E 02 3.102E=03 6.329E=03 7.263E 01 4.608E=01 4.713E 02 3.102E=03 6.329E=03 7.264E=02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03 7.264E=03 4.777E 02 3.102E=03 6.329E=03	4.877E 01	9.196E 00	2.547€ 02	3.284E#03	6.465E#02
5.282E 01	4.931E 01	7.371E 00	\$ 955E 05	2.949E+03	6.544E#02
5.483E 01	5.282E 01	2.572E 01 6.004E 00	3.067E 02	2.898E=03	4.693E=02
\$.625E 01	5.483E 01	8.671E 00	3.302E 02	2.917E003	3,752E=02
5.045E 01 1,287E 00 3.456E 02 2.836E=03 2.690E=02 5.653E 01 7.513E=01 3.463E 02 3.321E=03 2.629E=02 5.703E 01 2.248E 00 3.513E 02 3.309E=03 2.746E=02 5.703E 01 2.248E 00 3.513E 02 3.309E=03 2.446E=02 5.676E 01 1.125E 01 3.700E 02 3.408E=03 2.446E=02 6.079E 01 2.112E 01 3.911E 02 3.277E=03 3.137E=02 6.21E 01 1.356E 01 4.046E 02 3.264E=03 3.003E=02 6.407E 01 2.246E 01 4.471E 02 3.277E=03 3.137E=02 6.505E 01 2.246E 01 4.471E 02 3.277E=03 3.256E=02 6.505E 01 2.246E 01 4.471E 02 3.337E=03 3.256E=02 6.509E 01 3.112E=01 4.304E 02 3.417E=03 3.256E=02 6.509E 01 3.112E=01 4.304E 02 3.417E=03 3.257E=02 6.529E 01 1.619E 00 4.320E 02 3.417E=03 3.257E=02 6.529E 01 1.619E 00 4.320E 02 3.358E=03 2.56E=02 6.932E 01 4.694E 00 4.547E 02 3.285E=03 2.56E=02 6.912E 01 3.812E 00 4.547E 02 3.285E=03 1.284E=02 6.912E 01 3.812E 00 4.547E 02 3.285E=03 1.284E=02 7.067E 01 3.779E 00 4.652E 02 3.285E=03 1.284E=02 7.263E 01 4.606E 00 4.713E 02 3.137E=03 7.513E=03 7.263E 01 4.606E 00 4.713E 02 3.107E=03 6.329E=03 7.263E 01 4.606E 00 4.713E 02 3.107E=03 6.329E=03 7.353E 01 3.822E=03 4.713E 02 3.102E=03 6.344E=03 7.353E 01 3.822E=03 4.736E 02 3.102E=03 6.344E=03 7.466E 01 1.271E 00 4.749E 02 3.102E=03 6.344E=03 7.466E 01 1.271E 00 4.777E 02 3.102E=03 6.344E=03 6.442E 01 1.328E 00 4.827E 02 3.039E=03 7.264E=03 8.442E 01 1.328E 00 4.827E 02 3.039E=03 7.264E=03 8.442E 01 1.328E 00 4.827E 02 3.039E=03 7.264E=03 8.442E 01 1.328E 00 4.827E 02 3.039E=03 5.999E=03 8.728E 01 4.528E 00 4.827E 02 3.039E=03 5.999E=03	5.625E 01	3.309E 00	3.438E 02	2.874E=03	3.211E-02
5.681E 01 2.757E 00 3.491E 02 3.313E=03 2.7764E=02 5.773E 01 2.248E 00 3.513E 02 3.309E=03 2.776E=02 5.776E 01 7.372E 00 3.595E 02 3.308E=03 2.426E=02 6.079E 01 2.112E 01 3.911E 02 3.277E=03 3.137E=02 6.221E 01 1.356E 01 4.046E 02 3.277E=03 3.137E=02 6.467E 01 2.246E 01 4.046E 02 3.293E=03 3.258E=02 6.505F 01 2.993E 00 4.301E 02 3.337E=03 3.125E=02 6.505F 01 2.993E 00 4.301E 02 3.337E=03 3.250E=02 6.509E 01 3.112E=01 4.304E 02 3.417E=03 3.250E=02 6.509E 01 1.619E 00 4.304E 02 3.417E=03 3.250E=02 6.529E 01 1.619E 00 4.304E 02 3.417E=03 3.250E=02 6.529E 01 1.321E 01 4.492E 02 3.358E=03 2.318E=02 6.529E 01 1.321E 01 4.499E 02 3.340E=03 2.066E=02 6.539E 01 4.694E 00 4.499E 02 3.340E=03 2.066E=02 6.439E 01 4.826E 00 4.547E 02 3.221E=03 1.2264E=02 7.067E 01 3.81E 00 4.547E 02 3.221E=03 1.140E=02 7.067E 01 3.779E 00 4.652E 02 3.157E=03 7.313E=03 7.263E 01 4.439E 00 4.652E 02 3.157E=03 6.3249E=03 7.278E 01 4.696E 00 4.717E 02 3.102E=03 6.3249E=03 7.353E 01 3.82E=03 4.719E 02 3.102E=03 6.3249E=03 7.353E 01 3.82E=03 4.736E 02 3.102E=03 6.344E=03 7.368E 01 1.328E 00 4.736E 02 3.102E=03 6.344E=03 7.486E 01 1.271E 00 4.776E 02 3.102E=03 6.344E=03 8.442E 01 1.328E 00 4.821E 02 3.085E=03 7.264E=03 8.442E 01 1.328E 00 4.821E 02 3.085E=03 7.264E=03 8.442E 01 1.328E 00 4.821E 02 3.085E=03 7.264E=03 8.442E 01 1.328E 00 4.821E 02 3.085E=03 7.264E=03 8.442E 01 1.328E 00 4.821E 02 3.085E=03 7.264E=03 8.442E 01 1.328E 00 4.821E 02 3.085E=03 1.006E=02	5.045E 01	1,287E 00	3.456E 02	2.836E=u3	2.690E=02
\$\ 678E 01	5.681E 01 5.703E 01	2.757E 00	3.491E 02	3.3136-03	2.754E=02
6-221E 01 1-356E 01 4-046E 02 3-264E=03 3-063E=02 6-467E 01 2-246E 01 4-271E 02 3-293E=03 3-256E=02 6-505F 01 2-993E 00 4-301E 02 3-337E=03 3-195E=02 6-509E 01 3-112E=01 4-304E 02 3-417E=03 3-257E=02 6-529E 01 1-619E 00 4-320E 02 3-417E=03 3-257E=02 6-695E 01 1-321E 01 4-452E 02 3-358E=03 2-318E=02 6-695E 01 4-694E 00 4-499E 02 3-340E=03 2-066E=02 6-91E 01 3-81E 00 4-585E 02 3-245E=03 1-536E=02 6-91E 01 3-81E 00 4-585E 02 3-245E=03 1-140E=02 7-067E 01 3-779E 00 4-652E 02 3-157E=03 8-179E=03 7-110E 01 1-439E 00 4-652E 02 3-157E=03 8-179E=03 7-263E 01 4-606E 00 4-713E 02 3-107E=03 6-329E=03 7-278E 01 4-606E 00 4-713E 02 3-107E=03 6-329E=03 7-353E 01 1-987E 00 4-736E 02 3-102E=03 6-349E=03 7-353E 01 1-827E 00 4-736E 02 3-102E=03 6-349E=03 7-486E 01 1-271E 00 4-749E 02 3-114E=03 6-344E=03 7-486E 01 1-271E 00 4-776 02 3-146E=03 9-146E=03 8-442E 01 1-328E 00 4-821E 02 3-039E=03 8-442E 01 1-328E 00 4-821E 02 3-039E=03 1-006E=02	5.878E 01	1.125E 01	3.700E 02	3.408E=03	1.5558#02
6.505F 01 2.993E 00 4.501E 02 3.337Em03 3.195Em02 6.509E 01 3.112Em01 4.304E 02 3.419Em03 3.250Em02 6.529E 01 1.619E 00 4.320E 02 3.417Em03 5.257Em02 6.695E 01 1.321E 01 4.452E 02 3.417Em03 5.257Em02 6.695E 01 4.694E 00 4.4499E 02 3.358Em03 2.056Em02 6.839E 01 4.823E 00 4.547E 02 3.287Em03 1.536Em02 6.911E 01 3.812E 00 4.985E 02 3.245Em03 1.536Em02 7.972E 01 2.881E 00 4.614E 02 3.221Em03 1.140Em02 7.067E 01 3.779E 00 4.652F 02 3.157Em03 8.179Em03 7.210E 01 1.439E 00 4.652F 02 3.137Em03 7.313Em03 7.2623E 01 4.606E 00 4.713E 02 3.107Em03 6.283Em03 7.2623E 01 4.606E 00 4.713E 02 3.105Em03 6.283Em03 7.353E 01 3.822Em03 4.736E 02 3.105Em03 6.283Em03 7.353E 01 3.822Em03 4.736E 02 3.102Em03 6.344Em03 7.466E 01 1.271E 00 4.749E 02 3.102Em03 6.344Em03 7.466E 01 1.271E 00 4.749E 02 3.102Em03 6.344Em03 7.466E 01 1.271E 00 4.777E 02 3.108Em03 7.264Em03 6.402Em03 6.344Em03 6.402Em03 6.344Em03 6.402Em03 6.402Em03 6.544Em03 6.402Em03 6.544Em03 6.402Em03 6.544Em03 6.402Em03 6.544Em03 6.402Em03 6.4	6.551E 01	1.356E 01	4.046E 02	3.264E=03	3.003Em02
6.529E 01 1.619E 00 4.320E 02 3.417E=03 3.257E=02 6.695E 01 1.321E 01 4.4952E 02 3.358E=03 2.318E=02 6.629E 01 4.694E 00 4.499E 02 3.340E=03 1.536E=02 6.639E 01 4.823E 00 4.585E 02 3.245E=03 1.284E=02 6.9972E 01 2.881E 00 4.614E 02 3.221E=03 1.144E=02 7.067E 01 3.779E 00 4.652E 02 3.157E=03 8.179E=03 7.110E 01 1.439E 00 4.652E 02 3.157E=03 7.513E=03 7.263E 01 4.606E 00 4.713E 02 3.107E=03 6.349E=03 7.353E 01 4.606E 00 4.713E 02 3.107E=03 6.349E=03 7.353E 01 4.6987E 00 4.736E 02 3.102E=03 6.349E=03 7.353E 01 3.822E=03 4.736E 02 3.102E=03 6.349E=03 7.466E 01 1.271E 00 4.749E 02 3.111E=03 0.999E=03 7.771E 01 2.791E 00 4.807E 02 3.102E=03 6.349E=03 6.161E 01 3.029E 00 4.807E 02 3.085E=03 7.264E=03 8.442E 01 1.328E 00 4.821E 02 3.039E=03 8.728E 01 4.575E=01 4.827E 02 3.158E=03 1.006E=02	6.505F 01	2.993E 00	4.301E 02	3,337E=03	3.195E=02
6.762E 01 4.694E 00 4.499E 02 3.340E=03 2.066E=02 6.891E 01 4.823E 00 4.547E 02 3.287E=03 1.536E=02 0.972E 01 2.881E 00 4.614E 02 3.241E=03 1.140E=02 7.067E 01 3.779E 00 4.652E 02 3.157E=03 8.179E=03 7.110E 01 1.439E 00 4.066E 02 3.157E=03 7.513E=03 7.263E 01 4.606E 00 4.713E 02 3.107E=03 6.329E=03 7.278E 01 4.049E=01 4.717E 02 3.102E=03 6.329E=03 7.353E 01 3.822E=03 4.736E 02 3.102E=03 6.343E=03 7.486E 01 1.271E 00 4.749E 02 3.111E=03 6.999E=03 7.771E 01 2.791E 00 4.707E 02 3.146E=03 9.140E=03 8.161E 01 3.029E 00 4.821E 02 3.085E=03 7.264E=03 8.442E 01 1.328E 00 4.821E 02 3.085E=03 7.264E=03 8.728E 01 4.575E=01 4.827E 02 3.158E=03 1.006E=02	6.529E 01	1.619E 00	4.320E 02	3.417E-03	3.257E-02
0.972E 01 2.881E 00 4.614E 02 3.221E=03 1.14UE=02 7.067E 01 3.779E 00 4.652F 02 3.157E=03 8.179E=03 7.10E 01 1.439E 00 4.666E 02 3.137E=03 7.513E=03 7.263E 01 4.606E 00 4.713E 02 3.107E=03 6.329E=03 7.278E 01 4.049E=01 4.717E 02 3.105E=03 6.329E=03 7.353E 01 3.822E=03 4.736E 02 3.102E=03 6.343E=03 7.466E 01 1.271E 00 4.736E 02 3.102E=03 6.344E=03 7.471E 01 2.791E 00 4.749E 02 3.111E=03 6.999E=03 7.771E 01 2.791E 00 4.767E 02 3.146E=03 9.140E=03 8.161E 01 3.029E 00 4.821E 02 3.039E=03 8.728E 01 6.575E=01 4.827E 02 3.158E=03 1.006E=02	6.839E 01	4,823E 00	4.499E 02	3.287E-03	
7.110E 01 1.439E 00 4.666E 02 3.137E=03 7.513E=03 7.263E 01 4.606E 00 4.713E 02 3.107E=03 6.329E=03 7.278E 01 4.049E=01 4.717E 02 3.105E=03 6.283E=03 7.353E 01 1.987E 00 4.736E 02 3.102E=03 6.343E=03 7.353E 01 3.822E=03 4.736E 02 3.102E=03 6.343E=03 7.466E 01 1.271E 00 4.749E 02 3.114E=03 6.99E=03 7.771E 01 2.791E 00 4.749E 02 3.146E=03 9.140E=03 8.161E 01 3.029E 00 4.807E 02 3.085E=03 7.284E=03 8.442E 01 1.328E 00 4.821E 02 3.039E=03 8.728E 01 6.575E=01 4.827E 02 3.138E=03 1.006E=02	0.972E 01	2.881E 00	4-614E 02	3.2216-03	1.14UE-02
7.278E 01 4.049E 01 4.717E 02 3.105E 03 6.283E 03 7.353E 01 1.987E 00 4.736E 02 3.102E 03 6.343E 03 7.353E 01 3.822E 00 4.736E 02 3.102E 03 6.344E 03 7.486E 01 1.271E 00 4.749E 02 3.111E 03 6.949E 03 7.771E 01 2.791E 00 4.749E 02 3.146E 03 9.140E 03 8.161E 01 3.029E 00 4.807E 02 3.085E 03 7.284E 03 8.442E 01 1.328E 00 4.821E 02 3.039E 03 5.969E 03 8.728E 01 6.575E 01 4.827E 02 3.158E 03 1.006E 02	7.110E 01	1.439E 00	4.6666 02	3.137E=03	7.513E=03
7.353E 01 3.82REM03 4.736E 02 3.102E003 6.344E003 7.466E 01 1.271E 00 4.749E 02 3.111E003 6.999E003 7.771E 01 2.791E 00 4.777E 02 3.146E003 9.140E003 8.161E 01 3.029E 00 4.807E 02 3.085E003 7.224E003 8.442E 01 1.328E 00 4.821E 02 3.039E003 5.969E003 8.728E 01 6.575E001 4.827E 02 3.138E003 1.006E002	7.278E 01	4.049E-U1	4.717E 02	3.105E=03	6.283En03
8.161E 01 3.029E 00 4.807E 02 3.085E=03 7.284E=03 8.442E 01 1.328E 00 4.821E 02 3.039E=03 5.969E=03 8.728E 01 6.575E=01 4.827E 02 3.138E=03 1.086E=02	7.486E 01	1.271E 00	4.736E 02	3.111E=03	0,9596=03
8.728£ 01 6.575E=01 4.827E 02 3.138E=03 1.006E=02	8.161E 01	3.029E 00	4.807E 02	3.0858-03	7,204E=03
	8.728E 01	6.575E=01			

RAMJET PERFORMANCE

2		MANGET FEMORIE			
96	ENGINE PERFORMANCE			INLET	
	CALCULATED THRUST) M 	NGLE OF ATTACK	0.9824 0.0008 EFFICIENCY 0.1008 0.1172 50/ERSUNIC 0.4215 50/886/NIC 0.4215	
	REGENERATIVE-COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST) K	NLET PROCESS EFFICIENCY = INETIC EMERGY EFFICIENCY INETIC EMERGY EFFICIENCY NTHALPY AT PO = SUBSONIC.	SUBSONIC 0.9060 - SUPERSONIC 0.9365 - SUBSONIC 0.8856	(BTU/LBF)
			C	UMBUSTOR	
	NOMENTUM AND FORCES INLET PRICTION DRAG	E	UELWAIR RATIO	1.045 1.000 1.519 1ENTS 0.8426. 0.6750. NCZZLE ICIENT # CS 0.8716	0,7967, 0,7047
	 Stations		FUEL INJEC	TARA	
	- · · · · · · · · · · · · · · · · · · ·				
	NOMINAL COWL LEADING EDGE	v) v) v) v) v)	INJECTORS STATION 1A 40.400 1B 41.292 1C 44.300 2A 48.767 2C 46.755 3A 54.057 3B 56.242 44.792	В С Е	

t = 177.00 sec.

3-3-75

RAMJET PERFORMANCE

SUMMARY REPIRT Ċ \sim A/AC POMIM C IVAC PHI ETAC GAM A NOLWT SONV MACH VEL S VA WIND TUNNEL 0 S 0.000 749.749-3010 673.8(799) 1.2933 28.860 2590 =30.8(98) 1.3988 28.859 993 5.982 5938 1.829 0.10709 27.007 0.9846 5084 9.883 188.3 0.395 409 SPIKE TIP NS 0 4 18.137 3010 673.8(799) 1.2932 28.859 2590 0.600 652.6(779) 1.2950 26.659 2561 0.003 1031 2.085 0.10709 27.007 0.9646 4969 1.716 184.7 0.600 16.352 2941 WIND TUNNEL 0.000 749.749 3010 673.8(799) 1.2933 28.860 2590 *31.81 98) 1.3988 28.859 988 6.015 5942 1.829 0.10463 26.385 0.9846 4969 9.662 188.3 0.382 405 0.000 SPIKE TIP MS 0.000 18,137 3010 673.8(799) 1.2932 28.859 2590 653.7(780) 1.2953 28.859 2563 0.391 1003 2.085 0.10463 26.385 0.9846 4969 1.631 188.3 0.600 16.444 2944 INLET THROAT 40.40n 280.338 2974 662.8(789) 1.2945 28.859 2575 16,379 1490 239,9(369) 1,3494 28,859 1861 2,472 4600 1,893 0,94454 27,007 0,1116 4330 67,523 160,3 40.400 INLET UPNESK 280.338 2974 662.8(7g9) 1.2945 28.859 2575 40.400 14.058 1432 224.6(354) 1.3527 28.859 1827 2.564 4683 1.893 0.85868 27.007 0.1228 4373 62.490 161.9 40.400 INLET DANRSK 40.400 123,419 2974 662,8(789) 1,2945 28,859 2575 631.7(788) 1.2977 28.859 2533 0.493 1248 1.949 0.85868 27.007 0.1228 4373 16.659 161.9 40.400 105.720 2870 COMBUSTOR 279,681 2974 662,8(789) 1,2945 28,859 2575 40.410 240,3(370) 1.3493 28.859 1862 2.470 4598 1.893 0.94443 27.007 0.1116 4329 67,484 160.3 40,410 16.399 1491 COMBUSTOR 0 9 2965 2965 41 298 660.1(786) 1.2947 28.859 2572 278.6(408) 1.3417 28.859 1943 2.248 4369 1.908 0.94636 27.007 0.1114 4208 64.259 155.8 41.298 18.950 1634 COMBUSTOR 0 10 41.363 219.836 2964 659,9(786) 1.2948 28.859 2571 19.166 1645 281.6(411) 1.3412 28.859 1949 41.363 2.232 4351 1.909 0.94683 27.007 0.1114 4199 64.022 155.5 COMBUSTOR 41.500 212.566 2962 659.3(785) 1.2948 28.859 2571 287.8(417) 1.3401 28.859 1962 2.197 4312 1.911 0.94761 27.007 0.1113 4179 63.498 154.7 41.500 19.628 1668 COMBUSTOR 0 12 42,460 187,501 2948 654,91 781) 1,2953 28,859 2565 42.460 - 21.036 1742 308.1(437) 1.3366 28.859 2003 2.080 4166 1.918 0.93926 27.007 0.1123 4102 60.806 151.9 COMBUSTOR 0 13 44.083 177.132 2918 645,9(772) 1,2962 28.859 2553 20.441 1735 306.1(435) 1.3369 28.859 1999 2.062 4123 1.919 0.90713 27.007 0.1162 4070 58.126 150.7 44.0A3 COMBUSTOR 0 14 44.310 176.084 2913 644.6(771) 1.2963 28.859 2551 20.434 1735 306.0(435) 1.3370 26.859 1999 2.059 4116 1.919 0.90543 27.007 0.1165 4064 57.914 150.5 44.310 COMBUSTOR 0 15 44.798 172.830 2904 641.9(768) 1.2966 28.859 2547 20.518 1739 307.2(436) 1,3368 28.659 2001 2.045 4093 1.919 0.90189 27.007 0.1169 4050 57.364 150.0 44.798 COMBUSTOR 0 16 44.800 172,806 2904 641,9(768) 1,2966 28,859 2547 20.512 1739 307.1(436) 1.3368 28.859 2001 2.045 4093 1.919 0.90170 27.007 0.1169 4050 57.353 150.0 44.800 COMBUSTOR 0 17 10 46,260 157,895 2881 634,8(761) 1,2973 28,859 2537 46,260 19.611 1743 308.3(438) 1.3366 28.859 2003 2.018 4042 1.923 0.84934 27.007 0.1241 4016 53.352 148.7 COMBUSTOR 0 18 11 47.310 145.506 2865 630.1(757) 1.2978 26.859 2531 47.310 18.287 1738 306.6(436) 1.3368 28.859 2001 2.010 4022 1.927 0.79041 27.007 0.1334 4001 49.401 148.1

4206 20,221 155.8

GAMMA MOUNT SONV MACH VEL S מ אוצמא TVAC 2HT ETAC 4/4 2414 COMMUSTOR 0 19 12 4 47.323 145.348 2865 630.01 757) 1.2978 28.859 2531 47.323 16.253 1737 306.7(4tm) 1.3368 28.859 2000 2.011 4022 1.927 0.78924 27.007 0.1356 4001 44.335 148.1 COMBUSTOR 0 20 13 48,110 137.781 2854 626.7(753) 1.2982 28.859 2526 48.110 16.767 1716 301.0(430) 1.3378 26.859 1989 2.030 4037 1.929 0.73657 27.007 0.1432 4004 46.213 148.2 COMEL STOP n 21 14 48.773 132.803 2846 624.21 751) 1.2984 28.859 2523 40,773 14,882 1675 289,9(419) 1.3397 28,659 1966 2.080 4090 1.931 0.67851 27,007 0.1554 4026 43,130 149.1 COMBUSTOR 0 22 15 49.303 130.167 2840 622.41 749) 1.2986 28.859 2520 49.30% 15,419 1636 279.3(409) 1.3416 28.659 1945 2.131 4144 1.932 0.63457 27.007 0.1662 4049 40.862 149.9 COMPUSTOR 0 23 16 50,713 121,900 2826 618,3(745) 1,2991 28,859 2515 50.713 10.654 1560 258.6(388) 1.3495 28.859 1902 2.230 4241 1.935 0.54083 27.007 0.1950 4092 35.646 151.5 COMBUSTOR 0 24 17 52.813 110.705 2809 613.21 700) 1.2996 28.659 2508 52.813 8.106 1481 237,5(367) 1.3499 28.859 1856 2.357 4336 1.940 0.44327 27.007 0.2379 4133 29.867 153.0 COMMUNICAL 0 25 18 53.312 109.330 2805 612.1(739) 1.2997 28.859 2506 53.313 7.619 1460 231.90 361) 1.3511 28.899 1843 2.366 4362 1.940 0.42515 27.007 0.2480 4145 28.817 153.5 COMBUSTOR 0 26 10 54.063 107.049 2800 610.6(738) 1.2999 28.859 2504 6.996 1432 224.8(354) 1.3527 28.859 1827 2.405 4394 1.941 0.40077 27.007 0.2631 54.063 4160 27.365 154.0 COMMUNTOR 0 27 20 54.823 104.422 2795 609.2(736) 1.3000 28.839 2502 54.823 6.476 1410 218.9(348) 1.3539 28.859 1814 2.436 4419 1.942 0.37898 27.007 0.2782 4171 26.026 154.4 COMMUSTOR 0 28 21 100,968 2790 607.6(735) 1,3002 28,859 2500/ 55.76n 55.760 5.953 1389 213.3(343) 1.3552 28.859 1801 2.467 4442 1.944 0.35556 27.007 0.2966 4181 24.546 154.8 Corevetor 0 29 22 56.248 87.347 2788 607.0(734) 1.3003 28.859 2499 56.24A 4.589 1346 202.1(331) 1.3578 28.859 1775 2.536 4501 1.954 0.28657 27.007 0.3679 4211 20.045 155.9 COMBUSTOR 0 30 23 56.30% 87.261 2788 606.9(734) 1.3003 28.859 2499 56,303 4,573 1345 201.8(331) 1.3579 28.859 1774 2.538 4502 1.954 0.28581 27.007 0.3689 4211 19.997 155.9 0 31 24 COMBUSTOR 86,928 2787 606,7(734) 1,3003 28,859 2499 56.441 4.528 1343 201,2(330) 1,3580 28,859 1772 2,542 4505 1,954 0,28371 27,007 0,3717 56.444 4212 19.862 156.0 COMBUSTOR 0 32 25 4 56.521 88,112 2787 606,6(734) 1,3003 28,859 2499 56,523 4.575 1341 200.8(330) 1.3561 28.859 1772 2.544 4506 1.953 0.28704 27.007 0.3673 4213 26.101 156.0 COMBUSTOR 0 33 26 5 56 801 88.266 2786 606.3(733) 1.3003 28.859 2498 4.541 1337 199.8(359) 1.3583 28.859 1769 2.549 4510 1.453 0.28594 27.007 0.3688 56.60 4214 20.040 156.1 COMBUSTOR 0 34 27 57.029 88.472 2785 606.0(733) 1.3004 28.859 2498 57.029 4.520 1335 199.1(328) 1.3585 28.859 1767 2.553 4513 1.952 0.28545 27.007 0.3694 4216 20.018 156.1 COMBUSTOR 0 35 28 57.75% 88,227 2782 605.1(732) 1,3005 28,859 2496 51.752 4.410 1325 196.66 326) 1.3591 28.859 1762 2.567 4521 1.952 0.28097 27.007 0.3753 4219 19.741 156.2 COMBUSTOR 0 36 29 58.773 88,483 2778 604.0(731) 1.3006 28.859 2495 N 58.772 4.351 1317 194.6(324) 1.3595 28.859 1757 2.576 4526 1.952 0.27918 27.067 0.3777 4220 19.637 156.3 COPBUSTOR 0 37 30 CD 60.783 99,518 2772 602,3(729) 1,3008 28,859 2492 60.783 4.555 1326 196.9(326) 1.3590 26.659 1762 2.556 4504 1.950 0.28890 27.007 0.3650

A/AC MOPTH O GAMMA HOLAT SONV MACH VEL S */A * IVAC PHI ETAC 0 38 31 5 COMBUSTOR . CD 62,201 96.222 2769 601.3(728) 1.3009 28.859 2491 CO 62.203 4.728 1335 199.1(324) 1.3585 26.859 1768 2.538 4486 1.949 0.29673 27.007 0.3553 4196 20.687 155.4 COMBUSTOR 0 39 32 5 64,667 82,924 2763 599,5(727) 1,3011 28,859 2489 64.667 4.557 1348 202.66 332) 1.3577 28.659 1776 2.509 4456 1.955 0.28126 27.007 0.3749 4176 19.479 154.7 COMBUSTOR 0. 40 33 3 76.765 2762 599.21 726) 1.3011 26.859 2488 65.043 65.043 4.245 1350 203.1(332) 1.3576 28.859 1777 2.505 4452 1.960 0.26148 27.007 0.4032 4176 18.092 154.6 NOZZLE AE 41 34 3 87.279 76.765 2762 599.2(726) 1.3011 28.859 2488 87.279 0.384 697 38.9(168) 1.3945 28.859 1298 4.091 5295 1.960 0.05443 27.007 1.9371 4635 4.479 171.6 NOZZLE PV 42 35 3 87.279 76.765 2762 599.2(726) 1.3011 28.859 2488 0.395 703 40.3(170) 1.3943 28.859 1299 4.070 5288 1.960 0.05548 27.007 1.9005 4631 4.560 171.5 87.279 FICTIVE COMBUSTR 62 55 0 65.043 280,338 2762 599,2(726) 1,3011 28,859 2488 65.043 0.395 486 #12.2(117) 1.3991 28.859 1083 5.109 5531 1.871 0.08387 27.007 1.2572 4770 7.209 176.6 FICTIVE NOZZLE 63 56 0 87.279 194,614 2734 590,9(71A) 1,3020 28,859 2476 87.279 0.246 466 =17.1(112) 1.3991 28.859 1060 5.206 5516 1.893 0.05443 27.007 1.9371 4752 4.666 176.0

	READING = 0	0069 BFUCK	= /1	TTNF = 177.00#	NVCH	5. 0	PT # 7	49.749 11 = 3	0 <u>1</u> 0_1				PAGE 4
	XAFS	P=18	P≖ds	PhA	aox		- 1)=[R	R ≠NP	CANALL	P+18/P50	P=19/P10	P#05/P80	P=08/P10
	6.9R1E=01	1.0806 30	0.000	-4.4216-01	0.000		0.000	0.000	2.470E=02	2./355 00	1,0401=03	0.000	0.000
	1,8366 01	1,000 00	0.000	-3.595E 01	0.000		ሳልዕዕቀ	0.000	1.634E 02	2.735t 00	1,440k=03	0.000	0.000
	3.070F 01	2.300E 00	0.000	#1,730£ 02	0.000		0.000	0.000	5.053£ va	5.824F 00	3.06PE+03	0.000	0.000
	3.508F 01	3,934E 00	0.000	#3,750E 02	0.000		0.000	0.000	6.804E 02	9.9636 00	5.2486.03	0.000	0.000
	3.518E 01	3.948E 00		00 -4.4095 05	0.000		0.000	0.000	6.849E 02	9,999F (0	5,264F-03	1.476F 01	7.773E+03
	3.519E 01	3,9496 00		00 -4.4106 05	0.000		0.000	0.000	6.851L 02	1.000F 01	5.2678-03	1.467E 01	7.726E-03
	3.555F 01	0,000E 00		00 -4.4915 05			0.000	0.000	7.2151 02	1.0135 01	5.335E-03	9.235F 00	4.4598-03
	3.5P5F 01	3,964E 00		00 #4.639£ 02					7.523L 02	1 40041 01	5.288E-03	4.685F 00	2.467E=03
	3.606E 01	3.940E 00 4.246E 00		00 ~4.752E 02 00 ~4.950E 02					7.7368 02	9.9776 00	5.255t+03	6.939E NO	3.655E-03
	3.701E 01	4.570E 00		0n -5.210E 02					8.174E 02 8.731E 02	1.075E 01 1.157E 01	5,663E=03 6.095E=03	1.151E 01 1.728E 01	6.063E+03 9.101E+03
	3.7316 01	4.350E 00		00 =2.3346 05					9.057E 02	1.1025 01	5.802F=03	2.058# 01	1.0845-02
	3,803F 01	3.830E 00		01 45,4818 02					9 841E 02	9.6998 00	5.108E=03	3.446€ 01	1.8158-02
	3,8338 01	5.369E 00		01 -5.4595 02					1 018E 03	1.360E 01	7.161E=03	4.033E 01	2.1246+02
	5.875F 01	7,489E 00		01 -5.4668 02					1.1656 03	1 896E 01	9,968E=03	3.926E 01	2.068E=02
	3.889E 01	7.757E 00		01 =5.4686 02					1.071E 03	1 964E 01	1 035E=62	3.912E 01	2.061E=02
	3.901F 01	8.810E 00		01 -5.0676 02					1.0956 03	2.231E 01	1.175t=02	3.970E 01	2.091E-02
	3.931E 01	1.332E 01		01 -5.514E 02					1.1296 03	3.374E 01	1.7778-02	4.055E 01	2.136E-02
	3.950F 01	1.611E 01	1.168E	01 -5.597E 02	-2.486F	0.2	-1.756E	02 -7.293E 01	1.151E 03	4.080E 01	2.149E=02	2.9582 01	1.558E+02
	3.980E 01	1.696E 01		00 -5,828E 02					1.186E 03	4.294E 01	2.262E=02	1.184E 01	6.235E-03
	4.000F 01	1.751E 01		00 #6.01SE 05					1.209E 03	4.434E 01	2.335E+02	1.137E 01	5,989E=03
	4.040E 01	2.050E 01		00 =6,411E 02					1.256E 03	5,191F 01	2.734E#02	1.042E 01	5.490E=03
	4.041E 01	2.057E 01		00 -6.420E 02					1.258E 03	5.210E 01	2.744E=02	1.040E 01	5.478E+03
	4.130E 01	2.721E 01		00 -7.461E 02					1.363E 03	6.891E 01	3.6306-02	8.297E 00	4.370E=03
	4.136F 01 4.150E 01	2.770E 01 2.872E 01	3.216F	00 =7.544E 02	=3.771E	50	#2.484E	02 =1.287E 02	1.370E 03	7.014E 01	3,6956-02	8.143E 00	4.289E=03
	4.246E 01	9.937E 00		00 07.7218 02					1.387E 03	7.274E 01	3,831E=02	9.442E 00	4.973E=03
	4,408F 01	1.506E 01		00 =8.318E 02 01 =8.351E 02					1.502E 03 1.698E 03	2.5178 01	1.325E=02	1.8538 01	9.761E=03
	4.431E 01	1.578E 01		01 =8,363E 02						3.814E 91 3.996E 01	2.009E=02 2.104E+02	3.390E 01	1.786E+02
	4.480E 01	1.732E 01	1.2255	01 -8.424E 02	-A.428F	0.5	-/- 180F	A3 #8. 430E 02	1.785E 03	4.386E 01	2.310E=02	3.299E 01 3.103E 01	1.7385.02
	4.480F 01	1.732E 01		01 -8,423E 02					1.785E 03	4.387E 01	2.311E-02	3.102E 01	1.634E=02 1.634E=02
	4.626E 01	1.646E 01		00 -8,5100 02					1.965E 03	4.169E 01	2.1966=02	2.516E 01	1.3256+02
	4.731F 01	1.584E 01		00 #8.500E 02					2.095E 03	4.012E 01	2.1136-02	2.094F 01	1.103E=02
	4.732F 01	1.576E 01		00 #8 497E 02					2.0966 03	3 992E 01	2.102E-02	2.089E 01	1.1008-02
ORIGIN	4.811E 01	1.080E 01	9.499E	00 a8.351E 02	-1.273E	0.3	-5.604E	02 -7.124E 02	2.195E 03	2.735E 01	1,440E-02	2 405E 01	1.2676-02
නු	4.877E 01	1.055E 01	1.055£	0; -8.038E 02	#1.340E	03	-5.855E	02 47.547F 02	2.2786 03	2.6728 01	1.4078-02	2.6728 01	1.407E=02
Ω	4.930E 01	1 . 139E 01		01 =7.735E 02						2.885E 01	1.519E=02	2.885E 01	1.519E-02
J	5.0718 01	4.6508 00	4.650E	00 =1.145E 05	=1.501E	03	-6.531E	02 =8.480F 02	8.522E 03	1.178E 01	6.20ZE=03	1.178E 01	6.202E=03
S	5.28 E 01	5.5628 00		00 =6.5258 02						1.652E 01	8.753E=Q3	1.662E 01	8.753E=03
=	5,331E 01	5,857E 00		00 =6,363E 02					2.8528 03	1,483E 01	7.8132-03	1,483E 01	7.813E=03
	5,406E 01 5,482E 01	4.904E 00 3.937E 00		00 -6.155E 02					2.947E 03	1.242E 01	6.541E=03	1.242E 01	6.541E=03
₹	5.576E 01	3.334E 00	3673/6	00 =5.984E 02	-1.740E	0.5	#/# DAYE	02 *4.742K 02	3.045E 03	9.971E 00	5.252E=03	9.971E 00	5.252E-03
5	5.625F 01	3.020E 00		00 -5.813E 02 00 -5.494E 02					3.185E 03	8.443E 00	4 447E 03	8.443E 00	4.4476-03
5	5.630F 01	1.462E 00		00 #5.4856 02					3,209E 03	7.647F 00	4.028E=03	7.647F 00	4.0285=03
بنيا س	5.604E 01	1.462E 00	2.894F	00 =5.466E 0P	#1.812F	03	97.991F	02 91.0115 03	3.234E 03	3.704E 00	1.9516=03	7.558E 00	3.981E=03
3	5.0928 01	2.843E 00		00 -5.455E 02					3.245E 03	7.199E 00	1.9516=03 3.792E=03	7.329E 00 7.199E 00	3.860E#03
	5.680E 01	5.06SE 00		00 a5.419E 02					3.280E 03	64742E 00	3.551E-03	6.742E 00	3.792E=03 3.551E=03
	5.703F 01	2.851E 00		00 =5.392E 02					3.309E 03	7.244E 00	3.615E-03	7.244F 00	3.815E=03
	5.7758 01	3.495E 00	3.495F	00 m5.306E 02	≈1.855E	03	-8.167E	02 -1.039E 03	3.402E 03	8,850F 00	4.60ZE-03	8.850E 0U	4.662E=03
	5.877F 01	3.712g 00		So 3555.ce no					3.532E 03	9.401F 00	4.952E=03	9.401E 00	4.952E=03
	6.078F 01	1,500E 00	1.500E	00 =5.216E 02	•1.933E	03	.B.428E	02 =1.090F 03	3.790E 03	3,798F 00	2.001E-03	3.798F 00	2.0016-03
	6.220E 01	1.631E 00	1.631F	00. #2*519E 05	-1.958F	03	-8-521F	02 -1.106F 03	3.972E 03	4.131E 00	2.176E-03	4.131E 00	2.176E=03
ಬ	6.467E 01	2.706E 00	2.706F	00 -5.216E U2	-2.007F	0.3	*8.722E	02 -1.135F 03	4,289E 03	6.853E 00	3.610E-03	6.853F 00	3.610E=03
	6.50aF 01	4.275E uo	2.870F	00 -5.2168 02	-2.016F	43	-8.757E	02 #1.140F 03	4.337E 03	1.083F 01	5.702E=03	7.269E 00	3.828E-03
jeend	6.508F 01	4.275E 00	5.888E	00 #2.51PF 05	-2.01/E	0.3	48.761E	02 -1.1015 03	4.342E 03	1.083E 01	5.702F=03	7.313E 00	3.8528=03

XABS	P#18	P=0F	PDA	© 0 X	Q≈IR	ଡ⇔ባይ ~	CAWALL	PalbyPBO	P#IR/PIO	P#08/P80	P=08/P10
6.52AE 01	4.001E 00	2.975F 0n	-5.216E 02	#2.021E 05	-8.780E 02	1 -1 -1 4 3F 03	4,36AE 03	1.0138 01	5.337E-03	7.574E 00	3,968E+03
6.694E 01	1.730E 00					1 #1.165E 03	0.583E 03	4.381E 00	2.3076-03	1.590E 01	8.376E=03
6.76gE 01	1.528E 00	4.147E 00	-4.08PE 02	=2.070F 03	-9.951E 02	-1,175E 03	4.665E 03	3.866F 00	2.037t=u3	1.050F 01	5.532E-03
6.838E 01	1.295E UN	3.043E 00	#3.437E 02	=2.087E 03	₩8.991E 02	-1.188F 03	4.760E 03	3,279F 00	1,7276=03	7.706E 00	4,059E+03
6.910F 01	1.384E 00	2.0106 00	-2.953E 02	#2.103E 03	#9.023E 02	-1.201E 03	4.84BE 03	3.506E 00	1.846L-03	5.090E 00	5.681E=03
6.971E G1	1,460E 00	1.973E 00	₩2,587E 02	-2.117E 03	#9.046E 02	* #1.212E 03	4.922E 03	3.697£ 00	1.947E=03	4.996F 00	2.631E=03
7.066F 01	1.302E 00					-1.231F 03	5,036E 03	3.296E 00	1.736E=03	4,849E 00	2.554E-03
7.109E 01	1,230E 00					1.238F 03	5.08AE 03	3.115E 00	1,6416=03	4.374E 00	2.304E≠03
7.262F 01	1.216F 00					1.260E 03	5.273E (3	3.090F 00	1.6226=03	2.684E 00	1.410E=03
7.277E 01	1.215E 00					=1.262F 03	5,290E 03	3.0776 00	1.6216=03	2.777E 00	1.4638-03
7.352E 01	1.116E 00					1.272E 03	5.374E 03	2.826E 00	1.488£=03	3.241E 00	1.707E=03
7.353E 01	1.115E 00					! =1.272E 03	5.375E 03	2.424E 00	1.48AE-03	3.244E 00	1.709E=03
7.485E 01	9.400E=01	- 0.000				1.294E 03	5.427E 03	2.380E 00	1.2546-03	0.000	0.000
7.770F 01	9.600E=01	0.000				-1.294E 03	5.525E 03	2.431E 00	1.280E#03	0.000	0.000
8.160E 01	1,245E 00	0.000	3,177E 01	-5.553E 03	-9.290E 02	1.294F 03	5.630E 03	3.153E 00	1.661k=03	0.000	0.000
8,441F 01	1,1756 00	0.000				! =1.294E 03	5.6848 03	2.975E 00	1.567E-03	0.000	0.000
8,727E 01	1.290E 00	0.000				1.294E 03	5.707E 03	3.267E 00	1.721E=03	0,000	0.000
8.728E 01	1.590E 00	0.000	8.840E 01	-5.540E 03	=9.456E 02	-1.294F 03	9,707E 03	3.267E 00	1.721E=03	0.000	0.000

Y		DORAG	CURAG		CF	нс
4,040F	0.1	1.165E 02	1.1655	ج 0	2.247E=03	4.462E=02
4.0415	91	1.792E=01	1.1679	0.5	5.24RE=03	4.465F=02
4,13nE	01	1.598E Q1	1.326F	60	2.373E=03	4.7985=02
4.136E	01 01	1.180E 90 2.494E 09	1.338g	0 S	2.382E=03 2.402E+03	4.824E=02 4.850F=02
4.2465	חו	1.7366 01	1.537F	0.5	7.4628-03	4.999F=02
4.40AE	01	2.879E 01	1.825#	02	2.467E=03	4.837E=02
4.4316	01	3.950E 00	1.8646	ج ٥	2.470E=03	4.834E=02
4.480E	0.1	8.494E UO	1.949F	0.5	2.481E+03	4.8306.02
4.480E	01	3.920E=02 2.474E 01	1.949g 2.197=	20 S	2.481E+Q3	4.635E=02
4.731E	01	1.675E 01	2.364F	0 2	2.5076=03	4.280E=02
4.732E	0 i	1.835€=01	2.366E	ő	2.5068-03	4.273F=02
4.811F	0.1	1.174E 01	2.484E	02	2.4996=03	3.967F=02
4.877E	01	9,210E 00	2.5765	0.5	2.47PE=03	3,601E=02
4.930E 5.071F	01 01	6.864E 00	2.844E	0.5	2,445E+03	3.316E=02 2.740E=02
5.28(F	01	2.0598 01	3.014E	0 g 0 g	2.331E-03	2,1696#02
5.331E	01	4.344E 00	3.058€	02	2.315E-03	2,061E=02
5.406F	01.	6.203E 00	3.120E	0.5	2.294E-03	1.919E-02
5.482E	01	5.941E 00	3-179E	0.5	2.2775=03	1.7965-02
5.5768	01	6.911E 00 2.205E 00	3.248g	02	2.261E#03 2.217E#03	1.669E=02 1.312E=02
5,630E	01	3.127E=01	3.2748	0.5	2.216E=03	1.308E=02
5,644F	01	7.847E=01	3.281F	چ ٥	2.215E=03	1.2975-02
5.652E	01	4.5238-01	3.286E	0.5	2.2088=03	1.308E=02
5.680E 5.703E	01	1,579E 00	3.302E	95	2.202E=03	1.2998=02
5.7756	61	1.270E 00 4.036E 00	3.3558	0 2 0 2	2,197E=03 2,186E=03	1.293E+02
5.877E	01	5.614E 00	3.4115	0 ב	2.177E=03	1.250E=02
6.078F	0.1	1.119E 01	3.5232	02	2.179E+03	1.245E=02
9.550E	01	8-119E 00	3.604F	0.5	2.179E=03	1.3326-05
6.467E	01	1.393E 01 2.015E 00	3.743E	0.5	2.210E*03	1.283E.02
6.50gE	01	1.987E=01	3.766E	05	2.227E=03	1.075E=02
6.528E	01	9.399E=01	3.7758	20	2.221E=03	1.054E=02
6.694E	0.1	9.164E 00	3.857€	چ٥	2.238E=03	1.143E=02
6.76jE	01	2.904E 00	3.886E	0.2	2.171E=03	8.975E=03
6.638E	01	2.778E 00 2.181E 00	3,913F 3,935g	02 02	2,120E=03 2,074E=03	7,310E=03 6,056E=03
6.971E	01	1.696E 00	3.9525	0 >	2.073E=03	6.1025=03
7-056F	Ç.	2.572E 00	3.978F	02	2.0586-03	5.796E-03
7.109E	01	1.112E 00	3.989	و 0	2.043E=03	5.433E=03
7.262F	01	3.515E 00	4.024F	0 >	1.9958.03	4.438F=03
7.277E 7.352E	01	3,015E=01 1.503E 00	4.0275	05 20	1.996E#03	4.49UE=03
7.353E	01	2.914E=03	4.042F	95	1,9996-03	4.608E.03
7.485E	01	8.602E=01	4.0515	چ٥	1.954€=03	3.816F=03
7.770E	01	1.500E 00	4.066E	9	1.946E=03	3.857E=03
8-160E	01	1.759E 00	4.0837	و 0	1.9776+03	4.672E=03
8.441F	01	9.711E=01 4.068E=01	4.093E	ეგ ეგ	1,958t #03 1,965E #03	4.448E=03
8 728E	0.1	0.000	4.097#	0 2	1.965E=03	4.756F=03
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RAMJET PERFORMANCE

		RAMJET PE	REUPHONTE			
304	ENGINE PERFORMANCE			INLET		
# *	CALCULATED THRUST		AASS FLOW MATIC ACCITIVE DRAG (LIMITING PRESS) OFLIA PIZAAAAA	COVERY & SLPENSINIC	0.9846 0.0006 7, 0.1623	
	REGENERATIVE CODEFD FOGINE PERFOR CALCULATED STREAK THRUST	MANCE 0. (LBF) 0. (LBF) 0. (LBF=SEC/LBM)	TOTAL PRESSURE INLET PROCESS ! INLET PROCESS ! KINETIC ENERGY KINETIC ENERGY ENTHALPY AT PO	PETOVERY = SUBSCNIC EFFICIENCY = SUPERSONI EFFICIENCY = SURSCNIC. FFFICIENCY = SUPERSON FFFICIENCY = SUBSCNIC = SUPERSONIC	0.1646 0.8892 0.9035 10 0.9035 10 0.8936 0.8936	(BTU/LRM) (BTU/LBM)
				COMPUSTUR		
	INLET MOMENTUM CHANGE	540. (LBF)	EQUIVALENCE HA' COMBUSTOR EFFIT TOTAL PRESSURE COMBUSTOR EFFE INJECTOR DISCH VACHUM STREAM NOZZLE CCEFFIC PROCESS EFFICI	TIO	0.000 0.2738 0.6853	
	, STATIONS			FUEL INJECTORS		
	SPIKE THANSLATION	u.884 (IN) 0.400 (IN) 5.187 (IN) 3.527 (IN) 7.279 (IN) 6.443 (IN) 5.043 (IN)	INJECTORS 1A 1B 1C 24 2C 3A 3H	8TATION 40.400 41.288 44.300 48.763 46.250 54.053 56.238 44.788	VALVE	

t = 198.60 sec.

		76.76	- 73	(twie ,	≖ yγn _a g:	VM 1451	۱ و ۲			EUBWYWI E130		J [®] L		3	- s-	15		1
ಚ							S (I	м н д	r y	R F	9 0 F T							
6		Ť	H		GAMI A	ϻՈ <mark>Լ</mark> ΨΤ	SUMA	MALH	VFL	s	./4	₩	4/45	10414	r	TVAC	PhI	ETAC
	WIND TUNNEL	1	Ú 5						-									
	0.000 748.750				1.2956													
		393	⇒34.7 €	95)	1.3986	28.859	973	6,020	5859	1.821	0.10671	27,053	0.9898	5023	9.716	185.7		
	SPIKE TIP NS	2	0 5										-		-			
	0.600 18.087		651.36	777)	1.2955	28,859	2560											
	0.600 16.340	5869	631.20	758)	1,2977	26.654	2533	0,396	1002	2.078	0.19671	27.053	0.9248	4940	1.642	184.5		
	*INC TUNNEL	3	0 0						_		-		•					
	0.000 748.750	2936	651.31	777)	1.2956	28,860	2560											
	0.000 0.379	392	=35.0(9/1)	1.3986	28,859	972	6.031	5860	1.821	0.10584	26.831	0.9898	4983	9.638	185-7		
	SPIKE TIP NS	4	0 0		•								• . •					
	0.600 18.087	2936	651,3(777)	1.2955	28.859	2560											
	0,600 16.392	2870	631.66	758)	1.2976	28.859	2533	0.392	992	2.078	0.10584	26.831	0.9898	4983	1.632	185.7		
	INLET THROAT	5	0 4					•	-				•		• • • • • • •	• - • •		
	40,400 258,444	2889	637.10	764)	1.2971	28,859	2541											
	40.400 16.781	1481	237.7(367)	1.3498	28,859	1856	2.409	4471	1.890	0.94576	27.053	0.1117	4239	65.709	156.7		
	INLET UPNRSK	ь	0 3						-		•	- •	• , .			• • •		
	40.400 258.444	2889	637.16	764)	1.2971	28.859	2541											
	40.400 14.380	1423	222.3(352)	1.3532	28.859	1821	2.501	4556	1.890	0.85978	27.053	0.1228	4283	60.878	156.3		
	INLET DMNRSK	7	0 4				•	•		- •			• • • • •					
	40,400 120,543	2889	637.21	7641	1.2971	28.859	2541											
	40.400 102.812	2785	606.11	7335	1.3004	28,859	2498	0.499	1247	1.942	0,85978	27.053	0.1228	4283	16.662	158.3		
	COMBUSTOR 0	8	1 21		•	•					-		• • • •					
	40.410 216.664	2853	638,91	784)	1,2993	27.679	2580											
	40.410 12.515	1414	216,21	344)	1.3549	27.679	1855	2,479	4599	1.967	0,94880	27.143	0.1117	4238	67.812	156.1	0.11	0.07
		9	2 21										• . •		. •	• • • • •		
	41.286 165.554	2790	641.9(7941	1.3028	26.577	2607											
	41.286 15.674	1564	266.86	4217	1.3481	26.577	1986	2.182	4332	2.044	0.95410	27.232	0-1114	4114	64.239	151-1	55.0	0.04
	COMBUSTOM 0	10	3 21							. •	- ,,-					• • •		•
	41.296 172.825	2750	641.91	782)	1.3047	26.535	2593											
	41.296 15.710	1255	267.36	410)	1.3507	26,535	1962	2,206	4330	2.036	0,95441	27.232	0.1114	4113	64.219	151.0	0.22	0.01
	COMBUSTOR 0	11	4 21						•				• • • • •		•			· -
	114 9 4 T 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	~																

171,583 2743 641.7(780) 1.3050 26,529 2590 41.361 41.361 15.945 1526 270.4(4(1) 1.3505 26.529 1965 2.193 4310 2.036 0.95447 27.232 0.1114 4103 63.932 150.7 0.22 0.00 COMBUSTOR 0 12 5 21 41.500 167.679 2741 641.2(780) 1.3051 26.528 2589 41.500 16.924 1556 279.9(420) 1.3489 26.528 1985 2.143 4253 2.038 0.95504 27.232 0.1113 4082 63.116 149.9 0.22 0.00 COMBUSTOR 0 13 6 21 42,460 136,666 2729 637,5(776) 1,3055 26,528 2584 42.460 13:549 1543 275.6(416) 1.3496 26.528 1976 2.154 0255 2.052 0.94611 27.232 0.1124 3992 62.563 146.6 0.22 0.00 COMBUSTOR 0 14 44.081 134.750 2705 629.07 768) 1.3062 26.530 2573 44.081 25.343 1800 350.26 491) 1.3377 26.530 2124 1.758 3734 2.050 0.91426 27.232 0.1163 3916 53.057 103.8 0.22 0.00 COMBUSTOR 0 15 8 3 44.310 131.246 2715 627.6(771) 1.3056 26.546 2577 44.310 26.723 1844 358,7(504) 1.3358 26.545 2148 1.708 3667 2.053 0.91292 27.232 0.1165 3901 52.032 103.3 0.22 0.02 COMBUSTOR 0 16 44.796 121-129 2774 624-5(789) 1-3028 26-618 2598 44.796 29.650 1978 376.7(543) 1.3299 26.618 2216 1.589 3521 2.064 0.90908 27.232 0.1170 3868 49.738 142.0 0.22 0.08 COMBUSTOR 0 17 10 2 44.800 121.018 2775 624.4(789) 1.3028 26.619 2599 44.800 29.674 1979 376.9(544) 1.3298 26.619 2217 1.587 3519 2.064 0.90888 27.232 0.1170 3868 49.708 142.0 0.22 0.08 0 18 11 3 COMBUSTOR 46.260 115.174 2721 614.91 773) 1.3048 26,594 2576 46.260 26,986 1916 365,57 525) 1.3325 26,594 2185 1.617 3532 2.062 0.85612 27.232 0.1202 3808 06,990 101.3 0.22 0.06

GAMMA MOLHT BONY MACH VEI S IVAC PHI ETAC wlb AJAT KILKTH G COMPUSTOR 0 19 12 4 41.310 110.472 2802 008.1(796) 1.3009 26.701 2605 47.310 25.057 1963 347.3 (538) 1.3296 26.701 2204 1.659 3612 2.072 0.79676 27.252 0.1334 3910 00.731 103.7 0.22 0.15 0 20 13 COMBUSTOR 47.321 110.219 2806 608.1(798) 1.3007 26,706 2607 47.321 25.125 1969 347.6 (500) 1.3293 26.706 2207 1.636 3610 2.073 0.79616 27.232 0.1335 3915 00.666 103.8 0.22 0.15 COMBUSTOR 0 21 14 99-643 2995 603-3(885) 1.2918 26,926 2673 48.114 48.110 26.175 2190 349.27 604) 1.3188 20.926 2310 1.544 3566 2.095 0.74252 27.232 0.1472 3978 41.149 146.1 0.22 0.34 COMBUSTOR 0 22 15 48.774 102.611 2921 599.7(832) 1.2951 26.857 2646 48.771 20.696 1998 311.1(506) 1.3266 26.858 2215 1.716 3800 2.086 0.68417 27.232 0.1554 4040 40.399 148.3 0.22 0.28 ROTEURHOR 0 23 16 3 49.301 106.199 2859 596.9(813) 1.2978 26.800 2624 49.30i 17.204 1847 283.3 (502) 1.3330 26.800 2137 1.853 3961 2.079 0.63986 27.232 0.1662 4085 39.391 150.0 0.22 0.23 0 24 17 COMBUSTOR 50.711 95.351 2975 590.5(848) 1.2922 26.947 2663 50.711 14.587 1905 257.1(518) 1.3292 26.947 2162 1.890 4085 2.095 0.54534 27.232 0.1950 4186 34.619 153.7 0.22 0.36 COMBUSTOR 0 25 18 114,178 2769 583.0(785) 1,3014 26,749 2588 52.811 52.811 8.437 1458 185.0(389) 1.3522 26.749 1914 2.331 4462 2.065 0.44697 27.232 0.2379 4291 30.997 157.6 0.22 0.19 COMBUSTOR 0 26 19 53.311 123.700 2704 581.4(766) 1.3042 26.686 2563 53.311 7.317 1338 169.7(356) 1.3596 26.686 1841 2.466 4539 2.053 0.42870 27.232 0.2480 4307 30.242 158.2 0.22 0.14 COMBUSTOR 0 27 20 108.961 2786 \$79.3(790) 1.3005 26.780 2593 54.061 54-061 7.408 1438 170.1(383) 1.3530 26.780 1900 2.381 4525 2.069 0.40411 27.232 0.261 4329 28.417 159.0 0.22 0.22 COMBUSTOR 0 28 21 54.821 96.927 2869 577.3(815) 1.2966 26.876 2623 7.500 1540 170.77 4.23 1.3465 26.877 1958 2.303 4510 2.084 0.38215 27.232 0.2782 4352 26.786 159.8 0.22 0.30 54.821 ROTAUBMOR 0 29 22 55.760 97.613 2853 575.0(810) 1.2972 26.867 2617 55.760 6.682 1482 157.1(395) 1.3498 26.867 1920 2.377 4573 2.082 0.35848 27.232 0.2966 4378 25.476 160.8 0.22 0.29 COMBUSTOR 0 30 23 68.984 3049 573.9(649) 1.2881 27.084 2685 56.246 5.259 1722 162.71 462) 1.3354 27.085 2058 2.208 4536 2.122 0.28891 27.232 0.3680 4429 20.366 162.6 0.22 0.47 56.244 COMBUSTOR 0 31 24 56.301 108.504 2719 573.8(770) 1.3033 26.728 2568 4.212 1204 120.1(3(8) 1.3672 26.728 1750 2.722 4764 2.063 0.28815 27.232 0.3690 4431 21.335 162.7 0.22 0.17 56.301 COMBUSTOR 0 32 25 36.441 108,982 2718 573,5(770) 1,3033 26,727 2567 56,441 4-151 1197 118-50 316) 1.3676 26.726 1745 2.734 4772 2.063 0.28608 27.232 0.3717 4434 21.214 162.8 0.22 0.17 COMBUSTOR 0 33 26 21 56.521 44.196 3597 573.3(1037) 1.2594 27.720 2850 6.019 2315 155.7(632) 1.3057 27.732 2328 1.904 4571 2.181 0.28928 27.232 0.3675 4436 20.550 162.9 0.22 1.00 56.521 COMBUSTOR 0 34 27 21 56.801 43.962 3595 572.8(1036) 1.2595 27.720 2850 5.775 2294 149.8(626) 1.3065 27.732 2318 1.985 4603 2.181 0.28832 27.232 0.3688 4441 20.623 163.1 0.22 1.00 56.801 COMBUSTOR 0 35 28 21 57.627 43.853 3594 572.4(1036) 1.2595 27.720 2849 57,027 5.029 2281 145.4(622) 1.3070 27.732 2312 1.999 4622 2.181 0.28768 27.232 0.3693 4445 20.680 163.2 0.22 1.00 COMBUSTOR 0 36 29 21 57.751 42.867 3590 571.1(1035) 1.2596 27.720 2848 57.751 5.160 2244 134.2(611) 1.3083 27.732 2294 2.038 4676 2.182 0.2831 27.232 0.3753 4454 20.587 163.5 0.22 1.00 COMBUSTOR 0 37 30 21 58,771 42.355 3566 569.5(1033) 1.2598 27.720 2846 58.771 4.912 2221 127.2(604) 1.3091 27.732 2283 2.000 4704 2.183 0.28151 27.232 0.3777 4057 20.581 163.7 0.22 1.00

GAMMA MOLAT SONV MACH VEL S 4/4 AZAC FORTE G IVAC PHI ETAC COMBUSTOP CO 0 38 31 21 ─ 60.781 22,048 3577 567,2(1030) 1,2583 27,718 2841 CD 60.781 1.575 1974 53.2(530) 1.3184 27.731 2160 2.348 5072 2.229 0.29131 27.232 0.3650 4440 22.961 163.0 0.22 1.60 COMBUSTOR 0 39 32 21 42,581 3575 565,7(1030) 1,2603 27,721 2843 62.201 62.201 4.894 2209 123.41 600) 1.3096 27.732 2277 2.066 4704 2.181 0.29920 27.232 0.3553 4027 21.874 162.6 0.22 1.00 0 40 33 21 COMBUSTUR 64.665 45.598 3565 562.1(1026) 1.2609 27.721 2839 04.005 5.739 2461 26c.9(AB3) 1.2999 27.732 2404 1.753 4216 2.175 0.28361 27.237 c.3749 4407 16.582 161.8 0.22 1.00 COMBUSTOR 0 41 34 200 65.041 42.295 3563 561,6(10p6) 1,2608 27,721 2838 65.041 10.450 2629 253.17 728) 1.2948 27.732 2470 1.590 3928 2.181 0.26367 27.232 0.0032 4005 16.096 161.8 0.22 1.00 COMBUSTOR REGEN 42 35 3 65.041 42.295 3801 646.5(1103) 1.2500 27.710 2920 65.041 9.950 2795 300,0(780) 1.2889 27.731 2542 1.624 4128 2.204 0.26367 27.232 0.4032 4521 10.914 166.0 0.22 1.00 NOZZLE AE 03 36 U 87 . 277 42.295 3563 561.6(1018) 1.2608 27.721 2838 87.277 0.718 1371 -120.2(357) 1.3486 27.732 1821 3.208 5841 2.181 0.05489 27.232 1.9371 5300 4.982 194.6 0.22 1.00 NOZZLE PO 44 37 4 42.295 3563 561,6(1018) 1,2608 27.721 283A 87.277-87.277 0.383 1163 =177:1(300) 1.3617 27.732 1685 3.608 6080 2.181 0.03596 27.232 2.9566 5436 3.398 199.6 0.22 1.00 NOZZLE AE REGEN 45 38 4 42.295 3801 646.5(1103) 1.2500 27.710 2920 87.277 87.277 0.769 1515 -79.96 397) 1.3401 27.732 1908 3.160 6029 2.204 0.05489 27.232 1.9371 5484 5.143 201.4 0.22 1.00 NOZZLE PO REGEN 46 39 4 87.277 42.295 3801 646.5(1103) 1.2500 27.710 2920 87.277 0.383 1266 -149.1(328) 1.3551 27.732 1754 3.597 6310 2.204 0.03428 27.232 3.1014 5645 3.362 207.3 0.22 1.00 FICTIVE COMBUSTR 66 59 0 65.041 258,444 3567 561,6(1027) 1,2640 27,726 2844 65.041 0.383 709 .296.4(180) 1.3867 27.732 1328 4.934 6552 2.051 0.06356 27.232 1.6727 5710 6.472 209.7 0.22 1.00 FICTIVE MOZZLE 67 60 0 87.277 28.107 3533 551.4(1016) 1.2611 27.721 2827 87.277 0.876 1585 -60.1(417) 1.3362 27.732 1949 2.839 5531 2.207 0.05489 27.232 1.9371 5117 4.718 187.9 0.22 3.00

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¥	ARS	Pa18	Perm	PDA	юüх	U=18	Ģ 	ωB	CAMALL	PHTE/PS6	F=18/PT0	PmOR/PSQ	P+QP/PT0
6.	981E=01	1.0808 00	0.000	a4.405E=01	0.000	0.000	0.0	0.0	2,470£#02	2,817E 00	1,047E=03	(. 0 ^ 0	0.000
	836E 01	1.080F 00	0.000	-3.595E U1	0.000	0.000	0.0		1.6348 02	2.81/6 00	1,4428-03	0.000	0.000
	070E 01	2.295E 00	0.000	-1.72RE 02	0.000	0.000	0 0		5.053E 02	5,9865 00	3.065E-03	0.000	0.000
	508E 01	3.946E 00	0.000	m3.750£ 02	0.000	0.000	0 0		6.804E 02	1.029F 01	5.270E=03	0.000	0.000
	518E 01	3.960E 00	•	-4.392E 02	0.000	0.000	Ú . Ó		6.848E 02	1.053E 01	5.2696-03	1.476E 01	7.559E=03
	51 AE 01	3.961E 00		1 -4.392E 02	0.000	0.000	0.0		6.851E 02	1.033E 01	5.290E=03	1.4678 01	7.514E=03
	555E 01	0.015E 00		0 -4.48ne 02	0.000	0.000	0.0		7.2176 12	1.04/F 01	5.3626-03	9.275E 00	4.749E=03
	585F 01	3.971g 00		-4.629£ 02					7.522E 02	1.036F 01	5.3038.03	4.8258 00	2.471E=03
	505E 01	3.940E 00		1 -4.7442 02					7.736E 02	1.078E 01	5.2626-03	7.174E 00	3.674E=03
	648E 01	4.259E 00		-4.943E 02					8.1746 02	1.1116 01	5.688E-03	1.189E 01	6.089E-03
	701E 01	4,380E 00		5.189E 02					8.733E 02	1.142E 01	5.850£-03	1.784E 01	9.1386-03
	731E 01	#.230E 00		5.303E 02					9.056E 02	1.103E 01	5.649E=03	2.122E 01	1.087E-02
	803E 01	3.870E 00		n +5.5646 02					9.842E 02	1.0098 01	5.169E-03	2.088F 01	1.069E=02
	833F 01	5.424E U0		±5.655€ 02					1,018E 03	1,415F 01	7,244E+03	2.074E 01	1.0626-02
	875E 01	7.5888 00		-5.784E 02					1,065E 03	1.979E 01	1.013E-02	3.801E 01	1.946E=02
	880F 01	7.850F 00		-5.788E 02					1.071E 03	2.048€ 01	1.048E-02	4.010E 01	2.053E-02
-	9012 01	8.930E UO		-5.791E 02					1.095E 03	2.3295 01	1.1938-02	4.074F 01	2.086E-02
	931E 01	1.3322 01		-5.842E 02					1,129E 03	3.474E 01	1,779E=02	4.167E 01	2.134E-02
	950E 01	1.607E 01		-5.924E 02					1,151E 03	4-193E 01	2.1476-05	3.034E 01	1.554E-02
	980E 01	1.696E 01		-6.1486 02					1.186€ 03	4.483E 01	2.2656-02	1.232E 01	6.311E=03
	DOOF OL	1.754E 01		9 46.339E 02					1.210E 03	4.575F 01	2.343E+02	1.182E 01	6.053E=03
	040E 01	2.081E 01		-6.741E 02					1.257E 03	5,429E 01	2.78CE-02	1.081E 01	5.536E+03
	041E 01	2.089E 01		0 06.750€ 02					1.258E 03	3.450E 01'		1.079E 01	5.523E=03
	120E 01	2.806E 01		50 380A.7.					1.361E 03	7.319E 01	3.748E=02	8.576E 00	4.392E=03
	1305 01	2.014E 01		-7.821E 02					1.362E 03	7.340E 01	3.759E-02	8.551F 00	4.379E-03
	136E 01	2.8676 01		-7.907E 02						7.479E 01	3,830E=02	8.387E 00	4.295E+03
	150E 01	2.081E 01		-8.092E 02						7.776F 01	3.982E-02	1.053E 01	5.391E-03
	246E 01	1.740E 01		9818E 02						4.530E 01	2.324E#02	2.530E 01	1.295E=02
	408E 01	3.143E 01	1.926F 0	₽9.290E 02	-7.946E 0	2 -5 0176	02 =2 9	30E 02		6.197F 01	4.197E+02	5.023E 01	2.5726-02
	4312 01	3.341E 01	2.0000	69.395€ 02	-8 323F 0	2 -5.2076	02 93.1	16E 02	1.726E 03	8.714E 01	4-4625-02	5.226E 01	2.676E+02
	480F 01	3.761E 01		-9.650E 02						9.811E f1	5.024E=02	5.656F 01	2.896E-02
	480E 01	3.765E 01		=9.6526 02						9.820E 01	5.128E-02	5.660E 01	2.898E=02
	626E 01	2.733E 01		-9.622E 02						7.127E 01	3.649E=02	6.951E 01	3.559E=02
	731E 01	1.990E 01		#8.805E 02						5.190E 01	2,658E=02	7.8BOE 01	4.035E=02
	732E 01	2.000E 01		-8.794E 02						5.217E 01	2.6716#02	7.890E 01	4.040E=02
	SilE 01	2.730E 01		#8.049E 02						7.121E 01	3.646E=02	6.534E 01	3.346E-02
	877F 01	2.070E 01		-7.344E 02						5,398E 01	2.764E=02	5.398E 01	2.764E-02
4.	930F'01	1.720E 01		50 3058.0m						4.4878 01	2.290E-02	4.487E 01	2.298E=U2
5.	071F 01	1.459E 01	1.459F 0	-5.645E 02	-1.840F 0	3 -1.023E	03 .8.1	63E 02	2,921E 03	3.605E 01	1.948E-02	3.805E 01	1.94BE=02
5.	281E 01	8.437E 00	8.4372 00	-4,378E 02	-2.046E 0	3 -1.139E	03 =9.0	69E 02	2.788E 03	2.201E 01	1.127E+02	2.201E 01	1.127E+02
5,	331E 01	7.317E 00	7.317E 00	g a4.173£ 02	-2.088E 0	3 at:163E	5.90 20	42F 02	2.852E 03	1.9098 01	9.773E=03	1,909E 01	0.773E=03
5,	406E 01	7.408E 00	7.408E 00	n ≃3.888E 02	-2.146E 0	3 01.197E	03 09.4	92E 02	2.947E 03	1,932E 01	9.894E=03	1,932E 01	9.894E=03
5.	482E 01	7.500E 00	7.500E 00	0 -3,599E 02	-2,201E 0	3 -1.228E	03 49.7	36E 02	3.045E 03	1.956E 11	1.002E=02	1.956E 01	1.002E-02
5.	576E 01	00 358Ao	6.682F 0	03.265E 02	-2.264E 0	3 -1.2628	03 -1.0	02E 03		1.743E 01	8.924E@03	1.743E 01	8.924E#03
5.	625E 01	6.2592 00	6.2598 00	0 -2.731E 02	-2.293E 0	3 -1.276E	03 =1.0	17E 03	3.209E 03	1.6326 01	8,359t=03	1.632E 01	8.359E=03
5,	630E 01	2.212E 00	6.211E 0	0 42.714E 02	≈2.296E 0	3 =1.2788	03 -1.0	18E 03	3.216E 03	5.771F 00	2.9556003	1.620E 01	8,295E=U3
5.	644E 01	5*515E 00	6.089E 0(0 02.6738 02	#2.304E 0	3 01.282E	03 -1,0	55E 03	3,234E 03	5.771E 00	2.955E-03	1.588E 01	8,132E=03
5.	652E 01	6.019E 00	6.019E 0	0 m2.649E 02	-2.308E 0	3 -1.284E	03 =1.0	25F 03		1.570F 01	0.039E#03	1.570E 01	8,0392=03
	680E 01	5.775E 00		0 #2.572E 02						1.506E 01	7.7138 = 03	1.506E 01	7.713E-03
7. 1	703E 01	5.629E 00		0 -2.517E 02						1.468F 01	7.517E=03	1.4682 01	7.517E-03
	775F 01	5.160E 00		0 -2.3702 02						1.346E 01	6.891E=03	1.346E 01	6.891E=03
	877E 01	4,912E 00		0 =2.254E 02			-			1.281E 01	6.561E=03	1.281E 01	6.561E#03
	078E 01	1.575E 00		U 45.546E 05						4-108E 00	2.1048#03	4.10BE 00	2.104E-03
	220E 01	4.8948 00		0 -5.546E 05						1.276E 01	6.536E=03	1.276E 01	6.536E=03
	466E 01	8,739E 00		U -5 546E 05						2.279E 01	1.1678-02	2.279E 01	1.167E-02
6.	504E 01	1,159E 01	9.325F 0(0 =5.546E 05	-2.631E n	3 -1.401E	03 -1.2	30F 03	4.337E 03	10 3520°F	1.548E=02	2.432E 01	1.245E=02

XABS	P-19	P=ng s	YOO AGS	0=IP	Ե⇔пե	CAWALL	P-TH/PSO	P=18/PT0	P#06/P80	P#CR/PT0
6.508E 91	1.1598 01	9.388F 00 =2.	. 246t 02 =2.633E	03 -1.402E 0	3 #1.231F 03	4.342E 03	3.0224 01	1.5486-02	2.449F 01	1.2546-02
6.52AE 01	1.090E 01	9.7000 00 -2.	-246E 02 -2.641E	03 -1-405E 0	3 -1,2378 03	4 368E 03	5 444E C1	1.4566-02	2.530E 01	1.2956-02
6 694F 01	5.230E 00	5.490F 0n +1.	.364F 02 -2.697F	03 -1.425E 0	3 #1,271F 03	4.583E G3	1.364E 01	6.985t=03	1.562E 01	A*000E=03
6.761E 01	3.485E 00	3.0828 00 -4.	.639E 01 -2.712E	03 -1.431E 0	3 -1.281F 03	4.665E 03	9,090F 00	4.6552#03	₽.040€ ∩0	0,117E-03
6.838F 01	1.480E 00	3.055E 00 2.	.974E 01 -2.730E	03 =1.437E 0	3 -1.293F 03	4.760E U3	3,860F 00	1.977£#03	7,969E 00	4.081E=03
6.910E R1	1.515E 00	3.030F 00 8.	.624E 01 =2.752E	03 -1.441E 0	3 -1.311E 03	4 848E 03	3.952E 00	2.0246-03	7.9038 00	4.047E=03
6.971F 01	1.545E 00	2.913E 00 1	.336E 02 -2.772E	03 -1 -444E 0	3 =1.328F 03	4.922F 03	4.030E 00	2.063E+03	7.5978 00	3.890E=03
7.066F 01	1.363E 00	2.7308 00 1.	.990E 02 -2.801E	03 -1 -44AE 0	3 #1.350F 03	5.036E 03	3.554E 00	1_820E#03	7.121F 00	3.646E=03
7.109E 01	1.280E 00	2.465E 00 2.	.258r 02 =2.813E	03 -1.449E 0	3 -1.364E 03	5 0888 03	3,339€ 00	1.7106+03	6.428F 00	3.292E=03
7.262E 01	1,2398 00	1.520E 00 3.	.014E 02 -2.843E	03 =1.453E 0	3 #1.390E 03	5.2/3E 03	3.232E 00	1,655E=03	3.965E 00	2.030E=03
7.277E 01	1,235g 00	1.483F 00 3,	.073E 02 -2.846E	03 =1.453E 0	3 -1.392 F 03	5,290£ 03	3,221F 00	1.649E+03	3.8678 00	1.980E-U3
7.352E 01	1.148E 00	1.2958 00 3,	,520E 02 -2.858E	03 =1.455E 0	3 =1.403E 03	5.374E U3	2.995E 00	1.5346-03	3.378E 00	1.730E=U3
7.352E 01	1.148E 00	1,294F 00 3,	.545E 02 =2.856E	03 =1.455E A	13 =1.403E 03	5.375E 03	5.994E 40	1.5336-03	3.375F 00	1.728E=03
7.485F 01	9.950E=01	U.000 3,	.771F 02 =2.884E	03 =1.458E 0)3 =1.426E 03	5.427E 03	2.5958 00	1.3296+03	0.000	0.000
7.770E 01	9.850E=01	0,000 4,	.167E 02 -2.889E	03 -1.463E 0	3 w1.426F 03	5.525E 03	2.569E 00	1.3166-03	0.000	0.000
8.160E 01	1.290E 00		.653E 02 -2.895E			5,630E 03	3.365E 00	1.723E-03	0.000	0.000
8.441E 01	1.185E 00	0.000 4	.928E 02 =2,900E	03 -1.473 E 0	13 -1. 426E 03	5.684E 03	3.091F 00	1.583E=03	0.000	0.000
8.727E 01	1,320E 00		.230E 02 -2.909E			5.707E 03	3.443E 00	1.7635-03	0.000	0.000
8.728E 01	1,320E 00	v.000 5.	.231E 02 =2.909E	03 -1.482E 0)3 -1. 426E 03	5.707E 03	3.444E 00	1.763E=03	0.000	0,000

×	DORAG	CDRAG	CF	HC
4.049F 01 4.041E 01	1.112E 02	1.112F 02 1.114F 02	2.260F=03 2.526E=03	4.4936=02 3.511F=02
4.129E 01	1.777E 01	1.292E 02	2.670E+03	4.076E=02
4-130E 01	1.923E=01	1.2948 02	2.4596-03	4.327E=02
4,136F 01 4,150E 01	1.213E 00 2.573E 00	1.306F 02	2.433F=03 2.448E=(3	4.401F=02 4.570E=02
4.246E 01	1.789E 01	1.5118 02	2.508E=03	3.798E=02
4.408F 01	7.871E 01	1.79bE 02	2.557E+03	5.5000-02
4.431E 01 4.480E 01	3.749E 00 7.812E 00	1.835F 02 1.913E 02	2.570E=03	5.724E=02 5.975E=02
4.480F 01	6.240E-02	1.914E 02	2.6516=03	5.889E=02
4.626E 01	10 3868.2	2.104F 02	2.6476-03	5.455E=02
4,731E 01 4.732E 01	1.561E 01 1.527E=01	2.300g 02 2.301£ 02	2.579E = 03 2.646E = 03	5.241E=02 5.136E=02
4.811E 01	1.113E 01	2.413E 02	2.627E=03	5.217E=02
4.8778 01	8,957E 00	5.205£ 05	2.686E=03	4.333E=02
4.930g of 5.071g of	7.010E 00	2.572E 02 2.739F 02	2.600E=03 2.485E=03	3.889E=02 3.471E=02
5.281E 01	2.1602 01	2.9556 02	2.4598-03	2.278E=02
5.3316 01	4,616€ 00	3.001E 02	2.272E-03	2.134E-02
5,406E 01 5,482E 01	6.282E 00 6.004E 00	3.064E 02	5.100E=03.	2.167E#02 2.122E#02
5.5765 01	7.232E 00	3.197E 02	2.3178+03	1.900E=02
5,6258 01	2,319E 00	3.220E 02	2.279E=03	1.725E=02
5.630E 01 5.644F 01	3.447E = 01 8.497E = 01	3.233E 05	2.414E=03 2.081E=03	1.245E=02 1.332E=02
5,652E 01	5.222E=01	3.2378 02	2.806E=03	1.443E=02
5.680E 01	2.058E 00	3.258E 02	2,799E=03	10401E=02
5.703E 01 5.775E 01	1.665E 00 5.331E 00	3.274E 02	2.793E=03 2.785E=03	1.289E=02
5.877€ 01	7.487E 00	3.402F 02	2.780E=03	1.2426=05
6,07aF 01	1.629E 01	3.565F 02	3.024E=03	5.187E=03
6,22gE 01 6,466E 01	1.184E 01 1.785E 01	3,6842 02	2.775E=03 2.807E=03	1.8206-05
6.504E 01	2.377E 00	3.886E 02	2.877E=03	1.980E=02
6,5085.01	2.4798=01	3.8888 02	2.935E-03	2.025E=02
6.528E 01 6.694E 01	1.288g 00 9.759E 00	3.901E 02	2.932E-03 2.017E-03	2.005E=02 1.368E=02
6.761E 01	2.921E 00	4.028E 02	2.723E=03	9.430=03
6.838E 01	2.669E 00	4.055£ 02	5.654E-03	7.187E=03
6.910E 01 6.971E 01	2.218E 00 1.855E 00	4.077£ 02 4.096F 02	2.647E=03	7.181E#03 7.073E#03
7,066E 01	2.779E 00	4.123E 02	2.625E=03	6.630E#03
7.109F 01	1.199E 00	4.135F 02	2.609E=03	6.202E#03
7.262E 01 7.277E 01	3.777E 00 3.189E=01	4.1735 02	2.555E≈03 2.551E≈03	4.913E=03 4.855E=03
7.35>E 01	1.504E 00	4.191F 02	2.529E-03	4.4676.03
7.352E 01	2.783E=03	4.1916 02	2.5296-03	4.466E003
7,485E 01 7,770F 01	8.346E=01 1.466E 00	4.200F 02 4.214F 02	2.487E=03 2.477E=03	3.801E=03 3.751E=03
8.160E 01	1.698E 00	4.2318 02	2.502E-03	4.588F-03
8,4415 01	9.293E=01	4.241E 02	2.476E=03	4.2778=03
8,727F 01 Cu 8,728E 01	3.874E×01 0.000	4.245F 02	5.483E=03	4,625E=03 4,625E=03
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RAMJET PERFORMANCE

	•	RAMJET PERI	PARPORMANCE					
212				INLET				
	MEASURED SPECIFIC IMPULSE	(L8F) (L8F) (L8F*SEC/L8M) (L8F*SEC/L8M)	HASS PLOW RATIO. ADDITIVE DRAG COLLIFITING PRESSUR	EFFICIENT E RECOVFRY FFFICIE	NCY 0.1586)		
	CALCULATED THRUST COEFFICIENT		TOTAL PRESSURF P	FCCVERY - SIPERSC! ECOVERY - SUBSCNIC FICTENLY - SUPERSO	****** 0.1610			
	REGENERATIVE=CONLED #NGINE PERFORMANC CALCULATED		INLFT PROCESS EF	FTCTENCY = SURSOLI FFICIENCY = SUPFAS	C 0.9037			
	STREAM THRUST 5295.	(L8F)	KINETIC ENERGY E	FFICIENCY - SIESCH	IC 0.8895			
	MET THPUST	(L8F) (L8F⇔8Fr/L8M)	ENTHALPY AT PO -	SUPERSONIC	#3.59 (BTU/LBM)	t I		
	HOMENTUM AND FORCES			COMBUSTOP	•			
	INLET MOMENTUM CHANGE	(L8F) (L8F) (L8F) (L8F) (L8F) (L8F) (L8F)	EQUIVALENCE RATI COMBUSTOR EFFICI TOTAL PRESSURE R COMBUSTOR EFFECT	Chickers and the second at Insurance and Ins	0.224 1.000 0.1637 0.6138			
	NUZZLE MOMENTUM CHANGE	(L8F)		NOZZLF				
	EXTERNAL FRICTION DRAG	(LBF) (LBF)	NOZZLE COFFFICIEN PROCESS EFFICIEN	HUST COFFFICIENT = NI = CI CY FFICIENCY	0.9062			
	SNOITATE	•		FUEL INJECTORS				
	NOMINAL COML LEADING EDGE 34.88	4 (IN)	INJECTORS	9741104	VALVE			
	SPIKE TRANSLATION	9 (IN)	14	40.400	A			
	INLE! INCOME AND AND AND AND AND AND AND AND AND AND	0 (IN)	18	41,286	8			
	CUML LEADING EDGE	5 (IN)	10	44.300				
		5 (IN) 7 (IN)	24	48.761				
	SINUI LEADING EDGE SA GU	1 (IN)	2C 3A	46,250 54,051				
	STRUT TRAILING EDGE	1 (IN)	38	56,236				
	COMBUSTOR EXIT 65.04	i čivi	4	44.786				
			•					

t = 212.10 sec.

3/03/75

SHKPAPY HPPORT

T RAMMA MOLIT SONV MACH VEL 5 11/4 1/AC MIMON IVAL PHT ETAC WIND TUNNEL 1 0 5 744.999 3054 687.3(812) 1.2920 28.860 2607 0.000 0.000 0.403 419 028.5(101) 1.3989 20.659 1005 5.957 5985 1.833 0.10747 27.008 0.9812 5125 9.995 189.6 SPIKE TIP NS 18.062 3054 687,3(817) 1.2918 28.859 2607 0.600 10.222 2961 664.9(791) 1.2941 28.859 2578 0.410 1057 2.090 0.10747 27,008 0.4612 4964 1.766 185.6 0.600 WIND TUNNEL 0.000 749,999 3054 687.3(8(2) 1.2920 28,860 2607 0.000 0.381 412 -30.1(99) 1.3988 28.859 997 6.012 5991 1.833 0.10332 25.965 0.9812 4931 9.620 189.9 SPIKE TIP NS 18.062 3054 687.3(812) 1.2918 28.859 2607 0.600 16.381 2967 666.9(763) 1.2939 28.659 2580 0.391 1009 2.090 0.10332 25.965 0.0812 0.600 4931 1.620 189.9 INLET THROAT 295,938 2989 467,4(793) 1,2940 28,859 2581 40.400 40.400 15.908 1466 233.7(363) 1.3507 28.859 1847 2.522 4658 1.891 0.94382 27.008 0.1117 4366 68.326 161.6 INLET UPARSK 295.938 2989 667.4(793) 1.2940 28.859 2581 40.400 40.400 15.666 1409 218.7(348) 1.3540 28.859 1813 2.613 4738 1.891 0.85802 27.008 0.1229 4408 63.182 163.2 INLET DNNRSK 40.400 124,508 2989 667,4(793) 1,2940 28,859 2581 40,400 196,960 2887 636.66 763) 1.2972 28,859 2540 0.488 1240 1.950 0.85802 27.008 0.1229 4408 16.535 163,2 COMBUSTOR 248,355 2949 669,5(814) 1,2963 27,635 2622 40.410 40.410 12.875 1427 219.7(368) 1.3541 27.635 1865 2.544 4744 1.970 0.94698 27.102 0.1117 4365 69.814 161.0 0.12 0.07 COMBUSTOR 0 9 2 21 41.284 188,378 2880 672.2(824) 1,3000 26,527 2649 41.284 15.879 1572 269.7(425) 1.3477 26.527 1993 2.252 4488 2.047 0.95282 27.192 0.1114 4246 66.458 156.2 0.23 0.04 COMBUSTOR 0 10 41,294 196.794 2840 672.2(812) 1.3019 26.485 2635 15.913 1530 270.2(413) 1,3503 26.485 1970 2.277 4485 2.040 0.95215 27.192 0.1115 4245 66,363 156.1 0.23 0.01 41.294 COMBUSTOR 0 11 4 21 195.672 2834 671.9(810) 1.3022 26.479 2632 41.359 41.359 16,137 1534 273.1(414) 1.3502 26.479 1972 2.265 4467 2.040 0.95364 27.192 0.1113 4236 66.202 155.8 0.23 0.00 COMBUSTOR 0 12 41.500 191.586 2831 671.3(809) 1.3023 26.478 2631 41.500 . 17.583 1575 285.4(426) 1.3480 26.478 1997 2.201 4394 2.041 0.95363 27.192 0.1113 4215 65.125 155.0 0.23 0.00 COMBUSTUR 0 13 6 21 42.460 172.889 2815 666.2(804) 1.3028 26.478 2624 19.086 1642 304.8(445) 1.3448 26.478 2036 2.089 4253 2.047 0.94422 27.192 0.1124 4144 62.401 152.4 0.23 0.00 42.460 COMBUSTOR 0 14 44,079 119,565 3403 654.3(983) 1,2747 27,163 2818 44.079 39.367 2655 409.0(745) 1.2998 27.166 2513 1.394 3503 2.116 0.91292 27.192 0.1163 4133 49,696 152.0 0.23 0.57 COMBUSTOR 0 15 44.310 117.560 3438 652.2(994) 1.2728 27.211 2828 44.310 40.925 2721 415.7(765) 1.2970 27.214 2539 1.355 3440 2.119 0.91123 27.192 0.1165 4129 48.714 151.8 0.23 0.61 COMBUSTOR 0 16 44.794 113.840 3493 647.3(1010) 1.2698 27.291 2843 44.188 2838 429.7(801) 1.2922 27.296 2585 1.277 3299 2.124 0.90721 27.192 0.1170 4113 46.51/ 151.3 0.23 0.68 44.794 0 17 10 COMBUSTOR 44.800 113.788 3493 647.2(1010) 1.2698 27.291 2843 -44.229 2839 430.0(801) 1.2921 27.296 2585 1.276 3297 2.124 0.90722 27.192 0.1170 4112 46.489 151.2 0.23 0.68 44.800 ro⊬8UgtoR 0 18 11 46.256 106.393 3150 646.7(979) 1.2476 24.845 2849 41.857 2543 434.9(771) 1.3078 24.046 2580 1.262 3255 2.249 0.86148 27.394 0.1242 4102 43,577 149.8 0.48 0.26 46.250

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BEADING Z	0069	erock	Bull off #	B 212.1	C4 .4AC	H 6.	0 PT:	2 749,	999	TT # 305	4,3						
	P	۲	н	GAHMA	MOLWI	SUNA	MACH	VF(s	v / 4	Pi .	A/4C	HUNTH	ព	TVAC	Dat	ETAC
COMBUSTOR		-	12	GATT A	11. H.	JU. 17	· // Q · ·	* 14 L	Ü	,,-	"	4740	. 0. 1.				6174
			646.5(979)	1.2676	24.846	2849											
46.260			434,7(771)				1.262	3255	2.249	0.86097	27.394	0.1242	4103	43.555	109.8	0.48	0.26
COMBILETOR		20	13 4													-	•
			634,2(1029)														
47.310			415.3(8(6)	1.3005	25.043	2633	1.257	3309	2,263	0.80156	27.394	^.1335	4189	41.508	152.9	0,48	0.35
COMBUSTOR		21															
			634.1(1030)														
47.319	40.119		415.21 817)	1.3005	25.045	2634	1.257	3310	5.263	0.80089	27,394	0.1335	4190	01.192	153.0	0.48	0.35
COMBUSTOR		55	and the second s	4 3964	me	2014											
48.110			625.3(1065)					2166	2 272	0 78477	27 100	A 4 (172.72	4270	111 214	154 5	A 410	0. // 1
48.110 COMBUSTOR		2130	385,3(832)	1.24/0	530104	2040	10307	3400	C . C / G	V. /40/2	2/4374	101436	42/7	UP.216	130 12	O # H C	11 9 M 1
48.759			627.0(1051)	1.2866	23.350	29/19											
48.759			362.8(792)					3635	2.380	0-69364	27.573	0.1552	4351	39.188	157.6	0.71	0.25
COMBUSTOR			17 2		J. 10 - 1	u u .		5425	~~~		B . 9 • . –			2.00			
48.769			626,9(1051)	1.2866	23.360	2949											
48.769-			362,2(791)					3639	2.380	0.69274	27.573	0.1554	4352	39.174	157.8	0.71	0.26
COMPUSTUR	0		18 3														
49.299			621.9(1059)														
49.299			329.0(771)	1.3121	23,395	2590	1,478	3828	5.385	0.64788	27.573	0.1662	4425	38,544	160.5	0.71	0,27
COMBUSTOR			19 #		55 (US												
50.709	22 177	3427	610.2(1139)	1.2737	23,040	3029		#010	3 404	A 66344	37 G73	0.4050	4503	74 443			A 74
50,709 Comeustor	*******	27	288.88 826)	1,5050	23.032	2034	19311	4010	E - 400	0.55610	611013	0.1950	4345	34.412	100.0	V . / 1	0.50
52.809			595,8(1219)	1.2413	21.014	2005											
52.809	18.262	2684	226.5(862)	1-2957	21.924	2689	1.599	4299	2.424	0.45256	27.573	0.2379	4797	30.234	174-0	0-71	6-45
COMBUSTOR	0	28	21 4	* 0 111	400,44	200.	• • • • • • • • • • • • • • • • • • • •	- 4 ,		00	W. 421.4	016311	4, , ,			V # 1 4	., 4 2
53.309			592.8(1253)	1.2557	24.023	3121											
53,300			222.2(897)				1.578	4306	2,436	0.43407	27.573	0.2480	4839	29,649	175.5	0.71	0,49
COMBUSTOR		29															•
54.039			588.5(1268)														
54.059			199.6(B96)	1.2900	24.096	2724	1.619	4411	5.440	0.40917	27,573	0.2631	4898	28.049	177.6	0.71	0,51
COMBUSTOR		30															
54.819			584.4(1274)						2 " 4 2	4 50105	~~ ~~~				. = -		
54.819 Combustor		31	175.3(082)	1.2408	24-126	2706	1+8/4	4564	2.442	0.24643	2/10/3	0.2782	4452	27.205	179,6	0.71	0,52
55.760			579.8(12g3)	1 2502	24.144	21/12											
55.760			149.9(872)					4638	2.000	0.36292	27.573	0-2966	5010	26.157	181.7	6.71	0.54
COMBUSTOR			25 5	100.13		E 4.0			4 4	*****	C. 13, 5		2040		10111	V	0 2 3 7
56.244			577,6(1431)	1,2215	24,606	3238											
56.244			155.6(1048)					4596	2.483	0.29263	27,573	0.3679	5153	20,900	186.9	0.71	0.70
COMBUSTOR		33									•	• -					• • •
56-299	61.970	3873	577,4(1297)														
56.299	9,890			1.2944	24,218	2637	1.868	4926	2.453	0.29170	27,573	0.3691	5156	25.330	187.0	0.71	0,55
COMMUSTOR		34															
56,439			576,8(1298)						N 4 P 4								
56,439	9.782			1 . 5484	24.273	2033	1 . 6 / 4	4434	2,455	0.204/6	27,5/3	0,3715	5163	22.239	187.5	0.71	0,55
COMBUSTOR 56.519			28 21 576,5(16#1)	1 1720	25 2A2	1117											
56.519			142.4(1314)				1.519	4661	2.510	0.29205	27.573	0-3695	51 AA	21,219	187.4	0.71	1.00
COMBUSTOR			29 21							- + - · - · >			J. 0.			V 1 / /	
56.799	•		575,4(1641)	1,1730	25,284	3336											
56.799	12.037		130 04 (1304)					4719	2.509	0.29193	27,573	0,3688	5161	21.410	187.9	0.71	1.00
רָסייפּטפּזה#	0	37	30 21 .									· -	* =				
57.025			574.5(1640)											_			
57.025	11.558	3930	117.8(1293)	1.2176	25.563	3051	1,567	4781	2.509	0,29143	27,573	0.3694	5191	21.653	188.3	0.71	1.00

DAMMA POEMT SONV MACH VPL S 1 MIML# 3A1A h/A IVAC POT ETAC COMBUSION (3× 31 2) 57.749 42.794 4619 571.9(1438) 1.1730 25.285 5334 on 57.709 10.020 3845 80.3(1261) 1.2223 25.575 3023 1.641 4959 2.511 0.28686 27.573 0.3755 5213 22,109 189.1 0.71 1.00 0 39 32 21 COMBUSION 58.769 32.996 4793 568.8(1628) 1.1703 25.265 3323 58.769 5.137 3561 -38.4(1154) 1.2366 25.600 2924 1.865 5512 2.531 0.28500 27.573 0.3777 5221 26.417 189.3 0.71 1.00 0 40 33 21 COMBUSTOR 60.779 46.939 4813 563.6(1635) 1.1748 25.302 3333 60.779 16.200 4098 193.071357) 1.2090 25.537 3106 1.387 4306 2.502 0.29495 27.573 0.3650 5205 19.738 186.8 0.71 1.00 0 41 34 21 COMBUSTOR 62.199 47.724 4868 559.0(1634) 1.1754 25.308 3332 62.199 15.525 4650 170.9(1339) 1.2120 25.547 3091 1.427 4411 2.500 0.30295 27.573 0.3553 5193 20.765 188,3 0.71 1.00 FORBUSTOR 0 42 35 200 64.663 45.229 4792 551.7(1627) 1.1755 25,312 3326 64.653 18.325 4186 234.6(1391) 1.2040 25.519 3134 1.271 3983 2.502 0.28716 27.573 0.3749 5173 17.176 187.6 0.71 1.00 COMBUSTOR 0 43 36 200 65.039 41.952 4784 550.3(1624) 1.1748 25.307 3323 18.920 4254 268.8(1417) 1.1993 25.499 3154 1.190 3753 2.508 0.26696 27.573 0.4032 5170 15.571 187.5 0.71 1.00 65.030 CUMBUSTOR REGEN 44 37 3 65.034 41.952 4950 664.3(1690) 1.1653 25.176 3375 65.039 18.464 4425 362.1(1484) 1.1861 25.428 3203 1.214 3888 2.531 0.26696 27.573 0.4032 5239 10.132 190.0 0.71 1.00 NOZZLE AE 45 38 87.275 41.952 4784 550.3(1576) 1.1748 25.307 3323 87.275 1.167 2464 -450.5(757) 1.2837 25.626 2477 2.857 7077 2.508 0.05557 27.573 1.9371 6644 6.112 240.9 0.71 1.00 NOZZLE PO 46 39 87.275 41.952 4784 550.3(1576) 1.1748 25.307 3323 A7,275 0.403 1935 -631.2(576) 1.3047 25.627 2213 3.475 7689 2.508 0.02654 27.573 4.0557 7008 3.172 254.2 0.71 1.00 NOZZLE AE REGEN 47 40 87.275 41,952 4950 664,3(1690) 1,1653 25,176 3375 87.275 1.236 2665 =379.0(827) 1.2763 25.626 2569 2.813 7225 2.531 0.05557 27.573 1.9371 6805 6.240 246.8 0.71 1.00 NOZZLE PO REGEN 48 41 P7 . 275 41.952 4950 664.3(1690) 1.1653 25.176 3375 U.403 2075 -584.3(623) 1.2986 25.627 2286 3.457 7904 2.531 0.02544 27,573 4,2310 7210 3.125 261.5 0.71 1.00 47.27c FICTIVE COMBUSTR 68 61 65.039 295.938 4904 550.3(1669) 1.1960 25.444 3386 0.403 1192 -886.7(341) 1.3466 25.027 1765 4.772 8420 2.355 0.04719 27.573 2.2814 7452 6.175 270.3 0.71 1.00 65.039 FICTIVE MOZZLE 69 62 0 87.275 26.484 4713 526.1(1597) 1.1717 25.293 3295 87.275 1.446 2815 =324.81 8x1) 1.2706 29.625 2634 2.477 6525 2.539 0.05557 27.573 1.9371 6309 5.636 228.6 0.71 1.00

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	XAES	PaIR	Ponk	PPA	x o o	Malb	a⇔ua	(4 × 1 L l	P=1H/F50	P=IA/PTO	P⇔Ob/P\$&	P#GE/PTO
	•	-		#4.406E#01	0.000	0.000	0.000	2.4705=62	7.69#F 00	1.8476-03	0.000	0.000
	6.981F=01	1.085E 00	0.000	-			0.000	1.4341 12	2.694E 00	1 447E=03	0.000	0.000
	1.836F 01	1.085E 00	000	-3.611E 01	0.000	0.000		5.053E 02	5.7245 00	3.4736=03	0.000	0.000
	3.070€ 01	2.305E 00	0.000	=1.735t 02	0.000	0.000	0.000			5 320E 03	0.000	0.000
	3.508E 01	3.990E 00	0.000	-3,775E 02	0.000	0.000	0.000	6.804E 02	9.9085 00			7.917t=03
	3.518E 01	4.001E 60		02 3E 44.44 e	0,000	0.000	0.000	6.847E 02	9.936F 00	5.3356-03	1.474E 01	
	3.51gE 01	4.002E 00	5.9025 00	9 44.044E 05	0.000	0.000	0.000	6.850£ 02	9.93KE 00	5.336E=03	1.465E 01	7.869E#03
	3.555E 01	4.045E 00		04.526E 07	0.000	0.000	0,000	7.218E 02	1.004E 01	5.3936-03	9.143F 00	U . 909t ≈ 03
	3.585E 01	4.013E 00		50 3476 Be	₩3,301E n2	93.301E		7.521E 02	9.964F 00	5.350E=03	4,656E 00	2,500E+03
	3.606F 01	3.090E 00	2.788F 0n	₩4.791£ 02	#3.342F 08	-3.342E	00000	7,7388 02	4.938F 00	5,320E=03	6.9236 00	3.717E-03
	3.648F 01	4 289E 00		■4,992£ 02				8.174E 02	1.065E 01	5,7186003	1.143E 01	6.138E=03
	3.701E 01	4 380E 00	A . A 95 0 0 0	-5.335F 02	-3-708F 02	~3.531F	02 01.764E 01	8.734E 02	1.088E 01	5.P40E-03	1.712E 01	9.19#E=03
	3.731F 01	4.250E 00					02 02.321F 01	9.055E 02	1.055E 01	5.6666003	2.033E 01	1.095E=05
							02 -3.630E 01	9.843E 02	9.771E 00	5.2478 = 03	3.391E 01	1.821E=U2
	3.8036 01	3.935E 00						1.018E 03	1.383E 01	7.4288003	3.954F 01	2.1236-02
	3.833E 01	5.571E 00	1.3727 01	030463E U2	4 4 4 4 6 C C C C C C C C C C C C C C C	0340275	02 94.166F 01	1.0656 03	1.956E 01	1.0508=02	3.838E 01	2.061E=02
	3.875E 01	7.877E 00	1.5458 01	42.510E 05	040430E V6	93.7405	02 =4.917F C1		2,022F 01	1.0862.02	3.824E 01	2.053E=02
	3.880E 01	B.144E 00	1.540F 01	*5.514£ 02	64,461E C	3 . 7 6 1 L	02 -5.004F 01	1.0718 03		1.2408=02	3.884F 01	2.086E=02
	3,901E 01	9.300E 00	1,5648 01	95.524E 02	=4.505E 0	94.0285	02 =5.377E 01	1.095E 03	2.309E 01			2.132E=02
	3,93 E 01	1.362E 01	1.599E 01	=5,584E 02	04.721E 03	. =4.130E	02 95.9038 01	1.1298 03	3.383E 01	1.816E#02	3.970E 01	
	3.95oF 01	1,639E 01	1.190E 01	=5.6726 02	⇒4.825€ 02	2 =4.201E	02 =6.236E 01	1.151E 03	4.069E 01	2.1856-02	2.954E 01	1.586E=02
	3.980E 01	1.712E 01	5.500F 00	, =5.891E 02	₩4.996€ 02	2 a4.321E	02 =6.747E 01	1.186E 03	4.252E 01	2.283E=02	1.366E 01	7.333E+03
	4.000E 01	1.762E 01	5.313E 00	-6,076E 02	-5.117€ 08	4.400E	02 07,085E 01	1.210E 03	4.375E 01	2.349E-02	1.319E 01	7.084E=03
	4.040E 01	2.074E 01	4.941E 00	96.459E 02	□9.374E 02	04,593E	02 #7.805E 01	1.257E 03	5.150E 01	2.7656#02	1.227E 01	6.588E=03
	4.04 E 01	2 082E 01	4-932F 00	-6.468E 02	-5.381E 02	-4.598E	02 #7.824E 01	1.258E 03	5.170E 01	2.776E=07	1.225E 01	6.576E=03
	4.128E 01	2.764E 01	4-120F 00	#7.470E 02	#6.156E 02	#5.048E	02 -1.108E 02	1.361E 03	6.663E 01	3.685E-02	1.023E 01	5.493Ew03
	4.129E 01	2 772E 01	4.110F 06	97.483F 02	-6.167E 02	-5.054E	02 -1.113E 02	1.362E 03	6.883E 01	3,696E=02	1.021E 01	5,481E=03
	4.136E 01	5.822E 01	4.050E 0	7. SASE 02	-6-240F 02	M5.090F	02 m1,150E 02	1.370E 03	7.009E 01	3.763E=02	1.006E 01	5.400E=03
	4,1500 01	2.932E 01	5 962F 06	_9 739s 02	-6-404E 02	-5-170E	02 -1,235E 02	1.387E 03	7.282F 01	3.910E=02	1.451E 01	7.789E=U3
		2.014E 01	1.8016 00	_R 2985 02	~7.79AF 02	- R.827F	02 a1.965E 02	1.502E 03	5.001E 01	2.685E#02	4.478E 01	2.405E=02
	4.246E 01		7 BEOF 6	1 20 20 10 2	-1 105F 01		02 03.475E 02	1.698E 03	9.968E 01	5.352E=02	9.584E 01	5.146E-02
	4,408E 01	4.014E 01	DODAE O	-0 4465 05	ATTIONE OF	1 74 BUOF	02 031413E 02	1.726E 03	1.0686 02	5.7336002	9.648E 01	5.181E=02
	4.431E 01	4.300E 01	3,0058 01	00.1102 08	0101015 03	0 4446	02 =3,710E 02	1.785E 03	50 3912°I	6.530E=02	9.784E 01	5.253E=02
	4.479E 01	4.897E 01	3.940F 0	98 145F 05	@1"SA7E 0:	9 9 9 9 7 E	02 64.298E 02			6,540L=02	9.786E 01	5.254E=02
	4.480E 01	4.905E 01	3.941E 0	20 3461°80	*1.342F 0	98.047E	02 #4.306E 02	1.786E 03	1.2186 02		1.019E 02	5.473E=02
	4.6258 01	4.267E 01	4.1045 0	1 07,736E 02	91.746E 0.	a1.088E	03 =6.5818 02	1.964E 03	1.060E 02	5.6896=02		
	4.626E 01	4.263E 01	4.106E 0	1 a7,730E 02	□1,750E 0	5 =1.090E	03 #6,5096 05	1.965E 03	1.058E 02	5.683E=02	1.019E 02	5.474E=02
	4.73 E 01	3.801g 01	4,2242 0	1 m6,700£ 02	s2.087E 0;	3 m1.240E	03 08,474E 02	2.095E 03	9.438E 01	S.068E=02	1.049E 02	5.6326-02
	4.732E 01	3.799E 01	4.2258 0	06.692E 02	≈2.090€ 01	3 m10241E	03 ≈8.490E 02	2.0966 03	9.433E 01	2.062E-05	1.049E 02	5.633E=02
	4 81 F 01	3.630E 01	3.611E 0	65.690E 02	-2.331E 0	3 al.34RE	03 49.8258 02	2.195E 03	9.014E 01	0.6405-05	8.967E 01	4.815E=02
	4.876E 01	3.108E 01	3.108E 0	#4.666E 02	-2.512E 03	3 -1-432E	03 =1.080E 03	2.276E 03	7.717E 01	9.144E=05	7.717E 01	4,144E=02
	4.8776 01	3.100E 01	3.100F 0	-4.649E 02	₩2.514E 0:	3 -1.433E	03 =1.0A1E 03	2.277E 03	7.698E 01	4.133E+02	7.698E 01	4.133E=02
	4.930E 01	2.689E 01	2.689F 0	. #3.850E 02	-2.651E 07	3 m1,499E	03 -1.152E 03	2.344E 03	5,677E 01	3.585E-02	6.677E 01	3,585€≥02
	5.071F 01	2.314E 01	2.314F 0	-2.001E 02	⇒2.974E 01	5 -1.660E	03 =1,314E 03	2.5218 03	5.745E 01	3,085E-02	5.745E 01	3.085E-02
	5.28 E 01	1.8268 01	1,8267 0	2.785F 01	-3.370E 0	5 -1.86PE	03 -1.502E 03	2.788E 03	4.535E 01	2,435E-02	4.53SE 01	2.435E+02
	5.331E 01	1.807E 01	1.807E 0	7.508F 01	-3.453F 0	3 a1.912F	03 -1.542E 03	2 851E 03	4.488E 01	2.4105-02	4.488F 01	2.410E=02
	-	1.658E 01	1.658E 0	1 1315 03	-3-572F 0	9736	03 -1.599E 03	2.947E 03	4.118E 01	2.211E=02	4.118E 01	2.211E=02
	5.406E 01		1.507E 0:				03 -1.655F 03	3 045E 03	3.743E 01	2.010E+02	3.743E 01	2.010E=02
	5.492E 01	1.507E 01		1 2.037E VE	-1. h (15 A)	3	03 =1.719F 03	3 166E U3	3 3856 01	1.8186-02	3.385E 01	1.818E=U2
	5.576E 01	1.363E 01	1.363F 0					3.209E 03	3,201E 01	1.719E-02	3.201E 01	1.7196-02
	5.624E 01	1.289E 01	1.289E 0				03 #1.750E 03		1.732E 01	9.300E+03	3.180E 01	1.707E=02
	5.630E 01	6.975E 00	1.280E 0				03 -1.793E 03	3.216E 03			3.126E 01	1.679E=02
	5.644E 01	6.975E 00	1.259E 0				03 =1.762F 03	3.234E 03	1,732E 01	9.3000.03		
	5.652F 01	1.247E 01	1.247F 0				03 -1.767E 03	3.245E 03	3.096E 01	1.662E=02	3.096E 01	1.662£=02
	5.6 AOF 01	1.204E 01	1.204E 0				03 =1.7A5E 03	3.880E 03	2.989E 01	1.605E=02	2.9898 01	1.6056=02
	5.702f 01	1.150E 01	1.156F. 0				03 01.799E 03	3.309E 03	2.870E 01	1.5416-05	2.870E 01	1,541E=02
	5.775E 01	1.002E 01	1.002F 0				03 a1.843E 03	3.402E 03	2.488E 01	1,336E+02	2.488F 01	1.336E-02
	5.877E 01	5.137E 00	5.137F 0.	o 5.082£ 02	=4.115E 0	3 -5.221E	03 =1.894F 03	3.532E 03	1,2766 01	6,850E=03	1.276E 01	6.850E=03
Ç	6.07AF 01	1.620E 01	1.620F 0	5.107E 02	-4.260€ 0	3 ¤2.267£	03 •1.993F 03	3.790E 03	4.023F 01	5.16^E=02	4.023E 01	2.160E=02
}	4 6.22nF 01	1.552E 01	1.552E 0				03 -2.072F 03	3.972E 03	3.855E 01	2.07CE=02	3.855E 01	2,070E=U2
	3		-	• "		·				T.		

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	XABS	P=18	яп⊭ч	PDA	40 ×	3≈Ia	c • 1₽	CAPALL	P=18/P80	P-1F/P10	P=nH/PS0	P=68/PT0
بئ	6,460F 01	1.432E 01	1.6328 01	5.107E C2	-4.586E 0	3 -2.3746	03 -2.214F 03	0.259E 03	₽.550£ 01	2.4436-02	4.55VF N1	5.4436=05
بــر	6.504E 01	1.909E U1	1.875F 01	5.1076 62	-4.627F 6	3 -2.38RE	03 #2.238F 03	4.337F 03	4.740F C1	2,5456=62	4.657E 01	2.5008=02
фэ	6.50AF 01	1.90°E 01	1.680F 01	5.167E 02	=4.651F 0	3 -2.390E	03 -2.241F 03	4.342E 03	a june of	2.5451-02	4.668F 01	2.506E=02
	6.528F 01	1.798E 01	1.902F 01	5.107L 02	#4.651E 0	3 -2.39AE	03 #2.253F 03	4.364E 03	4.464F 61	7.39/E=02	0.724F 01	2.5376-02
	6.694E 01	8.750E 00	9.2005 00				03 #2.385F 03	4 583L 07	2.173E 01	1.167E=02	2.285E 01	1.227E=02
	6.761E 01	6.545E 00	9.127# 00	A. 1446 02	-4.847F 0	3 =2.467E	03 -2.3AOF 03	4 n69E 03	1.625E 01	8.726E-03	2.267E 01	1.2176-02
	6.838F 01	4 0105 00	6.951F 00	1.0148 03	.U. 904F 0	3 -2 482E	03 -2.422F 03	4.760E 03	9.95#F 00	5.3476-03	1.726E 01	9.267L=03
	6.910E 01	2.879E UO	4.915F 0A	1.132E 03	=4.961E 0	3 .2.4936	03 -2.468F 03	4 848E 03	7.14ct 00	3.838t = U3	1.220E 01	6.553E=03
	6:971F 01	1.920F 00	5.9F2F PA	1.204E 03	-5.007E 0	3 -2.50CE	03 -2.506E 03	4.922E 63	4.768E 00	2.560L-03	4.6496 00	5.310E=03
	7.066F 01	1.510E 00	2.5308 00				03 -2.553F 03	5.036E 03	3.751F 00	2.0146-03	6.282F 00	3.373€=03
	7.109F 01	1.325E 00	2.363F 00	1.307E 03	-5.082E 0.	3 -2.513E	03 -2.569F 03	5.08AE 03	3,290E 00	1.767E=03	5.868F NO	3.151E=03
	7.262F 01	1.339E 00	1.770 00				03 =2.617F 03	5.273E 03	3,324F 00	1.785E=03	4.395E 00	2.360E=03
	7.277F 01	1.340E 00	1.713# 00				03 -2.421# 03	5.290E 03	3.327F 00	1.7876-03	4.254E 00	5.284E-03
	7.352F 01	1.2446 00	1.430F On				03 #2.6#4F 03	5.374E 03	3.090E 00	1.659E=03	3.551E 00	1,9078-03
	7 3528 01	1.2445 00	1.4285 00	1.446E 03	#5.172E 0	3 -2.52AF	63 -2.644F 03	5.375E 03	3.099E 00	1.659E=03	3.547F 00	1.905E=03
	7.485E 01	1.0758 00	0.000	1.470€ 03	-5.227E 0	3 -2.536E	03 #2.691E 03	5.427E 03	2.669E 00	1.433E=03	0.000	0,000
	7.7708 01	2.325E 00	0.000	1.538F 03	#5.240E 0	3 #2.549E	03 -2.691F 03	5.525E 03	5.773F 00	3,100E=03	0.000	0.000
	8.16cE 01	1.455E 00	0.000	1.619E 03	-5.256F 0	3 -2.565E	03 =2,691F 03	5.630E 03	3.6138 00	1.940E=03	0.000	0.000
	B. HUIE CI	1.195E 00	0.000	1.6488 03	-5.270E 0	3 -2.579E	03 =2.691E 03	5.484E 03	2.967F 00	1.593L=03	0.000	0,000
	8.7278 01	5.680E 00	0.000	1,695E 03	-5.294E 0	3 -2.603E	03 -2.691F 03	5.707E 03	6.655E 00	3.573E=03	0.000	0,000
	8.727E 01	2.683E 00	0.000	1.695E 03	-5.294E 0	3 =2.603E	03 -2.691E 03	5.707E 03	6.663E 00	3.578E-03	0.000	0.000

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X	Drnag	COBIA		⊔ ≱
^	(/I-R2G	CDRAG	CF	HC.
4.04AF 01	1.176E 02	1.176F 12	2.211Fa63	4.3006.02
4.0418 01	1.9208=01	1.178E 02	2.4915-03	3.6325=02
4.1285 01	1.802E 01	1.158E 02	2.6276-03	4.1885-02
4.129E 01	1.955E=01			
		1.360F 02	2.417E=03	4.440E=02
4.136E 01	1.232E 00	1.3720 02	2.3496-03	4.515E=02
4.1505 01	5.648E 00	1.399# 02	2.4056-03	₽.777E#02
4.246F 01	1.776E 01	1.5769 02	2.046E=03	4.9416-02
4.408F 01	2.742E 01	1.851# 02	2,5471-03	7 411F=02
4.431E 01			0.0000.00	
		1.888g 02	2.8776-03	6.6966=05
4.479E C1	8.155E 00	1.969E 02	2.8998003	6,806E#02
4.48 ₀ F 01	1.019E=01	1.9700 02	2.9306-03	6.735Ea02
4.625E 01	2,438E 01	2.2145 02	3.148E=03	6.188E=02
4.626F 01	1.7116-01	2.216F 02	3.14RE=03	6.188E=02
4.731F 01	1,645E 01	2,380F 02	2.812E=03	6.678E=02
4.732E 01	1.140E=01			
			2.8126-03	6.678E=02
4,811E 01	1.138E 01	2.4958 02	2.851E=03	6.171E-02
4.876E 01	9.539E 00	2.5918 02	3.067E=03	5.379E=02
4,877F 01	1,447E=01	2.592E 02	2.827E=03	5.819E=02
4.930E 01	7.239E 00	2.664F 02	2.777E=03	5.381E=02
5.071E 01	1.776E 01		2.707E=03	
5.281E 01				4.850E=02
	2.339E 01	3.076F 02	2.726E-03	3,985E=02
5,331F 01	5.259E 00	3.1280 72	2.841E=03	3,776€#02
5.406E 01	7.794E 00	3°5066 05	2.857E□03	3.514E002
5.482E 01	7.676E Q0	3.283g 02	2.450E#03	3.276E=02
5.576F 01	9.162E 00	3,375E 02	2.828E=03	3.049F=02
5.624F 01	00 3506°2		2.793E=03	
5.630E 01				2.770E=02
	4.383E=01	3-4082 02	2.963E=03	2.224E+02
5.644E 01	1.134E 00	3.419F 02	2.766E=03	2.334Ea02
5.652E 01	6.690E-01	3.426F 07	3,291E-03	2.366E-02
5.680E 01	2.468E 00	3.451E 02	3.241£003	2.320E-02
5.702F 01	2.010E 00	3.4718 02	3.234E-03	2.265F-02
5.7758 01	6.543E 00		3.223E=03	
5,8778 01				2.070E-02
	9.925E 00	3.6368 02	3.305E=03	1.296E=02
6.07BF 01	1,857E 01	3.8218 02	3.217E=03	2.735E-02
6.220E 01	1.184E 01	3.940E 02	7.198E=03	2.697E=02
6.466F 01	1,962E 01	4.136E 02	3.243E=03	2.8336-02
6.504E 01	2.630E 00	4.1628 02	3,296E=03	2.761E=02
6.50RE 01	2.70BE=01	4.1656 02	3.374E=03	2.8316=02
6.528E 01	1.395E 00		3.369E=03	
				2.808E=02
	1-143E 01	4-2936 05	3.243E = 03	1.953E=02
6.761E 01	4.113E 00	4.334F 02	3.221E-03	1.795E=02
6.838F 01	4,3526 00	4.3788 02	3,1656-03	1.421E=02
6.910E 01	3.466E 00	4.4128 02	3.1132-03	1.1215002
6.971E 01	2.499E 00	4.4370 02	3.076E=03	9.1895-03
7.066F 01	3.234E 00	4.470F 02	3.0266-03	6.948E003
7.109E 01	1.279E 00			-
		4.4836 05	3.013E=03	6.486E=03
7.262E 01	4.186E 00	4.554E 05	2.9846#03	5.687E-03
7,277E 01	3.691E-01	4.528E 02	2.981E=03	5.608E=03
7.352E 91	1.727E 00	4.5457 02	2.9586-03	5.061E=03
7.352E 01	3.171E-03	4.545= 02	2,9586=03	5.058E=03
7.485F 01	9.485E=01	4.555F 02	2.921E=03	4.267F=03
7.770E 01	2.15°E 00		3,011E=03	
				7.6198-03
	2.485£ 00	4,6015 02	2.9276=03	5.3177003
8.441F 01	1.043E 00	4.6127 02	2.847 <u>L-03</u>	4 . 550F#03
8.7278 01	5,2916-01	4.617F 72	2.0846-03	9.324F-03
8.727F 01	0.000	4.617F 02	2.9846-03	8.351E-03

PANJET PERFORMANCE

	BANJET PE	RFOFMANCE			
320	D ENGINE BERECHMANCE		1/ LET		
	CALCULATED THRUST	MASS FLOW RATI ADDITIVE DRAG [IMITIMG PRESS DFLIA PTZ TOTAL PRESSURE TOTAL PRESSURF	O	0.0009 NCY 0.1637 0.000 (PSI) IC 0.3006 0.1660	
	REGENERATIVE-CODERT FNGINE PERFORMANCE CALCULATED	INLET PROCESS KINETIC ENERGY	EFFICIENCY - SUPERSC EFFICIENCY - SUPERS EFFICIENCY - SUPERS	C C.9052 GNIC Q.9343	
	STREAP THRUST	ENTHALPY AT PO	FFFICIENCY - SUBSIN - SUPERSONIC - SURSONIC	10 0.8841 ****** *1.30 (870/LBM) ***** 34.61 (870/LBM)	
	MOMENTUM AND FORCES		COMBUSTOR		
	INLET FRICTION DRAG	EDUTVALENCE RA COMBUSTOR EFFI TOTAL PRESSURE COMBUSTOR EFFE	TIO	0.705 1.000	10
	NOTZLE MOMENTUM CHANGE NOTZLE PRESSURE INTEGRAL EXTERNAL FRICTION DRAG O.00 (LBF) FXTERNAL PRESSURF INTEGRAL O.00 (LBF) TOTAL EXTERNAL DRAG TOTAL STRUT DRAG CAVITY FORCE CAVITY FORCE MEASURED LOAD CELL FORCE P1247 (LBF) MEASURED LOAD CELL FORCE FUFL VACUUM SPECIFIC IMPULSE O.0. 0.0. 0157,1: =117.0.	NOZ7LE COEFFIC PROCESS EFFICI	MOZZLE TMRUST COEFFICIENT - IENT - C1 ENCY EFFICIENCY	0,6718	
	, STATIONS		FUEL INJECTORS		
	NOMINAL COML LEADING EDGE	1 ** JECTORS 1 & 1 & 1 C 2 A 2 C 3 A 3 B	87 AT IUN 40.400 41.284 44.300 48.759 46.250 54.049 56.234 44.784	VALVE A B C E	

t = 226.50 sec.

1/29/75

SUPMARY REPORT

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CO ATLO TUNNEL	1	0 " 5		***		.	. ~ •	,	v	,,,,	.,	.,	• •	•	• • •		#1 v
0.000 /49.499	29/1		788)	1.2945	cd.060	6574											
E 0.000 0.389	431	- 32.9(96)	1,3987	28,059	495	6,002	5897	1.625	0.10688	27,056	0.9677	5054	9.795	186,9		
SPIKE TIP NS	ے	υ 4															
		995"1(
			768)	1,2966	28.859	2546	0.400	1019	5.081	0.10688	27.038	0.9677	4980	1,693	184.5		
WIND TUNNEL	3	U 0	7000	. 50.45	3 0.66	11 70			•								
0.000 749.499	29/1	002+1((40)	1.2945	20.000	2570	4 439	E00 A	(955	0. 10.006	J4 861	0 0877	// 0 4 5	9.624	187.0		
0.000 0.379 SPIKE 11P NS	4	u 0	401	149401	60.007	7/7	0.020	2700	11003	0.10496	£41222	0,7077	4702	7,024	10110		
		662.1(7861	1.2944	28.859	2574											
0.600 16.373	2906	642.2(769)	1.2965	28.859	2548	0.392	997	2.081	0.10496	26,553	0.9877	4965	1.627	187.0		
INLET THROAT	5	0 3		• • • • • •			•	•			- •						
40,400 268,072	2902	641.2(767)	1,2967	28,859	2546											
	1468	234.10	363)	1,3506	28,859	1848	2.442	4513	1.889	0.94525	27.038	0.1117	4264	66.298	157.7		
INLET UPNKSK	6	0 3															
40.400 268.072	2002	641.2(767)	1.2967	28,859	2546	5 F7C				3 W A 1 O	0 4220	0767	4 + 700	120 7		
40.400 14.116	1410		546)	1.3540	29.054	1814	4.232	4547	1.884	0.85932	27,030	0.1550	4307	61,388	127.5		
INLET ONNASK 40.400 121.358	20/2	6/11 2/	7485	4 3047	28 450	28/14											
40.400 103.727		610.01	7371	1 2000	24.450	250%	0.406	1202	1.04%	0.85932	21.038	0.1228	4367	16,582	159.3		
	8	1 21	,3,,	116777	C06034	£304	0 9 4 7 0	+676	48772	4103.36	2,1020		444.				
40,410 229,411			7901	1.2989	27.614	2589											
40.410 14.865		229.9(378)	1.3521	27.614	1888	2.410	4550	1.968	0.94847	27.134	0.1117	4263	67.072	157.1	0.12	0.07
COMBUSTOR O	9	2 21															
41,286 180,953	2801	647.30	801)	1.3006	26,480	2617											
41.286 18.141			432)	1.3467	26.479	2008	2.147	4310	2.044	0.95388	27.226	0.1114	4165	63.896	153.0	0.53	0.04
	10	3 21															
41.296 188.946	2/60	647.3(788)	1.3045	26.437	2602	3 4 3 3	u 7 6 0	2 477		27 214		0.448	42 BBA	.63.0	0 37	
41.296 18.179 COMBUSTOR 0	1220		414)	1.3443	20.420	1403	2112	4208	4.037	0.95419	8/4660	0.1114	4104	63,880	19617	0.23	4.41
41.361 168.013	11	4 21	7865	1 30//8	26.410	2600											
41,361 18,422	1553	279.20	4201	1.3492	26.430	1985	2-161	4290	2.036	0.95425	27.226	0-1114	4156	63.622	152.7	0.23	0.00
COMBUSTOR 0	12	5 21	16.07	*****	446-64		-1.0.	- L . y	4,4,2	*********	4.4		,,,,	**		* 1 * *	F M - V
41.500 184.342			785)	1.3049	26,429	2598											
41.500 . 19.847	1590	290.1(431)	1.3474	26,429	2007	2.104	4223	2,038	0.95482	27.226	0.1113	4139	62,657	152.0	0.23	0.00
	13	6 21															
42.460 171.326					26,429						(
42.460 21.791			446)	1.3445	26,429	5045	5.005	4088	2.041	0.94589	27.226	0.1124	4056	60,056	150.1	0 . 23	0.00
	14	7 6	000	. 2770	77 777	2024											
44.081 115.246					27.222			33//3	J 150	0.91405	J7 226	0 4163	//097	47,478	150.5	n . 9%	0.65
	15	8 3	1131	146730	21.50	2340	10310	3346	51150	0.41402	418564	0.1103	4071	411410	73613	V * # 2	4.42
44.310 114.003			9971	1.2714	27.259	2827											
44.310 43.930								3290	2.122	0.91272	27.226	0.1165	4094	46.664	150.4	0.23	0.68
	16	9 3			"							••••		. •			•
44,796 111,368	5480	622.2(1007)	1,2695	27,315	2836											
44.796 46.740			814)	1.2900	27.520	5600	1.218	3166	2.124	0.90887	27.226	0.1170	4980	44.724	149.8	0.23	0.72
	17						•										
44.800 111.324								•								0 .7	0 73
			214)	1.4900	51.351	2000	1.217	5165	2.124	0.90867	27.226	0.1170	4080	44.696	144 8	U≥∉⊅	V. / C
	18 7027		9521	מכסל ו	Du lau	วมอย											
								2150	באנ_ נ	0.66414	21.466	0.1-41	արևո	42.297	147.0	0.53	د ج د ٥
	05	450101		1 1 2 1 10	C-1300	6000	1966/	3170	****	A \$ 00 M 1 H	211-00	401241	4920		4-144	4477	~ @ b to

GAMPA MOLF I SONV MACH VEL S IVAC PHI LTAC * / A AZAC MUMIN R COMEUSTOR 0 19 12 2 104.079 3028 676.7(952) 1.2924 24.369 2625 46.260 42.787 2464 428.4(757) 1.3116 24.489 2566 1.227 3150 2.268 0.86348 27.466 0.1242 46.260 4050 42.271 147.5 6.53 0.22 COMBUSTOR 0 20 13 47 - 310 98.684 3122 614.2(983) 1.2880 24.517 2855 47.310 39.927 2536 407.2(780) 1.3075 24.518 2593 1.241 3218 2.278 0.80363 27.466 0.1334 4111 40.185 149.7 0.53 0.27 COMMUSTOR 0 21 14 2 98.621 5125 614.0(983) 1,2879 24.518 2856 47.321 39,916 2538 407.1(780) 1,3674 24,570 2594 1.241 3218 2.279 0.80301 27,466 0.1535 4112 40.153 149.7 0.53 0.28 47.321 CUMBUSTOR 0 22 15 48.110 93.369 3253 605.1(1027) 1.2814 24.675 2898 45.110 36,459 2663 394.4(821) 1,3012 24,677 2642 1,229 3247 2,292 0,74891 27,466 0,1432 4183 37.794 152.3 0.53 0.34 COMBUSTOR 0 23 16 48.761 89.289 2966 610.6(1006) 1.2963 22.501 2914 45.761 32.733 2343 376.3(775) 1.3173 22.501 2611 1.311 3424 2.424 0.69665 27.693 0.1552 4249 3/.075 153.4 0.62 0.19 COMBUSTOR 0 24 17 89.215 2968 610.5(1007) 1.2962 22.503 2915 20.771 48.771 32.697 2345 376.0(775) 1.3172 22.503 2612 1.312 3426 2.424 0.69574 27.693 0.1554 4250 37.042 153.5 0.82 0.19 COMBUSTOR 0 25 18 49.301 85.436 3080 605.5(1047) 1.2908 22.617 2956 49.301 30.796 2431 359,3(805) 1.3126 22.618 2648 1.325 3509 2.437 0.65069 27.693 0.1662 4331 35.487 156.4 0.82 0.23 CUMBUSTOR 0 26 19 50.711 75.680 3436 593.5(1176) 1.2731 22.982 3076 50.711 28.631 2770 333.41 924) 1.2961 22.986 2787 1.294 3607 2.473 0.55456 27.693 0.1950 4535 31.088 163.7 0.82 0.35 COMBUSTOR 0 27 52.811 70.691 5614 578.9(1241) 1.2632 23.193 3128 52.811 20.175 2750 236.6(912) 1.2939 23.202 2761 1.495 4126 2.489 0.45453 27.693 0.2379 4781 29.148 172.5 0.82 0.42 COMBUSTOR 0 28 21 4 53.311 68,987 3671 575,9(1262) 1,2600 23,256 3144 19.267 2786 225.6(924) 1.2918 23.268 2773 1.510 4186 2.494 0.43595 27.693 0.2480 4827 28.361 174.3 0.82 0.44 53.311 COMBUSTOR 0 29 22 54.061 67.483 3714 571.5(1277) 1.2574 23.312 3156 54.061 17.576 2780 200.9(921) 1.2913 23.324 2766 1.557 4306 2.498 0.41094 27.693 0.2631 4891 27.499 176.6 0.82 0.46 CUMBUSTOR 0 30 23 54.821 66.719 3728 567.3(1282) 1.2565 23.537 3159 54.821 15.862 2735 174.2(904) 1.2925 23.350 2744 1.616 4435 2.499 0.38861 27.693 0.2782 4948 26.785 178.7 0.82 0.47 COMBUSTOR 0 31 24 65.243 3763 562.7(1295) 1.2542 23,384 3168 55.760 55.760 14.386 2720 148.8(897) 1.2924 23.399 2733 1.665 4551 2.503 0.36454 27.693 0.2966 5010 25.782 180.9 0.82 0.48 . COMBUSTOR 0 32 25 5 56.246 50.611 4180 560.5(1449) 1.2261 23.829 3270 56.246 13.622 3226 155.5(1078) 1.2677 23.882 2918 1.543 0502 2.544 0.29380 27.693 0.3680 5159 20.554 186.3 0.82 0.63 COMBUSTOR 0 33 26 5 56.501 59,656 3802 560.3(1309) 1,2516 23,430 3178 56.301 10.368 2609 88.4(855) 1.2956 25.448 2677 1.815 4859 2.512 0.29302 27.693 0.3690 5162 22,128 186,4 0,82 0,50 COMBUSTUR 0 34 27 3 56.441 59.554 3807 559.7(1311) 1.2513 23.436 3179 10.258 2607 85.4(855) 1.2956 23.454 2676 1.821 4872 2.512 0.29092 27.693 0.3717 56.041 5170 22.026 186.7 0.82 0.50 COMBUSTOR 0 35 26 6 51.999 415# 559.4(1440) 1.2281 23,803 3264 56.521 13.190 3163 142.2(1055) 1.2706 23.652 2894 1.579 4569 2.541 0.29417 27.693 0.3675 56,521 5175 20,889 186.9 0.82 0.62 COMBUSTOR 0 36 29 3 56.801 52.939 4129 558.3(1450) 1.2500 23.779 3258 12.750 3104 130.0(1033) 1.2752 23.625 2872 1.612 4630 2.538 0.29320 27.693 0.3688 56.801 5189 21.095 187.4 0.82 0.61 COMBUSTOR 0 37 30 57.027 54,320 4081 557,4(14)3) 1,2334 25,731 3248 51.427 12.208 3014 116.1(1000) 1.2772 23.771 2838 1.656 4699 2.535 0.29275 27.695 0.3695 5199 21.379 187.8 0.82 0.60

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GAMMA MOLET SONV MACH VIL S Purim 0 IVAL PHI ETAC n/A AJAC COMBUSTOR 0 35 31 4 50.960 3916 554.8(1351) 1.2445 23.563 3207 57.751 10.470 2/16 74.6(893) 1.2900 23.588 2719 1.802 4901 2.518 0.28811 27.693 0.3753 5224 21.942 18d.7 0.82 0.54 57.751 COMBUSTOR U 39 32 B 58.771 111.437 3171 551.7(1078) 1.2850 22.030 2979 58.771 5.437 1535 -46.3(485) 1.3465 22.852 2122 2.576 5470 2.415 0.28627 27.693 0.3777 5234 24.336 189.0 0.82 0.30 COMMUSTOR 0 40 33 60.781 47.895 4584 546.5(1601) 1.1935 24.316 3346 17.212 3860 194.4(13:2) 1.2301 24.454 3107 1.351 4198 2.561 0.64624 27.693 0.3650 5222 19.324 188.6 0.82 0.81 60.781 0 41 34 COMBUSTOR 50.996 4420 542.6(1538) 1.2077 24.140 3316 62.201 62.201 15.787 3569 158.2(1203) 1.2465 24.234 3023 1.451 4366 2.550 0.30427 27.693 0.3553 5212 20.737 186.2 0.62 0.74 CORBUSTOR 0 42 35 64.665 44.670 4698 534.6(1641) 1.1867 24.475 3359 64.665 COMBUSTOR 6 43 36 40.970 4798 533.2(1679) 1.1722 24.592 3372 45.041 65.041 19.665 4317 263.9(1485) 1.1942 24.780 3216 1.141 3670 2.576 0.26813 27.693 0.4032 5190 15.294 18/.4 0.82 0.93 COMBUSTOR REGEN 44 37 21 65.041 40.970 4935 632,9(1736) 1.1643 24.460 3416 65.041 18,551 4434 333,1(1532) 1,1843 24,724 3250 1,192 3874 2,596 0,26815 27,693 0,4032 5250 16,141 189,6 0,82 0,93 NOZZLE AE 45 38 5 87,277 40.970 4798 533,2(1635) 1.1722 24,592 3372 87,277 1.221 2522 =488.4(800) 1.2812 24.928 2539 2.816 7150 2.576 0.05582 27.693 1.9371 6760 6.202 244.1 0.82 0.93 NOZZLE PO 87.277 40.970 4798 535.2(1635) 1.1722 24.592 3372 87.277 0.589 1947 -691.4(597) 1.3039 24,928 2250 3.479 7828 2.576 0.02522 27,693 0.2878 7165 3.068 258,7 0.82 0.93 NOZZLE AE REGEN 47 40 40.970 4935 632.9(1736) 1,1643 24.480 3416 87.277 87.277 1.282 2696 -424.8(863) 1.2749 24,927 2618 2.779 7275 2.596 0.05582 27.693 1.9371 6898 6.310 249.1 0.82 0.93 NOZZLE PO REGEN 48 41 87.277 40,970 4935 632,9(1736) 1.1643 24,460 3416 87.277 0.389 2066 *b50.3(638) 1.2987 24.928 2313 3.464 8013 2.596 0.02432 27.693 4.4454 7340 3.029 265.0 0.82 0.93 FICTIVE CUMBUSTR 68 61 0 65.041 268.072 5073 533.2(1783) 1.1826 24,904 3461 65.041 0.389 1314 498/.8(387) 1.3361 25,190 1862 4.687 8724 2.424 0.0207 27.693 2.5698 7765 5.704 280.4 0.82 1.00 FICTIVE MOZZLE 69 62 0 25.387 4724 508.4(1650) 1.1689 24.576 3342 87.277 87.277 1.532 2899 =348.8(937) 1.2671 24.926 2707 2.420 6549 2.609 0.05582 27.693 1.9371 6397 5,681 231.0 0.82 0.93

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	n	0.0									
XABS	P#IH	P=0H	PCA	i3 û ≯	k+1A	2=0F	CANALL	F-15/P50	F+18/P10	P=0d/rS0	P=08/PT0
6.981E=01	1.0506 10	0.000	#4,401E=V1	មុខប្រ	0.000	0.000	2.470E=02	2.604E 00	1.4546+03	0.000	0.000
1.836E 01 3.070E 01	1.090E 00	0.000	64 628E U1	0.00 0	0 # 0 0 0	0.000	1.634E 02	2.8045 00	1.4546-03	0.000	0.000
5.508E 01	2.390E 00 4.081E 00	9.000	-1.773E UZ	U ±000	0.000	0.000	5.053E U2	6.1486 00	3,189£-03	0.000	0.000
3.518E v1	4.0926 00	0.006 5.2375 00	40 3.870E 02	0.000	0.000	0.000	6,804E 02	1.(50E 01	5.444E=03	0.000	0.000
3.518F 01	4.093E UO) +4.522E 02 +4.523E u2	0.000	0.000	0.000	6.848E 02	1.053F 01	5.460E-03	1.476E 01	7-6546=03
3.5558 01	4.135E 00		#4.614E 02	0.000	0.000	0.000	6.8516 02	1.053E 01	5.461E=03	1.467E 01	7.611E=03
3.585E 01	4.108E 00			0.000	0.000	0,000	7.217E 02	1.064E 01	5.5176-03	9.697E 00	5,030E=03
3.6666 01	4.090E 00	320# 00	4.761F U2	-3 544E 0	5 -1 500c	02 0.000	7.522E 02	1.057E 01	5.482E+03	5.5958 00	2.902E=03
3.648F 01	4.346E 00		-5.075E UZ				7,736E 02	1.0526 01	5.4578=03	7.792E 00	4.041Em03
3.701E 01	4.405£ 00		5.3256 02			· · · · · · · · · · · · · · · · · · ·	8.170E 02 8.733E 02	1.115E 01	5,799E=03	1.220E 01	6.330E=03
3.731€ €1	4.3326 00					02 -1.628E 01	9.056E v2	1.149E 01	5.957E=03	1.777E 01	9.218E-03
3.803E 01	4.015£ 00					02 -3.351E 01	9.842E 02		5.780E=03	2.093E 01	1.086E=02
3.833F 01	5.7178 00	7.9255 00	-5.838£ 02	44.404E 1	2 04 0 0 3 M C	02 =3.850E 01	1.018E UZ	1.033E 01	5.35/E=03	2.055E 01	1.066Em02
3.875E 01	8.0891 00	1.464F 01	-5.080F 02	-4.40AF A	2 -4.2445	02 04.541E 01	1 # 0 65 E 03	1.471E 01 2.081E 01	7,628t=03 1,079t=02	2.039E 01	1.0576=02
5.88gE 01	8.377E 00	1.5456 01	e5.988F 02	-4.7106 0	2 -4 3646	02 -4.625E 01	1.071E 03	2.155E 01	1.118E=02	3.765E 01	1,9536=02
3.901F C1	9.5602 00		mb.0038 02				1.095E 03	2.459F 01	1,2766-02	3.974E 01	2.061E>02
3.931E 01	1.385E 01	1.607F 01	96.069E 05	-4.985F 0	2 -4.42E/E	02 #5.456E 01	1.1296 03	3.563E 01	1.848£=02	4,040E 01	2.096E=02
3.950E 01	1.655E U1	1.339F 01	86.149E 02	#5.092F 0	2 -4.5156	02 -5.7618 01	1.151E 03	4.257E 01	2.208E=02	4,135E 01 3,445E 01	2.1455-02
3.980E 01	1.719E 01	9.125E 00	#6.326E 02	#5.2/1F 0	2 a4.647F	02 m6.238£ 01	1.1868 03	4.422E 01	2.294E=02	2.347E 01	1.787E+02
4.000E 01	1.762E 01	9.046F 00	-6.466E 02	-5.395F 0	2 -4.7415	02 -6.547E 01	1.210E 03	4.531E 01	2.3506-02	2 - 3 2 7 E 01	1.217E=02 1.207E=02
4.040E 01	2.077E U1	8-8865 00	=6.758L 02	-5.663E 0	2 -4.9425	02 -7.2136 01	1.257£ 03	5.342E 01	2.771E+02	2.2866 01	1.186E=02
4.041E 01	2.085E 01	8 882F 00	-6-765E 02	-5.670F 0	2 -4.0476	02 #7.231E 01	1.258E 03	5.362E 01	2.781E=02	2.2856 01	
4.129E 01	2.775E VI	8.533E 00	-7.566E 02	=5.465E 0	2 = 5 4175	02 -1-027E 02	1.3616 03	7.138E 01	3,702E=02	2.1956 01	1.185E=02
4.130E 01	2.783E 01		#7.575E 02	#6.476E 0	2 =5 4415	02 #1.033E 02	1.362E 03	7.158E 01	3.713E=02	2.194E 01	1.138E=02 1.138E=02
4.136E 01	2.834E 01	8-503F 00	7 6441 02	-6.549F 0	2 -5 4826	02 -1.067E 02	1.370E 03	7.290E 01	3.781E=02	2.187E 01	1.1355-02
4.150E 01	2.948E 01	1.026F 01	97.787F 02	-6.713F 0	2 -5.5686	02 -1.145E 02	1.387E 03	7.572E 01	3.9281-02	2.638E Q1	1.368Ep02
4.246E 01	P.122E 01	2.23bE 01	e8.145E 02	-6.149E 0	3085.64 5	02 -1.829E 02	1.502E 03	5.460E 01	2.832£=02	5.751E 01	2.983E=02
4.408E 01	4.242E 01	4.279F 01	7.770f 02	01.1595 0	3 .8 168F	02 #3.217E 02	1.698E U3	1.091E 02	5.660E=02	1.101E 02	5.709E=02
4.431E 01	4.542E 01	4.244E 01	67.765E 02	01.195F A	3 -8.5145	02 03 431E 02	1.726E U3	1.168E 02	6.0606-02	1.092E 02	5.663E=02
4.480E 01	5.177E 01	4.171E 01	e7.8336 02	-1.350E 0	3 -9.3116	02 03,987E 02	1.785E 03	1.332E 02	6,907E=02	1.073E 02	5.5655=02
4.480E 01	5,1826 01	4.170E 01	97.833E 02	#1.331E 0	3 ng 319F	02 -3,992E 02	1.765E 03	1.333E 02	6.915E=02	1.073E 02	5.564E=02
4.625E 01	4.611E 01	3.952E 01	97.506E 02	#1.791E 0	3 -1.1738	03 -6.1848 02	1.964E 03	1.186E 02	6.1538-02	1.0165 02	5.272E=02
4.626E 01	# . 607E 01					03 06.201E 02	1.9658 03	1.185E 02	6.147E=02	1.016E 02	5.270E+02
4.731E 01	4.194E 01	3.792E 01	96.734E 02	-2.158E D	3 -1.336E	03 -8.025E 02	2.0956 03	1.079E 02	5.5956-02	9.753E 01	5.059E=02
4.732E 01	4.194E 01	3.79UE 01	-6.725E VZ	-2.142E 0	3 01.337E	03 -8.044E 02	2.096E 03	1.0796 02	5.5951-02	9.749E Q1	5.057E=u2
4.811E. 01	4.185E 01	3.507E 01	95.912E 02	-2.387E 0	3 -1.4526	03 +9.342E 02	2.195E 03	1.076E 02	5.5846+02		4.679E=02
4.876E 01	3.273E 01	3.273E 01	-4.889E 02	-2,572E 0	3 m1.543E	03 a1.030F 03	2,276E 03	8,420E 01	4.367E=02	8,420E 01	4.367E=02
4.877E 01	3.270E 01	3.270E 01	#4.872E 02	#2.575E 0	3 -1.544E	03 #1.031E 03	2.277£ 03	8.411E 01	4.363E=42	8.411E 01	4.363Ep02
4.930E 01	3.080E 01	3.080E 01	#3,995£ V2	#2.716E 0	3 -1 615E	03 *1.101E 03	2.344E 03	7.922E 01	4,109E=02	7.922F 01	4.109E=02
5.071E 01	2.863£ 01	2.863E 01	=1.799E 02	-3.047E 0	3 -1.790E	03 -1.258E 03	2.521E 03	7.365E 01	3.820E=02	7.365E 01	3.820E=02
5.281E 01	2.017E 01	2.017E 01	8.883L 01	-3.451E 0	3 #2.014E	03 #1.438E 03	2.788E 03	5.190E 01	2.692E=02	5.190E 01	2.692E-02
5.331E 01	1.927E U1	1.9278 01	1.401E 02	#3.536E 0	3 =2.061E	03 -1.475E 03	2,852E 03	4,956E 01	2.5/1E=02	4.956E 01	2.571E=02
5.406E 01	1.758E 01	1.758E 01	2.114E 02	-3.657E 0	3 =2.127E	03 -1.530E 03	2,947£ 03	4.521E 01	2.345E+02	4.521E 01	2.345E=02
5.482E 01	1.586E 01	1.586E 01		-3.771E 0	3 #2.189E	03 -1.582E 03	3.045E 03	4.080E 01	2.1166-02	4.080E 01	2.116E#02
5.576E 01	1.439E 01	1.439E 01	3.474E 02	=3.901E 0	5 #2.258E	03 -1.643E 05	3,165£ 03	3.701E 01	1.9196=02	3.701E 01	1.919E=02
5.625E 01	1.362E 01	1.365E 01	4.992E 02	-3.960E 0	3 -5.588E	03 =1.672E 03	3.2098 05	3.504E 01	1.818E-02	3.504E 01	1.818E=02
5.630E 01	7.200E 00	1.354E 01	5.030E 02	■3.906E 0	3 ×2.291E	03 -1.676E 03	5.216E 03	1.852E 01	9.606E=03	3.482E 01	1.806E=02
5.6446 01	7.200E 00	1.332E 01	• •	□5.982E 0	3 42,2986	03 -1.684E 03	3.234E 03	1.852E 01	9,406E=43	3.425E 01	1.7/75=02
5.652E 01	1.319E 01	1,319E 01		43.991E 0	2 -5.30SE	03 #1.689E 03	3.245E 03	3.393E 01	1.760E-02	3.393E 01	1.760E=02
5.680E 01	1.275E 01	1.275F 01	5.340E U2	=4.021E 0	3 =2.516E	03 -1.705E 03	3.280E 03	3.280E 01	1.7015-02	3.280E 01	1.701L=02
5,703t 01	1,2216 01	1.221E 01		-9.046E 0	2 -2.327E	03 -1.718E 03	3.309E 03	3.140E 01	1.629E-02	3.140E 01	1.629E=02
5.775E 01	1.0475 01	1.0475 01		#4.119E 0	-2.35RE	03 =1.761E 03	3.402E 03	2.693E 01	1,397E=02	2.693E 01	1.397E=02
5.477E 01 6.078E 01	5.437E 00	5.437E 00		#4.205F 0	> =2.394E	03 -1.8118 03	3.532E 03	1.399E 01	7.2556-03.	1,399E 01	7.255E=03
6.650F 01	1.5798 01	1.721E, 01 1.579E 01	ም ዕዝንድ "ል 34466 ብሄ	=4.344E 0	3 M2.442E	03 -1.907E 03	3.790E U3	4.428E 01	2.297E-02	4.428E 01	2.297E=02
~ * F F O F A T	, work wi	240175 91	J# 7500 UE		J ₩ € 0 4 / D L	03 -1.982E 03	3,972E 03	4.061E 01	2.106E=02	4.061E 01	2.106E=02

YABS	P-18	P=08	PTA	OOX	(a= I f•	Q≈CB	CANALL	F#IB/PSD	P#IB/PTU	P+06/PS0	P=08/P10
6.466E 01	1,894E U1	1.6948 01	5.980c 02	#4,6/6E 03	-2.560E 0	3 -2.116E 03	4.269E U3	4.671E 01	2.5271=02	4.871E 01	2.5276=02
6.504E 01	1.991E 01	1,9420 01	5,9801 02	=4./17E 03	-2.576E U	3 =2.141E 03	4.337£ U3	5.122k 01	2.6576-02	4.995E 01	2.591E+02
6.508E 01	1,9916 01	1.947E 01	5.980F 02	-4.721E 03	-2.578L 0	3 w2.143F 03	4.3426 63	5.122E 01	2.657E+02	5.008E 01	2.598E-02
6.528E 01	1.885E 01	1.972F 01	5.980L UZ	#4.742E 03	+2.587£ 0	3 -2.1556 03	4.368E 03	4.848E 01	2,5156-02	5.074E 01	2,6326,02
6.694E 01	1.001E 01	9.533E 0	7.5998 02	●4.891E 03	-2.547E 0	3 -2.244E 03	4.583E 03	2.575E 01	1.336E#02	2.451E 01	1.2726=02
6.761E 01	7.251t 00	9.217E 00	9.4206 02	#4.942E 03	#2.605E U	3 -2.277E 43	4.6055 03	1.865E 01	9.6746-03	2.371E 01	1.2304-02
0.838E 01	4.080E 00	7.015E 00	1.1298 03	-4.999E 03	#2.681E 0	3 -2.318E 03	4.760E 63	1.049E 01	5,444E-03	1.804E 01	9.359E=03
6.910E 01	3,176£ 00	4.955E 00	1.250E 03	#5.055E 03	#2.693E 0	3 -2.362E 03	4.6486 03	8.169E 00	4.237L-03	1.275E 01	6.611E=03
6.971E 01	2,410E 00	4.060E 00	1.3286 03	-5,100E 03	#2.707E 0	3 =2,399E 03	4.922£ 03	6.1998 00	3,215E=03	1.04ME 01	5.416E=03
7.066E 01	1.701E 00	2.465E 00	1.412E 03	-5.156E 03	-2.712E 0	3 42.444F 03	5.036E 03	4.375E 00	2.269E=03	0.855E 00	3,556E#03
7.109E 01	1.3806 00	2.477E 00	1.4406 03	45.176£ 03	-2.715E 0	3 02.461E 03	5.088£ 03	3.550E 00	1.841t-05	6.373E 00	3.305E=03
1.262E 01	1.453E 00	1.810F 00	1.523E 03	95.234€ 03	-2.726E 0	3 -2.508E 03	5.273E 63	3.737E 00	1.938Emu5	4.656F 00	2.415E=03
7.277E 01	1.460E 00	1.698E 00	1.530E 03	-5.239E 03	-2.727E 0	3 02.512E 03	5,290E 03	3.756E 00	1.948E=03	4.369E 00	2.266E=03
7.352E 01	1.304E 00	1-140E 00	1.578E 03	-5.268E 03	#2.732E 0	3 =2.535E 03	5.374E 03	3.510E 00	1.8206=03	2.932E 00	1.521E=03
7.352£ 01	1.364E 00	1.1376 00	1.5816 03	-5.268E 03	-2.732E 0	3 +2.536E 03	5.375L 03	3.508E 00	1.820£003	2.925E 00	1.517E=03
7.485F 01	1.195E 00	0.000	1.608E 03	₩5.324E 03	-2.740E 0	3 -2,583E 03	5,427E 03	3.074E 00	1.5946=03	0.000	0.000
7.770E 01	2.405£ 00	0.000	1.681E 03	-5.359E 03	#2.756E 0	3 42.583E 03	5.525E 03	6.341E 00	3,289E=03	0.000	0.000
8,160E 01	1.600E 00	0.000	1.768E 03	-5.357E 03	-2.774E 0	3 -2.583E 03	5.630E 03	4.116E 00	2.135E+03	0.000	0.000
8.441E 01	1.380E 00	0.000	1.801E 03	●5.574E 03	-2.791E 0	3 w2.583F 03	5.684E 03	3.550E 00	1.8416=03	0.000	0.000
8.727E 01	2.760E 00	0.000				3 +2.583E 03	5.707E 03	7.0998 00	3,6828=03	0.000	0.000
8.728E 01	2.763E UD	0.000	1.851E 03	-5.402E 03	#2.819E 0	3 -2.583E 03	5.707£ 03	/.107E 00	3,686E=03	0.000	0,000

ORIGINAL PAGE IS OF POOR QUALITY	

RANJET PERFURMANCE

ENGITE PERFURNANCE	INLET
CO CALCULATED THAUST	ANGLE OF ATTACK
REGENEUATIVERCUDLED ENGINE PERFORMANCE CALCULATED SIMEAM (HKUST	INLET PROCESS EFFICIENCY = SUBSUNIC 0.800/ KINETIC ENERGY EFFICIENCY = SUFENSONIC 0.9279 KINETIC ENERGY FFFICIENCY = SUBSUNIC 0.8819 ENTHALPY AT PO = SUPERSONIC = 3.68 (btu/lbm) ENTHALPY AT PO = SUPERSONIC 28.24 (BTU/lbm)
MOMENTUM AND FORCES	COMBUSTOR
INLET FRICTION DRAG	FUEL=AIR RATIO
STATIONS	FUEL INJECTORS
SPIKE TRANSLATION STATE THROAT	INJECTORS STATION VALVE 1A 40.400 A 1B 41.286 B 1C 44.300 2A 48.761 D 2C 46.250 E 3A 54.051 3B 56.236 4 44.766

Reading 69

t = 256.20 sec.

3-3-75

SUPMARY PEPORT .

J					•					(F F	,	•						
\supset	p	T	•		CAAFY	MOLAT	SAKV	MACH	VEI	5	~/A	W	A/AC	HCHTH	ĸ	TVAC	PH7	ETAC
	MING TUNNEL	. 1	0 5							•			~,~,	- ,		A 7 - U		£ 1.~C
	0.000 749,249	3049	685.7(811)	1,2921	28.860	2605											
	0.000 0.401	416	= 28 _* e (1011	1.3989	26,659	1003	5,960	5979	1.633	0.10732	24.978	0.9815	5114	9,972	189.6		
	SPIKE TIP AS	2	0 3				_											
	0,690 18,025	F		8(1)	1.2919	28,659	2605											
	WIND TUNNEL		663.46	784)	1.2943	28,859	2576	0.410	1056	2.089	0.10732	26.97A	0.9815	4955	1.761	183.7		
	0.000 749.249	3 30/19	0 0	9.43	4 2024	20 044	7675											
	0.000 0.379			offi	1,2721	20,000	2005	4 - 1 -										
	SPIKE TIP NS	4	0 0	947	1,2400	E0 * #24	449	9,012	2769	1.855	0.10371	25.945	0.9815	4922	9.000	189.7		
	0.600 18.025	-	-	Aiti	1 2010	24 850	2665											
	0.600 10.346		669.46	7011	1.2041	24.859	2578	0.391	1000	2.080	0.10321	25.045	0.0815	11000	1 417	100 7		
	INLET THROAT	5	0 3	. ,	.,		F-77.		1000	24001	441.4561	634743	0.4013	4766	1.617	16947		
	40.400 294.334	2987	666.7(792)	1.2941	28,859	2580											
	40,400 15,930	1468	234.10	363)	1.3506	28.859	1848	2.518	4653	1.891	0.94314	26.978	0.1117	4357	68,196	161.5		
	TNLET UPNESK	6	0 3					-	-	-•		,						
	40.400 294.334		666.71	792)	1.2941	26.859	2580						•					
	40.400 13.685	1411	219.00	348)	1,3539	28.859	1814	5.609	4733	1.891	0.85740	26.978	0.1228	4399	63.066	163.1		
	THLET ONNESK	2007	0 4						-									
	40,400 124,301 40,400 106,757	290/	666.71	/92]	1,2941	28.859	2580											
	COMBUSTOR 0	8 8	636.00	166)	1,2972	59.859	2939	0,484	1241	1,950	0.85740	26,978	0,1228	4399	16.530	163.1		
	40,410 253,715			R. 71	4 2047	37 444	2434											
	40.410 14.951			3011	1 261/	27.660	1801	2 //67	***	1 047	0.94623	27 474						
	COMBUSTOR 0	-	5 51	3011	143310	FIEGOV	.073	C 0 40 1	4004	10401	0.44852	21.010	0.1117	4330	68.662	190.9	0.11	0.07
	41.586 148.845		671.20	8233	1.3000	26.575	2644											
	41.286 18.445	1611		4-5	1.3057	26.575	2014	2.194	4420	2.040	0.95147	27-157	0.1114	4257	65,355	124.8	מב ח	0.0/
-	COMBUSTOR 0	10	3 21							484-0	0.13141	C. 8 () .		4551	025222	120,00	0 0 6 5	0404
	41.296 207.308	2841		8;1)	1.3015	26.534	2632											
	41.296 18.484		281.20	424)	1,3482	26,534	1992	2,218	4417	2,033	0.95178	27,157	0.1114	4256	65.339	156.7	0.22	0.01
	COMBUSTOR 0	11	4 21										•			• • -		
	41.361 206.020			8097	1,3021	26.528	2630											
	#1:361 18:744 COMBUSTOR 0	-	इ.७५० इ.८	425)	1,3480	26,578	1994	5,206	4399	2,033	0.95184	27.157	0.1114	4248	65.070	156.4	0,22	0.00
	41,500 201,248	12	5 21	0 - 0 >	1 7025	34	3430											
	41.500 20.221			nnoj	1 3/161	26 527	2017	5 484	0730	3 675	A 055.4	**			4			
		13	6 21	-301	113401	501251	6411	2 . 1 40	4364	2.035	0.95240	2/4157	9.1113	4231	64.073	155.8	0.22	0.00
	42.460 187.224		665.61	8681	1.3027	24.527	2625											
	42.460 20.967		306.40	4471	1.3443	26.526	2038	2.080	4240	2.038	0.94150	27.167	0.1124	4182	62,165	154 6	0 22	0.00
		14	7 6				27.24		72.40		007	21111	1141154	4102	GE 3 1 5 3	12410	0.22	u .
	44.081 119.320			047)	1.2638	27.460	2877											
	44.081 42.818	-	413.46	816)	1,2887	27.467	2600	1,335	3472	2.124	0.91173	27.157	0.1163	4206	49.193	154.9	0.22	0.79
		15	8 3						•									
	44.310 117.396			063)	1,2610	27,529	2891											
	44.310 45.073	_	466.96	844)	1,2848	27.537	2633	1.287	3389	2.127	0.91041	27,157	0.1165	4205	07.944	154.8	0.22	0,85
	CDMBUSTOR 0 44.796 114.149	16 2764	6/17 4 6 4			A4												
				0 4 E +	1 2777	27 440	4413	4 401	7365	A 4								
		17	442.3(10 2	1.421	T#2111	< (0 000	COAS	1 1 1 7 1	2605	c.132	0.40657	27.157	0.1170	4199	45,159	154.6	0.22	0 • 94
	44.800 114.104		647.6(1	0501	1.2544	27.454	2012											
	44.800 49.896	3157	442,5(8061	1.2776	27.661	2602	1.190	3500	2.182	0.00477	37 167	A 41 TC	4100	45 45		A AM :	
	COMBUSTOR 0	18	11 6	7-7		-: +001	44.6	-04,0	7604		V + TV D 3 /	210131	A#1710	4144	45,124	124.0	4.65	ロ・ソコ
	46.250 106.490	3373	459.5(1	0#2)	1.2778	24.363	2966											
	46.250 52.998	2886	461.5(300)	1.2942	24.345	2762	1,050	2984	2.317	0.86321	27.437	0.1241	ويروي	40.026	150.1	0.57	0.32
			•			•		-		•								~ # - -

READING #	0069	BLOCK	e 159	TINE	E 254.2	04 M4C	н оф	0 PT	= 749	.244	T7 = 304	9 0						
	Þ	T	Ħ		GAMPA	ዘቡር ሣፕ	SONV	масн	VEL	5	*/A	٨	A/AF	MOPTM	Ç	IVAC	Pnj	ETAC
COMBUSTOR 46.260 1	06 443	19	12 2	4 / 6 3 !		34 744	٠٠. ٦										-	
46.260	53,020	2891	481.5	(9 i 0 i	1,2777	24.300	2763	1.080	PORT	3.317	0.86255	27.//17	A (2/1)	4220	70 084	. E /: -:	,	A 27
COMBUSTOR	0	20	13 4						£ 7g	E # 2 4 7	0100533	611431	94(545	4230	34,986	12445	0.01	V . 3 C
47.310 1	02.523	3674	647.3	(1184)	1.2620	24.710	3054											
47.310 COMBUSTOR	22,466	21	4/0.2	(105%)	1.2782	24.717	2878	1.017	5956	2,337	0.80276	27,437	0.1334	4365	36.509	159.8	0.57	0.46
				(1146)	1.2618	24.714	3055											
47.321	55.336	3227	476.3	(1023)	1.2779	24.722	2880	1.015	2924	2.338	0.80214	27.437	0.1335	4386	36,452	159.9	0.57	0.46
COPAUSTOR		2020		a = E .		25 024	3130											
08.110	52.842	3470	454.9	(1873) (11a5)	1.2469	25.040	2952	1.027	3032	2.151	0,74810	27.437	0.14%2	4524	35.250	(68.0	0.57	n EQ
COMBUSTOR	0	23	16 6						3425		011-015	W . A . A .	(0143E	7.4.	379530	10007	0.57	0 6 3 7
48.761 48.761	94.094 42.495	3580	650 - 0	(1264)	1.2683	22.404	3175		7									_
COMBUSTOR		24		(1000)	1,2002	22,404	5424	10101	3407	5,523	0.69705	27,709	0,1552	4623	36.905	166.9	0.91	0.34
48.771	94.049	3582	649.9	(1264)	1,2682	22.405	3175											
48,771	42,340	3012	417.1	(1040)	1.2882	22,411	2934	1,103	3413	2,523	0.69614	27.709	0.1554	4625	36,923	166.9	0.91	0.34
COMBUSTOR 49.301		25 3633		* (2031	1.2654	22.466	3100											
44.201	35.162	2944	364.2	(1013)	1.2896	22.473	2898	1,293	3749	2.527	0.65106	27.709	0.1662	4725	37.930	170.5	0.91	0.36
COMBUSTOR	.0	26	19 5														V • · · ·	
50.711 50.711	31.312	4015 7290	724.5	([428) *****	1.2431	22.870	3294	+ 705	7070	2 662	0.55488	74 746	0 4050					
COMBUSTOR	0	27	20 u					1.300	3733	æ • >> /	8422400	2/8/04	0.1990	4452	33.930	178.7	0.91	0.48
52.811	77.335	4243	619.5	(1514)	1.2276	23.140	3345											
52.81 <u>1</u> COMBURTOR	24.012	33 <i>32</i> 28	220.91	(1144)	1.2657	23.189	3007	1.485	4456	2.573	0.45479	27.709	0.2379	5224	31.565	188.5	0.91	0.57
				(15n2)	1,2296	23.116	3338											
53.311	20.275	3555	188.4	(1108)	1.2702	23.163	2965	1,561	4628	2,571	0,43620	27.709	0.2480	5274	31.373	190.3	0.91	0.56
COMBUSTOR	0 76.378	5.9	55 7														- •	•
				(1212) (1099)	1,2270	23,218	2953	1.611	075A	2.573	0.41116	27.709	0.2611	5340	30,401	102 7	۸ ۵۱	A 57
COMBUSTOR	0	30	23 3				L		-,-5	293.3	4041110	1m * 4 0 *	012031	2340	301401	17601	V . 7 I	0 2 2 1
	75.892			(1515)	1.2268	23.172	3344								_			
COMBUSTOR	100212	3130	24 4	(1473)	1.2/20	230223	5454	1.6/2	4848	2.573	0.38883	27,709	0.2782	5399	29,595	194.9	0.91	0,58
55,760		4302	603.6	(1536)	1,2227	23.241	3354											
750760	15.277	3156	104+6	(1078)	1.2708	23.304	2925	1.708	4997	2.577	0.36475	27.709	0.2966	5464	28,325	197.2	0.91	0.60
COMBUSTOR 56.246			25 5	****	1.1838	21.742	2025					•			•			
96.246	14.605	3801	114.6	3 9 9	1,2318	23.948	3118	1,583	4936	2.615	0,29396	27.709	0.3680	5628	22.551	20%.1	0.01	0.78
COMBUSTOR	0	33	26 5					-						•		40011		
	66.942 11.239		38.8	(1560) (10/7)	1.2172	23,315	3366	t . n % 0	RZNL	2 560	0,29319	37 700	A = 4 B A	C 4 7 4	.			
COMBUSTOR		34	27 3	(104.)	186167	234373	2000	1 6 (1 4)	33110	E + 300	0.27317	21+104	0.3090	2021	24.174	205.2	0.91	24.0
	66.740		600.7	(1563)	1.2166	23.324	3368											
56.441 CO⊬BUSTOR	11.143		25 -8(25 21	(1048)	1.2722	23.404	9886	1,842	5317	2.589	80195.0	27.709	0.3717	5640	24.051	203,5	0.91	0.63
56,521	51.908			(1847)	1,1527	24.125	3080											
56.521	14.225	4349	101.00	(1527)	1.1768	24.594	3216	1.554	4999	2.626	0.29434	27.709	0.3675	5644	22.867	203.7	0.91	1.00
'COMBUSTOR 56.801	0 151.52	36	59 51										•= • • •					
	13.837				1.1528			1.874	505#	2.626	0,29337	27.760	A 4600	E4E0	37 004	201 5		
COMBUSTOR	0	37	30 21	1 - 3		~ 7 5 0 0 D	2610	• # 31"	J V J 4	# # ne p	V \$ 6 7 3 3 /	E/8/04	",5000	7037	23.041	204.2	0.91	1,00
	52.041		578.5	1846)	1.1528	24.128	3483			_								
57.027	13,072	4673	40.96	(1200)	1,1799	24.018	319A	1,609	5148	959.5	\$6262.0	27.709	0,3693	5670	23,433	204.6	0.91	1.00

33 11

GAMMA I OLWT SONV MACH VFL 9 AZAC MUNTH G IVAC PHI ETAC COMBUSTOR 0 38 31 21 ₩ 57.751 50.292 5101 595.811844) 1.1526 24.127 3461 N 57.751 19.620 4182 7.7(145A) 1.1860 24.659 3162 1.716 5425 2.628 0.28827 27.709 0.3753 5693 24.304 205.5 0.91 1.nu 0 39 32 21 COMBUSTOR 58.771 40.622 5071 592.8(1832) 1.1508 24.102 3470 58,771 5.887 3937 -116.1(1359) 1.1993 24.722 3082 1.933 5956 2.645 0.28644 27,709 0.3777 5699 26.511 205.7 0.91 1.00 COMBUSTOR 0 40 33 21 60.781 54.176 5101 587.6(1943) 1.1536 24,148 3881 60.781 10.837 4410 134.2(1552) 1.1748 24.573 3238 1.471 4763 2.620 0.29641 27.709 0.3650 5676 21.939 204.6 0.91 1.00 COMBUSTOR 0 41 34 21 62.201 54.955 5099 583.8(1842) 1.1539 24.155 3480 62.201 16.050 4368 108,5(1535) 1.1772 24,594 3224 1.512 4875 2.618 0.30444 27.709 0.3553 5659 23.065 204.2 0.91 1.00 COMBUSTOR 0 42 35 200 64 665 51.648 5083 576.0(1835) 1.1537 24.157 3474 64.665 18.230 4469 170.1(1577) 1.1717 24,543 3257 1.384 4506 2.622 0.28857 27.709 0.3749 5631 20.208 203.2 0.91 1.00 COMBUSTOR 0 43 36 200 65.041 47.717 5071 574.6(1831) 1.1530 24.149 3470 65.041 19.594 4553 224.6(1612) 1.1670 24.491 3284 1.274 4184 2.628 0.26828 27.709 0.4032 5627 17.445 203.1 0.91 1.00 COMBUSTOR REGEN 44 37 3 65.041 47.717 5150 648.2(1865) 1.1501 24.045 3500 65.041 17.121 4564 240.3(1617) 1.1641 24.462 3286 1.375 4518 2.643 0.26828 27.709 0.4032 5659 18.635 204.2 0.91 1.00 NOZZLE AE 45 38 5 87.277 47.717 5071 574.6(1791) 1,1530 24,149 3470 87.277 1.301 2849 -583,1(933) 1.2642 24,824 2686 2.834 7611 2.628 0.05585 27,709 1.9371 7200 6.606 259.9 0.91 1.00 NOZZLE PO 46 39 87.277 47.717 5071 574.6(1791) 1.1930 24.149 3470 87.277 0.401 2209 0820.2(698) 1.2877 24,826 2387 3.501 8394 2.628 0.02439 27,709 4.4358 7651 3.166 276.1 0.91 1.00 NOZZLE AE REGEN 47 40 87.277 47.717 5150 '648.2(1865) 1.1501 24.045 3500 87.277 1.346 2978 -533.2(982) 1.2589 24.822 2740 2.806 7689 2.643 0.05585 27.709 1.9371 7290 6.673 263.1 0.91 1.00 MOZZLE PO REGEN 48 41 47.717 5150 648.2(1865) 1,1501 24.045 3500 87,277 67.277 0.401 2299 -787.8(730) 1.2842 24.826 2431 3.486 8477 2.643 0.02378 27.709 4.5501 7768 3.132 280.3 0.91 1.00 FICTIVE COMBUSTR 68 61 294.334 5273 574.6(1910) 1.1704 24.372 3548 45.041 45.041 0.401 1427=1087.60 4301 1.3268 24.826 1947 4.684 9121 2.479 0.04121 27.709 2.6250 6125 5.841 293.2 0.91 1.00 69 62 0 FICTIVE NOZZLE 87.277 32.746 5001 551.3(1802) 1.1506 24.131 3443 87.277 . 1.538 3153 -463.8(1049) 1.2504 24.817 2810 2.536 7127 2.654 0.05585 27.709 1.9371 6901 6.186 249.1 0.91 1.00

	W 4 0 =	r. +B	0.00	nn 1	i30 X	₽ ₹19		an∍ū		CEMALL	P=Tb/PS0	P=1P/P10	P#08/P80	P-CP/PTQ
	XABS	P#IB	P#OB	PNA		-						48E=03		0.000
	5.9¤1F#11	1.0856 00	0.000	-4.397E=01	១∗១០០	0.000		0.000		2.4706-02	2.703E 00		0.000	•
	1,836E 01	1.085E 00	0,000	#3.611E 01	0.000	0.000		0.000		1.634E C2	a , 793F 90	1.00BE=03	0.000	0.000
	3.070E 01	2.455E 00	0.000	#1.796E 02	0.000	₽ • 0 € ₽		0.000		5.153E 02	6,117F 00	3.277t-03	u•00\$	0.000
	5.508E 01	4.031E 00	0.000	-3,898E Q2	0.000	0.000		0.000		6,804E U2	1.004E 01	5,380£=03	u.000	0.000
	3.51RE 01	4.069E 00		## 567E 02	0.000	0.000		0.000		6.84RE 02	1.014E 01	5.431E=03	1.474E 01	7.895E-03
	5.518F 01	4.072E GO		a4.567E 02	0.000	0.000		0.000		4.851E 02	1.0156 01	5.434E=03	1.466F 01	7.851E=03
	3.555F 01	4.215E 00		*4.654t 02	0.000	0.000		0.000		7.217E 62	1.0508 01	F.626E=03	9.661E 00	5.175E=03
										7,5228 02	1.027F 01	504E-03	5.544F 00	2.970E=03
	3.585F 01	# 124E 00		=4.802E 02								5.019E=03	7.645E 00	U 095E=03
	3,606E 01	4.060E 00		=4.915E 02						7.736E 02	1,012F 01			
	3.648E 01	4,306E 00		-5.110E 02						8.174E U2	1.0738 01	5.747E=03	1.187E 01	6.356E=03
	3.701E 01	4.460E 00	6.899F 0n	-5.358E 02	-3.610E	02 -3.479	E 02	-1.311F	01	8.733E 02	1.111E 01	5.953E=03	1.719F 01	9.208E=03
. :	5.731E 01	4.318E 00		■5.477E 02					01	9.056E 02	1.0768 01	5.764E-03	2.021E 01	1.083E-02
	3.803F 01	3.980E 00		-5.635E U2					01	9,A42E 07	9.917E 00	5.312E=03	3.376E 01	1.8U9E=02
	3.833F 01	5.580E 00		-5.425E 02						1.01AE 03	1.390E 01	7.047E=03	3,943E 01	2.112E=02
	3.875E 01	7.808E 00		-5.648E 02						1.05E 03	1.945E 01	1.0426-02	3.849E 01	2.062E=02
		8.078E 30		⇒9.653E 02						1.071E 03	2.013E 01	1.0781.02	3.837E 01	2.055E=02
	3.880E 01	-	10340- 1	-74073E VE	-416100	^2 =3 = · U =	C 07	-1 0000	× 1	1.095E 03	2.290E 01	1.227E=02	3,901E 01	2 0906-02
	3.901E 01	9,190E 00	1.500F V)	•5,661E 02	9443046	02 =3.707	E UZ	73.7735	7.1					· ·
	3.931E 01	1.360E 01		=5.719E 02						1.129E 03	3,3896'01	1.815E+02	3.993E 01	2.139E=02
	3.950E 01	1.637E 01	1.336F 01	.5.795E 02	=4.605E	02 -4.142	E 05	-4.632E	01	1.151E 03	4.050E 01	2.186E=02	3.329E 01	1.783E=02
	3,980E 01	1.710E 01	9.125E 00	=5.970E 02	44.763 E	02 =4.262	E 02	≈5.013E	01	1.186E 03	4.260E 01	2,282E-02	2.274E 01	1,218E=02
	4.000€ 01	1.757E 01	9.059F 00	-6.109E 02	44.874E	02 -4.348	E 02	⇔5 ,262€	01	1.210E 03	4.378E 01	2,345E+02	2.257E 01	1.209E=02
4	4.040E 01	2.090E 01		-6.401E 02						1,257E 03	5.207E 01	2,789E=02	2.224E 01	1.191E#02
	4.041E 01	2.098E 01		#6 408E 02						1.258E 03	5.227E 01	2.800F-0S	2.223E 01	1.191E=02
	4.129E 01	2.825E 01		-7.222E 02						1.361E 03	7.041E 01	3.7726=02	2.151E 01	1.152E+02
	4.130E 01	2.A34E 01		-7.231E 02						1.362E 03	7.062E 01	3.783E=02	2.150E 01	1.152E=02
		2.8888 01								1.370E 03	7.196E 01	3.8556-02	2.144E 01	1.149E=02
	4.136E 01			₩7.301E 02									2.592E 01	1.389E=02
	4.150F 01	3.004E 01		-7.848E 02						1.387E 03	7.484E 01	0.009E=02		
	4.5496 01	1.912E 01		⇒7.758E 02						1.502E 03	4.765E 01	2.553E=02	5,683E 01	3.044E-02
	4.40AE 01	4.188E 01		-7.250E 02						1.698F 03	1.043E 02	5,5905+02	1.090E 0S	5,840E-02
	4.431E 01	4.910E 01		■7.224E 02						1,726E 03	1.124£ 02.	6.019E=02	1.122E 02	6,013E=02
	4.480E 01	5.192E 01	4.779F 01	-7.201£ 02	-1.559E	03 08.61 2	E na	■3 。646E	0.2	1.785E 03	1.294E 02	6.929E=02	1.191E 02	6.379E=02
	10 3084.4	5.197E 01	4.782# 01	■7.200£ 02	01.227E	03 mB.619	E 02	03,651E	02	1.785E 03	1.2956 02	6.937E=02	1.191E 02	6.382E=02
	4.625E P.L	4.999E U1	5.600F 01	6.196E 02	≈1.666E	03 -1.089	E 03	=5.771E	0.5	1.9648 03	1.246E US	6,672E=02	1.395E 02	7.4756-02
	4.626E 01	4.998E 01		a6,181E 02						1,965E 03	1.2458 02	6.671E=02	1.397E 02	7.482Em02
	4.731E 01	4.854E 01		64.492E 02						2.095E 03	1.2108 02	6.479E-02	1.545E 02	8.2736-02
	4.732E 01	4.862E 01		#4.472E 02						2.096E 03	1.212E 02	6.490E-02	1.546E 02	8.282E=02
	4.8118 .01	5.435E 01		-2.992E 02						2.195E 03	1.354E 02	7.254E-02	1.2795 02	6.8516-02
										2,276E 03	1.0596 02	5.672E=02	1.059E 02	5.672E-02
	4.876F 01	4.2508 01		=1.567E 02										
	4.877E 01	4.236E 01		*1.545E 02						2.277E 03	1.055E 02	5.6546=02	1.0558 02	5,654E=02
	4.930E 01	3.516E 01		-4,739E 01						2.344E 03	8,761E 01	4.693E=02	8.761E 01	4,693E=02
	5.071E 01	3.131E 01	3.131E 01							2.521E 03	7.802E 01	4.179E=02	7.802E 01	4,179E=02
	5.281F 01	2.261E 01	5.361E 01							2.788E 03	5.634E 01	3.018E#02	5.634E 01	3.018E=02
	5.331E 01	2.027E 01	2.027F 01	5.510E 02	-3.344F	03 -1.923	E OT	-1.421E	03	2.852E 03	5.052E 01	2.706E=02	5.052E 01	2.706E=02
	5,406E 01	1.844E 01	1.8442 01	6.259E CP	-3.4638	03 -1.989	E 03	91.477E	03	2.947E 03	4.594F 01	2.461E=02	4.594E 01	2.461E=02
	5.482E 01	1.657E 01	1,657F 01	6.937F 02	-3.574F	03 -2.042	E 03	#1.532F	0.3	3.045E 03	4.130E 01	2.212E=02	4.130E 01	2.212E=02
	5.5768 01	1.528E 01	1.528F 01							3,165E 03	3.806E 01	2.039E=02	3.806F 01	2.039E+02
	5,6258 01	1,460E 01	1.460F 01							3.209E 03	3.6398 01	1.949E=02	3.639E 01	1.9496=02
	5.630E 01	7.950E 00	1.453E 01							3.216E 03	1.981E 01	1.061E-02	3.620E 01	1.939E=02
										3.234E 03	1.981E 01	1.0616-02	3.572E 01	1.913E>02
	5.644E 01	7.950E 00	1.434E 01											
	5.052E 01	1.422E 01	1.42SE 01							3.245E 03	3.544E 01	1.899E=02	3.544E 01	1.899E=02
	5.680E 01	1.384E 01	1.3845 01							3.580F 03	3.448E 01	1.847E=02	3.448E 01	1.847E=02
	5.703E 01	1.307E 01	1.3078 01							3.309E 03	3.257F 01	1.745E=U2	3.257E 01	1.745E=02
	5.775E 01	1.062E 01	1.062E 01							3.492E 03	2.646E 01	1.417E+02	2.646E 01	1.417E=02
	5.877E 01	5,887E 00	5.887F 00							3.532E 03	1.4678 01	7.858E=03	1.467E 01	7.858E-03
	6.07AE 01	1.684E 01	1,6845 01							3.790E 63	4.195E 01	2.247E=02	4.195E 01	2.247E-02
	6.220E 01	1.605E 01	1.605F 01	1.040E 03	04,251E	03 -2.305	E 01	=1.946E	0.3	3.972E 03	3.999E 01	2.142E=02	3.999E 01	2.142E=02

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RAAX	Pale	P+08	₽D.A	O O X	6=18	90*0	CAAALL	P=18/P50	P+18/PT0	P=C:3/PS0	P=0B/P10
6.4668 11	1.423E 01	1.823# 01		-4.468E 03		3 -2.084E 03	4.2898 03	4.5426 01	2.433E=02	4.542F 01	2.433E=02
6.504F 01	2.062E 01	1.856E 01	1.040E 03	₩# 507E 03	#2.400E 0	3 -2.107F 03	4.37E 03	5,139F 01	2.753t-02	# 625E 01	2.477E=02
6.50AF 01	2.062E)1	1.860F 01	1.040E U3	-4.511F 03	-2.40PE 0	3 +2,109F 03	4.3426 63	5,139F 01	2.753E-62	4.634F 01	5.485E=05
6.528E 01	1.954E 01	1.8777 01	1.040E 03	#4.531E 03	-2.410E 0	3 -2.121E 03	4.36BE 63	4.868E 01	2.607E=02	4.678E 01	2.506E+02
6.694E 01	1.050E 01	9.2407 00	1,201E 03	#4.675F 03	#2.466E 0	3 +2.209E 03	4.583£ (3	2,616E 01	1.401E=02	2.302E 01	1.2336.02
6.761E G1	7.510E 00	9.247E 00	1.385E 03	-4.723E 05	-2.483E 0	3 -2.241F 03	4.665E 03	1.871E 01	1.0026-02	2.304E 01	1.234E-02
6.838E 01	4.075E 00	7.045F 00	1.575E 03	=4.778F 03	-2.499E 0	3 +2.280F 03	4.760E 03	1.015E 01	5.039E+03	1.755F 01	9.402E=03
6.910F 01	3.466E 00	4.985E 00	1.698E 03	#4.833F 03	#2.510E 0	3 +2.323F 03	4.048E 03	8.636F 00	4,626E=03	1.2426 01	6.653E=U3
6.971E 01	2.950E 00	4.1466 00	1.782E 03	=4.877E 03	-2.51AE 0	3 -2.359E 03	4,922F 03	7,350E 00	3.937E#03	1.033E 01	5.534E=03
7.066E 01	1.904E 00	2.840F 00	1.874E 03	#4.929F 03	₩2.527E 0	3 -2.40ZE 03	5.036E 03	4.743E 00	2.541E=03	7.076E 00	3.790E>03
7.10gF 01	1.430E 00	2.6356 00	1.905E 03	≈4.947E 03	-2.530E 0	3 02.417E 03	5.08RE 03	3,563E 00	1,909E=03	6.565E 00	3.517E=03
7.262E V1	1,5446 00	1.9050 00	1.993E 03	-5.002E 03	≈2.540E 0	3 =2.4620 03	5.273E 03	3.847E 00	2.061E#03	4.747E 00	2.543E=03
7,2775 01	1.555E 00	1.796E 00	2.000E 03	-5,006E 03	-2.540E 0	3 ±2.466E °3	5 , 290£ 0%	3.8745 00	2.0756=03	4.475E 00	2.397E=03
7.352E 01	1.625E 00	1.250E 00	2.052E 03	-5.033E 03	-7.545E 0	3 -2.489F 03	5,374E 03	4.05UF 00	2.1696=03	3.115E 00	1.668E=U.
7,352F 01	1.626E 00	1.247E 00	2.055E 03	*5.033E 03	-2.545E 0	3 =2.489F 03	5.375E 03	4.051F 00	2.170E=03	3.197E 00	5.664E=03
7.485E 01	1.750E 00	0.000				3 =2.535E 03	5.427E 03	4,360E 00	2.336E=03	0.000	0.000
7.770E 01	2,550E 00	0.000	2.177E 03	-5.100E 03	*2,565E 0)3 =2.535E 03	5.525E 03	6.354E 00	3.403E=03	0.000	0.000
8.160E 01	1.775E OF	0.000)3 +2.535E 03	5.630E 03	4.423E 00	2.369E=03	0.000	r•000
8-441E 01	1.660E 00	0.000				3 -2.535E 03	5.684E 03	4.136F 00	5.516F-03	0.000	0.000
8,727E 01	3,240E VO	0.000				3 +2,535E 03	5.707E 03	8.073E 00	4.3242-03	0.000	0.000
8,728F 01	3,243E 00	0.000	5.309E 03	≈5.152E 03	#2.617E 0	3 =2.535E 03	5.707E 03	8.081E 00	4.329E=03	0.000	0.00

×	DDRAG	CDRAG	CF	нс
4.040E 01 4.041E 01	1.912E U2	1.212E 92	2.214E=03	4.302E#02 4.055Em02
4.129E 01	1.766E 01	1.391E 02	2.604E-03	4.675E002
4.130E 01	1.9125=01	1.393E 02	2.4072+03	4.951E#02
4.136E 01 4.150E 01	1.208E 00	1.405F 02	2.382E=03	5.032E=02 5.283E=02
4.2466 01	1.746E 01	1.6055 07	2.4161=03	5.319E=02
4.40BE 01	2.700E 01	1.675F 02	2,52°E - 03	7.866E=02
4.431E 01 4.480E 01	3.701E 00 8.178E 00	1.912F 02	2.947E⇔03 2.977E⇔03	6.908E#02 7.063E#02
4.480F 01	6.459E=02	1.994# 02	3.017E+03	6.902E=02
4.625F 01	2.387E 01	2.2335 05	3.2775-03	6.7105=02
4.626F 01 4.731E 01	1.560E=01 1.472E 01	2.235e 05	2.974E=03 2.938E=03	7.477E=02 7.569E=02
4.732E 01	1.432E=01	2.383E 02	3,067E=03	7.2206-02
4.811E 01 4.876E 01	1.074E 01	2,4915 02	3.022E=03	7.1536.02
4.876E 01 4.877F 01	9.234E 00 1.448E=01	2.5835 02 2.584F 02	3.263E=03 3.000E=03	6.198E#02 6.775E#02
4,930F 01	7.382E 00	2.658F 02	2.934E=03	6.267F=02
5.071F 01 5.281E 01	1,853E 01 2,522E 01	2.844E 02	2.875E=03 2.908E=03	5.790E=02 4.576E=02
5.3318 01	5.912E 00	3.096E 02	2.908E=03	4.1458.02
5.406E 01	8.779E 00	3.243E 02	2.944E003	3.913E=02
5.482E 01 5.576E 01	8.581E 00 1.020E 01	3.328# 02 3.430E 02	2,9316-03 2,903E-03	3.632E∞02 3.427E∞02
5.6258 01	3,239E 00	3.430E 02	2.881E=03	3.124E-02
5.630E 01	4.906E=01	3.468E 02	3.080E-03	2.512E=02
5.644E 01 5.652F 01	1.274E on 7.391E=01	3.480g 0g 3.488g 0g	2.867E=03 3.289E=03	2.638E#02 2.771E#02
5.680F 01		3.515F 02	3.2808#03	2.730E-02
5.703E 01	2.196E 00	3.5370 02	3.274E=03	2.6416.02
5.775E 01 5.877E 01	7.236E 00 1.100E 01	3.609E 02	3.272E=03 3.355E=03	2.315E#02 1.527E#02
6.078E 01	2.063E 01	3.925E 02	3.2506-03	3.041E=02
6.22gE 01	1,330E 01	4.058E 02	3.237E=03	2,982E#02
6.466F_01 6.504E 01	2.225E 01	4.2818 02 4.311E 02	3.268E=03 3.316E=03	3.097E#02 3.083E#02
6.508E 01	3.103E=01	4.3148 02	3.399E+03	3,165E=02
6.528E 01 6.694E 01	1.621g 00 1.311E 01	4.330g 02 4.461g 02	3,396E=03 3,326E=03	3.136E=02 2.216E=02
6.761E 01	4.630E 00	4.461E 02	3.308E=03	1.9996-02
6.838F 01	4.801E 00	4.555E 02	3.257E-03	1.519F=02
6.91nE 01 6.971E 01	3.805E 00 2.853E 00	4.593F 02 4.622F 02	3.218E-03	1.250Fm02 1.102E=02
7.066E 01		4.660 0 0 2	3.144E=03	8.163E=03
7.109E 01		4.6748 02	3.123E-03	7.2819.03
7.262E 01 7.277F 01		4.721E 02 4.725P 02	3.099E≃03 3.091E□03	6.411E=03 6.270E=03
7.352F 01		4.744E 02	3.0665003	5.568E+03
7.352E 01		4.744F 02	3.066E=03	5.564E=03
7.485E 01 47.770F 01		4.756E 02	3.084E-03	6,456E=03 8,531E=03
8.160E 01	2.948E 00	4.8118 02	3.049E=03	6.445E-03
8.441E 01 01 8.727F 01		4.824F 05	3.027F=03	6.095E=03
₩ 8.728E 01		4.831F 02	3,103F=03 3,103E=03	1.003F#02 1.003F#02
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PAMJET PERFORMANCE

PAMJET P	PERFORMANCE
CO ENGINE BEALUKANCE	INLET
ביישוניון אינוער אוער ביישוריון אינוער אוער ביישוריון אינוער אינער איינער אינער אינער אינער אינער אינער אינער אינער אינער אינער אינער אינער אינער אינער אינער אינער	TACE (
CALCULATED THRUST	ANGLE OF ATTACK ************************************
CALCULATED THRUST COFFFICIENT	OELTA PT2
CALCULATED STREAM THRUST	INLET PROCESS EFFICIENCY - SURSONIC 0.9050 KINFTIC ENERGY EFFICIENCY - SUPERSONIC 0.9351 KINFTIC ENERGY EFFICIENCY - SUESCNIC 0.8851
NET THRUST	ENTHALPY AT PO - SUPERSONIC
MOMENTUM AND FORCES	COMBUSTOR
TNLET FRICTION DRAG	FUEL-AIR RATIO
NOZZLE MGMENTUM CHANGE	NOZZLE VACIUM STREAM THRUST COEFFICIENT = C5 U.9584 NOZZLE COEFFICIENT = CT
STATIONS	FUEL INJECTORS
NOMINAL COWL LEADING EDGE	INJECTORS 8TATION - VALVE 1A 40.400 A 1B 41.286 B 1C 44.300 2A 48.761 D 2C 46.250 E 3A 54.051 3B 56.236
COMBUSTOR EXIT	4 44.786

Reading 69

t = 265.20 sec.

3-3-25

READING # 0069 BLOCK # 169 TIME # 265.204 MACH 6.0 PT # 749.750 TT # 2964.6
RAMJET PERFCRMANCE

46.250

ယ SUMMARY REPORT دب \Leftrightarrow GAMPA MOLKT SONV MACH YEL 8 AZAC MOMIN G IVAC PHI ETAC T н 4/A WIND THRNEL 749.750 2965 660.0(786) 1.2947 28.860 2571 0.000 0.388 399 ***33.2(96) 1.3987 28.859 981 6.006 5890 1.824 0.10690 27.057 0.9882 5051 9.784 186.7** SPIKE TIP NS 0.600 18.012 2965 660.01 786) 1.2946 28.659 2571 16.250 2896 634.3(766) 1.2968 28.059 2543 0.401 1020 2.081 0.10690 27.057 0.9882 0.600 4971 1.694 183.7 WIND THNNEL 0.000 749,750 2965 660.0(7A6) 1.2947 28.860 2571 0.000 -30.0(95) 1.3987 28.859 977 6.034 5893 1.824 0.104F0 26.527 0.98F2 4954 9.598 186.d 0.377 396 SPIKE TIP NS 0.600 18,012 2965 660.0(7A6) 1.2946 26.859 2571 0.600 16.328 2899 640.2(7A7) 1.2967 28.859 2545 0.392 996 2.081 0.10480 26.527 0.9882 4954 1.623 186.8 INLET THRUAT 278.394 2909 40,400 643,3(770) 1,2965 28,859 2549 40,400 16.127 1450 229.3(359) 1.3517 28.859 1837 2.477 4551 1.887 0.94593 27.057 0.1117 4289 66.880 158.5 THLET UPNESK 40.400 278.394 2909 643.3(770) 1.2965 28.859 2549 40,400 13,839 1393 214,4(344) 1.3550 28,859 1803 2.569 4633 1.887 0.85987 27.057 0.1229 4332 61.890 160.1 INLET DAMRSK 40.400 122.148 2909 643.3(770) 1,2965 28,889 2549 104,619 2808 40.400 612.8(700) 1.2996 28.859 2507 0.493 1235 1.943 0.85957 27.057 0.1229 4332 16.500 160.1 COMMUSTOR 1 21 40.410 238.837 2873 645.7(791) 1.2987 27.627 2591 15.049 1457 40.416 228.1(376) 1.3524 27.626 1883 2.427 4571 1.965 0.94872 27.152 0.1117 4288 67,395 157,9 U,12 0.07 COMBUSTOR 0 9 5 51 41.284 188.618 2811 649,41 8013 1,3022 26,563 2617 18.522 1592 41.284 275.4(430) 1.3467 26.563 2003 2.160 4326 2.037 0.95443 27.238 0.1114 4191 64.164 153.9 0.23 0.04 COMBUSTOR 0 10 3 21 41.294 196.294 2772 649.4(790) 1.3040 26.523 2603 41.294 16.561 1551 276.0(418) 1.3492 26.522 1981 2.182 4323 2.030 0.95376 27.238 0.1115 4190 64.072 153.8 0.23 0.01 COMBUSTOR 0 11 4 21 195.427 2766 649.2(788) 1.3043 26.517 2601 41.359 41.359 18.820 1554 278.7(419) 1.3491 26.516 1983 2.171 4306 2.030 0.95526 27.238 0.1113 4182 63.918 153.5 0.23 0.00 COMBUSTOR 0 12 5 21 41.500 191.025 2763 648.61 787) 1.3044 26.516 2600 41.500 . 20.403 1595 290,7(431) 1.3470 26.515 2007 2.109 4232 2.031 0.95524 27.238 0.1113 4165 62.825 152.9 0.23 0.00 COMBUSTOR 0 13 42.460 167.183 2811 644.3(801) 1.3020 26.580 2616 42.460 23,768 1750 316.7(476) 1.3391 26.580 2094 1.934 4049 2.046 0.94582 27.238 0.1124 4112 59.512 151.0 0.23 0.06 COMBUSTOR 0 14 44.079 114.002 3559 634.1(1029) 1.2660 27.449 2857 44.079 46.553 2931 424.2(827) 1.2876 27.455 2614 1.240 3241 2.123 0.91446 27.238 0.1163 4130 46.057 151.6 0.23 0.78 COMBUSTOR 0 15 44.310 112.681 3599 632,4(1041) 1,2638 27,502 2867 44-310 48.855 3007 433,4(850) 1.2844 27.509 2642 1.195 3156 2.125 0.91277 27.238 0.1165 4129 44.764 151.6 0.23 0.83 COMBUSTOR 0 16 44.794 110.605 3654 628.2(1057) 1.2607 27.583 2881 44.794 53.676 3134 451.7(890) 1.2791 27.591 2688 1.106 2972 2.128 0.90874 27.238 0.1170 4125 41.969 151.4 0.23 0.89 COMBUSTOR 0 17 10 44.800 110.377 3654 628.2(1057) 1.2607 27.583 2881 44.800 53.737 3135 452.0(890) 1.2791 27.591 2688 1.105 2969 2.128 0.90876 27.238 0.1170 4124 41.933 151.4 0.23 0.89 CCMBHSTOR 0 18 11 6 46.250 104.128 3186 646.4(1031) 1.2865 23.689 2921

57,671 2769 500,6(469) 1,2997 23,890 2747 0,983 2701 2,329 0,86653 27,555 0,1242 4153 36,374 150,7 0,62 0,25

339

READING P	0069	RFUCK	B 169	TTMF	= 265.2	04 MAC	H 6.	u PT:	749	750	rt = 296	4.6						
	P	Ť	н		GAWMA	አ በ <u>L</u> #1	SONY	MACH	VEL	S	W/A	A	A/AC	ተርቀገት	c	IVAC	PhI	ETAC
COMBLISTOR			12 2						-								,	
			646.3															
46.260 COMBUSTOR				(484)	1,2995	23.842	2747	0,905	2700	2.529	0.86605	27.555	P 1242	4155	36.336	150.5	0.62	0.25
) 20 1 3444	635.6	((150)	1 2736	24.176	3003											
47.310									2608	8.348	6.80596	27.555	9.1335	4315	32.665	156.6	0.62	0.36
COMBUSTOR		21																
47.319			635.5															
47.319				(989)	1,2859	24.181	2856	0.912	5606	2.348	0.40559	27,555	0.1335	4317	32,628	156.7	0.62	0.36
70"8USTCR 48,110		22			4 3804	34 464	1034											
48.110			627,8 478.6						2738	2.367	0.75111	27.545	0.1432	6862	31,902	161.9	0.62	0 - 48
COMBUSTOR		23		(10/-)	110.0.	H-4-6	L . 30		-100		V 0 1 2 1 1 1	2.6302		-406	319704	10441	4405	
48.759	91.933			(1881)	1.2784	21,645	3152											
48,759	45.611		442.2						3177	2.565	0.70121	27.874	0.1552	4565	34.619	163.8	1.02	0.27
COMBUSTOR		24																
46.769 48.769	71.001	3300	643.9	(1555)	1,2782	21.648	3153	1 485	7497	9 646	0.70030	3 9 B 9 //	A 465#	#E40	71 L1E	147 0		A 27
COMBUSTOR		25		(1052)	196747	611000	E 734	11003	3103	2,005	0.10030	211014	V • 1 2 2 4	4700	34,645	10344	TAVE	U + Z /
49.299	89.732			(1258)	1,2735	21.742	3183											
49.299	37.758								3542	2.573	0.65495	27.870	0.1662	4676	36.052	167.7	1.02	0.30
COMBUSTOR			19 5															
50.709			629,4					4 870							M M	. = .		
50.709 COMBUSTOR	36:137	27		(1110)	1.2796	28.107	5010	1.270	2055	2.004	0.55819	27.474	0.1950	4419	33,156	170.4	1.02	0.41
52,809			616.8	(1485)	1.2394	22.354	3348											
52.809	23.025	3191	233.8	(1127)	1.2741	22.384	3005	1.457	4377	2.622	0.49750	27.874	0.2379	5195	31,124	186.4	1.02	0.48
COMBUSTOR		26	21 3								Ť		•					. •
53,309			614.1													. .		
53.309 COMBUSTOR	დ და და უუ	50		(1084)	1.2779	22.200	2402	1,555	4541	5.050	0.43881	27.874	0.5440	5246	30,968	188.2	1.02	0.48
54.059			610.3	114073	1.2870	22.401	4156											
54.059	19.001		177.0	(1092)	1.2765	22.435	2964	1.571	4656	2.625	0.41363	27.874	0.2631	5314	29.931	190.7	1.02	0.50
COMBUSTOR		30	52 2									- •	. • • • •	• - •		• •		., •
54.819	73.001	4125	606.7	(1508)	1.2351	22.436	3360											
54.819 COFBUSTOR	1/.575	30/9	149.9	(1081)	1.2770	25.413	2444	1.621	4781	2.627	0.39115	27,874	0.2782	5376	29.061	192,9	1.05	0.51
55,760			605.6	(15581	1.2313	22.499	3372											
55.760	15.881	3089	124.3	(1083)	1.2756	22 543	2948	1.659	4892	2.632	0.36688	27.874	0.2966	5445	27,891	195.3	1.02	0.53
COMBILETOP	0	32	25 5					-	_		· ·	- • •	•••			,	• • • •	
56,244	55.521	4634	600.7	(1708)	1,1939	22,977	3460			_ _								
56,244 COMBUSTOR		3700		(1719)	1.2408	53.156	3142	1,530	4632	2.672	0.29582	27.874	0.3679	5612	22.212	201.3	1.02	0,68
56.299			26 5 600.5	/ 15e01	1.2266	22.561	17A1											
56,299	11.538	2995						1.800	5221	2.642	0.29489	27.874	0-3691	5616	23.928	201.5	1.02	0.50
COMBUSTOR		34	27 3		-			- • -						2-,-				
56,439			600.0	(1553)	1.5595	22,569	3384											
56.430	11.451		52.4	(1045)	1.2779	22.624	2901	1.805	9235	2,643	26262.0	27.874	0.3715	5625	23.829	8.105	1.02	0,55
COMBUSTOR 56.519	48, 384		28 21 599,8		1.1483	27.510	7577											
56.519	14.717	4467	120 0	(1625)	1.1627	24.000	3288	1.490	4890	2.692	0.29615	27.874	0.267E	5630	22.548	202 0	1 05	4 00
COMBUSTOR	Ō	36	29 21								A46,013	#1401H	*****	0000	0 M K & 2 2	さんにきれ	1 1 1 2	1900
50.799	48.488	5153	598.7	(1915)														
56.799	14.287	4468	107.3					1,511	4959	5,692	0.29512	27.874	0.3688	5645	22.742	202.5	1.02	1.00
COMEUSTOR			30 21		. (200	77 67.	2574			•								
57.025	13.447		597.9 86.2						5060	2.402	0.29462	27.874	A 440#	E464	27 (40	202.0	1 0*	4 00
			- 012	(1~0c)	* * T (1.40)	2	2647	****	2000	- + O 7 E	V 9 C 7 4 C C	E / PD / 4	7.5074	2020	23.169	CHEFA	1.02	1.00

READITNO # 0069 BLOCK # 169 TIME # 265.204 MACH 6.0 PT # 749.750 T1 # 2964.6

. GAMMA MOLWT SONV HACH VEL 'S AJAC MOMIM O IVAC PHI ETAC W/A COMBUSTOR 0 35 31 21 57.7.49 40.040 5143 595.5(1911) 1.1479 23.518 3533 CD 57.749 10.755 4329 20.6(1967) 1.1687 24.082 5232 1.660 5364 2.695 0.28999 27.874 0.3753 5661 24.172 203.8 1.02 1.00 COMBUSTOR 12 22 92. 0* 56,769 34,849 151.03 592.8(1894) 1.1457 23,481 3518 58,37,69 5.5%2 44090 -414.2(1457) 1.1772 24.171 3147 1.890 5948 2.718 0.28815 27.874 0.377/ 5686 26.635 204.0 1.02 1.00 COMBILSTOR 70 .40 33 21 60 2779 50,605 5448 588,0((942) 1,4489 23,542 3534 0.0,577.9 16.650,4522 138.7(1639) 1.1625 23.989 3301 1.437 4741 2.686 0.29817 27.874,7.3650 5664 21.970 203.2 1.02 1.02 COMBUSTOR 0 41 34 21 51.333 .51.47 584.5(19.12) 1.1492 23.549 3534 62,199 62,199 16-444-4503 425-6(1631) 1.1634 24.003 3294 1.455 4792 2.684 0.30626 27.874 0.3553 5648 22.807 202.6 1.02 1.00 COMBUSTOR . 0 42 35 24 64, 663 .48.791 51,33 577.2(1906) 1.1490 P3,592 3528 64.063 19.169 4607 196.5(1676) 1.1595 23.935 3331 1.310 4364 2.687 0.29030 27.874 0.3749 5622 19.690 201.7 1.02 1.00 COMBUSTOR 0 -43 36 200 65.039 45,400 5122 575,9(1901) 1,1484 23,543 3524 19.917 4662 238.3(1700) 1.1570 23.889 3350 1.227 4110 2.693 0.26988 27.874 0.4032 5618 17.239 201.6 1.02 1.00 65 030 COMBUSTOR REGEN 44 37 65.039 45.400 5160 614.3(1918) 1.1472 23.489 3540 65.039 19.894 47.03 272.8(1718) 1.1548 23.846 3365 1.229 4134 2.700 0.26988 27.874 0.4032 5636 17.339 202.2 1.02 1.00 NOZZLE AE 45 38 87.275 45.400 5122 575.9(1880) 1.1484-23.543 3524 87.27.5 1.422 3067 #604.0(1040) 1,2578 24,365 2806 2.739 7684 2.693 0.05618 27.874 1.9371 7363 6.709 264.1 1.02 1.00 NOZZLE PO 87.275 45.400 5122 57.5,9(1880) 1.1484 23.543 3524 P7.275 0.388 2326 -888.4(757) 1.2821 24,368 2467 3.470 8560 2.693 0.02251 27.874 4.8345 7896 2.995 283.3 1.02 1.00 NOZZLE AE REGEN 47 40 S 87.275 45.400 5160 614.3(1918) 1.1472 23.489 3540 67 275 1.446 3136 4576.4(1067) 1.2541 24.364 2833 2.725 7719 2.700 0.05618 27.874 1.4371 7406 6.739 265.7 1.02 1.00 NOZZLE PO REGEN 48 41 87.275 45.400 5160 614.3(1918) 1.1472 23.489 3540 87.275 0.388 2373 =670.9(774) 1.2805 24.368 2490 3.462 8621 2.700 0.02222 27.874 4.8978 7955 2.977 285.4 1.02 1.00 FICTIVE COMBUSTR 68 61 278.394 5348 979.9(1992) 1.1643 23.784 3607 63.039 65.059 0.388 1511-1177.1(468) 1.3201 24.368 2019 4.642 9366 2.540 0.03791 27.874 2.8706 8400 5.518 301.3 1.02 1.00 FICTIVE NOZZLE 69 62 87.275 27.345 5035 554.9(1865) 1.1448 23,501 3492 87.275 _ 1.801 3514 =413.2(1218) 1.2198 24.332 2959 2.352 6960 2.731 0.05618 27.874 1.9371 6924 6.077 248.4 1.02 1.00

YABS	P#18	HORS	PDA	Q D X	G#1₽	D≠nH	CANALL	P=18/650	P#18/P10	P=08/PS0	P=08/PT0
6.98(5.01	1.0906 00	0.600	-4.389E+01	-	0.000	0.000	2.470E=02	2.810E 0C	1.4506-03	0.000	0.000
1.836F 01	1,000 00	0.000	-3 A28E 01		0.000	0.000	1.634E 02	2.810E (6	1.4546=03	0.000	0.000
3.070E 01	2.465E 00	0.000	-1.804E 02		0.000	0.000	5.053E 02	6.355F 00	3.2686#03	0.000	0.000
3.508E 01	4.032E 00	0.000	-3.909E 07	0.000	0.000	0.000	6.804E 05	1.040F 01	5.378E-03	0.000	0.000
3.518E 01	4 075E 00		4 558E 02		0.000	0.000	5.847E CZ	1.051F 01	5.436E=03	1.4768 01	7.634E=03
3.518E 01	4.078E 00	5-692E 0	-4.559£ 02	0.000	0.000	0.000	0.850E 02	1.0516 01	5.#39E#03	1 . 467E 01	7.592E=03
3.555F 01	4.2406 00	3.781F 00	#4.653E 02	0.000	0.000	0.000	7.218E U2	1.0938 01	5,655E=03	9.747F 00	5.043E=03
3.585F 01	4.161E 00	2.225E 0	-4.803E 02	-2,936E 08	-2.9368 (0.000	7.521E U2	1.0736 01	5.5506-03	5.736F 00	2.968E=03
3.606F 01	4.105E 00	3.080F 00	-4.919E UZ	•2.971€ 02	! -2. 971E (0000-0	7.739E 02	1.05KF 01	5.075L=03	7.946F 00	4.108E+03
3.648E 01	4.315E 00) -5.117t 02				8.174E 02	1.1126 01	5.755E=03	1.535E 01	6.377E=03
3.7015 01	4.470E Q0					02 ≈9,538F 00	8.734E 02	1.1528 01	5.962£=03	1.786F 01	9.2398.03
3.731E 01	4.354E Qn					02 -1.254E 01	9.055E 02	1.123E 01	5.80FL=03	2.098E 01	1.085E=02
3.803E 01	4.075E 00					02 -1.960F 01	9.843E 02	1.051E 01	5.435t=03	3.494E 01	1.808E=02
5,833E 01	5.662E 00					02 =2.250F 01	1.0188 03	1.460f 01	7.552E=03	4.073E 01	2.107E=02
3,875E 01	7.499E 00					02 *2.654E 01	1,065E C3	2.036F 01	1.054E=02	3.975E 01 3.964E 01	2.057E=02 2.051E=02
3.880E 01	8.159E VO					10 3004.5- 20	1.071E 03	2.103F 01	1.238E=02	4.040E 01	2.090E=02
3.901F 01	9.280E 00					02 42,9015 01	1.095E 03	2.392F 01 3.510E 01	1.816E=02	4.147E 01	2.146E#02
3.931E 01	1.362E 01					02 -3.184E 01	1.151E 03	4.225E 01	2.186E=U2	3.467E 01	1.794E=02
3.950E 01	1.639E 01					02 =3.363E 01	1.186E 03	4.409E 01	2.281E=02	2.404E 01	1.244E.02
3.980E 01 4.000E 01	1.710E 01					02 -3.637E 01 02 -3.819F 01	1.210E 03	4.532F 01	2.3454-02	2.387E 01	1.235E-02
4.040E 01	2.089E 01					02 =4,226E 01	1.257E 03	5.386E 01	2.787L=02	2.353E 01	1.217E-02
4.041F 01	2.0986 01					02 =4.238E 01	1.258E 03	5.407E 01	2.7986-02	2.352E 01	1.217E-02
4.128E 01	2.821E 01					02 -6.607E 01	1.361E 03	7.2738 01	3.7636=02	2.277E 01	1.178E=02
4.129E 01	10 3628 2					10 3064.6 C	1.362E 03	7,294E 01	3,770E=02	2.276E 01	1 178E=02
4 136E 01	2.483E 01					02 -6.935E 01	1.370E 03	7.433E 01	3.845E-02	2.271E 01	1.175E-02
4.150F 01	3 000E 01					02 =7.601E 01	1.387E 03	7.7346 01	4.001E+02	2.786E 01	1.4416-02
4.246F 01	2.314E 01					02 m1.349E 02	1.5026 03	5.965E 01	3.086E-02	6.290E 01	3.254E=02
4.408E 01	4.579E 01					02 -2.518E 02	1.69RE 01	1.180E 02	6.107E=02	1.250E 05	6.311E=02
4.431E 01	4.902E 01	4.869g 0	47.340€ 02	.9.814E 0	-7.118E	05 #5.94E 05	1.726E 03	1.2648 05	6.538E#U2	1.255E 02	6.494E-05
4.479E 01	5.579E 01					02 -3. 163£ 02	1.785E 03	1.438E 02	7.441E=02	1.359E 05	6.877E-02
4.480E 01	5.587E 01					02 #3.170E 02	1.786E 03	1.440E 02	7.452E=02	1.330E 02	6.8828-02
4.625F 01	5.554E 01					05 -2.0056 05	1.0000 03	1.432E 02	7.407E-02	1.552F 02	8.0305=02
4+626E 01	5,553E 01					02 -5.0775 02	1.945E 03	1.432E 02	7.407E+02	1.594E 02	8.038E=02
4.731F 01	5.529E 01					03 =6.664E 02	2.095E 03	1.425E 02	7.374E=02	1.714E 02	8.869E=02
4.73gE 01	5.535E 01					03 *6.678E 02	2.096E 03	1.427E 02	7.382E=02	1.716E 02	8.876E=02
4.811E 01	6.060E 01					03 =7.810F 02	2,195E 03	1,562E 02	8.0836=02	1.4198 02	7.342E=02
4.876E 01	4.5618 01					03 #8,638E 02	2.276E 03	1.176E 02 1.172E 02	6,083£=02 6,064E=Q2	1.176E 02	6.064E=05
4.877E 01	4,547E 01					03 =0.650E 02 03 =9.255E 02	2.3448 03	9.734E 01	3.036E=02	9.7342 01	5.036Ep02
5.071E 01	3.214E 01	3.214E 0				03 =1.063E 03	2.9218 03	8.285E 01	4.2866-02	8.285E 01	4.286E+02
5.281E 01	2.302E 01	2.3025 0				03 -1.225F 03	2.788E 03	5.9368 01	3.071E=02	5.936E 01	3.071E-02
5.331E 01	2.065E 01	2.065E 0				03 =1.260F 03	2.851E 03	5.3256 01	2.755E=02	5.325E 01	2.755E+02
5,406E 01	1.900E 01	1.900F 0				03 -1.3118 03	2.947E 03	4.898E 01	2.534E=02	4.898E 01	2.534E=02
5.482E 01	1.732E 01	1.732F 0				03 =1.361E 03	3.0458 03	4.466E 01	2.3116=02	4.466E 01	2.311E=02
5.576E 01	1.588E 01	1.588F 0				03 w1.418E 03	3.166E 03	4.094E 01	2,118E=02	4.094F 01	2.118E-02
5.624E 01	1.514E 01	1.514F 0		-3.366E 0	-1-920E	03 -1.446E 05	3,209E 03	3,903E 01	2,019t=02	3,903E 01	2.019E=02
5.630E 01	8.0625 00	1.505E 0				03 -1.449E 03	3.216E 03	2.078E 01	1.075E=02	3.881E 01	2.008E-02
5,644E 01	9.062E 00	1.484F 0				03 =1.457E 03	3.234E 03	2.078E 01	1.075E=02	3.826E 01	1.979E=02
5.652E 01	1.472E 01	1 4728 0				03 *1.461 03	3.245E 03	3,794E 01	1.9636-02	3.794E 01	1 9635-02
5.6 POF 01	1.459E 01	1.429F 0				03 -1.477E 03	3.280E 03	3,6838 01	1.906E=02	3.683F 01	1.906E-02
5.702E 01	1.345E 01	1,3458 0				03 -1.489E 03	3.309E 03	3.467E 01	1.794E-02	3.467E 01	1.794E=02
5.775E 01	1.075E 01	1.0755 0				03 01.530E 03	3.407E 03	2.773E 01	1.434E=02	2.773E 01	1.434E-02
5,8775 01	5.512E 00	5.512F 0				03 -1.578E 03	3.532E 03	1.421E 01	7,3526=03	1.421E 01	7.352E>03
6,078F 01	1.665E 01	1.665F 0				03 -1.670F 03	3.790E 03	4.2926 01	5.221E=02	4.292# 01	2.221E=02
6.220E 01	1.644E 01	1.6445 0	1 1:0756 03	-3.014F 0;	: ₩2+U78E	03 =1.741F 03	3.972E 03	4.239E 01	2.193E=02	4.239E 01	2.193E=02

	XABS	Pal8	P=08	PDA	OOX	iş⊭IA	c=n8	CAWALL	P=18/PS0	P=18/PT0	P#08/PS0	P=08/P1'0
ယ	6.466F 01	1.9178 01	1.917F 01	1.095E 03		_	03 +1.870F 03	4.289E 03	4.9428 01	2.557E=02	4.9.2E 01	2.557E=02
×	6.50#E 01	2.025E 01	1.958F 01				03 =1.891F 03	4.337E 03	5.220E 01	2.7018-02	5.049E 01	2.612E=U2
100	6.508F 01	2.0256 01	1.963F 01				03 =1.893E 03	4.34PE 03	5,220E 01	2,701E=02	5.060F 01	2.618E#02
	6.528E 01	1.925E 01	1.985E 01	1.0956 03	04.079E 03	-2.175E	03 -1.904E 03	4.368E 03	4.963E 01	2.56RE=02	5.117F 01	2.648E=02
	6.694E 01	1.098E 01	9.390E 00				03 -1.984E 03	4.583E 03	2.831E 01	1,464E=02	2-421E 01	1.2526=02
	6.761E 01	7.779E 00	9.412E 00	1.450E 03	-4.254E 03	#2.243E	03 -2.011E 03	4.665E U3	2.005E 01	1.038E=02	2:42/E 01	1.255E=02
	6.838E 01	4.100E 00	7.1242 00	1.6438 03	□4.3u3E 03	-2.257E	03 m2.045E 03	4.760E 03	1.05/E 01	5.468E=03	1.837E 01	9.502E=03
	6.910E 01	3.499€ 00	4.985E 00	1.768E 03	04.351E 03	-2.268E	03 =2.083E 03	4.848£ 03	9.021E 00	4.667E0U3	1.285E 01	6.649E=03
	6,971E 01	2.990E 00	4.135E 00	1.852E 03	=4,389E 03	-2.275E	03 m2.114E 03	4.922E U3	7.7085 00	3.988t=03	1.066E 01	5.515E=03
	7.066E 01	1.933E 00	2.810E 00	1.945E 03	94.435E 03	9485°5"	03 02.152E 03	5.036£ 03	4.984E 00	2,5796,03	7.244E 00	3.748E-03
	7.109E 01	1.455E 00	2.655E 00	1.976E 03	04.451E 03	#2.286E	03 m2.165E 03	5.088E 03	3.751E 00	1.9416=03	6.845E 00	3.542E=03
	7.262E 01	1.601E 00	2.105E 00	2.067E 03	94.500E 03	-2.295E	03 -2.204E 03	5.273E 03	4.127E 00	2,1356=03	5.427E 00	2.808t=U3
	7.277E 01	1.615E 00	1.969E 00	2.074E 03	-4.504E 03	-2.296E	03 -2.208E 03	5.290E 03	4.163E 00	2.154E=03	5.076E 00	2,6266.03
	7.352E 01	1.674E 00	1.290E 00	2.130E 03	-4.526E 03	-2.300E	03 -2.228E 03	5.374E 03	4.317E 00	2.233E=03	3.326E 00	1.721E0U3
	7.352E 01	1.675E 00	1.286E 00	2.132E 03	-4.528E 03	#2.300E	03 ∞2.228E 03	5.375E 03	4.318E 00	2.234E=03	3.316E 00	1.716E003
	7.485E 01	1.780E 00	0.000	2.169E 03	-4.576E 03	-2.367E	03 -2.269E 03	9.427E 03	4.589E 00	2.374E=03	0.000	0.000
	7.770E 01	2.560E 00	0.000	2.256E 03	-4.589E 03	305E.5a	03 92.269E 03	5,925E 03	6,600E 00	3.414E=03	0.000	0.000
	8.160E 01	1.8600 00	0.000	2.350E 03	04.604E 03	.2.335E	03 -2.269E 03	5.630E 03	4.795E 00	2.481E=03	0.000	0.000
	8.441E 01	1.840E 00	0.000	2.391E 03	-4,619E 03	-2.349E	03 -2.269E 03	5,6848 03	4.743E 00	2.454E=03	0.000	0.000
	8.727E 01	3.235E 00	0.000	2,453£ 03	-4.643E 03	-2.374E	03 #2.269E 03	5.707E 03	E.340E 00	4.3156-03	0.000	0.000
	8.727E 01	3.238E 00	0.000	2.453E 03	-4.643E 03	-2.374E	03 02.269E 03	5.707E 03	8.347E 00	4.319E=03	0.000	0.000

RAMJET PERFORMANCE

ယ		KANGET FERRO	THE COLUMN THE COLUMN			
ķ	ENGINE PERFORMANCE			INLET		
76.4 CAL MEA CAL	ASURED THRUST	(LBF) (LBF#SFC/LBM)	MASS FLOW RATIO ADDITIVE DRAG COEF LIMITING PRESSURE DELTA PTZ TOTAL PRESSURE REC	FICTENT	0.9882 0.0000 0.1606 0.1193 0.5713	
SPE	REGENERATIVE-COOLED ENGINE PERFORMANCE CALCULATED REAM THRUST	(LBF)	INLET PROCESS EFFI KINETIC ENERGY EFF KINETIC ENERGY EFF ENTHALPY AT PO = SI	CIENCY - SUPERSONIC CIENCY - SUBSONIC ICIENCY - SUPERSONIC ICIENCY - SUBSONIC UPERSONIC UBSONIC	0.9047 0.9348 0.8871	(BTU/LBM)
	MOMENTUM AND FORCES			COMBUSTOR		
100 000 000 002 402 402 4 X T	LET FRICTION DRAG	(LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF)	EQUIVALENCE RATIO. COMBUSTOR EFFICIENI TOTAL PRESSUME RAT COMBUSTOR EFFECTIVE INJECTOR DISCHARGE VACUUM STREAM INHUI NOZZLE COEFFICIENT	CY	1.019 1.000 0.1631 0.8776 0.6841,	0.7912. 0.6794
FAL HEA	IAL STRUT DRAGOODOOSOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO	(LBF) (LBF) (LBF)	KINETIC ENERGY EFF	ICIENCY	0,8334 0,8648	
	STATIONS	•	FUI	EL INJECTORS		
INL COM NOZ NOZ STR	AINAL COMI LEADING EDGE	(IN) (IN) (IN) (IN) (IN) (IN)	INJECTURS 1A 1B 1C 2A 2C 3A 38	40.400	LVE A B D E	

Reading 71

t = 160.54 sec.

SILM VARY REEDRT

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ල ා	T	н		CAVEA	KUL MT	SILV	M A C H	v = 1	e	4/6			U.C.L.110	,	****		
WIND THRNEL	1	ი წ					-ac-	ALF	Ð	" / "		74/4	40×1×	ľ	TVAC	PHI	ETAP
0.000 742.749	2897	639.21	765)	1.2965	28,698	2542											
0.000 0.375	385	a36,51	935	1.3985	28.897	963	6.037	5815	1.814	0.10575	25.269	0.6329	4656	4.556	184.3		
SPIKE TIP NS	2	0 5					•							- # 350	211493		
0.600 18.200		639.21	765)	1.2964	28.897	2542											
0.600 16.549	2835	620.5(747)	1.2984	28,897	2516	0,385	969	2.073	0.10575	25.269	0.0379	4715	1,592	186.6		
WIND TUNNEL	_ 3	C C									·	• •		• • • •			
0.000 742.749		639.21	765)	1,2965	28.898	2542											
0.000 0.383	36R	e35,91	93)	1.3986	28.897	966	6.016	5812	1.818	0.10739	25,459	0.0329	4727	9.700	184.2		
SPIKE TIP NS	4	0 0	.											•			
0,600 18,200		639,20	745)	1,296/	24,897	2542											
0.600 16.491 INLET THROAT	2035	014"8(745)	1.2985	28,897	2515	0,497	9 7 6	2.073	0.10739	25,659	0,4329	4727	1.606	184.2		
40,400 185,499	7850	637 84	9-41														
40,400 18,590		627.71	1.2	1,67//	28,897	2526	2 440										
THET UPNESK	6	C X	נימויי	1.0413	501011	1442	2.149	4177	1.404	0.68523	25,269	0.1114	3810	57.457	150.8		
40,400 185,499	•	627.71	7243	1 2077	30 807	2524											
40.400 15.787		261.06	3001	1.3446	28.807	1004	2 2/16	//282	1 000	0.89476	24 240		7056				
INI ET DNNRSK	7	D 4	340)	193440	£010+1	1400	20240	4202	1.444	V • 07470	27.207	0-1559	3454	53,550	152.7		
40,400 107,681		627.71	7641	112977	28.897	2524											
40,400 90,110		593.41	7511	1.3014	28.897	2479	0.429	1310	1.946	0.80476	25.240	0.1226	***	16.388	(85 4		
COMBUSTOR 0	8	1 4								0100470	Engeo.	041650	3734	10.300	13601		
40,410 185,137	2859	627.76	754)	1.2977	26.897	2526											
40.410 18.571	1638	279.51	409)	1.3412	28,897	1944	2.147	4174	1.909	0.88513	25.269	0,1115	3809	57.421	150.7		
COMBUSTOR 0	9	2 4					•	•						2.146.			
41.306 152,720	_ : :	629.01	751)	1.2980	28,897	2523											
41.306 21.540		317.8(447)	1.3347	28.897	2021	1,940	3920	1.921	0,68770	25,269	0.1111	3692	54.080	146.1		
	10	3 4												•			
41.371 150.619 41.371 21.800	2049	624.71	751)	1,2980	28,897	2522											
41.371 21.800	1/40	320,9(459)	1.5343	28.897					_							
COMBUSTOR 0	11	8 4					1.924	3899	1.922	0.88814	52°596	0.1111	3683	53.818	145.7		
41,500 146,488		454 51	7013	1 2021	20 002	2522											
41.500 22.319	1812	326.97	466	1.2224	28 807	2746	00	TAEP		0.88852	AH 940						
	12	5 5	-5-,	10000	E 0 1 D 4 1	たいきょ	1 9 0 7 6	3031	1.754	V 4 0 P D 7 E	23.204	0 - 1110	3004	31.259	145.0		
42.460 - 127.528	2832		7461	1.2986	28.897	2516											
U2.460 24.667	1912	354.60	4845	1.3296	28.897	2091	1.742	3643	1.932	0.87885	26.240	0 (127	****	49.753	1/11 7		
COMBUSTOR 0	13	6 4						202	,	V	C 3 E C 4	W#11E3	2310	449100	14112		
44.091 113.898	1085	610.60	737)	1.2995	28.897	2503											
44,091 25,370	1961	368.11	497)	1,3278	28,897	2116	1.646	3483	1.936	0.84957	25.269	0.1161	3496	45,991	138.0		
	14	/ 4															
44.310 112.529		609.36	735)	1,2097	26,897	1025											
44.316 25.777 COMBUSTOR 0	1707	369.90	499j	1.3275	28.897	2120	1,633	3461	1.937	0.84812	25,269	0.1163	3486	45.617	138.0		
	12	0 4															
44,800 109,008 44,800 26,393	4004	606.50	733)	1,3000	28,897	2497											
	16	375.46	2047	1.3208	28.897	5130	1,597	3400	1.938	0.84458	25.269	0.1168	3460	44.627	136.9		
			7-21		30 004	2400											
	1989	375_4	6767	1 2370	20 07/	5477	4 204	2200		A 540AF			.				
	17 1	375,60	2027	102504	E 0 . 0 4 /	g 1 3 U	1 . 770	2244	10438	0.84485	25,769	P.1168	3460	44.625	136.9		
46.260 98.219		599.10	7261	1.3008	28.897	2489											
46,260 25,980	2011	382 3	5111	1.3259	28 897	2143	1.538	120 11	1.0/11	A TOEE+	35.340	6 4244	7/10	በል ከ ሚዋ	178 6		
COMBUSTOR 0	, n ,	11 5					- 5 12 0	J G 14	4 0 7 M J	סרכיונע	E20E04		2416	40,723	150.0		
47.310 91.218	2747	594.3(721)	1,3013	28.897	2480											
47.310 24.065	1998	378.41	507)	1.3264	28.897	2135	1.539	3247	1.946	0.74042	25.269	0.1332	1401	37,818	134 9		
			•					'				Bit my name	3-07	214010	4 3 M B I		

	JESPINS .		· · C·z·p·n	w 31	1 7 % (w ; 0) . § . t.	30 0	., 0.	· - · ·		.,-,) W (2117	. • .							
		Þ	Ť	h		GAHAV	MCLAT	SONV	масн	VFI	s	4/4	*	4/45	*CYT*	ß	TVAC	PHT	ETAC	
	COMBUSTOR	0	19	12 5		****		•			•				• , .			. ,	_ , ,, ,	
	47,331			594.21	7-11	1.3013	25.897	2480												
	47.331									TORE	1.946	0.74634	25.260	4,1333	1/102	77.100	134.A			
	COVEUSTOR		20			1.000	2	613	7022	2607	7	0 6 7 4 5 3 4	, ,,,,		2.007	211111	1,34,6			
	48.110			590.81	7781	1 7014	24 807	2/175												
	48.110									7720	1 0/10	A 48000	n= 3.0	3 4 11 77 0	20.5	75 (6)	17F A			
					490)	1.36/8	80.04/	2114	10211	3324	1.448	0.960343	63.704	0,1430	3417	35.691	122.0			
	COMBLISTOR	0		14 5																
	48.791			588 1(
	48.741				485)	1.3294	28.897	2094	1,628	3409	1,950	0.63485	29,240	0.1554	3437	33.635	136+0			
	COMBUSTOR			15 5																
	49.311	80.338	2719	586,2(713)	1.3022	28.897	2468												
	49.311				473)	1.3310	28.497	2072	1,680	3480	1.952	0.59373	25.269	0.1662	3461	32.114	137.0			
	COMPUSTOR		53																	
	50,721	74,469	2703	581.46	709)	1,3027	28,897	2461												
	50.721	13.313	1783	318,9(448)	1,3346	28.497	5052												
										3624	1.955	0.50603	25.269	0.1950	3511	28.497	138.9			
	COMBUSTOR	0	24	17 5							• • • • •			•	• - •	• •				
	52.821		2683	575.50	763)	1.3033	28,897	2453												
	52.821	9 930	1685	292.30	4511	1.3389	28.897	1970	1.910	3764	1.960	0.41475	25.269	0.2379	3561	24.262	140.9			
	COMBUSTOR		25		, ,			• .	•	•		• • • • •					• • • •			
	53,321			574.3	7021	1.3030	28-897	2051												
	53.321	9.324	1664	286.4	4767	1.3400	28 897	1956	1.938	1795	1-961	0.39780	25.269	0.2480	1571	23.463	141.4			
	COMBUSTOR		26		1								page.	D # E 11412						
	54.071			572.60	7601	1 3036	28.897	2449												
	54.071	8 5/10	1614	278.51	4681	1 3030	28 807	10/13	1.075	AFAF	1.042	0-37/07	25.240	0.2631	7422	22.353	1/12 0			
	COMBUSTOR	0.574	27	20 5	40 11111 3	1,30,10	E01077	1745	(7 -	3036	16,000	003,471	231501		3500	556373	14210			
	54,831			571.0	4481	1 2028	38 867	21114												
	54.631									7044	1 047	A 45/40	20 260	0.2782	7400	31 700	1.115 E			
	COMBUSTOR		28		4011	1,3420	£00041	1,54	E 4 (103	3001	14403	0.33400	23.207	45105	2000	21,309	1 45 4 3			
	55.760		. •		4-71	4 7000	30 904	2000												
	55.760			569.11						¥000	1 046	A 7730C	26 240	0.0040	7115	20 1/7				
					194)	102022	40.01	1719	2000	3044	1.405	0.33503	C2150A	0.2964	3018	20.167	145.4			
	ROTEUBHOD		29		4 - 4 5		** ***													
	56.256			568.31																
	56,256			520.2(380)	1,3008	26.847	1883	5-119	3448	1.974	0.26817	25.269	0.3679	3650	16,619	144.5			
	COMBUSTOR		30																	
	56.311			568.2(
	56.311				379)	1.3469	28.897	1485	5.150	3000	1.975	0.26737	25.269	0.3690	3651	16.577	144.5			
	COMBUSTOR		31																	
	56.451	52.117	2058	567.9(993)	1,3041	28 897	2442												
	56.451				378)	1.3471	28.897	1880	2,125	3994	1.975	0.26545	25.269	0.3717	3653	16.477	144.6			
	COMBUSTOR			25 4																
	56.531	52,860	2657	567,81	693)	1,3041	28,897	5445												
	56.531	5,472	1523	548,6(379)	1,3472	78.697	1879	2.127	3997	1.974	0.26857	25.269	0,3673	3654	16.6P1	144.6			
	COMBUSTOR			26 4																
	56,811	53.077	2656	567.4(695)	1,3042	28,897	2441												
	56.811	5.417	1516	246.B(376)	1.3476	28.897	1875	2.136	4005	1.973	0.26754	25.269	0.3688	3657	16.651	144.7			
	COMBUSTOR	0	34	27) 4												•				
	57.037	53.293	2655	567.00	695)	1.3042	28,897	2441												
	57.037	5.342	1511	245.51	375)	1.3478	28.697	1872	2.142	4011	1.973	0.26708	25.269	0.3694	3659	16.647	144.8			
	COMBUSTOR	0	35	28 4					_	-				•			• • • •			
	57.761			565,96	693)	1.3043	28,897	2439												
	57.761			242.16					2.159	4025	1.972	0.26289	25.269	0.3753	3665	16.445	145-0			
	COMBUSTOR			29 4						🛩	, 			+ - ·	2200		* m # O			
	58.78+			564.6(692)	1.3045	28,897	2437												
Ç	58.74								2.169	4033	1.972	0.26122	25.240	0.3777	3644	16.372	175 4			
1	CULBILLAU		37	30 6	,		- + 1						M . F.C.O.A	3/ / /	21/60	11.63.2	1 - 4 1			
-4	60.791			562,51	6001	1.3047	28.891	2430												
	60.791	5.390	1405	241.21	X701	1.3088	28.407	1867												
•		- · •		- +	. ,	* # M W//		,	2 457	4016	1.094	A 27A24	3F 3FV	0.3650	7457	16.8#4	4.0.0. 4			
									~0124	-010	ABTIV	A # E 1 A 3 I	43150A	# 202¢	2022	100048	144 10			

GAMMA KOLMT SOLV MACH VEL S AZAC HOMIM G 4: / A TVAC PHT FTAC CO COMBUSTOR 0 38 31 6 F 62.211 54.952 2635 561.3(689) 1.3048 28.897 2032 co 62.211 5.597 1502 243.0(372) 1.3084 28.897 1867 2.138 3991 1.968 0.27763 25.269 0.3553 3643 17.220 144.2 COMBUSTOR 0 39 32 4 64.675 50.816 2628 559.2(687) 1.3051 28.897 2429 5.377 1513 245.96 3751 1.3478 28.897 1873 2.114 3959 1.973 0.26316 25.269 0.3749 3626 16.193 143.5 64.675 COMBUSTOR 0 40 33 4 45.051 47.080 2627 558.91 686) 1.3051 28.897 2429 65.051 5.010 1514 246.3(375) 1.3477 28.897 1874 2.110 3955 1.978 0.24466 25.269 n.4032 3623 15.036 143.4 MOZZI D AE 41 34 3 47.080 2627 558.9(686) 1.3051 28.897 2429 87.289 87.287 0.421 774 57.5(187) 1.3912 28.897 1361 3.661 5009 1.978 0.05093 25.269 1.9371 4143 3.964 163.9 NO7ZLE PO 42 35 3 87.287 47.080 2627 558.9(686) 1.3051 28.897 2429 A7.227 0.375 749 51.50 181) 1,3923 28,897 1340 3,762 5039 1,978 0.04716 25,269 2,0918 4158 3,693 164.6 FICTIVE COMBUSTR 62 55 0 65.051 185,499 2627 558,9(696) 1.3051 28,897 2029 65.051 0.375 507 97.1(192) 1.3989 26.897 1105 4.815 5321 1.884 0.07352 25.269 1.3419 4308 6.080 170.5 FICTIVE PUZZLE 63 56 0 87.287 43.625 2603 551.8(680) 1.3059 28.897 2418 87.287 0.433 788 61.1(190) 1.3905 28.897 1373 3.608 4955 1.981 0.05093 29.269 1.9371 4107 3.922 162.5

YARq	P=IB	Pana	Pra	(i) O X	Solu	e-ne		CAAALL	P+tb/PS0	F#IP/PTC	P###/PSO	PHUR/PTO
6.98(Fm01	1.04PE 00	V. 000	-4.429E=01	0.000	0.000	0.000		2.470E=02	2.774F 00	1.4006.03	0.000	0.000
1.836F 01	1.0408 20	0.000		0.000	0.000	0.000		1.434E 07	2.7748 00	1.400E=03	0.000	0.000
3.070F 01	2.875E 00	0.000		0.000	0.000	0.000		5.053£ 02	7.6685 00	3.6716-03	0.000	0.000
3,50AE 01	3.844E 00	0.000	· · · · · · · · · · · · · · · · · ·	0.000	00000	0.000		6.804E 02	1.0256 01	5.176E-C3	9,000	0.000
3.519E 01	4.161E 30	-		0.000	0.000	0.000		6.852E 02	1.110F 01	5.6026-03	1.477E 01	7 456E-03
3.519F 01	#.178E 00			0.000	0.000	0.000		6.855E 02	1.114E 01	F.6256-03	1.470E 01	7.418E=03
3.555E 01	5.210E 00			0.000	0.000	0.000		7.211E 02	1.3908 01	7.010E003	1.020F 01	5.149E+03
3.586F 01	5.021E 00		00 95.091E 02 0					7.527E 02	1.3395 01	6.700E-03	6.268E NO	3.164E=03
3.60AE 01	4.900E 00		00 05.224E 02 0			000.0		7.731E 02	1.507F 01	6.597E+03	9.351F 00	0.720E=03
3.64RE 01	4.197E 00		10 05 417E 07 0					8.167E 02	1.1205 01	5.651E=03	1.585E 01	8 003E-03
3.701E 01	5.255E 00		nn -5.640E 02 -				01	8.729E 02	1.402E 01	7.075E+03	2.406E 01	1 214E-02
3.735E 01	4.8658 00		01 =5.752E 02 =					9.061E 02	1.298E 01	6.550E=03	2.887E 01	1.4576-02
3,8038 01	3.9758 00		01 a5.8716 02 a					9.436E 02	1.060€ 01	5.3526-03	3.868F 01	1.9526=02
3.8348 01	7,6128 00		11 -5.903E 02 -					1.01RE 03	2.0306 01	1.0251-02	4.298E 01	2.169EmU2
3.8758 01	1.240E 01		01 =6.093E 02 =					1.065E /3	3.307E C1	1.669E=02	4.684E 01	2.364E=02
3.801F 01	1.311E 01		01 m4.126E 02 m					1.0726 03	3.497E 01	1.765F = 02	4.741E 01	2.393E=02
3.90 E 01	1.544E 01		01 a6.231E 02 a					1.090E 03	4 118F 01	2.079E=02	4,689E 01	2.3676-02
3,932E 01	1.838E 01		01 06.427E 02 =					1.130E 03	4.902F 01	2.4756-02	4.608F 01	2.326E=02
3.950F 01	2.007E 01		0: =6.563E 02 =					1.151E 03	5.3548 61	2.703E-02	3 430F 01	1.731E-02
3.98 E 01	1.787E 01		nn =6.838E 02 =					1.187E 03	4.766E 01	5.406E-05	1.387E 01	7.001E-03
4.00nF 01	1.653E 01		00 -7.011E 02 -					1.209E 03	4.408F 01	2.225E+02	1.328E 01	6.701E=03
4.040F 01	1.982E 01		00 -7.3776 02 -					1.256E 03	5.287E 01	2.669E=02	1.202E 01	6.067E=03
4.04 E 01	1.990E 01		00 =7,386E 02 =					1.257E 03	5.308F 01	2.680E-02	1 199E 01	6.051E=0
4.13 E CL	2.728E 01		06 a8 406E 02 m					1.363E 03	7.275E 01	3.672E=02	9.173E 00	4 630E=03
4,137E 01	2.781E 01		00 -8.48AE 02 -					1.371E 03	7.418E 01	3.744E=02	8.968E 00	4.527E-01
# 150F 01	2.887E 01		00 mA 654E 02 m					1.386E 03	7.7028 01	3.888E-02	1.057E 01	5.338E=03
1.509E 01	1.950E 01		00 09 437E 02 00					1.501E 03	5.201E 01	2.625E=02	2.251E 01	1.136E=08
4.400E 01	2.441E 01		01 #9.923E 62 #					1.698E 03	6.512E 01	3.287E-02	4.279E 01	2.160E=0R
4.431E 01	2.507E 01		01 49,9925 02 4					1.725E 03	6.688E 01	3.376te02	4.1628 01	2.101E=08
4.48nE 01	2.655E 01		01 =1.018E 03 =					1.785E 03	7.081E 01	3.575E-02	3.900E 01	1.969E=08
4.481F 01	2.652E 01		01 -1.018E 03 =					1.7868 03	7.0748 01	3.5716-02	3.897F 01	1.967E-08
4.6268 01	2.004E 01		01 =1.045F 03 =					1.964E 03	5,345F 01	2.6986=02	3.120E 01	1.575E=08
4.731E 01	1.536E 01		00 al 040F 03 a					5.094E 03	4.096F 01	2.067E=02	2.558E 01	1 291E-02
4.733E 01	1.922E 01		00 al .041E 03 a					2.097E 03	4.059E 01	2.049E+02	2.547F 01	1.286E=08
4.811E 01	1.0108 01		0; +1.021E 03 -					2.194E 03	2.694E 01	1.360E=02	2.698E 01	1.362E=08
4.878F 01	1.060E 01		01 -9.875E 02 -					2.278E 03	2.828E 01	1.4276-02	2.828E 01	1.427E-02
4.931E .01	1.099E 01		01 -9-577E 02 -					2.345E 03	2.9318 01	1.4795-02	2.931E 01	1.479E-02
5.072E 01	6.362E 00		00 #8.936E 02 #					2.522E 03	1.6978 01	8.566E=03	1.697E 01	8.566E=03
5.28žE ni	6.150E 00		00 -8.247E 02 -					2.788E 63	1.640E 01	8.280E-03	1.640F 01	8.280E=03
5,332E 01	5.915E 00		00 -8.090E 02 -					2.8526 03	1.5788 01	7.964E=03	1.578E 01	7.964E=03
5.407E 01	4.877E 00		00 =7.881E 02 =:					2.948E 03	1.301E 01	6.866E-03	1.301E 01	6.566E=03
5.447E 01	3.825E 00	3.825F	00 07.713E 02 =:	1.725E 03	#8.380E (02 -8.873E	0.2	1.045E 03	1.020E 01	5,150E=03	1.020E 01	5,150E#03
5.5765 01	3.860E on		00 =7.534E 02 =					3.165E 03	1.0305 01	5.197E=03	1.030F 01	5 197E 03
5.626F C1	3.879E 00		90 =7.126E 02 =					3.209E 03	1.035E 01	5.2228-03	1.035F 01	5.222E=03
5.6315 01	1.912E 00		20 87.115E 02 4					3,216E 03	5.101E 00	2.575E=03	1.035E 01	5.225E=03
5,6458 01	1.912E 00		00 -7.090E 02 -:					3.234E 03	5.101F 00	2.575E=03	1.037E 01	5.232E=03
5.6538 01	3.889E 00		00 -7.074E 02 -:					3,245E 03	1,037E 01	5.236E=03	1.037E 01	5.836E=03
5.6818 01	3.900E 00		00 -7.023E 02 -					3,280E 03	1.040E 01	5.251E-03	1.040E 01	5.281E-03
5.704F 01	3.857E 00		00 a6.986E 02 a					3.109E 03	1.029F 01	5.193E=03	1.029E 01	5.193E=03
5.776F 01	3.720E 00	3.7205	00 06.883E 07 m	1.852F 03	₩8.960E (02 09.545F	υ 2	3.402E 03	9.922F 00	5.008E+03	9.922F 00	5.008E#03
5.878F 01	3.862E 00		00 a6,795E 02 a					3,432E 04	1.030E 01	5.200E=03	1.030E 01	5.200E-03
6.079F 01	1.325E 00		On 06,789E 02 0:					3,790E 03	3.534E 00	1.784E=03	3,534E 00	1.784E=03
6.221E 01	1.425E 00	1.425F	96 96,789E 02 #:	1.969F 03	≈9.366E (02 €1.032E	03	3,972E 03	3.801E 00	1,9196+03	3.801E 00	1.919E=03
6.467E 01	3,545E 00	3.545E	00 00°46 05 05	2.0238 03	09.554E (02 -1.067F	٥3	# 589E 03	9.455E 00	4.773E-03	9,455E 00	4.773E+03
) 6.505E 01	2.900E 00	3.868F	00 m6,789E 02 m	2.031F 03	#9.584E (02 -1,073F	0.3	0.337E 03	1.040E 01	5.251E-03	1.032F 01	5.208E.03
6.509E 01	3.900E 00	3.9036	ባለ #6.789೬ በን #7	2.032E 03	#9.588E (02 -1.073E	0.3	4.342E 03	1.000F 01	5.251E=03	1.041E 01	5.255E=03

	XARq	p= IB	Penp	PDA	ФОX	Gala	ยา อ อ	CA*&Li	PeTE/PSU	P=15/PT0	P=08/P80	P=0B/P10
ديم	6.529F 91	3.749E 00	4.075F 0n	#6.780F	2 -2.037F	03 +9,600E	02 =1.077F 03	U. TERE OF	1.0008 01	5.00AE+03	1 0 17E 01	5 486E 03
άŢ	6.6958 01	2.500E 00	4.810P 0n	-6.351E	2 -2.073E	03 69.718E	02 -1.101F 03	4.583E 03	6.668F 00	3.366E=03	1.283F 01	6.476EaU3
	6.762E 01	1.984F 00	3 457F 0c	-5.708E	72 -2.085E	03 #9.7556	CP -1.110F 03	4.665E 03	5,2908 00	2.671E=03	9.222F 00	4.655E+03
	16,1839F 01	1.3900 00	2.6A6F 00	#5.074E	2.099E	03 m9.792E	02 -1.120F 03	4.760E 03	3,707F 00	1.871E=03	7.165E 00	3.417Em03
	46.7911E 01	1-209E 00	1.9658 00	-0.619E	2 -2.111F	03 -9.821E	02 =1.129F 03	4.848E 03	3,224E 00	1.627E=03	5.241F 00	2.646E-03
	6:3972E 01	1.055E 00	1.5956 00	=4.309E	3151.5 = 50	03 -9.8425	02 -1.136E 03	4.922E 03	2.814F 00	1.420E=03	4.2558 00	2.148E-03
	7.0675 01	1.007E 00	1.020F 0n	-3.939E	02 -2.137E	03 =9.869E	02 -1.150F 03	5.036E 03	2.685F 00	1.356E-03	2.721F 00	1.373E-03
	7.110E 01	9.,850E=01					02 #1,156F 03	5.088E 03	2.6275 00	1.326E=03	2.879F 00	1.453E-03
	7.0263E 01	1.204E 00					02 =1,174F 03	5.273E 03	3.210E 00	1.620E-03	3.441E 00	1.737E=03
	7.278E 01	1.2256 00	· V				02 ml.176E 03	5.2908 03	3.267E 00	1,64°E=03	3.027F 00	1.5286-03
	7.353E 01	1.072E '00	3.6000001	-2°840E	02 #2.178E	03 =9.924E	02 -1.189E 03	5.374E 03	2.8598 00	1.443E+03	9.602E=01	4.847E-04
	7.353E 01	1.071E 00	3.559F+0(02 p1.185F 03	5,375E 03	2.856F 00	1.4426-03	9.491F=01	4.791E=04
	7.486E 01	8.000E=01	0.000				02 -1.204F 03	5.427E 03	2.134E 00	1.0776.03	0.000	0.000
	7.771E 01	8.050E=01	0.000				02 -1.204E 03	5.525E 03	2.147F 00	1,084E=03	0.000	0.000
	8.161F 01	8-a 600F=01	0.000				05 e1.504k 03	5,630E 03	2.294E 00	1.158E=03	0.000	0.000
	18.442E 01	6.050E=01	0.000	01.846E	02.206F	03 -1.002E	03 01.204E 03	5.684E 03	1.614E 00	8.145E=04	0.000	0.000
	'8.728E 01	7.2006=01	0.000				03 41.204E 03	5.707E 03	1.920E 00	9.694E+04	0,000	0.000
	8.7298 01	7.2026=01	0.000	-1.606E	4P05.50 50	03 -1.0052	03 m1.204E 03	5.707E 03	1.921F 00	9.697E=04	0.000	0.000

116-01811	_	AALT OF TH	קאון דע די	u 1004335	Carps as a
X		DARAG	CDRAG	CF	нC
4.0406	0 1	1.284E 05	1.284F 02	2.4346-03	4,605E=02
4.0415	0 1	1,65#E=01	1.286F 02	2.4356+03	4.607E-02
4.1319	01	1.472E 01	1.433P np	2.5518-03	4.9095402
4.137E	0.1		1.4445 02	2.540E=03	4,934Fa02
4.1505	0.1	S.150E 00	1.465F 02	2.577E-03	4.979F+02
4.24F	01		1.6195 92	2,6546-03	5.1156-02
4.4C9#	01		1.8725 02	2.698E#03	5.049E#02
4.4315	υŢ	3,296E 00	1.9055 02	2.70hE#C3	5.0586#02
4.480F	Λį		1.9798 02	2.729E=03	5.085E=02
4.48 j E	e i		1.979F 02	2,729E003	5,088E=02
4.6265	Λį		5.169k US	2.7685#03	4.8666#02
4.7318	0.1		2.531F 02	2.769E=03	4.525F.02
4.733F	01		2.333F 05	2.770E=03	4.5268005
4.8115	01		2.4325 03	2.755E=03	4.184E-02
4.876	01		2.512F 05	2,726E=03	3.7968-05
4,931F	CI		2.571F 0g	2.700E-03	3.503E-02
5,072F	01		2.715F 02	2.641E=03	2.89BE=02
5.2821	01		2.898# 02	2.579E=03	2,297##02
5.332E 5.407F	01		2.9378 02	2.5648#03	2.1852=02
5.483E	01		2,993E 02 3.047# 02	2,5448403	2.038E=02
5.576F	01		3.047# 02 3.109E 02	2.5288+03	1.9102=02
5.626F	01		3,130F 02	2.4588-03	1.3926.02
5.631E	01		3.133F 02	2.4578-03	1.3878=02
5.645F	01		3.140# 02	2.455E=03	1.375E=02
5.653E	01	,	3.144F 0g	2.447E=03	1.386E=02
5.685F	01	1.453E 00	3.199F 02	2.439E=03	1.375F=02
5.704E	01		3.170g 02	2,4336-03	1.369Fe02
5,776F	01	3,7198 00	3.207F 02	5.450E=03	1.3386-02
5.87gF	0.1		3,259E 02	2.410E=03	1.3226=02
6.079E	0.1		3.362E 02	2.010E=03	1.3686.02
0.251=	01		3.437P 02	5.408E#03	1.404E002
6.4475	01		3.565F 02	2.439E-03	1.3516-05
6.505E	01		3.584F 05	2.467E=03	1.2716.05
6.50gF	01		3.585# 02	2.441E-03	1.0766-05
6.529E 6.695E	01		3.594F 02	2.440E=03	1.078E-02
6.7625	01		3,688E 02	2.4196=03	1.023E-02
6.839E	01		4	5.300E=03	8,247E=03 6,657E=03
6.9118	01		3.711F 02	2.237E=03	5.517E=03
6.972E	ni		3.743# 12	2.221E=03	4.813E=03
7.067F	0 1		3.761F 05	2.1698-03	3.924E-03
7.110E	01	7.5836=01	3.769F 02	2.170E=03	3.976E-03
7.2635	0 1		3.798= 02	2.201E-03	4.576E=03
7.278F	٨ţ		3.800= 02	2.190E-03	4,389F=03
7.353F	01	1.156E 00	3.8128 02	2.100E=03	3.004E=03
7.353F	01		3,812F 02	2.0995-03	2.996E=03
7.486E	01		3.818# 02	2.1138003	3.259E=03
7.771F	01		3.830F 02	2.1046=03	3.2566-03
8.141F	01		3.843F 02	2.1015=03	3.3996.03
8.4427	01		3.650F 02	2.031E-03	2.591Ew03
8.728F	01		3.8520 05	2.051F=03	2.9416=03
8.729E	٥1	0.00	3.852= 05	2.0518=03	2,9425003

RAMJET PERFORMANCE

ယ		9 TELMAS	PERFORMANCE	
27	ENCT. E PAR. BRUINER		TN! ET	
	MEASURED THRUST:	. (LEF) . (LBF) . (LBF#\$EC/LBM) . (LBF#9EC/LBM)	ANGLE OF ATTACK	329 053
	CALCULATED THRUST COEFFICIENT	5	DELTA PTZ	196 (PSI) 497 450
	REGENERATIVE-COOLED FAGINE PERFORMAN CALCULATED	CF	INLET PROCESS EFFICIENCY - SUBSCRIC 0.8 KIRFIC ENERGY EFFICIENCY - SUPERSONIC 0.9	958
	MET TRRUST	. (LPF) . (LBF) . (LBF=SEC/LBM)	KINETIC EMPRGY PEPICIFACY = SUBSCAIC 0.8 ENTHALPY AT PO = SUPEPSCAIC	.38 (PTU/LPM)
			COMMUSTOR	
	TNLET MOMENTUM CHANGE	. (LBF)	FUEL-AIR RATIO	000 000 538 991 4429 4429
	STATIONS		FUEL INJECTORS	
	SPIKE TRANSLATION	84 (IN) 09 (IN) 00 (IN) 95 (IN) 35 (IN) 87 (IN) 51 (IN) 51 (IN) 51 (IN)	INJECTORS STATION VALVE 1A	

Reading 71

t = 171.39 sec.

SUPPARY REPORT

يتن					•					•	-								
٠١٤٠	I	p	, †	н		GAMMA	MOLWT	SONV	MACH	VFI	s	4/4	M.	AZAC	MOMIN	st.	TVAC	PHT	ETAP
	WIND-TUNNE	I.	1	n 5		G P III	12/14/11	00111	14017	100	•	,		M/FC		,,	1.1.0		£ 1 A1
				643.60	7901	1.2960	28.498	254B											
	₹0.000	0.377	THA						4-031	427	1 810	0.10579	36.588	0.0718	4645	9.586	184.6		
	SPIKE TIP				421	1.5.00	201011	701	0.50.51	2030	1 4014	4410314	239240	044210	4005	7 8 20 0	Toato		
			, 2	0 5			** ***												
		18,187		_ ~ • •			28.897							_					
	0.600	16.525.	. 2848		751)	1,5460	28.897	2525	0,387	975	2.074	0.10579	25.248	0,9318	4709	1.603	186.5		
	MIND TUNKE		. 3	0 0															
	0.000 7	43,249			770)	1,2960	28.898	2548											
	0.000	0.383	390						6.015	5828	1.819	0.10701	25.537	0.9318	4718	9.692	184.7		
	SPIKE TIP	NS	4	0 0		¥ -						. •		• . • -		• -	•		
	0.606	18.187.	2911	643.66	770)	1.2960	28.897	2548											
		16.481.	2846	624-01	7=11	1.2981	26.897	2521	0.392	QAA	2.074	0.10701	25.537	0-0314	4718	1.644	184.7		
	INLET THRO	AT	4	0 4	. 3		2000.,	G > L 1		,00	# G V 1 ~	01.0101	65455	1.3 3 1 0	~.,0	100	*0-11		
			2872	631.7(7081	1 2071	28.897	2672									-		
	40.400	18.458	1648	282.11	// ()	1 3/07	28 807	10EV	2 108	// (85		0.88524	25 245		3014	57.528	(E) A		
	THEET UPNE	100010		202036	43.11	1.3401	20,07/	1220	6.140	4105	4 4 7 4 4	0.00354	634540	9.1114	3014	31.320	131+0		
			3813	471.94	7-6:	4 2024		0000											
	40.400	10 044	2012	631576	(50)	105417	20.897	5225											
	40,400	124011		204.3(393)	1.3441	28.897	1913	2,242	4588	1.911	0.80476	25.248	0.1225	3863	53,622	153.0		
	INLET DANK		7	0 4															
	40.400	07.871	2872	631.76	758)	1,2973	28,897	2532											
	40.400	90.242	2756	597,21	7 - 4)	1,3010	28.897	2484	0.520	1315	1.948	0.80476	25.248	0.1225	3863	16.440	153.0		
	COMBUSTOR	0	8	1 21													•		
		58,032	2827	630.10	775)	1,2998	27,732	2567											
	40.410	12.472	1518	244.96	302)	1.3487	27.732	1916	2,292	4391	1.985	0.88800	25.331	0.1114	3813	60.594	150.5	0.11	0.07
	COMBUSTOR	0	9	5 57	٠					_	-	•	-			•			•
		25.990	2757	631.00	784)	1.3036	26,607	2592											
	41.300	16.110	1668						1.999	4089	2.060	0.89280	25.416	0.1111	3689	56,736	145.1	0.22	0.04
	COMBUSTOR		10	3 21					• • • •			***		*****					
		30.644	2717		7711	1.3055	26.565	2576											
		16.151		297.30	4.03	1.3451	26.569	2023	2.019	4086	2.05%	16598.0	25.416	0.1112	3687	56,675	145-1	0.22	0.01
	COMBUSTOR		11	4 21	-4-,		F0#007	4.63		-000		V, C. C.	451410		3001	308013	1-001		0 4 0 2
		29,946			7401	1.3054	26.559	Ne2c											
		16.417							2 - ANA	11061	3 AE2	0.89396	35 // 4	0.4110	7477	E4 #4E	• A A *	A 22	A AA
	COMBUSTOR		- 12		741)	103404	500000	6060	C 8 000	4004	# 6 C D D	0 6 6 7 5 7 6	ESTATO	001110	30//	56,465	14441	Vacc	U # U U
				5 21	7.0.		04 580												
		27.779					26,558		4 650		5 650		AF 847		7/60		4 11 9 41		
	WINDSON COD	17.438			~50)	1.5435	50.331	2044	1.454	4003	2.094	0.89416	25.410	0.1110	2020	55,630	145.9	0.22	0.00
	COMBUSTOR		13	6 21									•						
		09.944		954.46	763)	1,3065	26,557	2565											
	42.460	17.810			468)	1.3407	26.557	5090	1,852	3852	2.063	0.88538	25,416	9.1121	3554	52,997	139.8	0.22	0,00
	COMBUSTOR		14	7 21															
		01.704					26.567												
	44.095	28.852		396.20	539)	1.3311	26.567	1155	1.489	3292	2.066	0.85495	25.416	0.1161	3458	43.733	136.1	0.22	0.01
*	COMBUSTOR		15	8 21															·
		00.760	2649	611.16	750)	1.3077	26.559	2547											
	44.310	29,783	1972						1.461	3237	2.065	0.85346	25.416	0.1163	3444	42.937	135.5	0.22	0.00
	COMBUSTOR		16	9 21		-	•	. •	-						•	*			-
	44.800	97.454			7461	1.3082	26,558	2541								-			
	44.800				5541	1.3294	26.557	2238	1.390	3100	2.066	0.85014	25-416	0.1167	3410	41.075	134.5	0.22	0.00
	COLBUSTOR	0	17	10 21	- 2 /						-,	484444			W-10		7 3 4 6 C	~ # C	V . V V
	44.810			607.10	7001	1.1070	26.572	2546											
	44.810	31.874	2027	413.04	4501	1.2001	26.672	2246	1.785	2100	2 040	0.85015	3E #44	0 4447	2//00	# L A TA	170 4	A 22	۸ ۸ ۹
	COMBUSTOR	P. V V 4 4	18	11 21	47/1	193500	E. V & D 1 D	5547	303	3144	C # V O O	A # 0 3 A 1 3	53.410	A#1761	2404	41,078	12401	VECE	n an I
	46.260				7-61	1 3007	34 E 6 ^	25.34								_			
	46.260	27.274	4700	595.3((52)	1 2777	20.300	2764	4 858	710-	3 A4 ·	0.00001	5 5 044		~				
			1 - 30	37115	335)	1,3361	CO.300	2146	1.424	2140	6.000	0.80086	25.416	0.1239	5390	39,775	135.4	0.22	0.00

A/AC HONTH IVAC PHI ETAC GAMPA MOLFT SONV MACH VEL COMBUSTOR 0 19 12 21 47.310 93.113 2572 586.9(726) 1.3103 26.558 2512 23.946 1846 364.2(504) 1.3356 26.558 2148 1.554 3338 2.061 0.74517 25.416 0.1332 3454 36.660 135.9 0.22 0.00 47.310 COMBUSTOR 0 20 13 3 47.335 92.857 2578 586.7(728) 1.3100 26.565 2514 47.335 24,099 1855 364,7(507) 1,3352 26,565 2153 1,548 3333 2,062 0,74434 25,416 0,1333 3456 38,550 136,0 0,22 0,01 COMBUSTOR 0 21 14 48.110 83.834 2774 580.9(786) 1.3008 26.791 2988 48.110 25.765 2095 369.0(576) 1.3238 26.791 2269 1.435 3256 2.088 0.69435 25.416 0.1429 3515 35.138 138.3 0.22 0.20 COMBUSTOR 0 22 15 3 85.480 2715 576.4(768) 1.3033 26.742 2565 48.785 48.785 20.109 1916 329.5(523) 1.3310 26.742 2177 1.615 3515 2.081 0.63854 25.416 0.1554 3577 34.879 140.7 0.22 0.16 COMBUSTOR 0 23 16 49.315 P6.891 2679 573.2(797) 1.3048 26.715 2551 49,315 16.950 1802 303.7(490) 1.3357 26.715 2116 1.735 3672 2.076 0.59719 25.416 0.1662 3622 34.076 142.5 0.22 0.14 COMBUSTOR 0 24 17 21 50.725 97.625 2527 565.8(712) 1.3114 26,501 2490 10.312 1442 239,4(386) 1.3546 26.581 1911 2.114 4042 2.052 0.50897 25.416 0.1950 3708 31.969 145.9 0.22 0.02 50.724 COMBUSTOR 0 25 16 4 52.825 90.268 2563 557.1(722) 1.3094 26.647 2502 52.825 8.175 1409 210.0(376) 1.3558 26.647 1888 2.208 4168 2.061 0.41716 25.416 0.2379 3791 27.021 149.1 0.22 0.08 COMBUSTOR 0 26 19 88.639 2572 555.4(725) 1.3090 26.662 2506 53.325 53.325 7.737 1401 203.2(374) 1.3552 26.662 1862 2.230 4198 2.063 0.40011 25.416 0.2480 3807 26.101 149.8 0.22 0.09 COMBUSTOR 0 27 20 2 54.075 88,089 2569 552,9(754) 1,3090 26,667 2504 54.075 7.023 1366 192.0(364) 1.3561 26.666 1860 2.285 4250 2.063 0.37716 25.416 0.2631 3830 24.908 150.7 0.22 0.09 COMBUSTOR 15 85 0 54.835 89.254 2551 550.5(718) 1.3097 26.656 2496 54.835 6.300 1312 179.9(349) 1.3613 26.656 1825 2.359 4306 2.060 0.35666 25.416 0.2782 3851 23.868 151.5 0.22 0.09 COMBUSTOR 0 29 22 55.760 81.632 2606 547.9(734) 1.3071 26.722 2517 55.760 6.102 1368 176.2(364) 1.3575 26.722 1859 2.320 4313 2.072 0.33487 25.416 0.2963 3873 22.446 152.4 0.22 0.14 COMBUSTOR 0 30 23 56,260 55,527 2843 546,7(806) 1,2962 26,980 2606 6.037 1666 185.6(447) 1.3391 26.980 2028 2.096 4250 2.120 0.26978 25.416 0.3678 3928 17.821 154.6 0.22 0.36 56.260 COMBUSTOR 0 31 24 56.315 80.165 2559 546.6(721) 1.3092 26.678 2499 56.315 4.261 1221 148,2(323) 1.3665 26.678 1764 2.532 4465 2.068 0.26893 25.416 0.3690 3930 18.660 154.6 0.22 0.10 COMBUSTOR 0 32 25 56,455 79.331 2566 546.2(723) 1.3089 26.686 2501 4.249 1228 56.459 147.5(325) 1.3661 26.666 1768 2.927 4467 2.070 0.26700 25.416 0.3717 3933 18.533 154.7 0.22 0.11 COMBUSTOR 0 33 26 21 56.935 33.858 3520 546.1(1011) 1.2619 27.755 2820 6.010 2404 182.6(659) 1.3023 27.765 2368 1.801 4265 2.192 0.26999 25.416 0.3675 3935 17.894 154.8 0.22 1.00 56.535 COMBUSTOR 0 34 27 21 33.989 3518 545.4(1011) 1.2616 27.755 2820 56.815 56,815 5.962 2397 180.1(656) 1.3026 27.765 2364 1.808 4276 2.192 0.26909 25.416 0.3688 3941 17.880 155.0 0.22 1.00 COMBUSTOR 0 35 28 21 57.044 33.853 3517 544,9(1010) 1.2616 27.755 2R19 5.782 2381 175.2(652) 1.3032 27.765 2397 1.825 4301 2.192 0.26868 25.416 0.3693 3945 17.960 155.2 0.22 1.00 57.041 COMBUSTOR 0 36 29 21 57,763 32,887 3513 543,5(1009) 1,2618 27,755 2818 57,765 5.205 2335 161.4(638) 1.3048 27.765 2336 1.672 4373 2.194 0.26442 25.416 0.3753 3954 17.968 155.6 0.22 1.00 COMBUSTOR 0 37 30 21 ₩1 58,785 32.227 3507 541.6(1007) 1.2619 27.756 2816 ₩ 58,785 4.837 2303 151.47 628) 1.3059 27.765 2321 1.904 4419 2.195 0.26274 25.416 0.3777 3959 18.044 155.8 0.22 1.00

GAMPA MOLMT SONY MACH VEL S 4/4 AZAC MONTH G TVAC' PHI ETAC' -ADTRUBACO CO 0 38 31 21 UT 60.795 15.025 3497 539.0(1004) 1.2603 27.753 2810 60.795 1.375 2043 72.9(590) 1.3155 27.765 2194 2.201 4830 2.248 0.27188 25.416 0.3650 3944 20.406 155.2 0.22 1.00 COMBUSTOR 0. 39 32 21 62.215 31.768 3495 537.5(1003) 1.2624 27.756 2811 62.215 4.562 2270 141,4(618) 1.3071 27,765 2305 1.931 4452 2.194 0.27925 25.416 0.3553 3932 19.320 154./ 0.22 1.00 COMBUSTOR 0 40 33 21 64.679 35.752 3486 534.1(1000) 1.2631 27.757 2808 64.679 8-833 2506 232.8(709) 1.2967 27.765 2441 1.590 3882 2.185 0.26470 25.416 0.3749 3915 15.969 154.0 0.22 1.00 COMBUSTOR 0 41 34 21 65.055 33,505 3484 533,4(999) 1,2630 27,756 2807 65.055 9.973. 2676 267.3(743) 1.2928 27.765 2489 1.466 3649 2.189 0.24608 25.416 0.4032 3912 13.954 153.9 0.22 1.00 COMBUSTOR REGEN 42 35 3 45.055 33.505 3784 640.2(1097) 1.2491 27.743 2911 65.055 11.469 3025 379.4(852) 1.2802 27,763 2633 1.372 3612 2.219 0.24608 25.416 0.4032 4038 13.813 158.9 0.22 1.00 NOZZLE 43. 36 87.291 33.505 3484 533.4(990) 1.2630 27.756 2807 87.291 0.711 1413 -109.10 348) 1.3457 27.765 1846 3.072 5670 2.189 0.05123 25.416 1.9371 4832 4.514 190.1 0.22 1.00 NOZZLE 44 37 33.505 3484 533.4(990) 1.2630 27.756 2807 87.291 87.291 0.377 1198 -168.2(309) 1.3591 27.765 1708 3.470 5925 2.189 0.03349 25.416 2.9629 4967 3.084 195.4 0.22 1.00 NOZZLE AE REGEN 45 38 87.291 33.505 3784 640.2(1097) 1,2491 27.743 2911 87.291 0.775 1603 #55.5(422) 1.3349 27.765 1958 3.014 5900 2.219 0.05123 25.416 1.9371 5045 4.697 198.5 0.22 1:00 NOZZLE PU REGEN 46 39 87.291 33,505 3784 640,2(1097) 1,2491 27,743 2911 87.291 0.377 1334 4131.1(346) 1.3506 27.765 1796 3.459 6212 2.219 0.03153 25.416 3.1468 5211 3.044 205.0 0.22 1.00 FICTIVE COMBUSTR 66 59 0 65.055 185,190 3487 533,4(1000) 1,265R 27,760 2812 0.377 752 0285.7(191) 1.3847 27.765 1366 4.687 6402 2.067 0.05761 25.416 1.7224 5224 5.732 205.5 0.22 1.00 65.055 FICTIVE NOZZLE 67 60 0 87.291 19.491 3449 \$21.81 988) 1.2633 27.756 2794 87.291 0.938 1718 -22.7(454) 1.3292 27.765 2022 2.582 5220 2.225 0.05123 25.416 1.9371 4589 4.156 180.6 0.22 1.00

		0.00		204	G≠IP		8n - 0		CAWALL	P#147280	P=18/PT0	P#08/P80	P=08/PT0
XANS	P#18	P#OB	4 d 4 d 4 d 4 d 4 d 4 d 4 d 4 d 4 d 4 d	0.00 m	0.000		0.000		2.470E+02	2.760E 00	1.399E=03	0.000	0.000
6.98[F=01	1.0408 00	0.000	-4.426E=01	0.000	0.000		0.000		1.534E 02	2.760F 00	1.3996#03	0.000	0.000
1.836F 01 3.070F 01	1.040E 00 2.870E 00	0.000 0.000	-1.931E 07		0.000		0.000		5.4538 07	7.616F CO	3.861E=03	0.000	0.000
3.508E 01	3.847E 00	0.000	-4.108E 02		0.000		0.00		6.804E 02	1.021E 01	5.177t=03	0.000	0.000
3.519E 01	4.167E 00		0 44.753E 02		0.000		0.000		6.850E U2	1.106E 01	5.607E=03	1.477E 01	7.491E=03
3.520E 01	4.184E 00		0 -4.754E 02		0.000		0.000		6.857E 02	1.110F 01	5.630E=03	1.470F 01	7.453E-03
3.555E 01	5.180E 00		n =4.887E 02		0,000		0.000		7.209E 02	1.3758 01	6.9698-03	1.024E 01	5.190E-U3
3.5848 01	5.007E 00		0 -5.092E 02			- 02			7.529E 02	1.3296 01	6.737E-03	6.236F 00	3,1626-03
3.606E C1	4 900E 00		0 92.55 05				-		7.729E 02	1.30GE 01	6.5936-03	9.2206 00	4.675E-03
3.648F 01	4-196E 00		0 05.01AE 02						8,164E 02	1.113E 01	5.646E+03	1.364E 01	7.931E+03
3.701F 01	5.250E 00		0 -5.638E 02					61	8,7266 02	1,3936 01	7.064E-03	2.374E 01	1.204E=02
3.732E 01	4.9218 00		5 759E 02						9.063E 02	1.306F 01	6.621E-03	2.856E 01	1.448t-02
3.803F 01	4.185E 00		-5 A99E 02						9.434E 02	1,110E 01	5.631F=03	3.835E 01	1.9456-02
3.83gE 01	7.814E 00		-5.941E 02						1.018E 03	2,073E 01	1.051E=02	4.272E 01	2.166E=02
3.875F 01	1.248E 01		1 -6.139E UZ						1.064E 03	3,312E 01	1.6801-02	4.667E 01	2.366E=02
3.881F 01	1,323E 01		1 =6.175E 02						1.072E 03	3,511E 01	1.780E=02	4.730E 01	2,398E=02
3.901E 01	1.548E 01		#6.278E 02						-1.094E US	4.108E 01	2.0835-02	4.677E 01	2.371E=02
3.932E 01	1.840E 01		#6.480E 02						1.130E 03	4.882E 01	2.4766-02	4.591E 01	2.328E+02
3.950F 01	2.002E 01		50 3808.8						1.150E 03	5.314E 01	2.694E+02	3.445E 01	1.747E+02
3.981E 01	1.7868 01		0 -6.884E 02						1.187E 03	4.740E 01	2.4046-05	1.386E 01	7.030E=03
4.000F 01	1.659E 01		0 -7.054E 02						1.209E 03	4,403E 01	2.233E=02	1.326E 01	6.722E-03
4.040E 01	2.036E 01		0 -7.428E 02						1.256E 03	5.402E 01	2.739E=02	1.195E 01	6.05@EmQ3
4.041E 01	2.045E 01		0 -7.437E 02						1.257E 03	5.427E 01	2.752E=02	1.192E 01	6.042E+03
4.130E 01	2.883£ 01		0 98,506E 02						1.3528 03	7.650E 01	3.879E-02	9.0026 00	4.564E=03
4-131E 01	2.892E 01		0 #8.519E 02						1.363E 03	7,675E 01	3.891E=02	8.969E 00	4.548E=03
4.137E 01	2,9538 01	3.300E 0	50 3708,8m g	#3.924E	02 -2.575	E 02	01.3497	0.5	1:371E 03	7,8378 01	3.9746-02	8.757E 00	0 440E=03
4.150F 01	3.071E U1	4.16SF 0	0 -8,779E 02	-4.080E	02 02.649	E 02	01.434E	02	1.386E 03	8,150E 01	4.132E=02	1.105E 01	5.6032003
4.246E 01	2.482E 01		1 -9,659€ 02						1.501E 03	6.587E 01	3.340E-02	2.864E 01	1-4556-05
4,409E 01	3.562g 01	2.208g 0	1 =1.036E 03	-8.470E	02 -4.520	E 02	93.950E	20	1.699E 03	9,4528 01	4.792E-02	5.860E 01	2.971E=02
4.4312 01	3.704E 01	2.253E 0	1 #1.047E 03	∞8.809E	02 44.712	E 02	₩4.178E	02	1.725E 03	4.856E 01	4.984E~02	5.978E 01	3,031Ea02
4.480E 01	4.027E 01	2.354F 0	1 -1.074E 03	-9.881E	02 05.170	E 02	-4.711F	0.2	1.785E 03	1.069E 02	5.419E-02	6.245E 01	3.167E-02
4.481E 01	4.019E 01		1 =1.075E 03						1.786E 03	1.067E 02	5.408E-02	6.250E 01	3.169E=02
4.65PE 01	5*801E 01	2.654E 0	1 01.074E 03	-1.290E	03 -6.517	E 05	#6.385F	95	1.9646 03	7,4338 01	3.7696=02	7.042E 01	3.571E=02
4.7318 01	1.919E 01		1 =9.966E 0S						2.0948 03	5,093E 01	2.5826-02	7.6157 01	3,861E=02
4.733E 01	1,945E 01		1 -9.946E 02						2.097E 03	5,161E 01	2.617E+02	7.629E 01	3.868E#02
4.8112 01	2.740E 01		i =4.5255 05						2.194E 03	7.271E 01	3,687E=02	6.403E 01	3.247E=02
4.878E 01	2.011E 01		; ►8,557E 02						2.2/8E 03	5.336E 01	2.706E-02	5.336E 01	2.706E=02
4.931E 01	1.695E 01		1 -8.045E 02						2.345E 03	4,498E 01	2.281E-02	4.498E 01	2.281E=02
5.072E 01	1.031E 01		1 07.038E 02						2.922E 03	2.736E 01	1.387E=02	2.736E 01	1.387E=02
5.285E Of	8,175E 00		0 -6.0508 05						2.789E 03	2,1695 01	1.100E=02	2,169E 01	1.100E=02
5.332E 01	7.737E 00		o =5.813E 02						2.8520 03	2,053E 01	1.041E=02	2.053E 01	1.041E.02
5,407E, 01	7.023E 00		0 -5.527E 02						2,9486 03	1.8648 01	9.450E-03	1.864E 01	9.450E>03
5.483E 01	6.300E 00		02 369E 02						3.046E 03	1.6728 01	8.476E+03	1.672E 01	P.476E+03
5.576E 01	6.145E 00		0 -4.981E 02						3.164E 03	1.630E 01	8.264E=03	1.630E 01	8,264E=03
5,6268 01	6.057E 00		0 -4.410E 02						3,209E 03	1,607E 01	8-149E-03	1.607E 01	8.149E = 03
5.631E 01	2.475E 00		0 -4.3938 02						3.216E 03	6,567E 00	3.3306-03	1,6058 01	8.137E+03
5.645E 01	2.475E 00		o =4.353E 02						3.2388 03	6,5678 00	3.3306-03	1-598E 01	8.1092.03
5.653E 01	6.010E 00		o =4.329E 02						3.245E 03	1,995E 01	8.086E=03	1.595E 01	8.086E>03
5.681E 01	5.962E 00		0 =4.251E 02						3.280E (3	1.582E 01	8.022L=03	1.5826 01	8.022E#03
5.704E 01	5.782E 00		0 04.1946 02						3.409E 03	1,5348 01	7.780E=03	1.534E 01	7.780E=03
5.776E 01	5.205E 00		0 84.045E 02						3.402E 03	1.381E 01	7,003Ea03	1.381E 01	7.003E=03
15.878£ 01	4.837E 00		0 =3.929E 02						3,5378 03	1,2848 01	6,509E=03	1.284E 01	6.509E=03
' 6 . 079E 01	1.379E 00		0 -3.921E 02						3,7908 03	3,649E 00	1.850E=03	3-649E 00	1.8508.03
, 6.551E 01	4.562E 00		0 *3.9218 02		_				3.972E 03	1.211E 01	6,139E=03	1.211E 01	6.139E=03
6,468F 01	8.833E 00		0 =3.9218 02						4.289E 03	2.344E 01	1,1885=02	2.344E 01	1,1882=02
6.505E 01	1.046E 01	794065 7	o -3.921E 02	にゅりつしに	05 #1:#02	a ()5	#1 #401t	vo	4.337E 03	2.776E 01	1.4086-02	2.517E 01	1.276E>02

	YABB	P=IB	PHOB	PDA	DOX.	GelB	ងកម្ព	CAMALL	P=18/P80	F#IB/PTO	P=08/P80	P=08/PT0
ယ	6.50oF 01	1.046E 01	9.553F 0n	-3.921E 02	. =2,865 € 03	3 -1 -403E	03 =1.462F 03	4.342E 03	2.7766 01	1.4086-02	2.535E 01	1.285E.02
27	6.520E 01	9.906E 00	9.900F 00	-3.921E 02	. +2,873E 0;	3 m1.405E	03 =1.448E 03	4.36FE 03	2.629E 01	1.3336=02	2.627E 01	1.332E=02
~	6,695E 01	5.290E 00	4.630E 00	-3.099£ 02	-2.932E 01	3 -1.425E	03 -1.508E 03	4.583E 03	1.4046 01	7.117E=03	1.229E 01	6.229E-03
	6,76gE 01	4.071E 00	4.410F 00	-2.167E 02	#2.953E 01	5 a1 431E	03 #1.522E 03	4.665E 03	1.0FOE 01	5.4778=03	1.170E 01	5.9336.03
	6.839E 01	2.670E 00'	4.059E 00	-1.126E 02	-2.976E 0	5 =1.437E	03 -1.539F 03	4.760E 03	7.085E 00	3.5926-03	1.077E 01	5.461E=03
	6.911E 01	2.110E 00	3.730E 00	-3.316E 01	≈3.000E 0	3 -1 -442E	03 -1.558E 03	4.848E 03	5.598E 40	2.838E=03	9.898E 00	5.019E=03
	6.9728 01	1.635E 00	2.6725 00	2.059E 01	-3.020E 0	3 -1 -445E	03 m1.574E 03	4.922E 03	4.338E 00	2.200E-03	7.091E 00	3.595E-03
	7.067E 11	1.428E 00	1.0258 00	7.426E 01	-3.049E 0	1 450E	03 P1.599E 03	5.036E 03	3.790E 00	1.922E=03	2.720E 00	1.379E=03
	7.110E 01	1.335E 00	1.1288 00	9.2148 01	#3.061E 0	3 -1.451E	03 -1.610E 03	5 086E 03	3.542E 00	1.7962003	2.993E 00	1.518E+03
	7.263E 01	1.267E 00	1.4952 00				03 #1.639E 03	5.273E 03	3.361E 00	1.704E=03	3.967E 00	2.011E+03
	7.278F 01	1.260E 00	1.3035 00	1.608E 02	-3.098E 0	1 -1 -496E	03 m1 641E 03	5.290E 03	3.343E 00	1.695E=03	3.458E 00	1.754E=03
	7.353E 01	1-112E 00	3.4502.01				03 -1.659E 03	5.374E 03	2.951E 00	1.496L=03	9.155E=01	4.642E=04
	7.3548 01	1.111E 00	3.399F-01				03 m1.659E 03	5.375E 03	2.949E 00	1.4956-03	9.019Ep01	4.573E-04
	7.486E 01	8.500E=01	0.000				03 -1.684E 03	9.427E 03	2.2556 00	1.144E=03	0.000	0.000
	7.771E 01	8.300E=01	0.000				03 01.684F 03	5.525E 03	2.202F 00	1.117E=03	0.000	0.000
	8.16 E 01	8.650E-01	0.000				03 =1.684E 03	5.630E 03	2.295E 00	1.164E=03	0.000	0.000
	8.442E 01	6.050E#01	0.000				03 #1.684E 03	5.684E 03	1.605E 00	8.140E=04	0.000	0.000
	8.728E 01	6.150E=01	0.000				03 -1.684E 03	5.707E 03	1.632E 00	8.274E=04	0.000	0.000
	8.729F 01	6.150E=01	0,000				03 -1.684F 03	5.707E 03	1.632E 00	8.275E=04	0.000	0,000

×	DORAG	CURAG	CF	нс
441011 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1.283E 02 1.761E 01 1.661E 01 1.782E 01 1.127E 01 1.127E 01 1.2150E 01 1.625E 01 1.625E 01 1.625E 01 1.625E 01 1.625E 01 1.786E 01 1.340E 01 1.340E 01 1.340E 01 1.320E 01 1.320E 01 7.935E 00	00000000000000000000000000000000000000	2.6508E=003 2.6508E=003 2.6508E=003 2.6503E=003 2.6503E=003 2.6503E=003 2.751E=003 2.751E=003 2.751E=003 2.751E=003 2.751E=003 2.751E=003 2.751E=003	4.35542 4.2712=022 4.2712=022 4.2712=022 4.2712=022 4.3402=022 4.3402=022 4.35572=022 4.35572=022 4.35572=022 4.85572=022 4.85572 4.85
5.227 E E O O O O O O O O O O O O O O O O O	1 6.136E 00 1.508E 01 1.884E 01 3.913E 00 5.476E 00 1.6.250E 00 1.2.056E 00 1.3.054E=01 7.676E=01 4.972E=01 1.873E 00 1.513E 00 1.513E 00 1.4.862E	2.5828 0022 2.5838 0022 2.7838 0022 2.7921 0022 2.792	2.650225==0033 65025==0033 650225==0033 650225==0033 650225==0033 650225==0033 65025==0033 650225=0033 650225=0033 65	733E=022 2-33E=022 2-371E=022 2-171E=022 1-804E=022 1-804E=022 1-804E=022 1-3367E=022 1-359E=022 1-359E=022
5.878E 000 6.2468E 000 6.2468E 000 6.2468E 000 6.3268E 000 6.329E 000 6.329E 000 6.329E 000 6.329E 000 6.329E 000 6.329E 000 6.329E 000	1 6.863E 00 1 1.523E 01 1 1.112E 01 1 1.631E 01 1 2.140E 00	218 E E E E E E E E E E E E E E E E E E E	2.913Em03 3.2314Em03 2.914Em03 2.935Em03 2.995Em03 3.0446Em03 2.874Em03 2.874Em03 2.874EEm03 2.474EEm03 2.4742Em03	1.170E002 4.491E003 1.25E002 1.25E002 1.25E002 1.25E002 1.26E002 1.26E002 1.26E002 1.26E002 1.26E002 1.26E002 1.26E002 1.26E003 1.26
7.263E 0 7.278E 0 7.353E 0 7.353E 0 7.486F 0 7.471E 0 8.142E 0	1 3.11E 00 2.944E=01 1.1932 00 1.883E=03 1.883E=03 1.848E 00 1.334E 00 1.334E 00 1.334E 00 1.334E 00 1.334E 00	4.025E 02 4.026E 02 4.040E 02 4.046E 02 4.059E 02 4.059E 02 4.059E 02 4.059E 02 4.059E 02 4.059E 02	2.645E003 2.645E003 2.541E003 2.541E003 2.5466E003 2.5466E003 2.4537E003 2.4535E003	4.615E=03 4.551E=03 2.546E=03 2.546E=03 3.316E=03 3.233F=03 3.315E=03 2.518E=03 2.518E=03

RAMJET PERFORMANCE

ENGTAE PERFURIANCE	1	NLET
		0.0053 FFICIENCY 0.1428
REGENERATIVE-COOLED FNGTHE PERFORMANCE CALCULATED	INTER PROCESS EFFICIENCY * 8 KINETIC ENERGY EFFICIENCY *	SUBSONIC 0.8957 SUPERSONIC 0.9190
STREAM THRUST	BF) ENTHALPY AT PO = SUPERSONIC.	5088GNIC 0.8854
MOMENTUY AND FORCES	403	BUSTOR
INLET FRICTION DRAG	BF) COMBUSTOR EFFICIENCY	0,215 1,000 1,
BADITATS	FUEL INJECTO	RS
NOMINAL COWL LEADING EDGE	IN)	VALVE B

t = 174.94 sec.

SUMMARY REPORT

P	T	н_	(GAMMA	MOLMI	SONV	мАсн	VEI	S	W/A	₩	A/AC	момтм	Q	IVAC	PHI	ETAC
WIND TUNNEL 0.000 743.749	1 2940	0 5 652.3(7	78) 1	.2951	28.898	2560											
0.000 0.381	394	-34.3(95) 1	.3987	28.897	974	6.018	5861	1.822	0.10585	25.214	0.9300	4684	9.642	185.A		
SPIKE TIP NS 0.600 18.262	3θπυ 5	0 5 652.3(7	778) 1	2951	28.897	2560											
0.600 16.587	2876	633.01 7	759) 1	.2971	28.897	2534	0.387	982	2.077	0.10585	25.214	0.9300	4720	1.615	187.2		
WIND TUNNEL 0.000 743.749	3	0 0 652.3(7	7701 4	2051	08.80B	2540						-					
	396	-34.0(95) 1	3987	28.897	976	6.004	5860	1.822	0.10685	25.452	0.9300	4728	9.731	185.7		
SPIKE TIP NS	4	0 0															
0.600 18.262 0.600 16.551			778) <u>1</u> 759) 1	2951	28.897	2560	0.392	903	2.077	0.10685	25,452	0.9300	4728	1.648	185.7		
INLET THROAT	5	0 4	_				0.072	775	2,011	012000	G01.02						
40.400 192.342		633.11 7	759) 1	.2972	28.897	25,34				T 0000 T	05 040	n 1112	3030	58.100	+52 0		
40.400 18.155 INLET UPNRSK	1624 6	275.7(4	105) 1	*2414	28.897	1426	2.184	4229	7.408	()+86403	23.214	0.4114	3632	30.100	19240		
40.400 192.342	2877	633.1(7	759) 1	.2972	28.897	2534											
		258.2(3	387) 1	.3453	28.897	1900	2,280	4331	1.908	0.80366	25.214	0.1225	3880	54.097	153.9		
INLET DNNRSK 40.400 108.536	7 2877	0 4 633 .1 (7	759) 1	.2972	28.897	2534											
40.400 91.102	276 3	599.21 7	726) 1	.3008	28.897	2487	0.524	1304	1.948	0.80366	25.214	0.1225	3880	16.280	153.9		
COMBUSTOR 0 40.410 164.664	-	1 21 631.6(7	7771 1	. 2998	27.667	2571											
40.410 12.794			391) Î	3490	27.667	1915	.2.301	4407	1.986	0.88700	25.301	0.1114	3831	60.752	151.4	0.11	0,07
COMBUSTOR 0		2 21															
41.300 130.310 41.300 16.922		632.6(7	/85) 1 454) 1	.3423	26.581	2051	1.989	4081	∂. [‡] 059	0.89165	25.383	0.1111	3701	56.552	145.8	0.22	0.04
COMBUSTOR 0	10	3 21							• • • •								
41.310 134.920 41.310 16.968	2720	632.6(7 300.4(4	773) 1	.3054	26.540	2579	2 000	4077	A 053	0.80165	25.383	0.1112	3700	56,487	145.A	0.22	0.01
COMBUSTOR 0	11	4 21						4017	,2,000	0.00240	251000		0,00	55,7-1	2.500	- ,	
41.375 134.033	2713	632.3()	771) 1	.3057	26.534	2576	4 0-1				AF 4A7	0 1110	86.00	E4 280	4116 9	0 00	0.00
	1641	303.8(444) 1	.3445	26.534	2033	1.994	4054	2.052	0.89200	25.383	0.1118	2002	56,249	149*3	0.22	0 0.00
41,500 131,866	2710	631.6(7701 1	.3058	26.533	2575											
41.500 18.787	1682	316.0(456) 1	.3426	26.533	2057	1.932	3974	2.053	0.89301	25.383	0.1110	3669	55.151	144.6	0.22	0.00
COMBUSTOR 0 42.460 118.330	13 2692	6 21 625.9(764) 1	.3064	26.533	2567											
42.460 21.791	1782	345.6(486) 1	.3382	26.532	2114	1.772	3744	2.059	0.88424	25.383	0.1121	3580	51.455	141.0	0.22	0.00
COMBUSTOR (44.095 100.979	14	7 4 613.6(3	855) :	nePe.	26.897	2674											
	2369	414.3(659) 1	3128	26.897	2398	1.317	3158	2.096	0.85385	25.383	0.1161	3585	41.900	141.2	0.22	0.31
	15	8 3															
44.310 100.900 44.310 36.83	5 2378	611.8(662) 1	1.3123	26.913	26//	1.316	3160	2.097	0.85236	25.383	0.1163	3590	41.853	141.4	0.22	0.32
COMBUSTOR	16	93								••••		.,					
44.800 100.52	7 3017	607.6(862) <u>1</u>	1.2907	26.941	2681	1 310	31E~	2 007	o 84004	25.323	0.1167	3504	41,660	141.4	0.22	0.35
44.800 36.905 COMBUSTOR	2393	408.4(7001	1.2112	204742	Z400	1,315	213(180091	0 0 0 7 7 0 7	20.000	0.1101	55 g 4	47 6000	4-110	J. C.	
44.810 100.55	5 3017	607.50	861) 1	2.2907	26.941	2681					AF 45-	A 1./-	***	n + <	4114 4	0.00	0 20
44.810 36.860 COMBUSTOR	8 2391 0 18	408.1(11 5	665) <u>1</u>	1,3115	26.941	2406	1,313	3159	2.097	0.84905	25.383	0.1167	3594	41.679	141.6	0.22	0.24
46-250 98-76	7 2794	595.9(835)	1.3014	25.382	2669	r										
46.250 31.40	8 2127	376.3(618)	1.3241	25.382	2348	1.412	3315	2.169	0.80411	25.503	0.1238	3624	41.422	142.1	0.37	0.16

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READING =	0071	BLOCK	= 75	TIME	= 174.9	38 MACI	Н Б•	o Pr	= 743	.749	TT = 294	0.3						F
countered	Р	T _	н		GAMMA	MOLWI	SONV	мАсн	VΕι	S	W/A	₩.	A/AC	MTMON	Q	IVAC	PHI	ETAC
COMBUSTOR			12 2	/ 07E\	1 3014	OF 100	0660											
46.260 46.260	31 370	2/74	595 • 8 t	(617)	1.3014	25.382	2609	1 1110	771.	0 170	0.00760	0E E03	0.1070	3600	41 411	440 4	^	
COMBUSTOR		20		01//	1.0241	23,302	2340	1.41%	3319	20410	0.80362	25,543	0.1239	3024	41.411	142.1	0.37	0.16
			586.5	1 8401	1 3002	25.428	2670											
									3450	2 172	0.74774	95.503	0.1339	3675	40.184	144	0 37	o 10
COMBUSTOR		21			80000	200.20	200		0.100	4. 6 4 7 6	0014114	20.000	01+002	50.5	40,204	7-7-1	0.37	0.17
			586.2	840)	1.3003	25,428	2673											
									346 (2.172	0.74690	25.503	0.1333	3676	40.178	144.1	0.37	0.19
COMBUSTOR	Û	22	15 3						•									
48.110	92,592	2859	579.7	(855)	1.2978	25.496	2690											
48.110				(606)	1.3240	25,496	2325	1,527	3549	2.179	0.69674	25.503	0.1429	3725	38.428	146.1	0.37	0.22
COMBUSTOR		23																
48.775	88.212	2727	576.8	(853)	1.3046	24.146	2707											
48.775 COMBUSTOR	22,191	1955	17 2	2911	1,3310	24.146	2315	1.570	3634	2.258	0.64462	25.625	0.1552	3776	36,402	147.4	0.53	0.15
			576.7	9561	1 3005	20 100	4707			,								
48.785	22.161	1955	312.66	592)	1.3316.	24.148	2315	1 570	3630	So 258	0.64379	25.625	0.1554	3777	36.368	147 /	0 68	a 15
COMBUSTOR	0	25	18 4	. 0,0,	20020	. W. A. B. T. A. C.	2010	****	QCO:Q		0.04017	234020	014004	3711	30,300	141.44	0.55	0.10
			573.1	(874)	1.3016	24.215	2730			'-								
49.315	20.575	1986	298.1	601)	1.3296	24.215	2329	1,593	3709	2.267	0.60209	25.625	0.1662	3830	34.707	149.5	0.53	0.18
COMBUSTOR	0	26	19 4						(•	• • • • • •		.,	
50.725	81.238	2830	564.9	(887)	1,2994	24.278	2744											
50,725	15,662	1906	249.0	1 574)	, 1,3320	24.278	2280	1.743	3975	2.273	0.51315	25.625	0.1950	3948	31.702	154.1	0.53	0.21
COMBUSTOR		27	20 5															
52.825	66.079	3137	554.8	989)	1.2846	24.610	2853									. = 4		
52.825 COMBUSTOR	140421	2200	21 4	(000)	1.3161	29.011	2425	1,066	4036,	.2.314	0.42059	25.625	0.2379	4694	26.379	159.8	0.53	0,35
	70 - 005	, <u>20</u>	552.5	9541	1 2805	01.510	2017			"								
53.325	12,127	2007	198.1	604)	1.3252	24.517	2323	1 812	4914	2.301	0.40340	25.625	ក. ១៥៨ភ	#1.0H	26.398	160 0	n '63	กซ์รั
COMBUSTOR	0	29	22 3	. 00-11	1,000-	4.144.0	EULU	* ****	45.4		0440040	23063	-Dac-700	4 96.4	20,000	100.4	0.40	0.01
			549.0	947)	1.2904	24.500	2808											
54.075	10.704	1928	176.2	578)	1.3285	24.500	2280	1.895	4319	2.298	0.38025	25.625	0.2631	4162	25.525	162.4	0.53	0.30
COMBUSTOR	0	30	23 4					•										05,00
54.835	72.893	2961	545.80	(930)	1.2927	24.458	2789								_			
54.835	9.262	1809	152.41	(540)	,.1.3339	24.458	2215	2,003	4437	2.291	0.35959	25.625	0.2782	4194	24.795	163.7	0.53	0.28
COMBUSTOR		31					· -			-								
55.760 55.760	67.552	2 3040	542.4	956)	1.2889	24.546	2817	4 050		'A 707		ór cor	0.0047		A# 75.			
COMBUSTOR	3.011	1000	25 5	204/	1,3290	24,041	2230	1.374	4450	2.303	0.33762	25.025	0.5403	4229	23.351	102.0	0.53	0.32
56.260	48.895	3392	540.7	(1074)	1-2711	94.914	2033			•								
56.260	8.885	2310	156.4	699)	1.3093	24.919	2456	1.785	4385	2.353	0.27200	25,625	0.3678	4329	18.536	169.0	0.53	0.47
COMBUSTOR	0	33	26 5					-,	,,,,	!"		201025	0,00.0	402	10,000	10,40		441
	59,499	3114	540.6	981)	1.2852	24.626	2843											
56.315	6.910	1876	114.2	559)	1.3292	24,628	2244	2.059	4619	2.319	0.27114	25.625	0.3690	4332	19,462	169.0	0.53	0.35
COMBUSTOR	0	34	27 3															
56.455	58,979	3125	540.1	984)	1.2847	24,638	28#6					, .	n taka ta	454	4 *12	٠	1-11-1	بر ادراجي
56,455	6.641	1886	213.41	(562)	1.3286	24.640	2249	2,055	4621	2,320	0.26919	25.625	0.3717	4337	19.332	169.2	0.53	0.36
COMBUSTOR 56.535	110 LE	3505	28 7 539.90	44751	1 2700	00 010	0030			•								
56.535	8.812	2301	151.7	(6061	1 3005	24 4 2 1 3	2734	1 708	21.07	2 352	0.27220	05 605	0 3675	h 7 h 0	10 680			4 /119
COMBUSTOR	0	36	29 3	. 0,07	1,0000	_,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	4704	A . / 70	770/	E . JOZ	(1021220	40.040	0,50/3	4340	18.644	102.4	0.53	U.47
			539.0	(1078)	1.2706	24.929	2936											
56.815	8.737	2300	147.7	(695)	1.3095	24.934	2450	1,806	4425	2.352	0.27130	25,625	0.3688	4350	18.658	169.7	0.53	ก_48
COMBUSTOR	C	37	30 3										•	,	_,,,,,			
57.041	49.664	3416	538.4	(1082)	1.2698	24.946	2940											
57.041	8.757	2313	146.1	(699)	1.3088	24.952	2456	1.804	4431	2.353	0+27089	25.625	0.3693	4357	18.652	170.0	0.53	0.49

GAMMA MOLWT SONV MACH VET S A/AC MONTH 0 IVAC PHI ETAC ധ COMBUSTOR 0 38 31 4 57.765 48.529 3472 536.3(1101) 1.2667 25.012 2957 ₱ 57.765 8.820 2374 143.7(719) 1.3058 25.019 2482 1.786 4432 2.358 0.26659 25.625 0.3753 4378 18.362 170.8 0.53 0.51 COMBUSTOR 0 39 32 6 58.785 77.366 2938 533.8(921) 1.2934 24.468 2779 58.785 5.250 1529 59.2(450) 1.3470 24.469 2046 2.382 4873 2.283 0.26489 25.625 0.3777 4389 20.060 171.3 0.53 0.29 COMBUSTOR 0 40 33 60.795 68.969 3057 529.8(961) 1.2876 24.598 2820 60.795 6,225 1724 75.2(510) 1.3360 24.599 2158 2.211 4770 2.301 0.27411 25.625 0.3650 4381 20.319 171.0 0.53 0.34 COMBUSTOR 0 41 34 62,215 43.587 3835 527.0(1224) 1.2448 25.438 3054 62.215 12.356 2951 194.2(910) 1.2801 25.462 2716 1.503 408; 2.383 0.28154 25.625 0.3553 4375 17.856 170.7 0.53 0.69 COMBUSTOR 0 42 35 5 64.679 37,401 4178 521.2(1342) 1.2198 25.855 3130 64.679 15.871 3557 266.9(1116) 1.2495 25.911 2920 1.222 3567 2.407 0.26687 25.625 0.3749 4365 14.794 170.3 0.53 0.86 COMBUSTOR 0 43 36 65.055 34,712 4181 520.2(1343) 1.2188 25.863 3130 14,860 3568 268.1(1120) 1.2485 25.920 2923 1.215 3552 2.413 0.24810 25.625 0.4032 4363 13.694 170.3 0.53 0.87 65.055 COMBUSTOR REGEN 44 37 5 34.712 4418 632.1(1430) 1.2039 25.805 3201 65.055 65.055 17.752 3934 416.9(1252) 1.2284 25.888 3047 1.077 3282 2.439 0.24810 25.625 0.4032 4448 12.655 173.6 0.53 0.87 NOZZLE AE 45 38 5 87.291 34.712 4181 520.2(1318) 1.2188 25.863 3130 0.927 1936 -304.4(562) 1.3125 25.937 2207 2.911 6424.2.413 0.05165 25.625 1.9371 5576 5.156 217.6 0.53 0.87 87.291 . NOZZLE PO 46 39 5 34.712 4181 520.2(1318) 1.2188 25.863 3130 87,291 0.381 1559 -423.2(443) 1.3309 25.937 1994 3.446 6871 2.413 0.02817 25.625 3.5514 5819 3.008 227.1 0.53 0.87 87,291 NOZZLE AE REGEN 47 40 87.291 34.712 4418 632.1(1430) 1.2039 25.805 3201 0.992 2130 -241.1(625) 1.3045 25.937 2308 2.864 6610 2.439 0.05165 25.625 1.9371 5757 5.306 224.7 0.53 0.87 87.291 NOZZLE PO REGEN 48 41 5 87,291 34.712 4418 632.1(1430) 1.2039 25.805 3201 87.291 0.381 1695 -380.9(486) 1.3236 25.937 2074 3.433 7120 2.439 0.02685 25.625 3.7265 6034 2.971 235.5 0.53 0.87 FICTIVE COMBUSTR 68 61 192.342 4471 520.2(1443) 1.2150 26.209 3210 65.055 0.381 1113 -666.9(307) 1.3552 26.294 1689 4.563 7707 2.287 0.04486 25.625 2.2304 6356 5.373 248.0 0.53 1.00 65.055 FICTIVE NOZZLE 69 62 87,291 20.502 4134 503.9(1325) 1.2166 25.857 3110 87,291 1.207 2301 -184.5(681) 1.2980 25.937 2393 2.453 5869 2.449 0.05165 25.625 1.9371 5273 4.711 205.8 0.53 0.87

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XABS	P-IB	P=0B	PDA	QQX	Q-IB		G-08	CAWALL	P-IB/PS0	P-IB/PT0	P-08/P50	P-OB/PTO
	1.040E 00	0.000	-4.446E-01	0.000	0.000		0.000	2.470E-02	2.731E 00	1.398E-03	0.000	0.000
1.836E 01	1.040E 00	0.000	-3.464E 01	0.000	0.000		0.000	1.634E 02	2.731E 00	1.398E-03	0.000	0.000
3.070E 01	2.870E 00	0.000	-1.931E 02	0.000	0.000		0.000	5.053E 02	7.538E 00	3.859E-03	0.000	0.000
3.508E 01	3.860E 00	0.000	-4.112E 02	0.000	0.000		0.000	6.804E 02	1.014E 01	5.190E+03	0.000	0.000
3.519E 01	4.174E 00		-4.763E 02	0.000	0.000		0.000	6.854E 02	1.096E 01	5.613E-03	1.478E 01	7.566E-03
3.520E 01	4.191E 00		-4.764E 02	0.000	0.000		0.000	6.857E 02	1.101E 01	5.635E-03	1.470E 01	7.526E-03
3.555E 01	5.170E 00		-4.890E 02	0.000	0.000		0.000	7.209E 02	1.358E 01	6.951E=03	1.017E 01	5.206E-03
3.586E 01	5.000E 00		-5.100E 02			11.2	0.000	7.529E 02	1.313E 01	6.723E-03	6.106E 00	3.126E-03
3.606E 01	4.895E 00		-5.234E 02				0.000	7.729E 02	1.286E 01	6.582E-03	9.077E 00	4.647E-03
3.648E 01	4.195E 00		-5.425E 02				0.000 0.000	8.164E 02	1.102E 01	5.640E-03	1.547E 01	
3.701E 01	5.250E 00		-5.646E 02					8.726E 02	1.379E 01	7.059E-03	2.354E 01	7.920E=03
3.732E 01	4.890E 00	1.079F 01	-5.766E 02	#3 194E (2 -2 013E	112	-2 RIOE OI	9.063E 02	1.284E 01	6.575E=03		1.205E=02
3.803E 01	4.085E 00	1.449F 01	-5.895E 02	-3.4755 (2 43 040E	0.2	-4.351E 01	9.834E 02	1.073E 01	5.492E-03	2.833E 01 3.805E 01	1.450E-02 1.948E-02
3.834E 01	7.772E 00		-5.933E 02					1.018E 03	2.041E 01	1.045E-02	4.238E 01	2.170E=02
3.875E 01	1.252E 01	1.766F 01	-6.129E 02	-3.798E (2 -3 208F	0.5	-5.005E 01	1.064E 03	3.287E 01	1.683E-02		
3.881E 01	1.327E 01		-6.165E 02					1.072E 03	3.486E 01	1.785E-02	4.637E 01 4.701E 01	2.374E+02
3.901E 01	1.556E 01	1.768E 01	-6.269E 02	-3.932E (2 -3 285E	112	-6.462E 01	1.094E 03	4.087E 01	2.092E=02		2.407E=02
3.932E 01	1.855E 01	1.734E 01	-6.473E 02	## 105E	2 -3 3030	(16	~7.132E 01	1.130E 03	4.872E 01	2.494E=02	4.645E 01	2.378E-02
3.950E 01	2.021E 01	1.302F 01	-6.603E 02	-4 210E C	2 3 1605	,112	-7 E07E 01	1.150E 03	5.308E 01		4.553E 01	2.331E+02
3.981E 01	1.804E 01	E-250F 00	-6.883E 02	an 100E (2 WU.TOUL	114	-0 15/5 OI			2.718E+02	3,418E 01	1.750E-02
4.000E 01	1.677E 01	5.010F 00	-7.055E 02	-4 5335 C	2 3 6000	(14	-0 E30E 01	1.187£ 03	4.738E 01	2.426E=02	1.379E 01	,7.059E+03
4.040E 01	2.097E 01	0 E31E 00	-7.439E 02	-4.000E (2 -3 0000	92	-0 304E 01	1.209E 03	4.403E 01	2,254E-02	1.318E 01	
	2.108E 01	4.50gE 00	-7.448E 02	-T-017E (2 -7 0000	92	-0 414E 01	1.256E 03	5.509E 01	2.820E-02	1.187E 01	6.079E=03
4.130E 01	3.044E 01	# # 100E 00	-0 E74E 102	-40EOE (5 07.003E	112	-1 400E OF	1.257E 03	5.536E 01	2.834E=02	1.184E 01	6.062E=03
4.131E 01	3.055E 01		-8.574E :02					1.362E 03	7.995E 01	4.093E=02	8.929E 00	4.571E=03
4.137E 01	3.123E 01		+8.682E 02					1.363E 03	8.023E 01	4.107E-02	8.896E 00	4.554E-03
4.150E 01	3.255E 01	5.00UE 00	-8.862E 02	-5 0530 (2	04	-1 "EPE 03	1.371E 03	8.203E 01	4.199E-02	8.683E DO	4.445E=03
4.246E 01	2.539E 01	1.8105 01	-9.600E 02	-7 4205 (2 E 176	114	-0.000E 02	1.386E 03	8.549E 01	4.376E-02	1.319E 01	6.755E-03
4.409E 01	3.299E 01	100175 01	-9.298E 02	-1 0505	2 -6 1130E	02	72.292E UZ	1.501E 03 1.699E 03	6.668E 01	3.413Em02	4.778E 01	2.446E-02
4.431E 01	3.399E 01	1 GARE 01	-9.224E 02	-1 ngge (3 -4 6045	116	-4 124C 02		8.663E 01	4.435E+02	1.067E 02	5.462E-02
4.480E 01	3.626E 01	3.755E 01	-9.106E 02	#1 206E C	3 -7 047E	20	-F 200C 02	1.725E 03	8.926E 01	4.569E=02	1.042E 02	5.336E+02
4.481E 01	3.623E 01	3.751E 01	-9.105E 02	-1 200E C	3 . 7 004	112	-5 000F 02	1.785E 03 1.786E 03	9.524E 01	4.876E-02	9.861E 01	5.049E-02
4.625E 01	3.159E 01	3-10%F 01	-8,450E 02	-4.200E (3 -9 300E	0.0	-7 001E 02	1.963E 03	9.515E 01 8.296E 01	4.871E~02	9.850E 01	5.043E-02
4.626E 01	3.155E 01	3.11AF 01	-8.445E 02	-1 833E (3	02	-7 03EE 02	1.964E 03	8.287E 01	4.247E-02	8.202E 01	4.199E-02
4.731E 01	2.817E 01	2.661F fi	-7.786E 02	-1 777E C	3 -0 1085	UE	-1400DE UE	2.094E 03	7.398E 01	4.243E-02	8.190E 01	4.193E=02
4.733E 01	2.809E 01		-7.777E 02					2.097E 03	7.377E 01	3.787E~02	6.988E 01	3.578E-02
4.811E 01	2.565E 01	2.418F 01	-7.180E 02	-1 9485 6	3 -0 B16E	112	-0 4635 02	2.194E 03		3.777E=02	6.960E 01	3.563E=02
4.877E 01	2.219E 01	-2.910E 01	-6.455E 02	-2 07EE C	3 -1 0315	114	-1 0005 02	2.177E 03	6.737E 01 5.828E 01	3.449E-02	6.351E 01	3.251E-02
4.878E 01	2.216E 01	2.216E 01	-6.443E 202	₩2.073E (3 -1 0315	0.3	-1.045E 03	2.278E 03		2.984E=02	5.828E 01	2.984E=02
4.931E 01	2.057E 01	2.057F 01	-5.853E 02	#2.160E (3 -1 neme	7.2	-1.100E 03	2.345E 03	5.820E 01 5.404E 01	2,980E-02	5.820E 01	2.980E+02
5.072E 01	1.566E 01	1.566F 01	-4.514E 02	-2 370F (3 1 1620	73	-1 2175 03	2.522E 03	4.113E 01	2.766E=02 2.106E=02	5.404E 01	2.766E-02
5.282E 01	1.444E 01	1.444F 61	-2.856E 02	-2 637E (3 -1 28UF	73	-1 35/5 03	2.789E 03	3.792E 01	1.941E-02	4.113E 01	2.106E=02
5.332E 01	1.213E 01	1.2135 01	-2.511E 02	-2 696E (3 -1 300F	0.2	-1 TATE 03	2.852E 03	3.185E 01		3.792E 01	1.941E-02
5.407E 01	1.070E 01	1.070F 01	-2.069E 02	=2 786E C	3 -1 346E	0.3	-1 // 30 / 03	2.948E 03	2.811E 01	1.631E-02 1.439E-02	3.185E 01	1.631E-02
5.483E 01	9.262E 00	9.2625 00	-1.682E 02	#2.866E C	3 -1 3808	겠고	-1.495E US	3.046E 03	2.433E 01	1.435E-02	2.811E 01	1.439E=02
5.576E 01	9.017E 00	9.017F 00	-1.258E 02	-2.956E (3 -4 418E	03	-1.634E 03	3.164E 03	2.368E 01	1.212E-02	2.433E 01	1.245E-02
5.626E 01	8.885E 00	A.885E 00	-2.285E 01	⇒2.098E (3 11 435E	, 7.3	-1.550E 05	3,209E 03	2.333E 01		2.368E 01	1.212E-02
5.631E 01	4.950E 00	8.870E 00	-2.033E 01	-3.000E C	3 -1 4375	412	-1.562E 03	3.216E 03	1.300E 01	1.195E-02 6.655E-03	2.333E 01	1.195E-02
5.645E 01	4.950E 00	8.833E 00	-1.456E 01	+3.013E €	3 _1 LLOE	73	-1.571E 03	3.234E 03	1.300E 01		2.330E 01	1.193E=02
5.653E 01	8.812E 00	8.812E 00	-1.102E 01	-3.010F	3 -1 4445	03	#1.57EE 03	3.245E 03	2.314E 01	6.655E#03	2.320E 01 2.314E 01	1.188E=02
5.681E 01	8.737E 00	8.737E 00	4.407F=01	-3.041F C	3 -1.4535	0.3	-1.588E 03	3.280E 03	2.295E 01	1.185E-02 1.175E-02		1.185E=02
5.704E 01	8.757E 00	8.757E 00	8.951F 00	-3.05AF	3 -1 4405	υJ 73	-1.599E 03	3.309E 03	2.300E 01	1.175E=02	2.295E 01	1.175E-02
5.776E 01	8.820E 00	8.820E 00		-3.110F	3 -1 4785	η3 Λ3	-1.634E 03	3.402E 03	2.316E 01	1.186E-02	2.300E 01	1.177E=02
5.878E 01	5.250E 00	5.250E 00		+3.176F C	3 -1 5015	0.3	-1.675E 03	3.532E 03	1.379E 01	7.059E-03	2.316E 01 1.379E 01	1.186E+02
6.079E 01	6.225E 00	6.225E 00		~3.276F (3 m1.535F	63	-1.741E 03	3.790E 03	1.635E 01	8.370E-03		7.059E=03
6.221E 01	1.236E 01	1.236E 01		+3. 340F (3 -1 5555	0.3	-1.794E 03	3.972E 03	_		1.635E 01	8.370E=03
		71-10F 01	O TO VALL OI	COUTE (ųσ	-11124E 03	3.714E 03	3.245E 01	1.661E~02	3.245E 01	1.661E=02

READING	= (0071	BLOCK	= 75	TIME	= 174.	,938	MACH	6.0	PT:	747	749	ΤŢ	= :	2940.
x		OD:	RAG	CDF	RAG	CF		нс							
4.040E	01	1.2	81E 02	1.28	31E 02	2.400	-03	4,535	E-02						
4.041E			71E-01		3E 02	2.646		3,432							
4.1300	01		71E 01		0E 02	2.7698		4.111							
4.131E	01	1.7	65E-01	1.45	2E 02	2.5746	: +03	4.359	E-02						
4.137E	01	1.1	17E 00	1.46	3E 02	2.550E	~03	4.438	E-02						
4.150E	01	2.1	29E 00	1.48	5E 02	2.564E	-03	4,674	E-02						
4.246E		1.5	88E 01		3E 02	2.624E		4.983							
4.409E			51E 01		BE 02	2.683E		6,536							
4.431E			35E 00		9E 02	2.864E		6.115							
4,480E			46E 00		0E 02	2.859E		6.108							
4.481E	_		16E-01		2E 02	2.872E		6.076							
4.625E			62E 01 94E-01		18E 02	3,008E		5.405							
4.626E 4.731E			59E 01		5E 02	2.775E		5.414							
4.733E			36E-01		9E 02	2.746E		5.355							
4.811E			35E 01		2E 02	2.708		5.060							
4.8778			60E 00		6E 02	2.921		4.442							
4.878E			81E-01		1E 02	2.7018		4.770							
4.931E			39E 00	2.61	4E 02	2.665		4.539							
5.072E	01	1.5	55E 01		OE 02	2.610E		3,746	E-02						
5.282E			01E Q1		OE 02	2.5668		3,425	E-02						
5.332E			55E 00		5E 02	2.7335		2.868							
5.407E			76E 00		1E 02	2.635		2,683							
5.483E			00E 00		5E 02	2.5908		2.434							
5.576E	-		36E 00		9E 02	2.536		2.393							
5.626E			97E 00		3E 02	2.5546		2.207							
5.631E			48E+01		6E 02	2.7488		1.756							
5.645E 5.653E			47E-01 74E-01		SE 02	2.559E		1.848							
5.6818			71E 00		1E 02	2.750		2.044							
5.704E			78E 00		SE 02	2.7476		2.045							
5.776E			03E 00		2E 02	2.7416		2.047							
5.878E			75E 00		1E 02	2.754E		1.435							
6.079E	Ø1		21E 01		3E 02	2.340E		1.809							
6.221E		8.5	66E 00	3.62	9E 02	2,5869	-03	2.684	E-02						
6.468E	01	1.4	56E 01		5E 02	3,0568	-03	2.559							
6.505E			58E 00		6E 02	3.225		2,290							
6,509E			93E+01		18E 02	3,298E		2.342							
6.529E			59E 00		0E 02	3.296		2.336							
6.695E			53E 00		06E 02	3.162		1,731							
6.762E	_		69E 00		10E 02	3.135E		1.590							
6.839E 6.911E			89E 00 14E 00		7E 02	3.070E		1.261							
6.972E			06E 00		9E 02	2.973		8.391							
7.067E			05E 00		SE 02	2.865		5.013							
7.110E	_		99E-01		5E 02	2.856		4.830							
7,263E			01E 00		9E 02	2.871		5.276							
7.278E	01		18E-01		2E 02	2.858		4.969							
7.353E	01		98E 00		SE 02	2.763		3.170							
7.354E	01	5.0	34E-03	4 - 11	SE 02	2.762	E-03	3,159	E-03						
7.486E	01	6.8	46E-01	4.12	2E 02	2.781E	E-03	3.564	E∽03						
7.771E			48E 00		5E 02	2,763		3.482							
8.161E			35E 00		0E 02	2.750E		3,535	_						
ω 8.442E 5 8.728E			51E-01		7E 02	2,699E		2.929							
			93E-01		0E 02	2.7278		3.547							
8.729E	Ul	0.0	បម	4 • 16	0E 02	2.7276	<u>-</u> ≁03	3,548	E-03						

RAMJET PERFORMANCE

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9	ENGINE PERFORMANCE	INLET	
ආ	CALCULATED THRUST	ANGLE OF ATTACK	
	REGENERATIVE-COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	INLET PROCESS EFFICIENCY - SUBSONIC 0.8973 KINETIC ENERGY EFFICIENCY - SUPERSONIC 0.9125 KINETIC ENERGY EFFICIENCY - SUBSONIC 0.8774 ENTHALPY AT PO - SUPERSONIC	
	MOMENTUM AND FORCES	COMBUSTOR	
	INLET FRICTION DRAG	FUEL-AIR RATIO	,748
	STATIONS	FUEL INJECTORS	
	NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A	

t = 193.84 sec.

SUMMARY REPORT

O	P	т	н		GAMMA	MOLWT	SONV	VACH	VFi	s	W/A	W	A/AC	МОМТМ	©.	TVAC	Dut	ETAC
	WIND TUNNEL	1_	0 5						,		***	"	Ar no	HOPTP	· ·	TANC	LLit	ETAL
	+0.000 743.499 -0.000 -0.377		643.9(770)	1,2960	28.898	2548							_				
	-0.000 -0.377 SPIKE TIP NS	289	#35./€ 0 5	93)	1.3486	28.897	967	6,031	5832	1.819	0.10583	25.254	0.9317	4667	9.591	184.8		
	0.600 18.175			770)	1.2960	28.897	2548											
	-0.600 16,509	2849	624.8(751)	1.2980	28.897	2522	0.387	977	2.074	0.10583	25.254	0.9317	4706	1,606	186-4		
	WIND TUNNEL	3	0 0											11.00		20017		
	0.000 743.499 0.000 :0.383		643.91	770)	1,2960	28.898	2548	ما هلا م										
	SPIKE TIP NS	390 4	0 0	941	1.0480	28.897	969	6,016	5830	1.819	0.10691	25.512	0.9317	4714	9.686	184.8		
	0.600 18.175			770)	1.2960	28.897	2548											
	0.600 16.470		624.4(751)	1.2980	28.897	2522	0.392	986	2.074	0.10691	25.512	0.9317	4714	1.642	184.A		
	INLET THROAT	5	0 4													**5		
	40.400 192.600 40.400 17.880		265.71	745) 305)	1.2987	28.897	2514	0 100								_		
	INLET UPNRSK	6	0 3	3331	1,5450	20.091	1910	2,194	4202	1.903	0.88544	25.254	0.1114	3808	57,820	150.8		
	40.400 192.600	2828	618.51	745)	1.2987	28.897	2514											
	40.400 15.236		248.6(378)	1.3472	28.897	1879	2,290	4303	1.903	0.80495	25.254	0.1225	3855	53,823	152.7		
	INLET DNNRSK 40.400 107.876	7 2600	0 4															
	40.400 90.592	2716	618.5(7401	1.3002	28.897	2514	o Kon	100.		5 504BE	åe	0.1225	-4		'_		
	COMBUSTOR 0	8	1 21	* 4*	110054	201097	2407	0.023	127	1.943	0.80435	25.254	0.1225	3855	16,145	152.7		
	40.410 162.264		618.2(766)	1.3014	27.563	2556											
	40.410 12.727 COMBUSTOR 0		236.3(386)	1,3505	27.563	1904	2,295	4371	1.988	0.88869	25.350	0.1114	3807	60.369	150.2	0.12	0.07
	COMBUSTOR 0 41.300 127.825	2710	2 21	7751	. Bock	06 801	0500											
	41.300 16.496			4471	1.3443	26.391	2038	1 903	8060	0 067	0.00369	25 270	0.1111	* 601	EG #44		0 '04	
	COMBUSTOR 0	10	3 21					X , >30	4002	2.001	0102705	231435	0.1111	2001	56,411	144.7	0.24	0.04
	41.310 132.939		619.8(7621	1.3074	26.346	2565											
	41.310 16.539 COMBUSTOR 0		290.7(434)	1.3469	26.346	2014	2.015	405A	2.059	0.89342	25.439	0.1112	3680	56.349	144.7	0.24	0.01
	41.375 132.249	2668	4 21	7591	1 3077	26 - Xun	2542			r								
	41.375 16.814	1600	293.8(435)	1.3468	26.340	2017	2 802	4637	2.050	A . BQ&77	25.410	0.1110	2670	E6 174		0.00	
	COMPOSIUM 0	12	5 21						4007	2,000	0465411	201407	0.1110	3010	56.131	144.3	0.24	ប•្ចប់ប
	41.500 130.638	2656	618.6(758)	1.3078	26.339	2561											
	41.500 18.447 COMBUSTOR 0	1641	306.2(6 21	448)	1.3448	26.339	2041	1.937	3954	2.059	0.89498	25.439	0.1110	3650	54.990	143.5	0.24	0.00
	42.460 120.320			751)	1.3086	26.339	2550	•										
	42.460 23.739		344.5(486)	1.3390	26.338	2115	1.727	3653	2.863	0.88619	25.439	0.1121	3570	50.309	180 %	0 24	0.00
	COMBUSTOR 0	14	7 4								(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	200,00	*******	2370	00,009	140.2	0.24	0.00
	44.095 95.713 44.095 48.406	3085	595.2(887)	1.2871	26.873	2710											
		15	8 2	7467	1.3019	26.874	2522	1.065	2685	2.116	0.85573	25.439	0.1161	3562	35.710	140.0	0.24	0.42
	44.310 95.367	3086	592.8(888)	1.2870	26.882	2710			ř.								
	44.310 49.511	2659	453.8(752)	1.3012	26.883	2529	1.043	2637	2.116	0.85424	25.439	0.1163	3559	35,008	139.9	0.24	n.43
	COMBUSTOR 0	16	9 2													10,4,	4 24	0.40
	44.800 94.440 44.800 52.028	2671	586.9(7561	1.2880	26.873	2700	0 00.	۰				_ *					
	COMBUSTOR 0	17	10 2	1001	1.3009	20.073	2536	0.391	2513	2.114	0.85092	25.439	0.1167	3542	33.226	139.2	0.24	0.42
	44.810 94.417	3059	586.8(879)	1,2880	26.872	2700	•										
	44.810 51.972	2670	460.5(755)	1.3010	26.873	2535	0.992	2514	2.114	0.85092	25.439	0.1167	3542	33,245	139.2	0.24	0.42
	COMBOSION U	18	11 9						·	•					,			
	46.250 43.765	2231	588.7(446.8(6881	1.3230	23.929	2680	1 076	2665	A 250	0.000	OE / 7=	0.1238			. = -		
				-007	**OE90	EU 9 7 2 7	£410	1.0/0	400 5	2.258	0.80957	25.677	0.1238	3515	33,527	136.9	0.54	0.10

READING	= 0071	BLOCK	= 96	TIME :	= 193,8	38 MACI	H 6.0	D PT :	= 743.	499	TT = 291	2.6						i
	ρ	T	н		GAMMA	MOLWT	SONV	мАСН	VEI	s	W/A	W	A/AC	MOMTM	0	IVAC	PHI	ETAC
COMBUST			12 2															
46,260			588.6										4 4 6 7 7		77 506			
46,260					1,3230	23.930	2476	1.077	266 ₀	2.258	ი.80907	25.677	0.1239	3515	33.526	136.9	0.54	0.10
COMBUST			13 4		4 3050	0/1 079	0200											
47.310 47.310			574.9						2970	2 268	0.75281	25.677	0.1339	3501	33.636	430 E	0 '64	0.15
COMBUST		21			TAOPIC	244003	24/3	1.102	2010	2.200	0415201	23+011	041002	0001	,	10,42	0.54	04.20
47,335			574.6		1.3050	24.040	2709											
47,335		7 2242							2877	2.268	0.75197	25.677	0.1333	3582	33,625	139.5	0.54	0.15
COMBUST			15 4					•										
48.110			564.9								_	- 						
48.110				(717)	1.3165	24.173	2511	1,180	2962	2.282	0.70147	25.677	0.1429	3654	32.286	142.3	0.54	0.20
COMBUST			16 6			00 004	^~~											
48 .77 5 48 . 775			567.9						311/	0 1101	0.65159	25.002	n 1559	7719	31.557	143 4	0 03	0 11
COMBUST		24		(0037	140002	22,004	2490	1,247	2110	2.461	0.00100	204702	0.1002	3110	31,337	74940	0.03	0***
48.785			567.8	(883)	1.3118	22.006	2774											
	30.38							1.249	3118	2.421	0.65075	25.902	0.1554	3720	31,536	143.6	0.83	0.11
COMBUST	'aR ı	25	18 4							7								
49.315	73.70	5 2690	562.2	(916)	1,3073	22.099	2813					•						
49.315	28.12	2133	354.1		1.3266	22.099	2523	1,279	3227	2.434	0.60860	25.902	0.1662	3795	30,519	146.5	0.83	0.14
COMBUST		26	19 4			40 400				-								
50 .7 25 50 .7 25	22.64	7 50/0	549.0	(784) (738)	1.2782	22+295	2886	1 370	3500	a #50	0.51870	25. Qn2	0 1950	3068	28,413	153 0	A 03	0 21
COMBUST			20 5		1,0200	25.45.90	اددم	1,070	3525	2.400	0+21010	23.702	0.1930	3900	20.713	100.2	V.05	0.21
52.825			532.8		1.2844	22.589	2988											
52.825	18.56	2414	246.8	(804)	1.3099	22.590	2638	1,434	3783	2.492	0.42513	25.902	0.2379	4176	24.991	161.2	0.83	0.30
COMBUST	OR (28	21 4					1										
53,325			529,4							_			_					,
53.325	18,22	7 2495	248.3	(832)	1,3060	22.677	2673	1,423	3863	2.501	0.40776	25.902	0.2480	4220	24.100	162.9	0.83	0.33
COMBUST		3 29		/44731	4 0777	00 770	7070											
54.075 54.075			524.5						3000	2 506	0.38437	25 002	0.2631	#2B0	23,466	165 7	r 0 7	A 36
COMBUST	nR :	ነ ፍጥጋጥ በ ሻቡ	23 3		1,0035	220133	2000	1,712	J748	2.000	0+50451	234902	0.2031	4200	20,400	103.3	0.00	4.00
54.835			519.9		1.2765	22.762	3038											
54.835									4064	2,508	0.36348	25.902	0.2782	4335	22,954	167.4	0.83	0.36
COMBUST	OR	0 31	24 4					1										
55,760	54.69	3 3339	514.7	(1151)	1,2749	22.802	3047		٠									
55.760	13.41	8 2432	163.5	(807)	1.3065	22.806	2632	1,593	4192	₂ 2.511	0.34128	25.902	0.2963	4393	22.233	169.6	0.83	0.37
COMBUST 56.260	OK 12 1/2	32	25 5		1 2575	07 101	*461	1		•								
56.260	12.60	U 3/1/ U 2861	512.1	1 6607	1.2863	23,104	2000	1 400	8150	2 556	0.27494	25.902	0.3679	nsis	17.767	176 1	0 03	ń Jig
COMBUST	'oR	33	26 5		105000	201170	2007	7,400	4100	24000	0461727	234702	0,0070	4000	11,101	1.2+1	U. 00	0,45
56.315	-		511.9		1.2715	22.868	3066											
56.315									4500	2,524	0.27407	25.902	0.3690	4538	19.166	175.2	0.83	0.39
COMBUST	OR	0 34	27 3															
56.455			511.2															
56.455					1.3084	22.878	2586	1.746	4514	2.524	0.27210	25.902	0.3717	4545	19.088	175.5	0.83	0.39
COMBUST 56.535			28 6		1 0550	03 450	***											
56.535	12,15	6 2803	510.8 153.3	(938)	1.2887	23.173	2784	1 520	4234	2.552	0.27515	25,902	0.3675	4550	18.088	175 7	n pr	0 48
COMBUST	roR	0 36	29 3		******	201110	2,07		72311	2.002	11+51010	20+702	3.0013	4000	10.000	113.7	0.00	U+70
56.815			509.6		1.2565	23.138	3147	•										
56.815	11,70								4296	2.548	0.27424	25.902	0.3688	4564	18.309	176.2	0.83	0.48
COMBUST	oR	0 37	30 3															
57.041	45.75	5 3642	508.5	(1263)	1.2580	23.115	3139			_	- 6-	_			_			
57.041	11,32	5 2693	130.3	(898)	1,2931	23.127	2736	1,590	4350	2.545	0.27382	25.902	0.3693	4574	18.512	176.6	0.83	0.47

GAMMA POLWT SONV NACH VEL AZAC MOMTM Q · IVAC PHI ETAC **ω** COMBUSTOR 0 38 31 **~** 57.765 48.028 3554 505.4(1230) 1.2630 23.035 3113 Nº 57.765 10.125 2523 100.1(836) 1.3002 23.043 2660 1.693 4503 2.535 0.26947 25.902 0.3753 4598 18.858 177.5 0.83 0.44 COMBUSTOR 0 39 32 8 58.785 87.073 2860 501.7(975) 1.2976 22.389 2871 58,785 5.175 1429 -19.0(457) 1.3539 22.389 2073 2.462 5104 2.430 0.26776 25.902 0.3777 4610 21.239 178.0 0.83 0.24 COMBUSTOR 0 40 33 6 50,542 3515 495,2(1215) 1.2649 23.021 3099 60.795 10.050 2458 82.0(812) 1.3027 23.028 2629 1.729 4547 2.527 0.27708 25.902 0.3650 4600 19.579 177.6 0.83 0.44 60,795 COMBUSTOR 0 41 34 62.215 46.830 3731 490.4(1295) 1.2523 23.250 3161 12.312 2809 118.8(939) 1.2873 23.265 2780 1.551 4312 2.546 0.28459 25.902 0.3553 4592 19.073 177,3 0.83 0.51 62,215 COMBUSTOR 0 42 35 5 64.679 38.840 4182 481.3(1464) 1.2206 23.748 3269 64,679 17.582 3605 223.5(1235) 1.2483 23.798 3066 1,171 3591 2.582 0.26976 25.902 0.3749 4579 15.055 176.8 0.83 0.67 COMBUSTOR 0 43 36 4 35.647 4254 479.7(1491) 1.2141 23.832 3283 65,055 18.550 3780 261.2(1302) 1.2379 23.886 3121 1.059 3306 2.592 0.25078 25.902 0.4032 4578 12.886 176.7 0.83 0.70 65.055 COMBUSTOR REGEN 44 37 21 65,055 35.647 4507 614.8(1593) 1.1975 23.762 3360 65,055 30,478 4396 556.5(1548) 1.2028 23.790 3324 0,514 1708 2.623 0.25078 25.902 0.4032 4523 6.656 174.6 0.83 0.70 NOZZLE AE 45 38 5 87,291 35.647 4254 479.7(1458) 1.2141 23.852 3282 1.009 2013 -424.6(638) 1.3089 23.915 2340 2.874 6727 2.592 0.05221 25.902 1.9371 5916 5.458 228.4 0.83 0.70 87,291 NOZŽLE PO 46 39 5 35.647 4254 479.7(1458) 1.2141 23.832 3282 87,291 87.291 0.377 1586 -571.2(491) 1.3292 23.915 2094 3.464 7252 2.592 0.02668 25.902 3.7904 6204 3.007 239.5 0.83 0.70 NOZZLE AE REGEN 47 40 87,291 35.647 4507 614.8(1593) 1.1975 23.762 3360 87,291 1.086 2233 -346.3(716) 1.3001 23.915 2456 2.823 6935 2.623 0.05221 25.902 1.9371 6122 5.626 236.3 0.83 0.70 NOZZLE PO REGEN 48 41 5 87,291 35.647 4507 614.8(1593) 1.1975 23.762 3360 87.291 0.377 1738 -520.0(542) 1.3214 23.915 2185 3.449 7536 2.623 0.02531 25.902 3.9952 6453 2.964 249.1 0.83 0.70 FICTIVE COMBUSTR 68 61 192,600 5040 479,7(1790) 1,1774 24,716 3455 65,055 65,055 0.377 1427-1020.4(426) 1.3276 25.034 1939 4.467 8664 2.469 0.03711 25.902 2.7254 7238 4.996 279.5 0.83 1.00 FICTIVE NOZZLE 69 62 25,158 4191 452,2(1465) 1,2144 23,834 3258 87,291 87,291 1.187 2227 -348.2(714) 1.3003 23.915 2454 2.579 6329 2.614 0.05221 25.902 1.9371 5684 5.135 219.4 0.83 0.70

			•		<u>.</u> .				B 70 (000		0.004000	M. AM /DTA
.~	XABS	P=18	P⇒Op	PDA	χυρ	Q=1B	Q=0B	CAMALL	P-IE/PSO	019\81-4	P-08/PS0	P-OB/PTO
1	6.505E 01	1.837E 01	1.801E 01	1.5478 0	12 -4.036E 03	-2.172E	03 -1.8658 03	4.337E U3	4.895E 01	2.475E-02	4./99E 01	2.426E-02
22	6.509E 01	1.837E 01	1.80/E 01	1.5476 0	2 -4.041E 03	-2.174E	03 -1.867E 03	4.342E 03	4.895E 01	2.475E=02	4.813E 01	2.433E-02
100	6.529E 01	1.748F 01	1.632E 01				03 -1.877E 03	4.368E 03	4.6578 01	2.3546-02	4.882E 01	2.4682-02
	6-695E 01	1.006E 01	8.310E 00				03 -1.954E 03	4.583E 03	2.680E 01	1.355E=02	2.214E 01	1.119E-02
			8.025E 00				03 -1.982E 03	4.6658 03	1.987E 01	1.005E-02	2.138E 01	1.0816-02
	6.762E 01	7.459E, 00								6.020L=03	1.652E 01	8.351E-03
	6.839E 01	4.470E 00	6.201E 00				03 -2.0158 03	4.760E 03	1.191E 01			
	6.911F OL	3.515E 00	4.495E 00				03 -2.047E 03	4.848£ 03	9.363E 00	4.733E=03	1.197E 01	6.054E-03
	6.972E OL	2.705E, 00	3.760E 00	8.537€ (12 -4.401E 03	-2.3278	03 -2.074E 03	4.922E 03	7.2068 00	3.643E∞03	1-005E 01	5.064E-03
	7.067E 01	1.931E 00	2.615E 00	9.4021 0	2 -4.449E 03	-2.340E	03 -2.108E 03	5.036k 03	5.143E 00	2.600E=03	6.966E 00	3.5226-03
	7.110E 01	1.580E 00	2.441E 00				03 -2.1218 03	5.086£ 03	4.209E 00	2.1286-03	6.502E 00	3.287E=03
	7.263E 01	1.598E 00	1.820E 00				03 -2.158E 03	5.273E 03	4.258E 00	2.1526-03	4.849E 00	2.451E=03
							03 -2.1618 03	5.290E 03	4.262E 00	2.155E=03	4.242E 00	2.1456-03
	7.278E 01	1,600E 00	1.592E 00									
	7.353E 01	1.504E 00	4.550E-01				03 -2.178E 03	5.374E 03	4.008E 00	5.056F-03	1.212E 00	6.128E=04
	7.354E 01	1.504E 00	4.489E=01				03 -2.178E 03	5.375E 03	4.007E 00	2.026E=03	1.196E 00	6.046E-04
	7.486E 01	1.335E 00	0.000	1.1378 (3 -4.541E 03	-2.3776	03 =2.214E 03	5.4276 03	3.556E 00	1.798£-03	0.000	0.000
	7.771E 01	1.890E 00	0.000	1.202E (3 -4.553E 03	#2.395E	03 -2.,1382 03	5.525E 03	5.035E 00	2.545E-03	0.000	0.000
	8.461E 01	1.335E 00	0.000	1.2716	3 -42552F 03	-2.414F	03 -2.138E 03	5.630E 03	3.556E 00	1.798E=03	0.000	0.00.0
	8.442E 01	1.010E 00	0.000				03 -2.138E 03	5.684E 03	2.691E 00	1.360E-03	0.000	0.000
								5.707E 03	3.943E 00	1.993E=03	0.000	0.000
	8.728E 01	1.480E 00	0.000				03 -2.138E 03					
	8.729E 01	1.481E 00	0.000	1.327E (15 =4,597E 03	-2.459E	03 -2.138E 03	5.707E 03	3,945E 00	1.995E-03	0.000	0.000

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XABS	P=18	P=0b	PDA	x00	Q=IB	Q - Q8	CANALL	P-18/PS0	B 18 /MTA	004-4000	D 00 (0*0
6.981E=01	1.040E 00	0.000	-4.405E-01		0.000	0.000	2.470E-02	2.771E 00	P#18/PT0 1.401E=03	P=G5/PS0	P=0B/PT0
1.836E 01	1.040£ 00	0.000	-3.463E 01		0.000	0.000	1.434E 02	2.771E 00	1.401E-03	0.000	0.000
3.070E 01	2.970E 00	0.000	-1.972E 02		0.000	0.000	5.9536 02	7.912F 00	4.000E-03	0.000	0.000
3.508E 01	3.824E 00	0.000	-4.173E 02		0.000	0.000	6.804E 02	1.019E 01	5,150E+03	0.000	0.000
3.519E 01	4.141E 00		9-4-816E 02		0.000	0.000	6.854E 02	1.103E 01	5.5/7E=03	1.478E 01	7.47QE-03
3.520E 01 3.555E 01	4.158E 00	5.517E 0	-4.817E 02	0.000	0.000	0.000	6.857E 02	1.108E 01	5.600E-03	1-470E 01	7.430E-03
3.586E 01	5.145E 00 5.009E 00	3.144F 0	-4.944E 02	0.000	0.000	0.000	7.209E 02	1.371E 01	6.929E=03	1.011E 01	5.110E-03
3.606E 01	4.925E 00	3-406E 0) -5.156E 02) -5.292E 02	-5 444E 02	: ~5.420E (0.000	7.529E 02	1.334E 01	6.746E-03	5.994E 00	3.030E-03
3.648E 01	4.129E 00	5.895F 0) -5.482E 02	-5.401E 02	: *D•*61E (0.000	7.129E 02	1.312E 01	6.633E=03	9.075E 00	4.588E-03
3.701E 01	5.115E 00	9.035E 0	-5.691E 02	-5-968F 02	-5.7015C	2 -1.769E 01	8.164E 02 8.726E 02	1.100E 01	5.561E=03	1.570E 01	7.939E=03
3.732E 01	4.857E 00	1.090F 0	-5.803E 02	⇒9.136E 02	-5.900F	2 -2.361E 01	9.063E 02	1.363E 01 1.294E 01	6.869E=03 6.542E=03	2.407E 01 2.904E 01	1.2176-02
3.803F 01	4.280E 00	1.451E 0	i -5.941E 02	-6.523E 02	-6.157F C	2 =3.658F 01	9.834E 02	1 140E 01	5.764E=03	3.866E 01	1,468E=02 1,955E=02
3-834E 01	8.016E 00	1.612E 0	L -5. 990E 02	#6.704E 02	-6.281E 0	2 94.231F 01	1.018E 03	2.136E 01	1.080E-02	4.296E 01	2.172E=02
3.875E 01	1.282£ 01	1.766E 0	l =6.203E 02	-6.949E 02	-6.453E 0	2 -4.965F 01	1.064E 03	3.417E 01	1.727E-02	4.703E 01	2.378E=02
3-881E 01	1.359E 01	1.790E 0	1 -6.242E 02	-6.990E 02	-6.482E 0	2 -5.082F 01	1.072E 03	3,621E 01	1.831E-02	4.769E 01	2.411E-02
3.901E 01 3.932E 01	1.591E 01 1.870E 01	1.774E U	-6.353E 02	-7.115E 02	-6.571E C	2 -5.434E 01	1.094E 03	4.238E 01	2.143E=02	4.725E 01	2.389E=02
3.950E 01	2.025E 01	1 2115 0	L =0.503E 02	-7.324€ 02	-6.724E 0	2 +5.998E 01	1.130E 03	4.981E 01	2.518E=02	4.655E 01	2.354E-02
3.981E 01	1.805E 01	5-2756 0	1 ******** UK	#/#445E 08	-6.814E C	2 -6.310E 01	1.150E 03	5.395E 01	2.727E=02	3.493E 01	1.766E=02
4.000E 01	1.676E 01	5.047F 0) =0.7/25 V2	-7 910E 02	-0.485E (2 -6.860E 01 2 -7.178E 01	1.187E 03	4.809E 01	2.431E-02	1.405E 01	7.104E-03
4.040E 01	2.003E 01	4-555F 0	7 -7 -1436 UZ	-14010E 05	-7 331E 0	2 -7.1/8E 01	1.2098 03	4.464E 01	2.2576-02	1.345E 01	6.798E-03
4.041E 01	.2.011E 01	4.543E 0	7.523F 02	-8-131F 02	. 576334E (2 -7.906E 01	1.256E 03 1.257E 03	5.336E 01	2.6975-02	1.214E 01	6.135E-03
4.131E 01	2.747E 01	3.436E 0	-8.556t 02	99.016E 02	97.948E 0	2 -1.068E 02	1.363E 03	5.357E 01 7.318E 01	2.708E=02	1.210E 01	6.118E-03
4.137E 01	2.800E 01	3.356E 0) -8.639E 02	~9.092E 02	-7.995F 0	2 91.097F 02	1.371E 03	7.460E 01	3.700E=02 3.771E=02	9.154E 00 8.941E 00	4.628E-03
4-150E 01	2.902E 01	3.956E 0) =8.801E 02	~9.242E 02	' -8.089E ù	2 -1.154E 02	1.386E 03	7.732E 01	3.909E=02	1.054E 01	4.520E-03 5.328E-03
4.246E 01	2.085E 01	8.558E 0) - 9.613E 02	→1.057E 03	-8.852E 0	2 -1.716E 02	1.501E 03	5.554E 01	2.808E-02	2.280E 01	1.153E-02
4.409E 01	2.504E 01	1.639E 0	L =1.015E 03	-1.323E 03	-1.024E 0	3 -2.994F 02	1.699E 03	6.671E 01	3.373E=02	4.367E 01	2082-02
4.431E 01 4.480E 01	2.559E 01 2.685E 01	1.725E 0	-1.021E 03	-1.360E 03	-1.042E 0	3 -3.1818 02	1.725E 03	6.818E 01	3.447E-02	4.596E 01	2.353E=02
4.481E 01	2.687E 01	1 92/15 0	=1.034E 03	≈1.447E 03	01.085E 0	3 -3.622E 02	1.785E 03	7.153E 01	3.616E-02	5.116E 01	2.586E=02
4.625E 01	2.920E 01	2.49AF 0	1 =1.033E 03	-1 700E 03	=1.086E U	3 -3.631F 02 3 -5.004E 02	1.786E U3	7.157E 01	3.618E-02	5.126E 01	2.591E-02
4.626E 01	2.922E 01	2.502F 0	=1.023E 03	-1.700E 03	-1 2085 A	3 -5.013E 02	1.953E 03	7.780E 01	3.933E-02	6.654E 01	3.364E-02
4.731E 01	3.092E 01	2.920E 0	-9-674E 02	#1.897E 03	-1.202F 0	3 -6.050£ 02	1.964E 03 2.094E 03	7.784€ 01 8.238E 01	3.935E=02	6.665E 01	3.3696-02
4.733E 01	3.113E 01	2.930E 0	-9.664E 02	=1.902E 03	-1.294F 0	3 -6-0758 02	2.097E 03	8.292E 01	4.165E-02 4.192E-02	7.779E 01 7.806E 01	3.933E-02
4.611E 01	3.745E 01	6.750E 0	9.061£ 02	~2.036E 03	-1.354E 0	3 =6.820F 02	2.194E 03	9.977E 01	5.044E=02	7.294E 01	3.946E>02 3.687E>02
4.877E 01	2.573E 01	2.573E 0	-8.254E 02	-2.147E 03	-1.404F 0	3 -7.424F 02	2.277E 03	6.855E 01	3.4658-02	6.855E 01	3.465E-02
4-878E 01	2.571E 01	2.571E U	-8.241E 02	~2.148E 03	-1.405E 0	3 =7.433F 02	2.278E 03	6.846E 01	3.462E=02	6.848E 01	3.462E=02
4.931E 01 5.072E 01	2.439E 01	2.439E 0	-7.549E 02	#2.233E 03	-1.444E 0	3 =7.890F 02	2.345E 03	6.498E 01	3.285E-02	6.498E 01	3.285E-02
5.282E 01	1.973E 01 2.355E 01	2 7565 0	-5.918E 02	-2,451E 03	-1.543E 0	3 -9.073E 02	2.522E 03	5.256E 01	2.657E-02	5.256E 01	2.6576-02
5.332E 01	1.990E 01	1 9905 0	-2 0705 02	-2.754E 03	-1.680E 0	3 -1.084E 03	2.789E 03	6.274E 01	3.172E-02	6.274E 01	3.1726-02
5.407E 01	1.790E 01	1.790E 0	. =2.9fVC VC	-2 047E 07	-1.710E 0	3 =1.127E 03 3 =1.188E 03	2.852E 03	5.30SE 01	2.680E-0S	5.302E 01	2.680E=0Z
5.483E 01	1.586E 01	1.58eF 0	-1.584F 02	-3.047E 03	=1 = 755E U	3 -1.188E 03	2.948E 03	4.768E 01	2.410E=02	4.768E 01	2.410E-02
5.576E 01	1.418E 01	1.418E 0	=8.875F 01	-3.168F 03	-1 - R// RE A	3 -1.320E 03	3.046E 03	4.226E 01	2.1366-02	4.226E 01	2.136E-05
5.626E 01	1.327€ 01	1.327E 0	6.518E 01	+3.227F 03	#1.870F 0	3 -1.357E 03	3.164E 03 3.209E 03	3.778E 01	1.9108-02	3.778E 01	1.910E-02
5.631E 01	7.350E 00	1.317E 0	6.894E 01	-3.234E 03	91.872F 0	3 -1.361E 03	3.216E 03	3.536E 01	1.787E=02 9.899E=03	5.536E 01	1.787E-02
5.645E 01	7.350E 00	1.292E 0	7.744E 01	-3.249E 03	-1.877E 0	3 -1.372E 03	3.234E 03	1.958E 01	9.899E=03	3.509E 01#	
5.653E 01	1.277E 01	1.277E 0	. 8.260E UI	-3.257E 03	-1.880E 0	3 -1.377F 03	3.245E U3	3.402E 01	1.720E=02	3.402E 01	1.740E#02 1.720E#02
5.681E 01	1.559E 01	1.550E 01	. 9.894E 01	-3.287E 03	-1.890E 0	3 -1.397E 03	3.280E 03	3.267E 01	1.652E-02	3.267E 01	1.652E-02
5.704E 01	1.136E 01	1.136E 01	1.104E 02	-3.311E 03	-1.898E 0	3 -1.413F 03	3.309E 03	3.026E 01	1.5306-02	3.026E 01	1.530E-02
5.776E 01 5.878E 01	8.460E 00 5.025E 00	8.460E 00	1.373E 02	=3.384E 03	-1.921E 0	3 -1.465E 03	3.402E 03	2.254E 01	1.139E~02	2.254E 01	1.1396-02
6.079E 01	1.002E 01	5.025E 00	1.529E 02	+5.4/5E 03	-1.951E 0	3 -1.524E 03	3.532E 03	1.339E 01	6.768E=03	1.339E 01	6.768E=03
6.221E 01	1.434E 01	1.434E 01	1 5/175 02	-1 7505 03	=2.004£ 0	3 -1.636E 03	3.790E 03	2.671E 01	1.350E+02	2.671E 01	1.350E-02
6.468E 01	1.753E 01	1.753E 0	1.5476 02	-3.100E 03	₩2.04/E 0	3 -1.713E 03	3.972E 03	3.821E 01	1.932E=02	3.821E 01	1.932E-02
	V1	, V	********	-247705 03	-c + 12cF 0	3 -1.844E 03	4.289E 03	4.670E 01	2.361E-02	4.670E 01	2.361E-02

IVAC PHI ETAC GAMMA MOLWT SONV MACH VEL S AZAC MOMTM Q W/A 0 38 31 6 K COMBUSTUR N 58.785 81.983 2797 546.8(910) 1.3011 23.329 2785 **58.785** 5.025 1402 63.0(429) 1.3563 23.330 2013 2.444 4920 2.342 0.26627 25.758 0.3//7 4425 20.559 171.8 0.66 0.20 0 39 32 6 COMBUSTOR 60.795 47.202 3467 540.4(1144) 1.2678 24.000 3018 60.795 10.025 2456 163.2(777) 1.3039 24.006 2575 1.687 4344 2.439 0.27553 25.758 0.3650 4415 18.605 171.4 0.66 0.44 COMBUSTOR 0 40 33 5 41.446 3865 535.8(1285) 1.2438 24.432 3128 62.215 62.215 14.344 3108 235./(1003) 1.2750 24.456 2838 1.365 3875 2.471 0.28500 25.758 0.3553 4407 17.041 171.1 0.66 0.60 COMBUSTOR 0 41 34 4 64.679 37.028 4089 526.6(1365) 1.2273 24.706 3178 17.529 3543 297.4(1159) 1.2529 24.745 2987 1.134 3387 2.488 0.26825 25.758 0.3749 4394 14.118 170.6 0.66 0.70 64.679 COMBUSTOR 0 42 35 4 65.055 34.135 4136 525.0(1381) 1.2231 24.763 3187 65.055 18-195 3676 328.0(1207) 1.2454 24.804 3029 1.036 3139 2.496 0.24939 25.758 0.4032 4392 12.167 170.5 0.66 0.72 COMBUSTOR REGEN 43 36 21 65.055 34.135 4329 617.2(1455) 1.2110 24.725 3247 65.055 23.205 4047 487.4(1347) 1.2252 24.769 3155 0.808 2548 2.518 0.24939 25.758 0.4032 4437 9.877 172.3 0.66 0.72 NOZZLE AE 44 37 87.291 34.135 4136 525.0(1363) 1.2231 24.763 3187 0.956 1920 -316.3(581) 1.3149 24.826 2249 2.885 6488 2.496 0.05192 25,758 1.9371 5669 5.235 220.1 0.66 0.72 87.291 NOZZLE PÓ 45 38 5 87.291 34.135 4136 525.0(1363) 1.2231 24.763 5187 0.375 1527 -444.9(452) 1.3343 24.826 2020 3.449 6966 2.496 0.02751 25.758 3.6554 5929 2.978 230.2 0.66 0.72 87.291 NOZZLE AE REGEN 46 39 87.291 34.135 4329 617.2(1455) 1.2110 24.725 3247 1.010 2075 -264.1(633) 1.3084 24.826 2332 2.848 6641 2.518 0.05192 25.758 1.9371 5818 5.358 225.9 0.66 0.72 87.291 NOZZLE PO REGEN 47" 40 87.291 34.135 4329 617.2(1455) 1.2110 24.725 3247 87.291 0.375 1634 -410.5(487) 1.3285 24.826 2085 3.439 7171 2.518 0.02646 25.758 3.7999 6106 2.949 237.1 0.66 0.72 FICTIVE COMBUSTR 67 60 0 196.222 4804 525.0(1622) 1.1956 25.542 3344 65.055 0.375 1264 -822.7(362) 1,3420 25.718 1811 4.534 8212 2.373 0.04058 25.758 2.4783 6813 5.179 264.5 0.66 1.00 65.055 77. ZLE 68 61 0 27.477 4085 503.3(1362) 1.2243 24.767 3168 FICTIVE NOZZLE 87.291 87.291 1.054 2037 -277.0(620) 1.3100 24.826 2312 2.703 6248 2.508 0.05192 25.758 1.9371 5525 5.041 214.5 0.66 0.72

	P	Т	H	GAMMA	MOLWT	SONV	MACH	VEL	\$	h/A	W	AZAC	мгмом	Q	IVAC	PHI	ETAC
COMBUSTOR		19	12 3												=		
47.510	84.315	2583	592.7(760)	1.3107	25.472	∠570											
47.310	30.063	2011	408.7(5/7)	1.3304	25.472	₹ 285	1.328	3034	2.141	0.74777	25.505	0.1332	3431	35.259	134.5	0.54	0.04
COMBUSTOR	U	-0	15 2														
47.335 47.335	70.74	2000	592.5(761)	1.5104	25.477	2572											
COMBUSTOR	30.214	2014	409.4(579)	1.3500	25,477	2289	1.322	3027	2.142	0.74694	25.505	0.1333	3431	35.136	134.5	0.34	0.04
48+110			14 4	. 3000	00											,	
48,110	30.444	2217	587.3(812)	1.3028	25.057	2635		200.									
COMBUSTOR	764414	22	419.6(646)	1.3201	25.050	2345	1.211	2846	2.164	0.69677	25.505	0.1429	3463	31.363	136.5	0.34	0.15
48.775			598.4(774)	1 7217	J2 470	2627										1	
48.775	25.730	1834	403.2(579)	1 2/15	24 637	2711	4 750	7120	2 74 6		25 710					_	
COMBUSTOR	0	23	16 2	1.3413	66.037	2314	1.220	2142	2.310	V-64/4/	25.750	0.1552	3525	31,471	136.8	0.66	0.01
48.785		2394	598.3(775)	1 3212	22 846	242/1							•				
48.785	25.706	1836	403.0(580)	1.3010	22.840	2215	1 150	7124	2 444	A 4/1717	25 258	A 4550	7576	7			
COMBUSTOR	Ö	24	17. 4	* • • • • • •	L	-213	X 6 3 2 V	2120	C 1 2 1 1	0.04713	23./30	V = 1 2 2 4	2250	31.441	130.4	V.00	0.01
49+315	71.295	2483	595.0(805)	1.3170	22.926	2663					Ł				•		
49.315	24,392	1906	392.0(603)	1.3376	22-926	2351	-1.356	3187	2.325	0.60521	26.758	0.443	3500	20 .077	170 //	0 44	A AC
COMBUSTOR	v	45	18 4		•		1435-	2201	47769	0.0025.		VALGOR	3370	29.977	\$3744	0.00	0.03
50.725	65.612	2633	586.6(856)	1.3099	23.080	2726					•	7					
50.725	19,731	1965	350.1(621)	1.3334	23.080	2376	1.448	3440	2.349	0.51581	25.758	0.1950	3739	27.573	144.2	0.44	0.11
COMBUSTOR	V	20	134,5										3.3.	-, -,	*	****	
52.825	52.533	3224	574.4(1060)	1.2816	23.667	2946											
52.825	23.550	2691	375.6(866)	1.3060	23.669	2711	1.164	3154	2.418	0.42277	25.758	0.2379	3960	20.723	153.7	0.66	0.32
COMBUSTOR	·	G (20 6												,		
53.325	52.546	3216	571.6(1057)	1.2820	23.666	2943											
53.325	19.902	2581	336.0(827)	1.3038	23,668	2659	1.291	3433	2.417	0.40549	25.758	0.2480	4013	21.633	155.8	0.66	0.32
COMBUSTOR		28															
54.075 54.075	71.550	36/4	567.5(1078)	1.2789	23.734	2962											
COMBUSTOR	1/4070	205	310.0(826)	1.3054	23.737	4054	1.352	3590	2.423	0.38223	25.758	0.2631	4080	21.322	158.4	0.66	0.35
54.835		29	E67 E/100E\	4 3774	77 7/7	20/0											
54.835	15.842	2517	563.5(1085)	1.2//0	1010C3	CY00	4 030	*== ^	5 455								
COMBUSTOR	30002	30	261.2(809)	1.3040	23.//0	2030	1,429	3758	2.425	0.30145	25.758	0.2782	4139	21,110	160.7	0.66	0.36
55.760	49-726	3334	558.8(1098)	1 2756	37 B + L	2070					1					,	
55.760	14.180	2514	254.2(800)	1 3042	21.420	2414	1 //02	300#	3 439	0 77070	26 766	0 0047	0202	20 500			
COMBUSTOR	0	31	24 5	1.3045	#2 FOEA	2010	1 4 4 7 5	3704	C+460	V-33730	22.130	0.5403	4202	20.589	103.1	U.00	0.38
56.260			556.4(1236)	1.2532	24.224	3005								•			
56.260	13.272	2951	256.2(950)	1.2835	24.239	2787	1.391	3876	2.470	0.27341	25 758	0 7678	11757	16 067	160 0	0 44	A 63
COMBUSTOR	Ó	32	25 5	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		4.0,		20.0	44710	0.61241	236130	V . 30 / 0	4333	16.467	704.0	V.00	V.52
56.315	44.667	3426	556.2(1130)	1.2705	23.916	3008											
56.315	10.261	2465	198.5(782)	1.3046	23.921	2586	1.636	4230	2.445	0.27254	25.758	0.3690	4356	17.918	160.1	0.66	0.41
COMBUSTOR	U	د د	26 S										7020	,14		4,00	U . W .
56.455	44.615	3430	555.6(1132)	1.2702	23.921	3009											
56.455	10.134	2462	195.3(780)	1.3046	23.927	2584	1.644	4246	2.443	0.27059	25.758	0.3717	4364	17,855	169.4	0.66	0.41
COMBUSTOR	v	54	27 5												,	• • • •	• • • •
56.535 56.535	40.697	3702	555.3(1228)	1.2545	24.204	3089											
56.535	12.772	2843	242.6(929)	1.2858	24.219	2764	1.431	3955	2.467	0.27362	25.758	0.3675	4369	16.818	169.6	0.66	0.52
COMBUSTOR 56.815	U	35	26 S														•
56.815	12.545	30/4	554.1(1220)	1.2559	24.184	3082			_					•			
COMBUSTOR	*C*COK	203/	229.8(909)	1.2881	£4.197	2740	1.470	4028	2.464	0.27271	25.758	0.3688	4383	17.073	170.2	0.66	0.51
57.041		36 3602		1 3445	5/1 107	70.0											
57.041	11.358	2600	553.2(1193) 209.7(841)	1 20"0	24 112	2000	1 605	114 20 .	7 11 12 12			.					
COMBUSTOR	0.44.5	37	209.7(861)	1 . 5740	E-4+110	5007	1.545	4146	6.457	0.2/230	45.758	0.3693	4393	17.544	170.6	0.66	0.48
CO 57.765		3295	550.3(1084)	1.2772	24,800	2065											
57.765	8.460	2188	145.6(687)	1.3160	23.801	2457	1.835	4500	3.032	0 76707	משל שם	0 7251	11 11 4 4	10 7 114			
. =			017		~74043	23	1.000	~ J v V	C . 4 C 3	V. C0/9/	C3./30	0.5/53	4416	18.741	1/1.4	V.66	0.37

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SUMMARY REPORT

æ P	T	н		CAMMA	WOLWI	SONV	MACH	VFI	s	W/A	bá Í	A/AC	MOMIM	0	IVAC	DLT	5740
WIND TUNNEL	1	0 5		איוויואט	111111111111	CONT	HAUN	¥ L L	J	117 (4	rı	AZAC	HORID	v	IVAÇ	FUT	CIRG
0.000 742.499	2902	640.76	767)	1.2963	28.898	2544				*							
(0.000 0.375	386	-36.2(93)	1.3986	28.897	964	6.035	5820	1.818	0.10570	25.242	0.9323	4656	9.561	184.5		
SPIKE TIP NS	٤	0 5										,					
		640.70	767)	1.2963	28.897	2544			_								
0.600 16.436		621.7(748)	1.2983	28.897	2518	0,388	976	2.074	0.10570	25,242	0.9323	4691	1.604	185.8		
WIND TUNNEL 0.000 742.499	~ 3	0 0	7671	1 2047	20 000	35.00											
0.000 142.447	348	-35 01	931	1 7006	20.070	044	4 422	Eato	1 010	0 10669	3E //77	0.9323	4400	0 - 114	404 4		
SPIKE TIP NS	4	0 0	73,	1,3700	20.071	700	0.055	2014	1.010	0. Ĭ ABBB	62.412	0.4353	4070	7,040	104,4		
		640.7(767)	1.2963	28.897	2544											
0.600 16.402		621.3(748)	1.2984	28.897	2518	0.392	987	2.074	0.10668	25.473	0.9323	4698	1.636	184.4		
INCET THROAT	5	0 4										., .,.	,	••••			
40.400 196.222		608,60	735)	1.2997	28.897	2500											
40.400 17.430		255.4(384)	1.3458	28.897	1893	2.220	4204	1.898	0.88501	25.242	0.1114	3795	57.820	150.4		
INLET UPNRSK 40.400 196.222	6 2705	0 3	7751	. 2007	20 004	2504											
40.400 14.862		608.6(4700		A 54454	20 202		2864	#3 * 6*			
	_	02- 4	3601	1.3443	20.011	1031	C.310	4502	1.040	0.00450	45.445	0.1225	3841	55./87	125.5		
40:400 107-593	2795	05- 4 608-6(735)	1.2998	28.897	2500	7 1	2 +		,	· . '						
40.400 90.524	2685	57.6.06	703)	1.3032	28.897	2454	0.520	1276	1.940	0.80456	25.242	0.1225	3841	15.956			
COMBUSTOR - 0	8	1 4									12.0 G G 1.0	* 0 2 4 2 2	504.		* ~ * 0 6		
40.410 195.820	2795	608.5(735)	1.2997	28.897	2500											
40.410 17.450	1550	255.7(385)	1.3458	28.897	1894	815,5	4202	1.898	0.88490	25.242	0.1114	3794	57.784	150.3		
COMBUSIDK 0	, 9	2 4				,	. `								•		
41.310 159.509 41.310 20.253	2/85	605.0(732)	1,3001	28,897	2495											
COMBUSTOR 0	1000	3 4	4223	1,5586	20.077	1975	2,004	3951	1,911	0.88648	25.242	0.1112	3676	54.432	145.7		
41.375 157.355		604.70	7721	1 3002	28.807	2/105											
41.375 20.519	1699	296.00	425)	1.3383	28.897	1978	1.087	2021	1.012	0.88782	35.5/12	0.1110	7667	5/1 373	1/IE 7		
COMBUSTOR 0	11	4 4		.,	,	.,,		- 7 - 4	10,10	0100,00	639676	001110	3001	349535	. 4 . 6		
41.500 152.908	2780	604.1(731)	1,3002	28.897	2494											
41.500 20.989	1720	301.60	431)	1.3373	28.897	1989	1:956	3891	1.914	0.88803	25.242	0.11107	3649	53.692	144-6		
COMBUSTOR 0	12	5 5															
42.460 132.007	2762	598.9(726)	1.3008	28.897	2486											
42.460 23.247 COMBUSTOR 0	13	520.6	458)	1,3332	28.897	2042	1.801	3677	1.922	0.87931	25.242	0.1121	3552	50.252	140.7		
44.095 116.921	2727	588.4(7163	1 7010	24 857	5/174	•										
44.095 24.073	1864	341.30	4701	1.3314	28-897	2066	1, 701	3516	1.027	0.88900	25 2/12	0.1161	3/17/1	#4 704	177 6		
	14	7 3			204011	2000	*414*	2210	Fasci	0.04707	234545	0.1101	24/4	40.371	13100		
44.310 115.613	2722	566.9(714)	1.3021	28,897	2469			•	-				`			
44.310 24.224	1869	342.6(472)	1.3312	28.897	2069	1.690	3496	1.927	0.84761	25.242	0.1163	3464	46.055	137.2		
	13	6 2								_	_		-	•			
44.800 112.889			711)	1.3024	28.897	2464		,									
44.800 24.527			474)	1,3309	28.897	2073	1.667	3455	1.927	0.84431	25.242	0.1167	3444	45.334	136 ô 4		
	16	9 3	7413	. 1004	20 007	20/0											
	1877	583.4(4741	1 7700	20.07/	2404		7050	4 022	A 40074	5E 945		7007	45 .07			
COMBUSTOR 0	17	10 21	7,7,	102207	20.041	6413	1.0000	3434	1.461	0.04.07	65,646	0.1167	5445	45.325	130.4		
		600.20	7843	1.3075	25.526	2603								•	-		
46.250 27.091	2029	396.76	582)	1.3291	25.526	2562	1,392	3190	2,151	0.80415	25.505	0.1238	3388	39,872	132-0	0.34 0	.07
COMBOSIUR 0	18	11 21										- 4 - 4 - 4					
46.260 87.283	2554	600.1(751)	1.3123	25.421	2560											
46.260 27.119	1919	396.9(549)	1.3344	25.421	5538	1.425	3189	2.136	0.80365	25,505	0.1239	3388	39.826	132.9	0.34 0	.01

t = 285.64 sec.

RAMJET PERFORMANCE

7						
_				INLET		
Ġ,	CALCULATED THRUST	(LBF) (LBF) (LBF=SEC/LBM) (LBF=SEC/LBM)	MASS FLOW RATIO ADDITIVE DRAG COEF LIMITING PRESSURE DELTA PT2 TOTAL PRESSURE REC TOTAL PRESSURE REC	FICIENT	0.9321 0.0053 0.1427 0.1161 0.2648	
	REGENERATIVE-COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	(LBF)	INLFT PROCESS EFFI INLET PROCESS EFFI KINETIC ENERGY EFF KINETIC ENERGY EFF ENTHALPY AT PO - S	CIENCY = SUPERSONIC CIENCY = SUBSONIC ICIENCY = SUPERSONIC ICIENCY = SUBSONIC UPERSONIC UBSONIC	0.8740 0.9003 0.8979 0.8619	(BTU/LBM)
	440 F 10 F 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			COMBUSTOR		
	INLET FRICTION DRAG	(LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF)	EQUIVALENCE RATIO. COMBUSTOR EFFICIEN TOTAL PRESSURE RAT COMBUSTOR EFFECTIV INJECTUR DISCHARGE VACUUM STREAM THRU NOZZLE COEFFICIENT PROCESS EFFICIENCY	CY	0.660 0.711 0.7719 0.7019 0.7019 0.6687	
	,					
	STATIONS		FU	EL INJECTORS		
	NOMINAL COWL LEADING EDGE	3 (IN) 2 (IN) 2 (IN) 3 (IN) 5 (IN) 5 (IN) 6 (IN)	INJECTORS 1 A 1 B 1 C 2 A 2 C 3 A 3 B	STATION 40.400 41.300 44.300 48.775 46.250 54.065 56.250 44.800	VALVE D E	

x	DORAG	CDRAG	CF	нс
4.041E 01 4.131E 01 4.137E 01 4.137E 01 4.137E 01 4.137E 01 4.409E 01 4.409E 01 4.481E 01 4.481E 01 4.625E 01 4.625E 01 4.625E 01 4.625E 01 4.625E 01 4.625E 01 5.733E 01 4.8778E 01 4.8778E 01 5.237E 01 5.237E 01 5.235E 01 5.235E 01 5.235E 01 5.235E 01 5.235E 01 5.235E 01 5.235E 01 5.235E 01	1.287E 01 1.455E 01 2.528E 00 1.530E 01 2.530E 01 3.530E 01 3.530E 01 3.530E 01 3.530E 01 3.530E 01 3.530E 01 3.6433E 01 3.6433E 01 3.6433E 01 3.6433E 01 3.6433E 01 3.6433E 01 3.73E 01 1.373E 01 1.373E 00 1.373E	1.284E 0002222222222222222222222222222222222	2.3756E=0033 3756E=0033 456E=0033 4504E=0033 3756E=0033 4504E=0033 2.66476E=0033 2.66476E=0033 2.66476E=0033 2.66476E=0033 2.7663 2.7663 2.77663	42.22.22.22.22.22.22.22.22.22.22.22.22.2
5.626E 01 5.631E 01 5.645E 01	2.389E 00 3.538E-01 9.270E-01	3.133E 02 3.136E 02 3.145E 02 3.151E 02 3.169E 02 3.233E 02 3.233E 02 3.304E 02 3.3515E 02	2.849E-03 2.996E-03 2.843E-03 3.203E-03 2.985E-03 2.972E-03 2.872E-03 2.385E-03 2.852E-03	2.614E=02 2.144E=02 2.143E=02 2.263E=02 2.363E=02 2.363E=02 2.363E=02 2.363E=02 2.363E=02 2.363E=02 2.363E=02 2.363E=02
6.505E-01 6.509F 01 6.529E 01 6.695E 01 6.762E 01 6.911E 01 6.911E 01 7.067E 01 7.110E 01	2.011E 00 2.053E=01 1.043E 00 9.141E 00 3.502E 00 3.745E 00 3.067E 00 3.097E 00 1.238E 00	3.684E 02 3.694E 02 3.786E 02 3.821E 02 3.851E 02 3.859E 02 3.912E 02 3.913E 02 3.913E 02	3.101E-03 3.257E-03 3.337E-03 3.332E-03 3.136E-03 3.136E-03 3.070E+03 3.022E-03 2.989E-03 2.918E-03	2.665E=02 2.464E=02 2.519E=02 1.901E=02 1.724E=02 1.358E=02 9.740E=03 7.594E=03 6.945E=03
7.263E 01 7.278E 01 7.353E 01 7.353E 01 7.486E 01 7.771E 01 8.161E 01 8.442E 01 8.728E 01 8.729E 01	4.042E 00 3.531E=01 1.475E 00 2.410E=03 8.516E=01 2.087E 00 8.928E=01 3.807E=01	3.996E 02 3.999E 02 4.014E 02 4.014E 02 4.024E 02 4.063E 02 4.063E 02 4.076E 02 4.076E 02	2.889E-03 2.878E-03 2.799E-03 2.799E-03 2.839E-03 2.806E-03 2.750E-03 2.795E-03 2.795E-03	6.144E=03 5.840E=03 4.043E=03 4.042E=03 5.095E=03 6.559E=03 4.055E=03 5.367E=03 5.370E=03

	XABS	P-IB	P=08	PDA	Q0X	G-IB	0-0B	CAWALL	P-I8/PS0	P-18/PT0	P=08/PS0	P-OB/PTO
-	6.505E 01	1.837E 01	1.796E 01	1.430E 02	-4.011E 03	3 -2.191E	03 -1.821E 03	4.337E 03	4.890E 01	2.475t+02	4.730E 01	2.419E=02
	6.509E 01	1.837E 01	1.801E 01	1.430E 02	-4.015E 03	3 -2.193E	03 -1.823£ 03	4.342E 03	4.890E 01	2.475E-02	4.794E 01	2.426E-02
4	6.529E 01	1.748E 01	1.827E 01	1.430E 02	-4.036E 03	3 -2.203E	03 -1.833E 03	4.368E 03	4.651E 01	2.3546-02	4.863E 01	2.461E=02
	6.695E 01	1.005E 01	8.290E 00	2.929E 02	-4.185E 03	3 -2.276E	03 -1.908E 03	4.583E 03	2.674E 01	1.354E-Q2	2.206E 01	1.116E=02
	6.762E 01	7.454E 00	8.025E 00	4.640E 02	-4.234E 03	3 -2.299E	03 -1.936E 03	4.665E 03	1.983E 01	1.004E=02	2.135E 01	1.0815902
	6.839E 01	4.470E 00	6.196E 00				03 -1.968E 03	4.760E 03	1.189E 01	6.020E-03	1.649E 01	8.344E=Q3
	6.911E 01	3.515E 00	4.485E 00	7.635E 02	-4.336E 03	3 +2.336E	03 -2.000E 03	4.848E 03	9.352E 00	4.733E=03	1.193E 01	6.04QE+03
	6.972E 01	2.705E 00	3.756E 00	8.413E Q2	=4.373E 03	3 -2.346E	03 -2.027E 03	4.9228 03	7.198E 00	3.643E-03	9.994E 00	5.058E=03
	7.067E 01	1.937E 00	5.650E 00	9.279£ 02	-4.420E 03	3 -2.360E	03 -2.060E 03	5.036E 03	5.156E 00	2.609E=03	6.972E 00	3,5296-03
	7.110E 01	1,590E 00	2.443E 00				03 -2.073E 03	5.088E 03	4.231E 00	2.141E-03	6.502E 00	3.291E=03
	7.263E 01	1.608E 00	1.815E 00	1.046E 03	#4.489E 03	3 -2.379E	03 -2.109E 03	5.273E 03	4.279E 00	2.166E-03	4.830E 00	2.444£±03
	7.278E 01	1.610E 00	1.588E 00				03 -2.112E 03	5.290E 03	4.284E 00	2.168E=03	4.227E 00	2.139E=03
	7.353E 01	1.513E 00	4.550E-01				03 -2.130E 03	5.374E 03	4.025E 00	2.037E-03	1.211E 00	6.128E=04
	7.354E 01	1.512E 00	4.489E-01				03 -2.130E 03	5.3/5E 03	4.024E 00	2.037E=03	1.195E 00	6.046E-04
	7.486E 01	1.340E 00	0.000				03 -2.166E 03	5.427E 03	3.566E 00	1.805E-03	0.000	0.000
	7.771E 01	1.895E 00	0.000				03 -5.535E 03	5.525£ 03		.2.552t=03	0.000	0.000:
	8.161E 01	1.350E 00	0.000				03 -2.232E 03	5.630E 03	3.592E 00	1.818E=03	0.000	0.000
	8.442E 01	1.015E-00	0.000				03 -2.232E 03	5.684E 03	2.701E 00	1.367E-03	0.000	0.000
	8.728E 01	1.480E 00	0.000				03 -2.232E 03	5.707E 03	3.938E 00	1.993E-03	0.000	0.000
	8.729E 01	1.481E 00	0.000	1.316E 03	-4.712E 03	3 -2.480E	03 -2.232E 03	5.707E 03	3.941E 00	1.9956-03	0.000	0.000

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				20-1120	ijeçii o	•	46+477 II # 6'	700.7				PAGE 14
	XABS	P-IB	P=08	PDA	. 00x	Q-IB	G=08	CAWALL	P=18/PS0	P=IB/PTO	P=08/PS0	P=08/PT0
	6.981E=01	1.040E 00	0.000	-4.405E=01	0.000	0.000	0.000	2.470E-02	2.767E 00	1.401E=03	0.000	0.000
	1.836E 01	1.040E 00	0.000	-3,463E 01	0.000	0.000	0.000	1.634E 02	2.767E 00	1.401E=03	0.000	0.000
	3.070E 01	2.975E 00	0.000	-1.974E 02	0.000	0.000	0.000	5.053E 02	7.917E 00	4.007E-03	0.000	0.000
	3.508E 01	3.8266 00	0.000	-4.178E 02	0.000	0.000	0.000	6.804E 02	1.018E 01	5,153t-03	0.000	0.000
	3.519E 01	4.14ZE 00	5.552E 00	-4.821E 02	0.000	0.000	0.000	6.854E U2	1.102E 01	5.578E-03	1.478E 01	7.478E-03
	3.520E 01	4.158E 00	5.523E 00	-4.82ZE 02	0.000	0.000	0.000	6.857E 02	1.107E 01	5.601E-03	1.470E 01	7.439E=03
	3.555E 01	5.140E 00	5.810E 00	-4,948E U2	0.000	0.000	u . 000	7.209E 02	1.368E 01	6.9236≈03	1.014E 01	5.1326=03
	3.586E 01	5.010E 00	2.275E 00	-5.160E 02	-5.492E	02 -5.492E	02 0.000	7.529E 02	1.333E 01	6.748t-03	6.054E 00	3.064E=03
	3.606E 01	4.930E 00	3.430E 00	-5.296E 02	+5.553E	02 - 5.553F	02 0.000	7.729E 02	1.312E 01	6.640E=03	9.126E 00	4.619E=03
	3.648E 01	4.140£ 00	5.914E 00	-5.485E V2	₽5.689E (02 -5.689E	02 0.000	8.164E 02	1.102E 01	5.576E-03	1.574E 01	7.966E=03
	3.701E 01	5.115E 00	9.050E 00	~5.694E 02	-6.043E	02 -5. 868E	02 -1.752E 01	8.726E 02	1.361E 01	6.889L=03	2.408E 01	1.219E-02
	3.732E 01	4.857E 00	1.091E 01	-5.806E 02	-6.212E	02 -5.9 78E	02 -2.339E 01	9.063E 02	1.293E 01	6.542E-03	2.904E 01	1.470E=02
	3.803E 01	4.280E 00	1.452E 01	-5.943E 02	-6.601E	02 =6.239E	02 -3.624E 01	9.834E 02	1.139E 01	5.764E=03	3.863E 01	1.9556-02
	3.834E 01	8.020E 00	1.612E 01	-5.993E 02	-6.783E (02 -6.364F	02 = 4.193F 01	1.018E 03	2.134E 01	1.080E=02	4.291E 01	2.1726-02
	3.875E 01	1.283E 01	1.768E 01	-6.506E 05	-7.030E (02 -6.538 <u>E</u>	02 -4.921E 01	1.064E 03	3.415E 01	1.728E-02	4.704E 01	2.381E-02
	3.881E 01	1.360E 01	1.792E 01	-6.244E 02	+7.070E	02 -6.567E	02 -5.037E 01	1.072E 03	3.620E 01	1.832E=02	4.770E 01	2.414E=02
	3.901E 01 3.932E 01	1.592E 01	1.//SE 01	*6.355E 02	₩7.196E	02 -6.657E	02 -5.385E 01	1.094E 03	4.236E 01	2.144E=02	4.724E 01	2,3916=02
	3.950E 01	-1.870E 01	1.74/E 01	-0.565E 02	=7.407E	02 -6.812E	02 #5.944E 01	1.130E 03	4.977E 01	2.5194-02	4.650E 01	2.354E=02
	3.981E 01	2.025E 01 1.805E 01	1.312E 01	-6.696E 02	-7.528E	02 -6.903E	02 -6.253E 01	1.150E 03	5.389E 01	2.727E-02	3.492E 01	1.767E=02
	4.000E 01	1.676E 01	5+3005 00	-6.974E 02	-7.755E (7.075E	10 3664.9m 20	1.187E 03	4.803E 01	2.431E-02	1.410E 01	7.138E=03
	4.040E 01	2.003E 01	7 E44E 00	≈/*146E 02	-7.894E	2 -7.183E	02 -7.115E 01	1.209E 03	4.459E 01	2.257E-02	1.349E 01	6.825E=03
		-2.011E 01	44200E 00	-7.516E 02	-8.508E (2 -7.426E	02 -7.818E 01	1.2568 03	5.330E 01	2,6976-02	1.215E 01	6.150E=03
	4.131E 01	2.747E 01	1,4256 00	-A ##76 A3	-0 1.36 (72 =7.0338	02 -7.836E 01	1.257E 03	5.351E 01	2.708E=02	1.212E 01	6,1336603
	4-137E 01	2.800E 01	3-3446 00	-8.557E 02	-0 1745 (12 -0 0025	02 -1.057E 02 02 -1.085E 02	1.363€ 03	7.310E 01	3.700E=02	9.115E 00	4.613E+03
	4.150E 01	2.902E 01	3.947F 00	-8.802E 02	-7-1/DE (12 -0 - U 4 3 E	02 =1 +083# 05	1.371E 03	7.451E 01	3.771E-02	8.898E 00	4.503E=03
	4.246E 01	2.085E 01	8.576E 00	-9.614F 02	=1.065E ()2 -0.10/C	02 -1.141E 02	1.386E 03	7.724E 01	3.909L=02	1.050E 01	5.316E-03
	4.409E 01	2.504E 01	1.646E 01	-1.015E 03	-1.350E	33 -1.045E	03 -2.951E 02	1.501E 03 1.699E 03	5.548E 01 6.664E 01	2.808E=02 3.373E-02	2.282E 01	1,155E#02
	4.431E 01	2.559E 01	1.727E 01	-1.021E 03	-1.368E (3 -1.054E	43 -3.135F 02	1.725E 03	6.811E 01	3.447E-02	4,380E 01 4.594E 01	5.217E=02
	4.480E 01	2.685E 01	1.910E 01	-1.034E 03	~1.453E (3 -1.097E	03 -3.567E 02	1.785E 03	7.145E 01	3.616E-02	5.083E 01	2.573E=02
	4.481E 01	2.686E 01	1.914E 01	-1.034E 03	-1.455E (3 -1.09BE	03 =3.576F 02	1.786E 03	7.149E 01	3.618E-02	5.093E 01	2.5785-02
	4.625E 01	2.901E 01	2.454E 01	-1.025E 03	-1.711E C	3 -1.220E	03 #4.913E 02	1.963E 03	7.718E 01	3.906E-02	6.529E 01	3.304E=02
	4.626E 01	2.902E 01	2.457E 01	-1.024E 03	-1.713E (31 -1. 221E	03 -4.922E 02	1.964E 03	7.722E 01	3.908E-02	6.539E 01	3.3092-02
	4.731E 01 4.733E 01	3.058E 01	2.851E 01	-9.709E 02	=1.899E ()3 -1. 306£	03 -5.928E 02	2.094E 03	8.138E 01	4.119E-02	7.586E 01	3.839E=02
	4.811E 01	3.079E 01 3.730E 01	5+000E 01	-9.700E 02	-1.903E (3 -1.308E	03 -5.952E 02	2.097E 03	8.193E 01	4.147E-02	7.611E 01	3.852E=02
	4.877E 01	2.561E 01	2 6415 04	-9.114E 02	-2-036E ()3 -1.369E	03 -6.676E 02	2.194E 03	9.926E 01	5.024E=02	7.182E 01	3.635E-02
	4.878E 01	2.559E 01	2.5505 01	-8 403E 05	-2-145E (3 -1-419E	03 -7.265E 02	2.277E 03	6.815E 01	3,449E-02	6.815E 01	3.449E=02
	4.931E 01	2.449E 01	2.4406 01	-8.302E 02	-2 344E C	13 -1.420E	03 *7.274E 02	2.278E 03	6.809E 01	3.446E=02	6.809E 01	3.446E>02
	5.072E 01	1.962E 01	1.9626 01	-5 0806 02	-2 447E (73 -1 459E	03 -7.721E 02 03 -8.802E 02	2.345E 03	6.516E 01	3.298E-02	6.516E 01	3.298E¤02
	5.282E 01	2.355E 01	2-355F 01	-3.604E 02	-2.75AE 0)3 ~ 1 607E	03 -4 0430 02	2.522E 03	5.221E 01	2.642E-02	5.221E 01	2.642E+02
	5.332E 01	1.965E 01	1.965E 01	-3.042E 02	-2-840E 0	13 -1.7275	03 ~1.062E 03 03 ~1.103E 03	2.789E 03 2.852E 03	6.267E 01	3.1726-02	6.267E 01	3.1/25002
	5.407E 01	1.7626 01	1.762E 01	-2.321F 02	-2-945F 0	13 -1.7726	03 -1.163F 03	5.94AF 03	5.230E 01	2.6475-02	5.230E 01	2.6478-02
	5.483E 01	1.556£ 01	1.556€ 01	-1.678E 02	-3.057E 0	3 -1.815F	03 -1.222E 03	3.046E 03	4.689F 01	2.373t-02	4.689E 01	2.3/3E=02
	5.576E 01	1.400E 01	1.400E 01	-9.920E 01	-3.157F 0	3 -1.866F	03 -1.291E 03	3,164E 03	4.141E 01 3.726E 01	2.096t-02 1.886E-02	4.141E 01	2.096E-02
	5.626E 01	1.316E 01	1.316E 01	5.377E 01	-3.215E 0	5 ~1.888F	03 -1.327E 03	3.209E 03	3.502E 01	1.772E-02	3.726E 01 3.502E 01	1.886E=02
	5.631E 01	7.312E 00	1.30/E 01	5.750E 01	-3.221E 0	1.890E	03 -1.331E 03	3.216E 03	1.946E 01	9.848E-03	3.477E 01	1.772E=02 1.760E=02
	5.645E 01	7.312E 00	1.283E 01	6.593E 01	-3.236E 0	3 -1.895E	03 =1.341E 03	3.234E 03	1.946E 01	9.848E-03	3.415E 01	1.728E=02
	5.653E 01	1.270E 01	1.270E 01	7.106E 01	-3.245E 0	3 =1.898F	03 =1.347E 03	3.245E 03	3.379E 01	1.710E=02	3.379E 01	1.710E=02
	5.681E 01	1.222E 01	1.222E 01	8.733E 01	-3.274E 0	3 -1.908E	03 =1.366E 03	3.280E 03	3.253E 01	1.646E-02	3.253E 01	1.646E=02
	5.704E 01 5.776E 01	1.133E 01	1.133E 01	9.879E 01	-3.29/E 0	3 -1.916F	03 -1.381F 03	3.309E 03	3.015E 01	1.526E=02	3.015E 01	1.526E=02
	5.878E 01	8.460£ 00 5.025£ 00	8.460E 00	1.250E 02	-3.369E 0		03 -1.430E 03	3.402E 03	2.251E 01	1.139E-02	2.251E 01	1.1396=02
_	6.079E 01	9.950E 00	5.025E 00	1.412E 02			03 =1.488E 03	3.532E 03	1.337E 01	6.768E-03	1.337E 01	6.788E=03
1	6.221E 01	1.426E 01	9.950E 00 1.426E 01	1 4305 02	-3+614E 0	2.022E	03 -1.596E 03	3.790E 03	2.648E 01	1.3406-02	2.648E 01	1.340E=02
٠	6.468E 01	1.747E 01	1.747E 01	1.0306.02	マル・/ ル/ 性 り	2.065E	03 -1.672E 03	3.972E 03	3.794E 01	1.920E-02	3.794E 01	1.920E=02
•			TTTTC VI	***305 08	-3.7/16 0	-c.1/1E	05 -1.800E 03	4.289E 03	4.649E 01	2.353t=02	4.649E 01	2.3536-02

GAMMA MOLWT SONY MACH YEL S W/A A/AC MOMTH Q IVAC PHI ETAC COMBUSTUR 0 38 31 6 81.527 2789 548.5(907) 1.3015 23.328 2781 No 58.785 58.785 5.025 1399 60.8(428) 1.3566 23.528 2011 2.441 4909 2.541 0.26618 25.749 0.3777 4415 20.308 171.5 0.66 0.19 COMBUSTOR 0 39 32 6 60.795 47.431 3448 542.2(1137) 1.2689 23.985 3012 60.795 9.950 2435 165.4(770) 1.3049 23.992 2566 1.692 4342 2.437 0.27544 25.749 0.3650 4405 18.587 171.1 0.66 0.43 COMBUSTOR 0 40 33 5 62.215 41.394 3846 537.6(1278) 1.2451 24.417 3123 62.215 14.256 3087 237.7(996) 1.2761 24.439 2831 1.368 3874 2.469 0.28291 25.749 0.3553 4398 17.031 170.8 0.66 0.59 COMBUSTOR 0 41 34 4 64.679 36.943 4073 528.6(1358) 1.2285 24.693 3174 64.679 17.471 3526 299.9(1153) 1.2540 24.730 2982 1.134 3382 2.487 0.26817 25.749 0.3749 4384 14.096 170.3 0.66 0.69 COMBUSTOR 0 42 35 4 34.053 4120 527.0(1375) 1.2243 24.750 3183 65.055 18.168 3661 331.0(1202) 1.2465 24.790 3025 1.035 3132 2.495 0.24931 25.749 0.4032 4383 12.133 170.2 0.66 0.71 65.055 COMBUSTOR REGEN, 43 36 21 65.055 34.053 4324 623.8(1453) 1.2116 24.711 3246 19.825 3928 444.5(1302) 1.2316 24.767 3117 0.961 2995 2.518 0.24931 25.749 0.4032 4445 11.605 172.6 0.66 0.71 65.055 NOZZLE AE 44 37 5 87.291 34.053 4120 527.0(1356) 1.2243 24.750 3183 0.952 1908 -311.0(577) 1.3157 24.810 2243 2.887 6475 2.495 0.05190 25.749 1.9371 5655 5.222 219.6 0.66 0.71 87.291 NOZZLE PO 45 38 5 34.053 4120 527.0(1356) 1.2243 24.750 3183 87.291 0.376 1519 -438.1(450) 1.3350 24.810 2016 3.448 6949 2.495 0.02761 25.749 3.6413 5912 2.982 229.6 0.66 0.71 87.291 NOZZLE AL REGEN 46 39 5 87.291 34.053 4324 623.0(1453) 1.2116 24.711 3246 87.291 1.009 2071 -256.2(631) 1.3089 24.810 2330 2.848 6636 2.518 0.05190 25.749 1.9371 5811 5.352 225.7 0.66 0.71 NOZZLE PO REGEN 47 40 5 34.053 4324 623.8(1453) 1.2116 24.711 3246 87.291 0.376 1631 -402.0(486) 1.3289 24.810 2084 3.438 7165 2.518 0.02650 25.749 3.7931 6099 2.951 236.9 0.66 0.71 FICTIVE COMBUSTR 67 60 0 65.055 196.619 4804 527.0(1622) 1.1956 25.548 3344 0.376 1264 -820.7(361) 1.3421 25.724 1811 4.535 8212 2.372 0.04064 25.749 2.4737 6810 5.187 264.5 0.66 1.00 65.055 FICTIVE NOZZLE 68 61 0 87.291 28.149 4057 499.7(1351) 1.2265 24.756 3161 87.291 1.031 1995 =281.7(606) 1.3120 24.810 2290 2.730 6253 2.504 0.05190 25.749 1.9371 5516 5.043 214.2 0.66 0.71

GAMPA MOLWT'SONV HACH VEL S MOMIN Q IVAC PHI ETAC A/AC 0 19 12 3 COMBUSTOR 47.310 84.678 2569 593.8(756) 1.3114 25.449 2565 47.310 29.544 1988 407.3(570) 1.3314 25.449 2274 1.343 3055 2.140 0.74757 25.498 0.1332 3428 35.488 134.5 0.34 0.03 COMBUSTOR 0 20 13 47.335 84.447 2574 593.0(757) 1.3111 25.454 2567 47.335 29.695 1996 408.0(573) 1.3311 25.454 2278 1.338 3047 2.141 0.74674 25.498 0.1333 3429 35.365 134.5 0.34 0.03 COMBUSTOR 0 21 14 48.110 77.416 2741 588.4(809) 1.3033 25.638 2632 48.110 32.145 2224 419.8(642) 1.3208 25.638 2387 1.217 2905 2.163 0.69659 25.498 0.1429 3479 31.444 136.4 0.34 0.14 COMBUSTOR 0 22 15 19 74.760 2386 599.4(772) 1.3216 22.840 2620 48.775 48.775 25.609 1827 404.1(577) 1.3419 22.840 2310 1.353 3127 2.309 0.64776 25.749 0.1552 3520 31.475.136.7 0.66 0.01 COMBUSTOR 0 23 16 2 48.785 74.687 2388 599.4(772) 1.3215 22.842 2621 25.588 1829 403.9(577) 1.3418 22.842 2311 1.353 3128 2.309 0.64691 25.749 0.1554 48.785 3522 31.443 136.8 0.66 0.01 COMBUSTOR 0 24 17 49.315 71.086 2482 596.1(804) 1.3171 22.932 2662 49.315 24.487 1908 394.3(603) 1.3375 22.932 2353 1.351 3177 2.325 0.60501 25.749 0.1662 3585 29.875-139.2 0.66 0.05 COMBUSTOR 0 25 18 65.643 2625 587.7(853) 1.3103 23.080 2722 50.725 50.725 19.619 1956 350.9(617) 1.3339 23.080 2371 1.452 3442 2.547 0.51564 25.749 0.1450 3734 27.583 145.0 0.66 0.10 COMBUSTOR ³⁰ 26 19 5 . . 52.825 52.452.3219 575.6(1058) 1.2819 23.669 2944 23.550 2688 377.5(865) 1.3002 23.671 2709 1.162 3149 2.417 0.42263 25.749 0.2379 52.825 3955 20.681 153.6 0.66 0.32 COMBUSTOR 0 27 20 3 53.325 52.621 3200 572.8(1052) 1.2827 23.657 2937 53.325 19.655 2559 335.4(819) 1.3048 23.659 2649 1.301 3447 2.415 0.40536 25.749 0.2480 4007 21.713 155.6 0.66 0.32 COMBUSTOR 0 28 21 4 54.075 51.492 3253 568.8(1070) 1.2800 23.720 2954 54.075 17.622 2553 309.0(816) 1.3042 23.722 2641 1.365 3606 2.420 0.38210 26.749 0.2631 4073 21.410 158.2 0.66 0.34 COMBUSTOR 0 29 22 3 54.835 50.960 3270 564.8(1075) 1.2790 23.746 2959 54.835 15.562 2500 279.8(796) 1.3057 23.749 2614 1.445 3776 2.422 0.36133 25.749 0.2782 4131 21.206 160.4 0.66 0.35 COMBUSTOR 0' 30 23 ,4 55.760 49.836 3311 560:2(1090) 1.2767 23.800 2972 55.760 14.003 2486 254.5(791) 1.3055 23.803 2604 1.502 3911 2.426 0.33926 25.749 0.2963 4193 20.620 162.8 0.66 0.37 COMBUSTOR 0 31 24 5 39.859 3703 557.9(1228) 1.2545 24.208 3089 56.260 56.260 13.161 2927 257.4(941) 1.2847 24.223 2778 1.396 3878 2.468 0.27332 25.749 0.3678 4343 16.471 168.7 0.66 0.51 COMBUSTOR 0 -32 25 56.315 44,669 3408 557.6(1124) 1.2715 23.903.3002 56.315 10.190 2447 200.4(775) 1.3055 23.909 2577 1.640 4228 2.441 0.27245 25.749 0.3690 4347 17.901 168.8 0.66 0.40 COMBUSTOR 0 33 26 3 56.455 44.597 3413 557.1(1125) 1.2712 23.910 3003 10.072 2445 197.3(774) 1.3055 23.915 2576 1.647 4243 2.442 0.27050 25.749 0.3717 4354 17.835 169.1 0.66 0.41 56.455 COMBUSTOR 0 34 27 56.535 40.650 3684 556.8(1221) 1.2557 24.191 3083 56.535 12-697 2874 244.5(923) 1.2868 24.205 2756 1.434 3953 2.465 0.27353 25.749 0.3675 4359 16.803 169.3 0.66 0.51 COMBUSTOR 0 35 28 3 41.296 3665 555.6(1214) 1.2568 24.174 3078 56.815 56.815 12.225 2823 232.3(904) 1.2888 24.187 2735 1.471 4022 2.465 0.27262 25.749 0.3688 4373 17.039 169.8 0.66 0.50 COMBUSTOR 0 36 29 4 57.041 42.807 3589 554.7(1187) 1.2613 24.097 3056 11.529 2687 212.5(857) 1.2946 24.107 2678 1.545 4138 2.455 0.27221 25.749 0.3693 4383 17.505 170.2 0.66 0.47 57.041 COMBUSTOR 0 37 30 5. 50.270 3286 551.9(1081) 1.2777 23.796 2962 57.765 57.765 8.460 2183 149.2(685) 1.3164 23.800 2450 1.832 4489 2.425 0.26789 25.749 0.3753 4406 18.689 171.1 0.66 0.37

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SUMMARY REPORT .

⇔		P	T	н		CAMMA	M21 M4	COLV	14.CH	u.e.	•					_			
W	IND TUNNE		1	0 ິ່າ		Би при	MOLWT	2014	MAUN	VEL	\$	H/A	Ħ	A/AC	MUMTM	Q	IVAC	PHI	ETAC
	0.000	142_499		641.8(7481	1 2063	38 804	15 /1 A											
	0.000	0.376	297	-34.00	071	1 7004	20.040	6340		F									
	PIKE TIP		20,	0 5	43)	1.3400	20.07/	700	0.054	2854	1.814	0.10570	25.234	0.9321	4658	9.567	184.6		
	0.600	18-100	200A	641.8(7485	1 3043	20 607												~
	0.600	16-434	2842	422 71	7401	1.6405	20.071	2540						- -					
	IND TUNNE		3	0 0	1473	1.2405	20.04/	2250	0.386	9/7	2.074	0.10570	25.234	0.9321	4690	1.006	185.9		
			2004	641.8(7:05	1 3043	30 400	3501											
	0.000	75.0477 A ZON	100	-25 16	1001	1.2004	20+090	2240											
	PIKE TIP	N.C.	4	0 0	933	1.3460	28.897	967	0.022	5853	1.819	0.10660	25.451	0.9321	4697	9.646	184.5		
	0.600	18.100		641.8(7485	1 20-3	20 007	15.04	_										
	0.600	16.402	28/11	13.464	740)	1.2702	20.09/	2540											
	NLET THPO	TO TO	5	0 4	/47)	1.2902	20.04/	2214	0.392	987	2.074	0.10660	25.451	0.9321	4697	1.636	184.5		
			2707		77-1	4 2005													
	0.400	17 /113	1540	609.3(1301	1.2997	20.897	2501											
	VLET UPNA	110416	1244	0 3	300)	1.5458	28.897	1894	2.222	4208	1.898	0.88476	25.234	0.1114	3797	57.857	150.5		
	0.400 1	0	5		7745		20 1122												
	0.400	1/1 8/19	£171	609.3(7,00	1.2997	28.897	2501											
	NLET DANK	14.040	1490	230.01	2001	1.3492	28.897	1857	2.318	4306	1.898	0.80432	25.234	0.1225	3843	53.818	152.3		
	3.400 I	07 445	7	0 4	/-	4 2208													
	0.400 i	07.545	2441	609.3[730)	1.2997	28.897	2501											
	PRUSTOR	40+20T	2000	2/0./(7043	1.3035	28.897	2455	0.520	1276	1.940	0.80432	25.234	0.1225	3843	15.951	152.3		
	1 2 2 2 1 7 12	U		1 4															
	0.410	70.61/	2141	609.5((36)	1.2997	28.897	2501											
~ `	MBUSTOR	1 (9 4 3 6	7.330	522.01	382)	1.3458	28.897	1894	5.550	4206	1.899	0.88465	25.234	0.1114	3796	57.821	150.4		
// /	110001UN		7	~ +															
	1.310	24.140	6100	605.7(/55}	1.5000	28.697	2496											
	DABUSTOR	E0467E	1000	243.21	422)	1.5588	28.897	1972	2.005	3955	1.911	0.88623	25.234	0.1112	3678	54,470	145.8		
	, , , , , , , , , ,	U	T A														-		
	1.375	30 4033	4400	605.4((32)	1.3001	28.697	2496											
	MBUSTOR	E0.441	1044	%A0.1(425)	1.3585	28.897	1978	1.989	3935	1.912	0.88757	25.234	0.1110	3669	54.270	145.4		
	1.500 1	57 470	11	4 4															
	1 500	23.1/4	2704	604.8((32)	1.3001	28,897	2495											
	L#500 DMBUSTOR	50.461	1/20	301.86	431)	1.3373	28.897	1989	1.958	3894	914	0.88777	25.234	0.1110	, 3650	53.730	144.7		
	AG LOK	v	* *	2 2															
	2.460	22.614	2/03	599.7((27)	1.3007	28.897	2487											
	MOHOTOD	<>.<<>.	1014	328.8(458)	1.3331	28.897	2042	1,803	3681	1.922	0.87906	25.234	0.1121	3554	50.291	140.8		
	/· · · · · · · · · · · · · · · · · · ·	v		0 3							•								
	1.095	17.129	2/29	589.1(716)	1.3018	28.897	2472											
	MBUSTOR	24.041	1005	341.4(470)	1.3314	28,897	2067	1.703	3520	1.927	0.84884	25.234	0.1161	3476	46.438	137.7		
	TWDOSION	U	14	/ 5															
	4.310 1 4.310	13.050	2724	587.7(715)	1.3020	28.897	2470											
	**310	E4+141	1004	342.76	472)	1.3312	28.897	2069	1.692	3501	1.927	0.64736	25.234	0.1163	3466	46.103	137.4		
		v	• •																
	1 008-1	13.065	4/15	584.3(711)	1.3024	28.897	2466											
	1.800	24.499	1878	345.10	474)	1.3309	28.897	2073	1.669	3459	1.927	0.84406	25.234	0.1167	3446	45.378	136.5		
	11.000 1 PM	U	10	9 3															
	1.810 1	12.050	4/13	584.20	711)	1.3024	28.897	2465											
	4.810	c4.50B	10/8	345.1(474)	1.3309	28.897	2074	1.668	3458	1.927	0.84407	25.234	0.1167	3445	45.367	136-5		
	11.0001011	v	4 7	40 CI											- · ·				
	250	02.863	2663	601:1(785)	1.3074	25.520	2604											
	0.520	26.770	2027	395.9(581)	1,3292	25.520	2291	1.399	3205	2-152	0.80393	25.498	0.1238	3389	40.037	132.0	0 - 3.4 A	.07
												· -						4 4 A A	
	500	87.139	2557	601.10	752)	1.3122	25.415	2562											
46	0.260	26.796	1916	396.0(548)	1,3345	25.415	2237	1,432	3203	2.137	0.80344	25.498	0.1239	3380	30.002	132.0	0.3/6.0	. 64
										/ =					2209		7	v s _3 ↔ ()	

t = 284.74 sec.

RAMJET PERFURMANCE

ENGINE PERFORMANCE	INLET
CALCULATED THRUST	ANGLE OF ATTACK
REGENERATIVE DOOLED ENGINE PERFORMANCE CALCULATED	INCET PROCESS EFFICIENCY - SUBSONIC 0.9008 KINETIC ENERGY EFFICIENCY - SUPERSONIC 0.8953
STREAM THRUST:	KINETIC ENERGY EFFICIENCY - SUBSONIC 0.6592 ENTHALPY AT PO - SUBSONIC 0.24 (BTU/LBM) ENTHALPY AT PO - SUBSONIC 24.75 (BTU/LBM)
MOMENTUM AND FORCES	COMBUSTOR
INLET PRICTION DRAG	PUELBAIR RATIO
BROITATE	` FUEL INJECTOR8
NOMINAL CUML LEADING EDGE	INJECTURS STATION VALVE 1A 40,400 1B 41.300 1C 40.300
NOZZLE SHRQUD TRAILING EDGE	2A 46.775 D 2C 46.250 E 3A 54.065 , 3B 56.250 4 44.800

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ORIGINAL PAGE

	XABS	P=18	P=OB	PBA	60x	UmIR	Q≂0B	CAMALL	Pale/PSU	F-18/PT0	P#067P\$0	P#08/PT0
	6.505E 01	1 897E 01	1.8356 01			2.462F (3 #2.117E 03	4.337E 03	5.040E 01	2.553E+02	4.673E 01	2.469E-02
	6.509E 01	1 897E 01	1.843E 01				3 =2.120E 03	4.342E 03	5.040E 01	2.553E002	4.895E 01	2.480E-U2
	6.529E 01	1 8116 01	1.685E 01				3 02.131E 03	4,368€ 03	4.B11t 01	2,437e~02	5.0078 01	2.5366002
*	6.695E 01	1.096E 01	8.630E 00				3 -2.217E 03	4.563E 03	2.911E 01	1.4756002	5.545E 01	1.1616002
	6.762E 01	7.933E 00	8.715E 00				3 -2.247E 03	4.6656 03	2,107E G1	1.067E=02	2.315E 01	1.1736=02
G	6.839E 01	4.455E 00	6.723E 00				3 -2.282E 03	4,760E U3	1.183E 01	5.994E=0,3	1.780E Q1	9.045E>03
-	6.911E 01	3.499E 00	4.860E 00	1.128E 03	94.956E 03	39E6.50	03 #2.317E 03	4.848E 03	9.295E 00	4.708£# 03	1a291E 01	6.5398=03
	0.972E 01	2.690E 00	4.062E 00	1.209E 03	04,998F 03	42.652E	03 =2.346E 03	4.922E 03	7.145E 00	3.619E=03	1.079E 01	5.466E003
	7,067E 01	2.108E 00	2.820E 00	1.301E 03	-5,054E 03	3866.5 P	03 a2.386E 03	5.036E 03	5.600E 00	2,8376003	7.490E 00	1.794E=03
	7.110E 01	1 845E 00	2.627E 00	1.334E 03	≈\$.076E 03	#2.674E	03 m2.402E 03	5,088£ 03	4,900E 00	2,482E-03	6.977E 00	3.534E=03
	7.263E 01	1.695E 00	1.940E 00	1,429E 03	₩5,157E 03	3590,5≈ 8	03 ≈2,449E 03	5,273E 03	4,501E 00	2,280E003	54153E 00	2.610E=03
	7.278E 01	1.680E 00	1.702E 00	1.437E 03	-5.142E 01	5 ≈ 2,693€ (03 ¤2.449E 03	5 290E 03	4 4625 00	5.5606-03	4.520E 00	2.2096-03
	7.393E 01	1.611E 00	5.100E-01	1.481E 03	-5.168E 03	3 -2.701E (03 #2.467E 03	5,374E 03	4.280E 00	2.1686-03	1.355E 00	6.862E=04
	7.354E 01	1.611E 00	5.0366.01	1.482E 03	=5.108E 03	-2.701E	03 #2.468E 03	5,375E 03	4.279E 00	2.16BE=03	1.338E 00	6.7768=04
	7.486E 01	1.490E 00	0.000	1,515E 03	#5,214E 03	3 =2,7 <u>13</u> E (03 =2.50ēE 03		3.957E 00	2,005E-03	0 <u>,0</u> 00	0.000
	7.771E 01	2.180E 00	0.000	1,589E 03	-5.241E 01	. ≈2.735E (03 #2,506E 03	5.525E 03	5.790E 00	2,9336-03	0.000	0,000
	8.161E 01	1.500E 00	0.000	1,667E 03	-5.204E 03	3 #2.758E (03 - 2,506E 03	5,630E 03	3.984E 00	2,018E-03	0.000	0.000
	8.442E 01	1,105E 00	v • 0 <u>.</u> 00				03 ±2,506E 03	5,6846 03	2.935E 00	1.487E=03	0.000	0.000
	8.728E 01	1.575E 00	0.000				03 42.506E 03	5,707E 03	4.183E 00	2.119E-03	0.000	0.000
	8.729E 01	1.576E 00	0.000	1.728E 03	#5.319E 03	5 .02.813E (03 =2,506E 03	5.707E 03	4,186E 00	2,120E#03	0.000	0.000

XABS	Pel8	P≈0 B	PDA	rox	UPIB	<u> </u>	CANALL	P=IE/FSO	P=IB/P10	Pa08/PS0	P=G8/PT0
6.981E+01	1.040E 00	0.000	#4.406E#U1	0.000	0,000	0.000	2.470E=02	2.7628 00	1.399E=03	0.000	0.000
1.836E 01	1.040E 00	0.000	-3.463E 01	0.000	0.000	0,000	1 634E 02	2.762E 00	1.3996-03	0.000	0.000
3.070E 01	3.005E 00	0.000	-1.986E U2	0.000	0.000	04400	5.053E 02	7.981E 00	4.043E=03		•
3,908E 01	3.8321 00	0.000	=4,201E 02	0.000						0.000	0.000
3.519E 01	4.154E 00				0.000	0.000	6.804E 02	1.018E 01	5.150E-03	0.000	0.000
_ 7 . 7 . 7			S0 3988.6m	0.000	0.000	0.000	6,854E 02	1.103E 01	5,589£=03	1.477E 01	7.4836003
3,520E 01	4,171E 00		} ≈4.847E U2	0.000	0.000	0.000	6,857E 02	1.108E 01	5,612E-03	1,470E 01	7,445E=03
3.555E 01	5.175E 00) -4,973 € 02	0.000	0,000	0.000	7.209E 02	1.574E 01	6,963E=03	1.031€ 01	5.222E.03
3.586E 01	5.048E 00	2.4008 00) ≈5.183E 02	≈5.951E 0	2 95.951E	0000 0 50	7.529E 02	1.341E 01	6.792E=03	6.374E 00	3.229E=03
30606E 01	4.970E QO	3.538E 00	05.319E U2	96.018E 0	2 -6.018E	000.0 50	7.729E 02	1.320E 01		9.397E 00	4.760E=03
3.648E 01	4.158£ 00	5.987E 00	95,507E U2	96.165E 0	2 86.1656	02 0.000	8 164E 02	1.104E 01	5.595E-03	1.590E 01	8.055E=03
3.701E 01	5.170E 00	9-077F 00	95.717F 02	#6.528F 0	2025 4- 2	02 -1.683E 0	1 8 726E 02	1.373E 01			
3.732E 01	4.897E 00	1.0912 0	-5 BIDE 00	704F 0	3 -4 0300	02. #2.246E 0	1 0 04 3C 02		6.956E+03	2.411F 01	1.221E=02
3.80%E 01	4.2858 00	FRANK A	39 43EP 4E	-91145 U	5 00 4175	VC. VC.LCARE. V.	9.003E 02	1.301E 01	6.588E=03	2,89BE 01	1.468E-02
3.834E 01		104015 01	43*413C 05	aleinac o	g =0.10gF	02 -3.479E 0	1 9.834E 02	1.138E 01	5.765E003	3.853E 01	1.952E=02
	8.04ZE 00	1.0116.01	-0.053F 05	₽7,590£ 0	2 =6.697E	02 -4.024E 0	1 1.018E 03	2.136E 01	1,082E902	4.279E 01	2.1685908
3.875C 01	1.2888.01	14.107E 01	-0.234E 03	e7.559E_0	2 -7.987E	02 94.721E 0	1 1.064E QX	3.420E Q1	1.7335.02	4.083E 01	2.3722.02
3.881E 01	1.365E 01	1.787E 01	₩6.278E 02	≈7,602E 0	2 =7,119E	02 -4,832E 0	1 1.072E 03	3,626E 01	1.8376-02	4.748E 01	2.405E-02
3.901E 01	1,598E Q1	1.771E Q1	₽6.391£ 02	*7.735E 0	2 a7.218E	02 #5.166E 0	1 1.094E 03	4.244E 01	2.150E#02	4.703E 01	2.382E=02
3, <u>93</u> 2E 01	1.872E 01	1.744E 0	-6.603E 02	₹7.958E 0	2 =7.368F	.02 .m5.702E Q	1 1 130E 03		_2.519E-02_	4.6315 01	20-346E-02
3.950E 01	2.025E 01	1.310F 01	#6.734F 02	-8-088F 0	2 -7 - UARE	02 -5.997E 0	1 1,150E 03	5.378E 01	2.7255-02	1 4 4 5 5 5 6 5 6 5 6 6 6 6 6 6 6 6 6 6 6	
3.981E 01	1.804E 01	5.3000 0/	7. 4136 42	-6.330E A	2 -7 4005	02 06,5198 0	1 101306 03				1.762E>02
4.000E Q1		5-0646 00	, -7 1876 VE	~ N 670E 0	5 314044E	02 96.821E 0	1 1,1476 03	4.790E 01	2,4276002	1.408E 01	7.1316-03
4.040E 01	1 0065 01	- 460000 A	A LOTERO OF	SOSTIAL D	C 9/0/9/E	05 40.0516 0	1 1.209E 03	4.445E 01	5°5256*05	1.340E 01	6.816E=03
	1.996E 01	HODOLK OF	ALPOSTE AR	#0 0 10E 0	2 98.067E	02 a7.494E 0	1 1.256E 03	5,302E 01	2,6866-02	1,212E 01	6.137E∞03
400416 01	2.004E 01	4.5466 0(50 310E,70	≈8.825E 0	2 00.074E	02 #7.511E 0	1 1.257E 03	5,323E 01	2,6976002	1.208E 01	6.120E+03
4 4.1 2 1 5 1/2	2.239E 01	3a413E QQ)_ 98,989E_(/ <u>?</u> _	-9.7.65E.O.	2 .98.752E	02 -1.013E 0	2 1.3635 03	7.252E 01	3.673Ea02	9.066E 00	4.592E=03
4.1578 01	207835 01	3,331E 0() -8.671E 02	≈9.845E 0	2 w8.805E	02 91.000E 0	2 1.371E 0S	7.391E 01	3,744E=02	8,648E 00	4.402Ep03
4.150E 01	2.884E 01	3,9338 00	SO 35E8.80 (91.000E 0	3 #8.908E	02 -1.094E 0	2 1.3866 03	7.699E 01	3.880E002	1.044E 01	5.291E=03
4-246E Q1	2.074E.01	8.544E 00	50 38E 6.Pm	w1.136E 0	3 09.75AF	02 01.6242 0	2 _1.501E 03	5.500€ 01	2.790E002	2.269E 01	1.150E>02
4.409E 01	2.511E 01	1.640E 01	91.017E 03	e1.413F A	3 a1.130F	03 92.825E 0	2 1.699E 03	6.67UE 01	3.379E=02	4.355E 01	
4-431E 01	2.569E 01	1.8775 0	-1.027F 08	-1.452E 0	2 -1 151E	03 =3.009E 0	9 4 7755 67				5.500E=05
	_2.700E 01	3.410F A	THE AZAC AZ	-1 640E 0	5 G 1 0 1 3 1 C	03 434009E 0	2 1.725E 03	6.853E 01	3.456E+02	4.987E 01	2.526E-02
4.481E 01	2.70BE 01	2 12 42 41 41 41 41 41 41 41 41 41 41 41 41 41		TEDAXE U	3 51 1 1 405	03. e3.505E_0	2 1.765E 03	7-171E 01	3.633E-02	_6,425E_01	.1,255E-02
		# 450E 01	#1.030F 03	alebaig o	3 0101996	03 93,516E 0	2 1.786E 03	7.193E 01	3.644E#02	6.454E 01	3,2692=02
4.625E 01	3.903E 01	4.021E 01	64,743E 02	#1.6/4E 0	3 01,335E	03 -5.382E 0	8 1.963E 03	1.037E 02	5.2518-02	1.068E 02	5.410E=02
4.626E 01	3.911E 01	4+035E 01	. ≠9.736E 02	•1.876E.Ω	3 ml.336E	03 -5.397E Q	2 1.964E.03	1.039E 02.	5.242Ee02	1a071E 02	5.425E+02
4.731E 01	4,782E Q1	5.193E 01	, #8.561E 02	-2.125E 0	3 01.431E	03 *6.939E 0	2 2.094E 03	1.270E 02	6.434E-02	1.379E 02	6.986E002
4.733E 01	4.794E 01	5.220E 01	•8.537E 02	∘2.131E 0	3 m1.433E	03 m6.975E 0	2 2.097E 03	1.273E 02	6,450E+02	1.386E 02	7.023E-02
4.811E_01	5.170E_01.	. 4.17.7E. 01	87.429E_02	≈2.308E.0	3	03.08.074E Q	2 2.194E.Q3.		5.956E@02	1.109E 02	5.620E-02
4.8778-01	3.283E 01	3.2835 01	86.293E 02	-2-452P N	1 al.5586	03 -8,946E 0	2 2.277E 03	8.7198 01	4.4176002		
4.878E 01	3.269€ 01	3.2698 0	#6.276F 02	m2.AMAF O	3 ~1.5E0C	03 -8.959E 0	2 2 2 2 2 2 2 2 2 2			6.719E 01	4.417E=02
4.931E DI		2.5545 01	~ C D 7 15 ND	-2 5446 O	2 -1 VV60	0 3800.00 20	2 2,2788 03	8,6838 01	4.399E#02	6.683E 01	4.3992002
5.072E 01	2.877E 01	4.877c 04	. ሚመርቀየታው ነው። . ግር ማጀታለ ምር	- 7 UILE 4	3 4100035	O2 BASONCE A	2 2.345E 03	6.789E 01	3-4396-02	6.789E 01	3.419Ep02
5.282E 01		2 2224 VI	4 5200 of	040033E V	30101305	03 -1.119E 0	£0 3555,5	7.641E 01	3.8715-02	7.641E 01	3.871E#02
	2.227E 01	2 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	. 00,530E 01	a501A2E 0	5 mI.673E	03 -1.322E 0	3 2,789E 03	5.916E 01	2097E002	5.916E 01	2,9076002
5.3328 01	2.122E 01	delade 01	. 90 768E 00	≈3°5214E 0	3 m1,909E	03 -1.366E 0	3 2.652E 03	5.636E 01.	2.855Ep02	5.636E 01	2.855E002
5.407E 01	1.889E U1	1.889E 01	6.885E 01	n3.369E 0	3 01.960E	03 -1,429E 0	3 2.948E Q3	5.018E 01	2.542E-02	5.016E 01	2.5426.02
5.483E 01	1 0 654E 01	1.6548 01	1.375E 02	≈3.501E 0	3 ¤2.011E	03 01,490E 0	3 3,046E 03	4.3926 01	2.225E-02	4.3928 01	200325502
5.576E 01	1.514E 01	1.5148 91	2.110E 02	5.631E 0	3 m2.070E	03 -1.561E 0	3 3 164E 03	4 020E 01	2.0306-02	4.020E 01	2.0365902
5,6268 01	1,438E 01	1.438E 01	3.749E 02	≈3.694E 0	3 02.096E	03 91.598E 0	3 3.209E 03	3.819E 01	1.935E=02	3.819E 01	1,935E+02
5.631E 01	7.725E 00	1.430E 01		93.70DE 0	3 m2.008F	03 91060ZE 0	3 3.216E 03	2.052E.01	1.0396-02		
5.645E 01	.7.725E Q0	1.4082 01		93.716F 0	3 -2 1046	03 91.612E Q	1 1.31/15 07			3.797E 01	1,9235=02
5.653E 01	1.396E U1	1.396E 01	1,0305 00	-3.72SE 0	3 -0.1000	03 w1,618E 0	3 3.234E 03	2.052E 01	1.039E=02		.1.895E=02.
5,681E 01	1.354E 01	1.3548 01	/L (186 NO)		3 -3 1100	03 -1 (77E 0	3 3.245E 03	3.708E 01	1,878£=02	3.708E 01	1.8785.02
5.704E 01	1.254E 01			Patrice C	3 0601175	03 -1.637E 0	3 3.280E 03	3.596E 01	1.851E-05	3,596E 01	1.0216-03
		1.254E 01	4.2435 02	03.701E 0	i aš rseE	03 +1.653E 0	3 3.309E 03	3.332E 01	1.668E202	3,332E 01	1,688E=02
5.776E 01	9,360E 00	9.360E 00		0 3868.54	3 02.156E	03 =1.703E 0	3 3,402£ 63	2.486E Q1	1.259E-02	2.486E 01	1.259E=02
5.878£ 01	5.5501 00	5.550E 00		≈1.955E 0	3 m2.192E	03 #1.764E 0	3 3.532E 03	1.474E 01	7.467E-03	1.474E 01	7.4676003
6.0795 01	1.122E 01	1,122E 01	. 4.734£ 02	#4.132E 0	3 02.257E	03 -1.875E 0	3 3.790E U3	2.981E 01	1.510E-02	2.981E 01	1.5106002
6.221E 01	1.240E 01	1.240E 01	4.734E 02	=4.265E 0	3 -2.309E	03 m1 956E 0	3 3,9726 03	3.293E 01	1.668E-02	3.293E 01	1.668E=02
6,468E 01	1.756E 01	1.750E 01	4.734E 02	-4.554E 0	3 -2.438F	03 -2.095E 0	3 4 289E 03		2,3636=02	4.664E 01	
	_						y	Andrew At	7 01-2 2 1 F 1 C	FRANCE AT	FBSGBFAK '

GAMMA MOLAT SUNV MACH VEL S AZAC MUMIM Q IVAL PHI ETAC M/A COMBUSTOR 0 38 31 6 58.785 85.035 2990 546.4(1037) 1.2932 22.135 2947 7.0(501) 1.3482 22.136 2160 2.405 5195 2.472 0.26811 25.936 0.3777 4725 21.646 182.2 0.87 0.24 58.785 5.550 1541 COMBUSTOR u 39 32 6 60.795 49.226 3738 539.6(1315) 1.2539 22.058.3193 11.225 2721 127.0(919) 1.2921 22.873 2765 1.644 4544 2.574 0.27744 25.956 0.3650 4712 19.592 181.7 0.87 0.46 60.795 COMBUSTOR 0 40 33 4 48.440 3822 534.4(1347) 1.2485 22.956 3215 62,215 12.400 2868, 141.7(973) 1.2855 22.975 2825 1.569 4433 2.579 0.28496 25.936 0.3553 4702 19.633 181.3 0.87 0.49 0 41 34 5 62,215 COMBUSTOR 64.679 39,944 4281 524,1(1521) 1,2148 23,461 3320 64.679 17.560 3682 247.5(1279) 1.2443 23.523 3112 1.196 3720 2.616 0.27011 25.936 0.3749 4685 15.616 180.6 0.87 0.65 COMBUSTOR 0 42 35 4 65.055 36,542 4370 522,3(1555) 1,2065 23,562 3335 18,661 3885 288.6(1358) 1,2314 23,632 3172 1,077 3418 2,627 0,25111 25,936 0,4032 4683 13,339 180.5 0,87 0,69 65.055 COMBUSTOR REGEN 43 36 21 65.055 36,542 4530 611,7(1621) 1,1959 23,512 3385 12.552 3769 238.1(1312) 1.2358 23.640 3130 1.382 4324 2.647 0.25111 25.936 0.4032 4782 16.874 184.4 0.87 0.69 65.055 NOZZLE AE 44 37 87.291 36,542 4370 522.3(1531) 1.2065 23.562 3335 87.291 1.041 2097 ~421,9(675) 1.3052 23,672 2398 2.867 6874 2.627 0.05227 25.936 1.9371 6058 5.584 233.6 0.87 0.69 NOZZLE 45 38 87.291 36,542 4370 522,3(1531) 1,2065 23,562 3335 87.291 0.377 1643 0581.0(516) 1.3260 23.672 2139 3.473 7430 2.627 0.02608 25.936 3.8828 _ 6364 3.011 245.4 0.87 0.69 NOZZLE AE REGEN 46 39 87.291 36.542 4530 611.7(1621) 1.1959 23.512 3385 87.291 1.091 2241 m369.8(727) 1,2995 23,672 2473 2.834 7008 2.647 0.05227 25.936 1.9371 _ 6191 _5.693 238.7 0.87_0.69_ NOZZLE PO REGEN 47 40 87.291 36.542 4530 611.7(1621) 1.1959 23.512 3385 87.291 0.377 1742 -547.0(550) 1,3210 23,672 2198 3,464 7614 2.647 0.02521 25,936 4,0168 6526 2.983 251.6 0.67 0.69 FICTIVE COMBUSTR 67 60 65.055 197.699 5166 522.3(1862) 1.1699 24.444 3506 65.055 0.377 1504+1056.6(455) 1.3219 24.865 1993 4.462 8894 2.501 0.03584 25,936 2.8254 7442 4.954 287.0 0.87 1.00 FICTIVE NUZZLE 68 61 87.291 29.323 4309 493.8(1530) 1.2079 23.569 3314 67.291 _1.149 2216 =378,91 717) 1,3004 23,672 2460 2,696 6608 2,639 0,05227 25,936 1,9371 _ 5895 5,369 227,3 0,87 0,69 _

	READING =	9071	<u> P</u> LOLK	= 18t	tirE =	= 2/0.3	38 MAC	н 6.	U PT :	743	249	TT = 290	8.5							F
		p	Ť	۴		GAMMA	พณะพา	80kV	MACH	VEL	S	*/A	14	A/AC	41404	Q	TVAC	Рит	ETAC	
	COMBUSTOR			12 4							•	• • • •		2.71.4			# * * * #	. 31*		
	47.310	82.946	2785	594.0(849)	1.3021	24.861	5083												
	47.310	49.872	2471	487.3(7443	1.3125	24.861	2547	0.908	2311	5.516	0.75040	25.594	0.1332	3540	20.954	136.3	0.44	0.16	
	COMBUSTOR 47.335		20 222		0501	. 1050	14 4 £ 1													
	47.335	50.070	2075	595,8(745	1.3020	24.003	2694	0.000	3201	1 710	6 . # OF 1								
	COMBUSTOR	0.010	51	14 / 1	/43/	1.5124	24,004	C247	0.404	2303	6.614	0,74956	22.24"	0.1555	3542	50.858	138.4	0.44	0,16	
	48,110			586,9(9121	1.2928	25.071	2764												
	48.110	46,736	2637	468.76	7961	1.3042	25.077	2611	0.931	2431	2.238	55669.0	25.594	0.1429	3645	26,421	142.4			
									• • •			••••	0010.	* • • • • •			7.4.1.4.4	0.44	0.26	
	CUPBUSTOR	0	22	15 11														•••	.,	
	48.775	75,331	2574	604,50	887)	1,3141	21,646	2787												
	48,775 COMBUSTOR	32,027	5105	426.60	7103	1.3306	21.646	2535	1.177	2982	2.446	0.69245	25,916	0.1552	3709	30.240	143.0	0.87	0.08	
	48.785		23 2575	604.3(RA71	1 31/11	21.607	2788												
	48.785	32.693	2101	425.71	7101	1.3306	21.647	56100	1.180	2080	2.1116	0.65160	26 016	0 .654	77.4	70 347			0.40	
	COMBUSTUR	0	24	17 0	,		# T 2 O 4 1	5234	11100	E 70 9	6 5 4 4 0	4403400	634730	V . 1 2 3 4	3/11	30,267	142+1	V . O /	0 0 0 0	
	49.315	75.389	2564	600.10	883)	1.3145	21.647	2782												
	49,315	25.562	1966	374,30	660)	1,3357	21.647	2456	1.363	3346	2.445	0,60940	25.956	0.1662	3785	31.690	106.0	0.87	0.08	
	COMBUSTOR	U	63	10 5										-,,			*		.,	
	50.725	64,173	2495	569.60	1041)	1,2942	55.091	2957												
	50,725 COMBUSTOR	20.764	2485	391.9(846)	1,3115	28.042	2711	1.160	3106	3.505	0.51938	25,936	0.1950	3972	25.389	153.2	0.87	15.0	
	52,825	47 670	26	19 5		4 1746	** 70*	****												
	52,825	22.275	2708	575.7(41/11	1 2000	22 /100	3700	1 220	3034	2 5 4 4	0.0004.0	A= 014							
	COMBUSTOR	0	27	20 4	*63)	102747	669410	6174	8 6 6 7 10	3370	6.234	0.42569	25,430	0.2379	4255	23,619	163.3	0.87	0.35	
	53,325	56.297	3421	572.70	11981	1.2727	22.472	3164												
	53,325	21.220	2756	306.90	940)	1.2962	22.476	2811	1,297	3646	2.546	0.40829	25.936	0.2480	4267	23.137	145.3	0-87	0 - 3 #	
	COMBUSTOR	0	C 23	21 4										- # 5	1041		10010	•••	0 # 3 7	
	54.075	55.216	5471	568.20	12171	1.2699	22.530	3119												
	54.075	18,894		275.50	932)	1,2959	22,535	2799	1.307	3027	2,551	0,48487	25,936	0,2631	4358	22.891	168.0	0.87	0.36	
	COMBUSTOR 54.835	54.859	29		. 2.01	. 5400	22 540													
	54,635			240.40	9041	1.2982	22,545	3147	1 466	JI N D D	2 66.	0.36395	7C D24	A # 505	41.41.51.4	55 545				
	COMBUSTOR	0	30	23 4	,041	TARIOR	EW 0 % 7 T	2/03	1 4 4 2 0	4022	C + 221	0.30343	\$2.470	0.2782	4421	22,748	170.4	0.87	0.37	
	55.760	53.287	3540	558.9(12#21	1.2659	22.618	3139												
	55.760	15.136	2685	216.3(910)	1.2966	22.625	2766	1.497	4140	2.557	0.34172	25.936	0.2963	4486	21,987	173.6	0.87	n . Tô	
	COMBUSTOR	Đ		24 5									m ~ K · D •		1700	40001	11210	4.07	0 8 2 7	
	56.260	42.518	3971	.556.5(1405)	1,2389	23.054	3257												
	56.260	14.378	3187	223.0(1094)	1.2722	23.083	2955	1,582	4085	2.601	0.27530	25,936	0.3678	4648	17.478	179.2	0.87	0,52	
	COMBUSTOR 56.315			25 5	43905	. 3500														
	56.315	11.010	2641	556.2(12071	1 2044	220142	3168	4 6 7 6	# # T #	~ ~ ~									
	COMBUSTOR	0 1010	33	26 3	976)	7 6 5 700	661133	¢/30	10000	4414	6.3/3	0.27443	25.420	0 2 3 6 4 0	4651	19.103	179.3	0.87	0.42	
	56,455			555.6(1283)	1.2594	22.731	3170												
	56,455	10.904	2646	152.20	893)	1.2964	22.743	2738	1.641	4493	2.573	0.27246	25.936	0.8717	4660	19,023	179.7	0.67	0.42	
	COMBUSTOR	Û	34	27 5										42141	4000		* 1 7 8 1	V B W /	0075	
	56,535	43,245	3959	555.3(1400)	1,2397	23.045	3254												
	56,535 Curbustur	124465	3145	210.1(1078)	1.2740	23,075	2938	1.419	4156	2.599	0.27551	25.936	0.3675	4665	17.794	17908	0.87	0.52	
	56,815	42 776	497.E	28 3 554.0(. 7041	4 3400	** **													
14	56.816	13.51/	3145	198.20	1062)	1 2756	23.021	3431	1	4.136	3 601	0.27460	30 07/							
· ·	CO⊁BUSTOR	0	36	29 4			539704	E 7 6 E	19444	4550	C+34/	V = E / 400	42,470	v.3688	4000	18,009	180,5	0.87	0,52	
Ç.	57.041	45.299	5867	553.1(1365)	1.2459	22.956	3230												
	57.041	12.544	2958	175.30	1007)	1.2822	22.978	2865	1,518	4348	2,590	0.27418	25,936	0.3693	4641	18,526	180.0	0.47	0.49	
	COMBUSTOR	v	.ə (3 0 5										400.0		4	70011	7 5 Q F	4841	
	57.765	32.878	3539	550.10	1241)	1.2657	22.638	3137												
	57.765	7.300	54VB	10€ 35€	(ፎህን)	1.3051	22,045	2627	1.802	4734	2.557	0.26983	25.936	0.3/53	4716	19.050	181.8	0.87	0.40	

PAGE 1

SUMPARY REPORT

Note 1		p	т	H		GAMEA	MOLWT	50NV	MACH	VFL	5	W/A	Ħ	A/AC	MUM1	¢	IVAC	PHI	ETAC
SPIRE TIP NS 20	3	WIND TUNNEL	1														• , , •		3 .
SPIKE TIP WG 0.600 18.100 206 642.77 (767) 1.2061 28.807 2547 0.600 0.800 18.100 206 642.77 (767) 1.2061 28.807 2547 0.600 0.800 18.100 206 642.77 (767) 1.2061 28.807 2547 0.600 0.800 18.100 206 642.77 (767) 1.2061 28.008 2547 0.600 0.800 18.100 206 642.77 (767) 1.2061 28.008 2547 0.600 0.800 18.100 206 642.77 (767) 1.2061 28.007 2547 0.600 18.100 206 642.77 (767) 1.2061 28.007 2547 0.600 18.100 206 642.77 (767) 1.2061 28.007 2547 0.600 18.100 206 642.77 (767) 1.2061 28.007 2547 0.600 18.100 206 642.77 (767) 1.2061 28.007 2547 0.600 18.100 206 642.77 (767) 1.2061 28.007 2547 0.600 18.100 206 642.77 (767) 1.2061 28.007 2547 0.600 18.100 206 642.77 (767) 1.2061 28.007 2547 0.600 18.100 206 642.77 (767) 1.2061 28.007 2649 0.600 197.000 2792 607.77 7351 1.2068 28.007 2649 0.600 197.000 2792 607.77 7351 1.2068 28.007 2649 0.600 197.600 279		, 00000 143+E-							4 475	÷ (1.1.44									
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44.005 23.821 1651 337.7(467) 1.3319 28.897 2060 1.714 3530 1.925 0.84950 25.254 0.1161 3479 46.601 137.8 COMBUSTOR 0 14 7 3 44.310 116.786 2716 565.2(712) 1.3022 28.897 2467 44.310 23.940 1854 338.6(468) 1.3318 28.897 2061 1.704 3513 1.926 0.84803 25.254 0.1163 3470 46.292 137.4 COMBUSTOR 0 15 8 3 44.800 115.166 2703 581.4(709) 1.3027 28.897 2461 44.800 23.946 1852 337.9(467) 1.3318 28.897 2060 1.694 3490 1.925 0.84472 25.254 0.1167 3456 45.817 136.9 COMBUSTOR 0 16 9 3 44.810 15.157 2703 581.3(709) 1.3027 28.897 2461 44.810 25.967 1852 337.9(467) 1.3319 20.897 2060 1.694 3490 1.925 0.84473 25.254 0.1167 3456 45.814 136.8 COMBUSTOR 0 17 10 13 46.250 86.948 2591 603.9(787) 1.3113 24.644 2618 46.250 39.620 2142 454.2(658) 1.3266 24.644 2618 46.250 39.620 2142 454.2(658) 1.3266 24.644 2394 1.143 2736 2.197 0.60697 25.594 0.1238 3433 34.313 134.1 0.44 0.05 46.260 86.875 2593 603.8(788) 1.3112 24.646 2619				6 3										•	¥ - • •				
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46,260 86,875 2593 603,8(788) 1,3112 24,646 2619			20 2142	454.21	658)	1,3266	24.644	5200	1.143	2736	2.197	0.80697	25.590	0.1238	2422	30.212	184-1		1.05
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		HO, COO 39.7	10 2146	424.6(600)	1,3264	24.646	2396	1.140	2732	2.197	0.80648	25.594	0,1239	3454	34.239	134.2	0.44 0	0,05

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	RAMJET PERFORMANCE
ENGINE PERFORMANCE	The T
ENGINE PERFORMANCE	INLET
CALCULATED THRUST	
NET THRUST	ENTHALPY AT PO - SUPERSONIC
	COMBUSTOR .
MOHENTUM AND FORCES INLET FRICTION DRAG	FUEL-AIR RATIO
SHOITATS	FUEL INJECTORS
NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A 40.400 1B 41.300 1C 44.300 2A 48.775 D 2C 46.250 E 3A 54.065 3B 56.250 4 44.800

X	DORAG	CDRAG	CF	ĤС
4.041EE 01 4.137EE 01 4.137EE 01 4.137EE 01 4.137EE 01 4.246E 01 4.2409E 01 4.480EE 01 4.480EE 01 4.480EE 01 4.4877313E 01 4.8778E 01 4.8778E 01 4.8778E 01 4.8778E 01 5.0282E 01	DD RASE = 001 1.6253E = 001 1.6253E = 001 1.6253E = 001 1.6253E = 001 1.6253E = 001 1.6253E = 001 1.6253E = 001 1.62531E = 001 1.6253	24222222222222222222222222222222222222	33333333333333333333333333333333333333	22222222222222222222222222222222222222
6.529E 01 6.695E 01 6.762E 01 6.839E 01 6.911E 01 6.972E 01 7.067E 01	1.136E 00 9.845E 00 3.749E 00 4.000E 00 3.258E 00 2.445E 00 3.321E 00	3.724E 02 3.822E 02 3.860E 02 3.900E 02 3.932E 02 3.957E 02 3.990E 02	3.346E-03 3.202E-03 3.172E-03 3.106E-03 3.059E-03 3.028E-03 2.983E-03	2.727E=02 2.079E=02 1.896E=02 1.482E=02 1.219E=02 1.052E=02 8.477E=03
7.110E 01 7.263E 01 7.278E 01 7.353E 01 7.354E 01 7.486E 01 7.771E 01 8.161E 01 8.442E 01 9.728E 01	1.357E 00 4.415E 00 3.803E-01 1.599E 00 2.638E-03 9.358E-01 2.181E 00 2.344E 00 2.344E-01 4.123E-01	4.048E 022 4.048E 022 4.0568E 022 4.068E 022 4.077E 02 4.079E 02 4.132E 02 4.136E 02 4.136E 02	2.937E=03 2.937E=03 2.926E=03 2.855E=03 2.855E=03 2.855E=03 2.866E=03 2.803E=03 2.843E=03 2.844E=03	7.945E-03 6.776E-03 6.428E-03 4.528E-03 5.778E-03 7.643E-03 5.889E-03 4.515E-03 5.930E-03

		'XABS	P=18	P=08	PDA	Q0x	U⇒IB		G≂OB		CAMALL	_P=I8/PSU	P=1B/PT0	P=08/PS0	P=OB/PTO
		6.505E 01	1.894E 01	1.832E 01	4.408E 0	2 -4.626E	05 -2.501E	03 *	-2.124E (03	4.337E 03	5.025E 01	2,551E-02	4.851E 01	2,468E=02
	ယ	6.509E 01	1.894E U1	1.840E 01	4.408E 0	2 -4.651E	03 -2.504E	03 -	-2.127E (٤0	4,342E 03	5.025E 01	2.551E=02	4.883E 01	2,480E=02
-	9	6.529E 01	1.807E 01	1.882E 01	4.408E 0	2 -4.656E	03 -2.517E	03 -	-2.138E (0.3	4.368E 03	4.795E 01	2.435E-02	4.995E 01	2.536E=02
	\odot	6.695E 01	1.091E 01	8.590E 00	5.967E 0	2 =4.832E	03 -5.608E	03 +	•2.224E (03	4.583E 03	2.895E 01	1.470E=02	2.279E 01	1.157E-02
		6.762E 01	7.906E 00	8.700E 00	7.795E 0	2 -4.889E	03 -2.635E	03 -	-2.254E (03	4.665E 03	2.098E 01	1.065E+02	2.308E 01	1.172E#02
		6.839E 01	4.455E 00	6.713E 00	9.698E 0	2 =4.951E	03 -2.661E	03 -	-2.290F (03	4.760E 03	1.182E 01	6.002F-03	1.781E 01	9.044E~03
		6.911E 01	3.494E 00	4.855E 00			03 -2.681E	-			4.848E 03	9.271E 00	4.707E-03	1.288E 01	6.541E=03
		6.972E 01	2.680E 00	4.0678 00	1.175E 0	3 -5.049E	03 =2.694E	03 -	-2.355E (03	4.922E 03	7.111E 00	3.611E-03	1.079E 01	5.479E-03
		7.067E 01	2.146E 00	2.840E 00			03 -2.710E				5.036E 03	5.695E 00	2,892E#03	7.535E 00	3.826E-03
		7-110E 01	1.9055 00	2.641E 00			03 -2.716E				5.088E 03	5.054E 00	2.567E-03	7.008E 00	3.559E=03
		7.263E 01	1.746E 00	1.935E 00			03 -2,734E	• -		_	5.273E 03	4.632E 00	2.352E=03	5.134E 00	2.607E=03
		7.278E 01	1.730E 00	1.699E 00			03 -2.736E	-		_	5.290E 03	4.590E 00	2.331E-03	4.508E 00	2.289E-03
		7.353E 01	1.645E 00	5.200E-01			05 -2.743E				5.374E 03	4.365E 00	2.217E-03	1.380E 00	7.006E-04
		7.354E 01	1.645E 00	5.137E-01			03 -2.743E				5.375E 03	4.364E 00	2.216E=03	1.363E 00	6.921E-04
		7.486E 01	1.495E 00	0.000			03 -2.756E	-			5.427E 03	3.967E 00	2.014E-03	0.000	0.000
		7.771E 01	2.185E 00	0.000			03 -2.778E				5.525E 03	5.797E 00	2.944E-03	0.000	0.000
		8.161E 01	1.560E 00	0.000			03 -2.802E				5.630E 03	4.139E 00	2.1028-03	0,.000	0.000
		8.442E 01	1.105E 00	0.000			03 -2.823E				5.684E 03	2.932E 00	1.489E=03	0.000	0.000
		8.728E 01	1.595E 00	0.000			03 -2.857E	-		_	5.707E 03	4.232E 00	2.149E-03	0.000	0.000
		8-729F 01	1-596F NO	0.000	1.700F 0	3 - 5.316F	03 -2-857F	ሰኝ 🛮	.J.USQF (0.5	5_707F 03	4.235F 00	2.1505-03	0.000	ስ በበበ

				"	- ,							FAUC 4
	XABS	6-18	P=0#	PDA	x o a	Q=IB	Q=08	CAWALL	P=IB/PS0	P-18/P10	P=08/PS0	P=OB/PTO
	6.981E-01	1.040E 00	0.000	-4.409E-01	0.000	0.000	0.000		2.759E 00	1.401E-03	0.000	0.000
	1.836E 01	1.040E 00	0.000	-3.463E 01	0.000	0.000	0.000	1.634E U2	2.759E 00	1.401E-03	0.000	0.000
	3.070E 01	3.020E 00	0.000	-1.992E 02	0.000	0.000	0.000	5.053L U2	8.013E 00	4.069L-03	0.000	0.000
	3.508E 01	3.840E 00	0.000	-4.215E 02	0.000	0.000	0.000	6.804E 02	1.019E 01	5.173E=03	0.000	0.000
	3.519E 01	4.162E 00	5.568E 00	-4.860E 02	0.000	0.000	0.000	6.854E 02	1.104E 01	5.607E+03	1.477E 01	7.501E-03
	3.520E 01	4,179E 00		-4.861E 02	0.000	0.000	0.000	6.857E 02	1.109E 01	5.630E-03	1.470E 01	7.464E=03
	3.555E 01	5.180E 00	3.911E 00	-4.987E 02	0.000	0.000	0.000	7.209E 02	1.374E 01	6.979E=03	1.038E 01	5.269E=03
	3.586E 01	5.060E 00	2.450E 00	-5.197E 02	-6.056E 0	2 -6.056E	000.0 50	7.529E 02	1.542E 01	6.817E-03	6.500E 00	3.301E-03
	3.606E 01	4.985E 00	3.581E 00	-5.331E 02	-6.123E 0	2 -6.123E	000.0	7.729E 02	1.323E 01	6.716E-03	9.502E 00	4.825E=03
	3.648E 01	4.162E 00	6.016E 00	-5.519E 02	-6.273E 0	2 ~6.273E	02 0.000	8.164E 02	1.104E 01	5.608E-03	1.596E 01	8.105E=03
	3.701E 01 3.732E 01	5.190E 00	4.088E 00	-5.730E 02	-6.639E 0	2 -6.471E	02 -1.680E 01	8.726E 02	1.377E 01	6.992E-03	2.41TE 01	1.224E=02
	3.803E 01	4.912E 00	1.041E 01	-5.846E 02	-6.817E 0	2 -6.5928	02 -2.242E 01	9.063E 02	1.303E 01	6.618E+03	2.895E 01	1.470E=02
	3.834E 01	4.290E 00	1.4516 01	-5.988E 02	-7.227E 0	2 -6.880E	02 -3.472E 01	9.834E 02	1.138E 01	5.780E=03	3.849E 01	1.955E=02
	3.875E 01	8.049E 00 1.289E 01	1 7435 01	-0.034F 05	=7.420E 0	2 =7.018E	02 -4.016E 01	1.018E 03	2.135E 01	1.084E=02	4.275E 01	2.171E-02
	3.881E 01	1.366£ 01	1 7878 01	-4 200E VZ	-7.682E 0	2 -7.211E	02 -4.712E 01	1.064E 03	5.419E 01	1.736E-02	4.678E 01	2.375E=02
	3.901E 01	1.599E 01	1 7712 01	-6 407E 02	-7.720E U	2 -7.2445	02 -4.823E 01	1.072E 03	3.624E 01	1.840E-02	4.743E 01	2,408E=02
	3.932E 01	1.872E 01	1.7005 01	-6 440/E 02	P/ . 800E U	2 ~7.345E	02 -5.156E 01	1.094E 03	4.242E 01	2,154E-02	4.698E 01	2.386E=02
	3.950E 01	2.024E 01	1.3115 01	-6 7505 02	-8 3185 A	2 =/.01/E	02 -5.690E 01 02 -5.985E 01	1.130E 03	4.967E 01	2.522E-02	4.627E 01	2.349E#02
	3.981E 01	1.802E 01	5.325F 00	-7-028E 02	-8.45ZE 0	2 -7 9175	02 -6.506E 01	1.150E 03	5.369E 01	2.727E-02	3.478E 01	1.766E=02
	4.000E 01	1.672E 01	5-091F 00	-7. 199E 02	-8.41/E 0	2 -4 043E	02 -6.807E 01	1.187E 03	4.781E 01	2.428E+02	1.413E 01	7.174E-03
	4.040E 01	1.9948 01	4-584E 00	47.566F 02	-8.0%FF 0	2 -6.2086	02 =7.479E 01	1.209E 03	4.4358 01	2.252E+02	1.351E 01	6.858E=03/
	4.041E 01	-2.002E 01	4.572E 00	97.575F 02	-8-964E A	2 -0.2166	02 -7.496E 01	1.256E 03	5.290E 01	2.686E+02	1.216E 01	6.176E=03,
	4.131E 01	2.727E 01	3.452E 00	-8.6008 02	-9.917F 0	2 48.904F	02 -1.013E 02	1,257E 03 1,363E 03	5.3118 01	2.697E=02	1.213E 01	6.159E=03
	4.137E 01	2.779E 01	3,350E 00	-8.682E 02	-9-998E 0	2 -8-958E	02 -1.040E 02	1.371E 03	7.235E 01 7.374E 01	3.674E=02	9.107E 00	4.6345-03
	4.150E 01	2.880E 01	3.952E 00	-8.843E 02	-1.016E 0	3 +9.063F	02 -1.095E 02	1.386E 03	7.641E 01	3.744E=02 3.880E=02	8.888E 00	4.513E-03
	4.246E 01	2.074E 01	8.568E 00	≈9.647E 02	-1-156E 0	3 -9.9285	02 -1-631F 02	1.501E 03	5.502E 01	2.794E=02	1.049E 01 2.273E 01	5.324E=03
	4.409E 01	2.509E 01	1.0455 01	-1,018E 03	"1.455E 0	3 -1.150E	05 =2.849F 02	1.699E 03	6.656E 01	3.380E-02	4.359E 01	1.154E=02 2.213E=02
	4.431E 01	2.560E 01	1.0005 01	-1.023E 03	~1.475E 0	3 #1.171F	03 63.035F 02	1.725E 03	6.808E 01	3.457E-02+		2.517E=02
	4-480E 01	2.696E 01	S. sore of	~1.031E 05	-1.5/3E 0	3 -1.220F	03 =3.5358 02	1.785E 03	7.154E 01	3.633E-02	6.318E 01	3.208E-02
	4.481E 01 4.625E 01	2.704E 01	2.3918 91	-1.031E 03	-1.5/5E 0	3 -1.221F	03 =3.5UAF 02	1.786E 03	7.175E 01	3.643E-02.		3.2228-02
	4.626E 01	3.875E 01	2.844F 01	-9.800E 02	-1-901E 0	3 -1.359E	03 -5.4138 02	1.963E 03	1.028E 02	5.221E-02	1.035E 02	5.253E=02
	4.731E 01	3.883E 01 4.737E 01	2.4105 01	₩9.794E 02	-1.903E 0	3 -1.360E	03 -5.428E 02	1.964E 03	1.030E 02	5.232E-02	1.037E 02	5.267E-02
	4.733E 01	4.749E 01	5 0 7 E 01	#0.690E UZ	~4.154E 0.	5 -1.457E	03 -6.967E 02	2.094E 03	1.257E 02	6.382E-02	1.329E 02	6.7485-02
	4-811E 01	5.115E 01	4.0425 01	-7 4146 02	-2.740C 0	=1.459E	03 -7.004E 02	2.097E 03	1.260E 02	6,398E-02	1.336E 02	6.7836002
	4.877E 01	3.190E 01	3-190F 01	-A 5175 A2	-2 /425 A	-1.520E	03 =8.099E 02 03 =8.970E 02	2.194E 03	1.357E 02	6.891E-02	1.072E 02	5.445E-D2
	4.878E 01	3.177E 01	3-177F 01	-6.501E 02	-E-403E 0.	7 -1 -380E	03 -8.98ZE 02	2.277E 03	8.464E 01	4.2985-02	8.464E 01	4.298E¤02
	4.931E 01	2.498E 01	2.498E 01	-5.717E 02	-2.505E 0	2 -1 6725	03 -9.629E 02	2.2/8E 03	8.430E 01	4.281E-02	8.430E 01	4.281E+02
	5.072E 01	2.844E 01	2.844E 01	+3.742F 02	-2.868F 0	3 -1.7476	03 -1.121E 03	2.345£ 03	6.629E 01	3.366E-05	6.629E 01	3,366€#02
	5.282E 01	2.227E 01	2.227E 01	-9.497E 01	-3.231F 0	5 m1 - 907E	03 ×1,324E 03	2.522E 03 2.789E 03	7.547E 01	3.832E=02	7.547E 01	3.832E-02
	5.332E 01	2.104E 01	2.104E 01	-3.866£ 01	-3.310E 0	943F	03 -1.367E 03	2,652E 03	5.910E 01 5.583E 01	3.001E+02	5.910E 01	3.0D1E-02
	5.407E 01	1.877E 01	1.877E 01	3.836E 01	-3.426E 03	91.995F	03 -1.430E 03	2.948E 03	4.979E 01	2.835E+02	5.583E 01	2.835E=02
	5.483E 01	1.646E 01	1.646E 01	1.066E 02	-3.539E 0	3 -2.047E	03 w1.492F 03	3.046E 03	4.368E 01	S.218E*05	4.979E 01 4.368E 01	2.528E=02
	5.576E 01	1.508E 01	1.508E 01	1.798E 02	=3.6/UE 0:	-2.107E	03 -1.563E 03	3.164E 03	4.001E 01	2.031E=02	4.001E 01	2.218E=02 2.031E=02
	5.626E 01	1.433E 01	1.433E 01	3.423E 02	-3.733E 01	5 ⇒2.133€	03 ~1.600F 03	3.209E 03	3.802E 01	1.9316-02	3.802E 01	1.931E=02
	5.631E 01	7.650E 00	1.425E 01	3,464E 02	-3.740E 0	5 -2.135E	03 -1-604E 03	3.216E 03	2.030E 01	1.031E-02	3.780E 01	1.920E=02
	5.645E 01	7.650E 00	1.404E 01	3,556E 02	-3.756E 0	3 -2.141E	03 =1.614E 03	3.234E 03	2.030E 01	1.051E+02	3.725E 01	1.891E=02
	5.653E 01 5.681E 01	1.392E 01	1.392E 01	3.612£ 02	-3.705E 03	3 ⇒2.145£	03 -1.620F 03	3.245E 03	3.693E 01	1.875E-02	3.693E 01	1.875E=02
	5.704E 01	1.350E 01 1.252E 01	1.350€ 01	3.791E 02	-3.796E 0;	3 -2.156E	03 -1.640E 03	3.280E 03	3.582E 01	1.819E-02	3.582E 01	1.819E-02
	5.776E 01	9.390E 00	1.252E 01	3.918E 02	-5.822E 0	-2.165E	03 -1.656E 03	3.309E 03	3.322E 01	1.687E-02	3.322E 01	1.687E=02
	5.878E 01	5.587E 00	5.587E 00	4.2135 02	45.900E 0.	-2.193E	03 -1.707E 03	3.402E 03	2.491E 01	1.2656-02	2.491E Q1	1.2656-02
	6.079E 01	1.102£ 01	1.102E 01	4.300E VE	-3.99/E 0:	3925-2-6	03 -1.768E 03	3.532E 03	1.482E 01	7.528E-03	1.482E 01	7.528E-03
د	6.221E 01	1.234E 01	1.234F 01	4.4086 02	-4.1/DE 0.	-2.294E	03 -1.881F 03	3.790E 03	2.925E 01	1.485E-02	2.925E 01	1.485E-02
	6.468E 01	1.753E 01	1.753E 01	4.408E 02	=4.5/95 01	, =2,340E	03 -1.962E 03 03 -2.102E 03	3.9/24 03	3.275E 01	1.663E=02	3.275E 01	1.663E-02
ĩ				-4	- 412176 03	-c.4//E	U3 ₩4.102E U3	4.289E 03	4.651E 01 -	2.3626=02	4.651E 01	2.3626-02

A/AC MOMTH G IVAC PHI ETAC GAMMA MOLWT SONV MACH VEL S 0 38 31 6 COMBUSTOR 82.916 2971 546.6(1030) 1.2941 22.116 2940 CD 58.785 5.587 1542 14.9(502) 1.3483 22.117 2162 2.386 5158 2.473 0.26759 25.886 0.3777 4690 21.450 181.2 0.87 0.23 ₩ 58.785 COMBUSTOR 0 39 32 6 60.795 49.115 3683 539.7(1295) 1.2571 22.802 3177 11.025 2665 129.0(899) 1.2948 22.815 2742 1.653 4534 2.571 0.27690 25.886 0.3650 4678 19.509 180.7 0.87 0.45 60.795 COMBUSTOR 0 40 53 4 62.215 47.974 3784 534.6(1333) 1.2508 22.916 3205 12.344 2838 146.6(962) 1.2872 22.933 2814 1.566 4406 2.578 0.28441 25.886 0.3553 4668 19.474 180.3 0.87 0.48 62,215 COMBUSTOR 0 41 34 5 39.593 4239 524.1(1505) 1.2180 23.415 3311 64.679 17,529 3643 252.1(1265) 1.2470 23.470 3102 1.169 3689 2.615 0.26959 25.886 0.3749 4651 15.457 179.7 0.87 0.64 64.679 0 42 35 4 COMBUSTOR 65.055 36.247 4323 522.3(1537) 1.2102 23.511 3326 18,629 3840 293,1(1342) 1,2348 23.573 3163 1.071 3387 2.626 0.25063 25.886 0.4032 4649 13.192 179.6 0.87 0.67 65.055 COMBUSTOR REGEN 43 36 21 65.055 36.247 4488 612.1(1605) 1.1993 23.464 3377 34.521 4453 593.6(1591) 1.2010 23.473 3366 0.286 962 2.646 0.25063 25.886 0.4032 4339 3.746 167.6 0.87 0.67 65.055 NOZZLE AE 44 37 5 87.291 36.247 4323 522.3(1515) 1.2102 23.511 3326 1.028 2059 -411.0(662) 1.3075 23.608 2381 2.871 6836 2.626 0.05217 25.886 1.9371 6010 5.543 232.2 0.87 0.67 87.291 . 45 38 5 NOZZLE PO 36.247 43230 522.3(1515) 1.2102 23.511 3326 87.291 0.377 1610-0566.3(507) 1.3281 23.608 2126 3.471 7381.2.626 0.02630 25.886 3.8434 6309 3.016 243.7 0.67 0.67 87.291 NOZZLE AE REGEN 46 39 5 36.247 4488 612.1(1605) 1.1993 23.464 3377 87.291 1.079 2203 -359.7(714) 1.3017 23.608 2457 2.838 6973 2.646 0.05217 25.886 1.9371 6146 5.654 237.4 0.87 0.67 87.291 1 1 1 1 NOZZLE PO REGEN 47 40 "5... 87.291 36.247 4488 612.1(1605) 1.1993 23.464 3377 0.377 1715 -532.4(541) 1.3230 23.608 2186 3.462 7567 2.646 0.02541 25.886 3.9778 6472 2.988 250.0 0.87 0.67 87.291 FICTIVE COMBUSTR 67 60 0 65.055 197.281 5166 522.3(1863) 1.1698 24.443 3506 0.377 1505-1058.4(455) 1.3218 24.864 1994 4.459 8894 2.501 0.03584 25.886 2.8199 7428 4.954 286.9 0.87 1.00 65.055 FICTIVE NOZZLE 68 61 0 29.847 4267 495.7(1514) 1.2117 23.517 3306 4 87.291 1.117 2159 -375.5(698) 1.3034 23.608 2434 2.712 6602 2.636 0.05217 25.886 1.9371 5866 5.353 226.6 0.87 0.67 87.291

	READING =	0071	BLOCK	= 177	TIME =	266.73	8 MACH	4 6.0) PT =	742.	249	11 = 2916	0.0						1
		P	T	н		CAMKA	MOLWT	รถผบ	масн	VEI	s	W/A		A/AC	мтмом	Q	TVAC	рыт	ETAC
	COMBUSTOR	•		12 4		O KITTER	1102.71	JOHT	114011	V 1 6.	•	117.4	"	M/ NO	1101-111	VIII	****	1111	F120
	47.310			595.0		1.3025	24.836	2690											
	47-310	48.729	2452	485.1	(738)	1.3133	24.836	2539	0.924	2345	2.219	0.74898	25.546	0.1332	5524	21.295	137.9	0.44	0.15
	COMBUSTOR	0	50	13 2															4
	47.335	82.442	2777	594.8	(847)	1.3025	24.838	2691											
	47.335 COMBUSTOR	40.410	2450	405.01	(/39)	1.3132	24.839	2541	0.920	2337	2.219	0.74814	25,546	0.1333	3526	27.171	138.0	0.44	0.15
	48.110		21	587.8	(905)	1 2010	26 019	2754	•										
	48.110								0.944	2453	2.237	0.69790	28.546	0.1029	3423	26.602	141_A	0.00	0.25
	COMBUSTOR			15 11		1,000		4000	0 1 7 7 2	6423		010///0	624240	011467	2022	FOIGUE	14110	V 8	0 4 6.2
	48.775			605.1		1.3158	21.612	2771											
	48.775	31.901	2057	424.9	(694)	1.3327	21.612	2511	1.196	3003	2.442	0.65119	25.886	0.1552	3684	30.387	142.3	0.87	0.07
	COMBUSTOR		53																
	48.785	75.042	2558	605.0	(874)	1.3158	21.613	2771	4 400	7.0.	* " " "								
	48.785 COMBUSTOR			17		1.3361	21.613	2511	1.190	2000	2.445	0,65034	25.886	0.1554	2000	30.410	142.4	0.87	0.07
	49.315			600.8		1.3163	21.611	2765								•		•	
		24,983	1924	376.6	(646)	1.3378	21.611	2433	1.377	3350	2.440	0.60822	25.886	0.1662	3758	31.660	145.2.	0.87	0.07
	COMBUSTOR	U	25	18 5							.,,	********		*****	2.0-	,	14		***
	50.725	63.697	2956	590.2	(1026)	1.2961	22.004	2942									,,		
	50.725	28,444	2449	394.0	(833)	1.3133	22.005	2696	1.163	3134	2.500	0.51837	25.886	0.1950	3942	25.247	152.3	0.87	0.20
	COMBUSTOR 52.825	E7 090	26	19 5		4 3767	22 762	70/0					•			,	•	•	
	52.825	27.075	2684	576.2	(1157)	1.2/03	45.70K	3059	. 270	7577	2 5 7 0	0 "2"02	3E 004		4507	A7 75/	442 4		
	COMBUSTOR	0	27	20 4	(713)	1.3005	KE+303	6100	1.2/0	323/	£.230	0.42487	43.000	0.2579	4243	23.356	105.4	9.07	0+31
	53.325			573.2	(1183)	1.2749	22.430	3090											
	53.325	21.042	2719	310.2	(927)	1.2980	22.434	2797	1,297	3627	2.544	0.40750	25.886	0.2480	4255	22.972	164.4	0.87	0.33
	COMBUSTOR	0	28	21 4															
تست	54.075	54.754	3431	568.7	(1202)	1.2721	22.489	3106				_							
í 😜	54.075 COMBUSTOR	10./50	2706	279.4	(450)	1.2977	22.494	2786	1.366	3805	2.549	0.38413	25.886	0.2631	4326	22.712	167.1	0.87	0.35
¥	54.835			564.4	(1205)	1 2715	22 500	7100											
出	54.835	16.462	2638	245.3	(894)	1.2998	22.513	2752	1.452	1005	2.540	0.36325	25.886	0.2782	#TRA	22.554	140.5	0.87	0.34
ORIGINAL:	COMBUSTOR	Ö	30	23 4	• • • • •			-150	.,.,	5,15	40077	0.50565	234000	0.5105	*	26.334	10713	AFOL	0.530
<u> </u>	55.760	52.765	3504	559.3	(1228)	1.2679	22.581	3127							,				
	55.760	15.078	2657	221.3	(900)	1.2981	22.587	2755	1.493	4112	2.556	0.34106	25.886	0.2963	4453	21.797	172.0	0.87	0.38
Ę	COMBUSTOR		31		(4355)														
	56.260 / 56.260	14.330	2157	556.8	(1984)	1.2416	25.010	3247	. 777	(10E)	2 (6 6	0 17477	20 00/						
,	COMBUSTOR	140330	3133	25 5	(1002)	1-5/41	£3.V30	2743	1.5//	4025	2.000	0.27477	23.000	0.3678	4015	17.318	178.2	0.87	0.51
4	56.315			554.5		1.2621	22.682	3157											
}	56.315	10.949	2613	160.5	(881)	1.2982	25.695	2726	1.633	4452	2.571	0.27390	25.886	0.3690	4617	18,950	178.3	0.87	0.41
	COMBUSTOR	0	33	26 3					1									,	
	56.455	47.198	3610	555.9	(1268)	1.2616	22.691	3159											
	56.455 COMBUSTOR	10.844	2616	157.5	(882)	1.2980	22.701	2727	1.637	4465	2.572	0.27193	25.886	0.3717	4625	18.870	178.7	0.87	0.41
	56.535			27 5		1 2/127	22 002	7744											
	56.535	13.919	3112	555,6	(1066)	1 2758	23.002	2028	1 //00	#1.2k	2 506	0.27498	26 004	0 7675	11476	17 473	490 0	4 07	A E4
	COMBUSTOR	0	35	28 3	(1000)	145120	E3#460	6760	1.407	4150	2.370	V+2/470	23,000	0.30/3	4630	17.632	1/6.9	V.0/	0.51
	56.815	43.339	3909	554.4	(1381)	1.2430	22.995	3241											
	56.815	13.500	3074	203.6	(1051)	1.2773	23.020	2912	1.439	4189	2.596	0.27407	25.886	0.3688	4646	17.844	179.5	0.87	0.51
	COMBUSTOR	0	36	29 4								•							• • •
	57.041 57.041	44.800	3831	553.4	(1352)	1.2482	22.918	3221	4										
ယ	COMBILETOD	16.766	37	101.5	(448)	1.2837	ZZ.938	2056	1.511	4316	2,589	0.27365	25.886	0.3693	4657	18.353	179.9	0.87	0.48
9	E7 74F			550.3	(1232)	1.2670	22.611	3120											
Ų(57.765	9.390	2397	109.6	(802)	1.3068	22.618	2624	1.790	4696	2.556	0.26931	25.884	0.3751	4481	19.655	180.8	ሰ.ጸን	0.30
				_											4001	. / . 4		A 2 0 1	0 9 3 7

SUMMARY REPORT

Ç							- •		• •										
×	` P	T	н		GAMMA	MOLWI	SONV	MACH	VFI	s	W/A	Ħ	A/AC	HOMEM	Q	TVAC	PHI	FTAC	
	WIND TUNNEL	1	υ `` 5		Q 34444	,	00111	117.0	,	•	717.73	"	~/ ~~		•	1140	. 112	LING	
	0,000 742.249			7711	1.2959	28.698	2550												
	0.000 0.377	389	35.50	041	1.3986	24.897	SAP	6 020	SATE	1.820	0.10565	25 205	0.0316	4661	0 580	18/10			
	SPIKE TIP NS	2	0 5	777	1.3400	2010,,	700	00067	2025	11050	0.10707	20202	0.4315	4001	9.580	104.4			
			644.9(771)	1 2058	24 R07	2550												
	0.600 16.443	3853	436 11	7531	1 2070	20.077	2520		040	2 076	0 105/5	26 206	0.0345						
	WIND TUNNEL	ÉODE		1561	1.54/4	50.071	Z7Z4	0.300	490	2.0/2	0.10565	25.205	0.9315	4691	1.609	186.1			
		3014		***	4 5050	30 566	255												
	0.000 0.381	243	->>·<(94)	1.3986	26,897	969	6.018	5834	1.820	0.10646	25.400	,0.9315	4697	9.652	184.9			
	SPIKE TIP NS	4	0 0																
	0.600 18.112	2410	644.9((71)	1.2958	28.897	2550												
	0-600 16-414	2851	625.4(752)	1,2979	28.897	2523	0,392	989	2.075	0.10646	25,400	0,9315	4697	1.036	184.9			
	INLET THROAT	5	0 4													-			
	40.400 197.281	2797	609.40	736)	1.2997	28.897	2501		•	•		•							
	40.400 17.340		254.70	384)	1,3460	28.897	1892	2.227	4213	1.898	0.88373	25.205	0.1114	3795	57.859	150.6			
	INLET UPNESK	6	0 3																
	40.400 197.281	2797	609.4(736)	1.2997	28.897	2501												
	40.400 14.789	1484	238*1(367)	1.3494	28.697	1856	2,322	4310	1.898	0.80339	25.205	0.1225	3841	53.814	152.4			
	INLEY DNNRSK	7	0 4																
	40.400 107.605	2797	609.4(736)	1.2997	28.897	2501									,			
	40.400 90.580	2688	576,9(704)	1.3031	28.897	2455	0.519	1275	1.940	0.80339	25.205	0.1225	3841	15.918	152.4			
	COMBUSTOR 0	8	1 4													,			
	40.410 196.881	2797	609.4(736)	1.2997	28.897	2501												
	40.410 17.360	1547	255.D(384)	1.3459	28.897	1893	2.225	4211	1.898	0.88362	205.25	0.1114	3794	57.823	150.5			
	COMBUSTOR 0	9	2 4				-							•					
	41.310 160.585	2785	605.6(732)	1,3001	28.897	2496												
	41.310 20.109	1683	291.8(421)	1.3390	28.897	1969	2.012	3963	1.911	0.88520	25.205	0.1112	36/7	54.512	145.9			
	COMBUSTOR 0	10	34													•			
	41.375 158.432	2784	605.3(732)	1.3001	28.897	2495												
	41.375 20.369	1694	294.6(424)	1.3385	28.897	1975	1 996	3942	1.912	0.88654	25.205	0.1110	3668	54.316	145.5			
	COMBUSION 0	11	4 4						-				• • • • •						
	41.500 153.976	2781	604.6(731)	1.3002	28,897	2494												
	41.500 20.829	1714	300.2(429)	1.3376	28.697	1986	1.965	3903	1.914	0.88674	25.205	0-1110	3650	53.784	144.B			
	COMBUSTOR 0	12	5 5												244104				
	42.460 133.061	2763	599.1(726)	1.3008	28.897	2487												
	42.460 23.019	1810	320.5(456)	1.3335	28.897	2038	1.812	3693	1.922	0.87804	25.205	0-1121	3554	50.391	141.0			
	COMBUSTOR 0	13	6 3		- •			•								* - * 0 *			
	44.095 117.978	2726	588.0(715)	1.3019	28.897	2471												
	44.095 23.773	1853	338.30	4671	1.3318	28.897	2061	1.715	3534	1.926	0.84786	25,205	0-1161	3476	46-571	137.0*			
	COMBUSTOR 0	14	7 3	•		•			- -				- 4 - 4 - 4	₽∵IV					
	44.310 116.770	2720	580.4(714)	1-3021	28.897	2469												
	44.310 23.890	1856	339.20	468)	1.3317	28.897	2062	1.706	3517	1.926	0.84638	25.205	0.116%	3467	46.262	137 6			
	COMBUSTOR 0	15	8 3					- •			****	200200	007102	5401	-01202	10140			
	44.800 115.099		582.5(7101	1.3025	28.897	2463												
	44.800 23.928	1854	338.66	4681	1.3318	28.897	2061	1.405	3/19/1	1.026	0.84308	26 265	0 1167	3/150	AE 776	137 A			
	COMBUSTOR 0	16	9 3	,	.,,,,,				J 7 7 4	44720	080-200	27.203	0.1101	3432	434110	13/10			
	44.810 115.085			710)	1.3025	28.897	2461												
	44.810 23.928	1854	338-51	4681	1.3318	28.897	2061	1.605	3407	1 - 024	0.84309	25.205	0 1147	2/150	ለፍ ማካን	177 A			
	COMBUSTOR 0	17 1	10 14	0-3				* • 0 7 3	J473	7	A • O = 3 O A	¢3.503	4.110/	3436	40.112	13/00			
			604.9(7841	1.3119	24.617	261#												
	46.250 38.672	2122	452-61	6321	1 7275	24.617	>10E	1 167	2740	2.104	0.80545	25 544	0 (270	2815	28 602	170 4			
	COMBUSTOR 0	18 1	11 2	- 247		- T - U + /	-203		F100	60170	0.00342	E3034D	V . 1 & 3 O	2462	34.333	134.1	U-94 (1 0 Q 4	
			604.6(7841	1.3118	24.420	2615												
		2126	454-01	6341	1 3273	24.620	2013		275/	3 107	0.80495	10 044	0 4770		7.0 000				
	-12-7 500,00	~ · · ·	425446	-37)	. 0 7 5 1 7	L-40EV	G#01	7 4 1 33	E130	21141	0.00442	C7.740	A * 152A	3462	24,400				
								•							~ ~	مذر	0 = 44 (3.04	

Reading 71

t = 266.74 sec.

RAPJET PERFORMANCE

ENGINE PERFORMANCE	INLET
CALCULATED THRUST	ANGLE OF ATTACK
REGENERATIVE COOLED ENGINE PERFORMANCE CALCULATED STREAM THRUST	INLET PROCESS EFFICIENCY - SUPERSONIC 0.8733 INLET PROCESS EFFICIENCY - SUBSONIC 0.9000 KINETIC ENERGY EFFICIENCY - SUPERSONIC 0.8972 KINETIC ENERGY EFFICIENCY - SUBSONIC 0.8618 ENTHALPY AT PO - SUPERSONIC 1.93 (BTU/LBM) ENTHALPY AT PO - SUBSONIC 26.04 (BTU/LBM)
	COMBUSTOR
INLET FRICTION DRAG	FUELDAIR RATIO
_ STATIONS	FUEL INJECTORS
NOMINAL COML LEADING EDGE COOCCEPTOR COOCCEP	INJECTURS STATION VALVE 1A

X	DORAG	CDRAG		CF	нс
4-040E 01	1.297E 02	1.2978	02	2.3856=03	4.4/5E=0c
4.041E 01	1.6266-01	1.294E	űΖ	2.3866-03	4.417E-02
4.131E 01 4.137E 01	1.458E 01	1.445E	02 20	2,503E+03 2,512E+03	4.7/6E=02
4.150E 01	2.03RE 00	1.476E	02	2.528E=03	4.804E=02 4.847E=02
4.246E 01	1.538E 01	1.629E	05	2.573E#03	4.9145.02
4.409E 01 4.431E 01	2.564E 01 3.306E 00	1.886E 1.919E	05 05	2.520t=03 2.501E=03	4.621E=02 4.5/9E=02
4.480E 01	7.6485 00	1.995E	05	2.5766-03	6.110E=02
4.481E 01	1.503E=01	1,9978	05	2,4556-03	4.4/8E=02
4.625E 01 4.626E 01	1.938E 01	2.191E 2.192E	05 20	3.452E=03 2.894E=03	5.7515m02 7.045E=02
4.731E 01	7.852E 00	2.270E	02	2.950E+03	6.442E=02
4.733E 01 4.811E 01	1.609E#01 5.100E 00	2.272E	0.5	2.927E=03	6:492E=02
4.8775 01	5.5986 00	2.379E	02 20	2.814E=03 3.368E=03	6.952E#02 5.972E#02
4 878E 01	9.532E=02	_2.380E	22	2.915E903	7.031E=02
4.931E 01 5.072E 01	4.856E 00 1.392E 01	2.428E 2.567E	02 02	2.814E#03 2.758E#03	6.980E#02 5.906E#02
5.282E 01	8.073E 01	2.775	02	2.796E=03	5.009E=02
5.332E 01	4.796E 00	2.8235	50	2.966E-03	4.624E=02
5.407E 01 5.483E 01	7.253E 00 7.274E 00	2.895E	2.0 2.0	2.969E+03 2.957E+03	4.306E+02 5.909E+02
5,576E 01	8.636E 00	3.054E	ŠŠ	2.933E=03	3.7/56=02
5.636E 01	2.860E 00 4.259E=01	3.0832	0.2	2.9158=03	3.415E-02
5.631E 01 5.645E 01	1.121 00	3.097E	20 20	3.086E#03 2.928E#03	2.013E#02
5.653E 01	6.448E#01	3.105E	02	3,285E-03	3.007E-02
5.681E Q1 5.704E 01	2,240E 00	3.127E 3.145E	05 05	3.079E=03	3.137Ee02
5.776E 01	5.946E 00	3,2058	30	2.9698#03	3.017E=02 2.536E=02
5.878E 01 6.079E 01	8-6315 00	3.2916	02	2.739E+03	1.876E-02
6.079E 01 6.221E 01	1.527E 01	3.444E 3.546E	02 20	2,462E=03 2,959E=03	3.436E@02 3.404E#02
6.468E 01	1.7995 01	3.726E	02	3,140E+03_	3.406Ee02
6.505E_01 6.509E_01	2.481E 00 2.556E=01	3.751E	20	3.293E=03	3-1075-02
6.529E 01	1.2998.00	3.767E	02 02	3.379E+03	3.209E=02
6.695E 01	1.113E VI	3.878E	02	3,2556-03	2.3768=02
6.762E 01 6.839E 01	4.171E 00 4.388E 00	3.920E 3.964E	02 02	3.228E@03	2.133E=02 1.640E=02
6,911E 01	3.526£ 00	3.999E	So	3.1266+03	1.3426=02
6.972E 01 7.067E 01	2.629E 00	4.0258	02	3.0976#03	1.153E=02
7.067E 01 7.110E 01	3.559E 00	4.061E 4.075E	05 05	3.057E=03 3.047E=03	9.310E=03 8.769E=03
7.263E 01	4.790E 00	4.123E	0.5	3.022E#03	7.663E+03
7.278E 01	4.159E=01	4.127E 4.145E	02	3.011E#03 2.946E#03	7.257E+03
7.354E 01	2.888E-03	4.145E	02	2.9466=03	5.139E=03 5.127E=03
7.486E 01	1.039E 00	4.155E	9.0	2.988E=03	0.759E=03
7.771E 01 8.161E 01	2.368E 00	4.179E	02 02	3.008£003 2.945£003	8.201E=03 6.413E=03
8,442E 01	1.0566 00	4.214E	0.2	2.8886#03	4.946E+03
8.728E 01 8.729E 01	4.542E=01	4.219E	05	2.9348=03	6.937Em03
	~ 0 0 0 0	400746	45	2.934E=03	6.941E#03

	RBAX	P=1B	₽ ∞ 08	PDA	Q0 x	Q=18	υ⇔D∰	CANALL	P#Ib/PSU	b=1R/b10	P#95/P\$0	P=08/P10
	6.505E 01	2.047E 01	2,0618 01	1.0021 03	#5.726E 03	-2.587E	03 =3.139E 03	4.337t 03	5,426E 01	2.757L002	5.763F 01	2.775Ep02
	6.509E 01	2.047E 01	5.099E 01	1.062£ U3	-5./32E 03	42.590E	03 =3.142E 03	4.342E 03	5.426E 01	2.757E=02	5.476E 01	2.782E+02
	6,529E 01	1.950E 01	5.035E 01	1.062E 03	□5,703E 03	>2,605E	03 #3.158E 03	4.368E 03	5.1682 01	5,6266#02	5.546k 01	2.8176-02
,	6.695E 01	1.142E, 01	9-110E 00	1.231E 03	95.478E 05	92.709È	03 m3.268E 03	4,583E 03	3,0276 01	1.5386=02	2.414E 01	1.2276.02
5	6.762E 01	8.168£ 00	8.910E 00	1.421E 03	-6.044E 03	-2.740E	03 +3,304E 03	4,665E 03	2.165E 01	1.100E=02	2.361E 01	1.2006=02
>	6.839E 01	4,430E 00	6.869E 00	1.616E 03	-6,112E 03	□2.768E	03 -3,345E 03	4,760E 03	1.174E 01	5,9645-43	10 450E 01	9,248E=03
	6.911E 01	3.456E 00	4.960E 00				03 =3.384E 03	4.848E 03	9.158E 00	4.652E003	1.315E 01	6.678E#03
	6.972E 01	2.630E 00	4.156E 00				03 03.416E 03	4,922E 03	6.970E 00	3.501€003	1.1028 01	5.596E=03
_	7.967E 01	2.138E 00	2,905E 00	1.9158 03	*6,201E 03	.2.820E	03 03,4628 03	5,036E 03	5.666E 00	2.8786003	7 a 6 9 9 £. 0 Q	3.911E-03
	7-110E 01	1.915E 00	2.733E 00				03 =3.480E 03	5.0886 03	5.075E 00	2,578E=03	7.243E 00	3.679E=03
	7.263E 01	1,760E 00	2.120E 00				03 m3.527E 03	5,273E v3	4.665£ 00	2,370t=03	5.619E 00	2,8546=03
	7.278E 01	1.745E 00	1.863E 00				03 m3.531E 03	5.290E 03	4.625E 00	2,3496=03-	4.938E 00	2.5096-03
	7.353E 01	1.7118 00	5.800Em01				03 -3.551E 03	5.374E 03	4.534E 00	2.303E=03	1.537E 00	7.809E#04
	7.354E 01	1.711E 00 -					03 =3.552E 03	5.375E 03	4.534E 00	2.303E=03	1.519E 00	7.717E=04
	7.486E 01	1,650E 00	0.000				03 =3. 593E 03	5.427E 03	4.373E 00	2,221E=03	0.000	0.000
	7.771E 01	2.155£ 00	0.000				03 #3.593E 03	5.525£ 03	5.711E 00	2,901E=03	0.000	0.000
	8.161E 01	1.565E 00	0.000				03 #3.593E 03	5.630E 03	4,148E 00	2.107E=03	0,000	0.000
	8.442E 01	1.135E 00	0.000				03 #3.593E 03	5,684E 03	3.008E 00	1.528E-03	0,000	0,000
	8.728E 01	1.760E Q0	0.000				03 -3.593E 03	5.707E 03	4.665E 00	2.370E#03	0.000	0.000
	8.729E 01	1.761E 00	0.000	2,302E 03	- 20 + 20 AE 03	∞2.976E	03 =3.593E 03	5.707E 03	4,668E 00	2.371E=03	0.000	0,000

XABS	b⇔1g	P=08	POA	COX	C+IP	ถ≖∩β	CANALL	P=16/450	f = 18/P10	P=04/P80	P=08/PT0
5.981E=01	1.040E UO	0.000	-4.412E=01	0.000	0,000	0,000	2.470E#02	2.756E 00	1.400E=03	0.000	0.000
1.836E 01	1.040E 00	0.000	●3,463E 01		0.000	0.000	1.654E U2	2.756E 00	1.400E=03	0.000	0.000
3.070E 01	3,025E 00	0.000	-1,994± V2	0.000	0.000	0.000	5.053E 02	8.017E 00	0.073E=03	0.000	0.000
3.508E 01	3.884£ 00	0,000	-4.233t u2	0.000	0.000	0.000	6.604E 02	1.029E 01	5 2296-03	0.000	0.000
3.519E 01	4.195£ 00	5.571E 00	#4.879E 02	0.000	0,000	0.000	6.854E 02	1.112E 01	5.648E-03	1.476E 01	7.5008-03
3,520E 01	4.515£ 00	5.546E 00	-4.880E 02	0.000	0.000	0.000	6.857£ 02	1.116E 01	5.6/06-03	1.470E 01	7.467E=03
3.555E 01	5.180E 00		#5.004E 02		0.000	0.000	7.209E 02	1.3738 01	6.974E=03	1.090E 01	5.535E=03
3.586E 01	5.069E 00		+5.203£ 02		2 -5.59AF	02 0.000	7.529E 02	1.343E 01	6.824E-03	7.487E 00	3.8035-03
3.606E 01	5.000E 00	3.889F 00	-5,331£ 02	-5.65/F 0	2 -5.6575	02 0.000	1.729E 02	1.325E 01	6.732£=03	1.031E 01	
3.648E 01	4.227E 00		-5,512E 02				8.164E 02	1.120E 01	5.692E=03		5.2376-03
3.701E 01	5.290E 00	9-0705 00	~5 7304 02		L 2311736	02 -1.451E 01				1.638E 01	8.3205-03
3.732E 01	5.0008 00	1.4705 61		40 1 1 2 K C V	5 00.7//E	05 -1 034E 01	8,726E 02	1.402E 01	7.122E=05	2.404E 01	1.221E=02
3.803E 01	4.350E 00	1 1/155 01	- 4 0105 03	- / (LAS A	20.070	02 =1,936E 01	9.063E 02	1.325E 01	6.732E=03	2,859E 01	1.452E-02
3.834E 01	8.073E 00	TENNOC OF		*0.0722 0	S 40.330F	02 -2.995E 01	9.8348 02	1.1538 01	5.857E=03	3,830E 01	1.946E=02
3.075E 01		1 35045 01	#0.0045 UE	#5.030E 0.	2 46,483E	02 -3.463E 01	1.018E 03	2-140E 01	1.0875-02	4.264E 01	5.166E=05
	1.287E 01	1 # / 30E VI	*0.2016 VE	67.06/E 0	#6.001E	02 -4.0696 01	1.064E 03	3.410E 01	1.7326=02	4,655E 01	2,3656=02
3.88 E 01	1.363E 01	1 . 700 0 0 1	-6.320E 02	+7.106E 0	2 =6.691E	02 -4.155E 01	1.072E 03	3.6138 01	1.835£=02	4.718E 01	2.397E=02
3.901E 01	1.594E 01	1.7005 01	*6,433E 02	₩7.227E 0	2 =6.783E	02 -4.441E 01	1.094E 03	4.225E 01	2.146E=02	4.680E 01	2.377E=02
3.932E 01	1.869E 01	1:/42E 91	*6.64%E 02	.=7.431E 0	2 -6.9426	02 -4.898E 01	1.130E 03	4.954E 01	2.517E=02	4.618E 01	2,3465-02
3.950E 01	5.055E 01	1.3156 01	. ⇔6, 775€ 02	•7.550€ 0	2 -7.035E	10 3021.8m So	1.150E 03	5.360E 01	2.723E=02	3.476E 01	1.766E=02
3,9818 01	1.800E 01	5.375E 00	• ≠7.05 2€ 02	₩7.7/1E 0	2 -7.211E	02 •5.596E 01	1.187E U3	4.770E 01	2.423E-02	1.425E 01	7.237E#03
4.000E 01	1.669E 01	5.123E 00	• -7. 222£ 02	P7.906E 0	2 97.321E	02 -5.85%E 01	1.209E 03	4.424E 01	2.247E=02	1.358E Q1	6.898£#03
4.040E 01	1.978€ 01	4,580E 00	• =7. 587£ 02	*8,213E 0	2 -7.571E	02 96.425E 01	1.256E 03	5.2426 01	2.663E=02	1.214E 01	6.167E=03
4.041E 01	1.986E 01	4.567E 00	■7.596E 02	98.221E 0	2 07.577E	02 mb.440E 01	1.257E 03	5.263E 01	2.6736.02	1.210E 01	6.148E=03
4-131E 01	.2.681E 01	.3.345E 00	-8.607E 02	. #9.074E Q	3205.80	02 98.688E 01	1.363E 03	7.105E 01	3.6095.02	8 864E QO	4.503Ee03
4-137E 01	2.731E 01	3.256E 00	48.688£ 02	99.146E 0	8 254F	02 -6,919E 01	1.371E 03	7.238E 01	3.677E=02	8.6302 00	4.3845.03
4.150E 01	2.827E 01	5.227E 00	98.841E 02	99.288E 0	2 64.3506	02 -9.385E 01	1.3866 03	7.494E 01	3.807E-02	1.385E 01	7.038E+03
4.246E 01	2.066E 01	2.434E 01	#9.323E 02	#1.055E 0	3 e9.154F	02 #1.396E 02	1.501E 03	5.476E 01	2.7826 = 02	5.392E 01	2.739E=02
4.409E 01	4.374E 01	4.608F 01	#8.934F 02	m1-317F 0	3 -1.0735	03 =2.436E 02	1 5996 03	1.159E 02			
4-431E 01	4.678E 01	4.809F 01	BR 8975 02	m1.368F 0	3 ~1 0046	03 42.620E 02	1.725E 03		5.840E=02	1.221E 02	6.205E+02
4.480E 01	5.370E 01	5.265F 01	-8-830F 02	-1.4196 0	3 _ 1 1/85	03 03.305£ 02	1.785E 03	1.2408 02	6.298E=02	1.274E 02	6.4745-02
4.481E 01	5,378€ 01	5.2745 01	-8 830c va	-1.44477E 0	2 - C 6000	03 #3.383E 02		1.423E 02	7.230E=02	1.395E 02	7.088E.02
4,625E 01	6.567E 01	A-615F 01	27.7545 02	-1-976E 0	3 -1 3075	03 06.7368 02	1.784E 03	1.425E 02	7.2416.02	1-398E 02	7.101E+02
4.626E 01	6.595E 01	A.624E 01	-7 7445 AD	PARTICE O	2 0143030	03 %6.766E 02	1.963k 03	1.7468 02	8.868E+02	1.753E 02	8.906E=U2
4.731E 01	7.476E U1	7.6025 01	-6 AZAS AZ	-3 3075 A	2 -1 0145	03 #9.866E 02	1,964E 03	1.748E 02	8.8796.02	1.756E 02	8,9196,02
4.733E 01	7.473E 01	7.4288 01	-E 000F 05	UUTE 0	3 04 1 4 4 7 2	03 #9,940E 02	2.094E 03	1.9818 02	1.007E=01	3.015E 05	1.0236=01
4.811E 01	7.365E 01	4.374E 01	-/ 7/76 OE	#6447/E U	3 41 417	03 -1.210E 03	2.097E 03	1.9816 02	1.006E=01	S.051E 05	1.027E=01
4.877E-01	5.305E 01	5-1055 01	_2 EURE 02	-2 028E 0	2 2 5 5 7 6	03 -1.210E 03	2,194E 03	1.952E Q2	9.9165.02	1.690E 02	8.584E=02
4.878E 01	5.289E 01	5.380¢ 01	-2 6246 45	-3 044E 0	2 Pla005E	03 -1.375E 03	2.2776 03	1.406E 02	7.1426-02	1.406E 02	7.1428.02
4.931E 01	4.435E 01	0 43EE 01	-1 1775 VE	-7 007E 0	5 m1 * 254E	03 =1.377E 03	2.278E 03	1,402E 02	7,120E=02	1.402E 02	7.120E#02
5.072E 01	2.957E 01	2,9578 01	. WIGHT UE	- 2 //47C A	3 41 400WE	03 -1.493E 03	2,345E 03	1.175E 02	5.970E=02	1.175E 02.	
5.282E 01	2.400E 01		. 1,5305 VE	#3.403E U	2 ×1./30E	03 -1.753E 03	S-255E 03	7.837E 01	3.981L-02	7.837E 01	3.981E=02
5.332E 01	2.349E U1	2,400g 01	4.5036 06	-3.43/E U	9 -1.40PF	03 -2.051E 03	2,789E 03	6.361E 01	3.231E=02	6.361E 01	3,231E=02
5.407E 01	2.108E 01	2.349E 01	3.16EC VE	-4,050K U	3 61.740E	03 -2.113E 03	S.852E 03	6.225E 01	3.162E=02	6.225E 01	3.162E-02
5,483E 01	T	2.108E 01	3.404F 05	=4,205E 0	3 ₩2.003E	03 =2.203E 03	2.948E 03	5.586E 01	2.838E#02	5,586E 01	2.8386=02
5.576E 01	1.8648 01	1.864E 01	0,7542 02	#4.348F 0	3 060E	£0 3885.5	3.046E 03	4.939E 01	2.509E=02	4.939E 01	2.509E002
	1.713E 01	1.7138 01	7.5048 02	#4.510E 0	3 *2.126E	03 #2.385E 03	3.164E 03	4.540E 01	2.306£=02	4.540E 01.	. 2.306E#02
5.626E 01	1.632E 01	1.632E 01	4.5146 05	*4.588E 0	3 -2.156E	03 =2.433E 03	3.209£ 03	4.324E 01	2,197E#02	4.324E 01	2.197E+02
5.631E 01	9.112E 00	1.623E 01	9.560E 02	#4.596E 0	3 +2.158E	03 #2,438E 03	3.216E 03	2,415E 01	1.227E-02	4.301E 01	2.185E#02
5.645E 01	9.112E 00	1,600E 01	9.665E Q2	□4.616E Q	3 M2.165E	03 =2.451E 03	3.254E 03	2.415E 01	1.227E-02	4.240E 01	2.154E-02
5.653E 01	1.587E 01	1.587E 01	9,729E 02	=4.627E 0	3 02.169E	03 #2.458E 03	3,245E 03	4.206E 01	2.136E=02	4.206E 01	2.136E=02
5.681E 01	1.541E 01	1.541E 01	9,933E U2	□4,666E 0.	3 -2.182E	03 #2.484E 03	3,280E 03	4.085E 01	2.0756=02	4.0858 01	2.075E-02
54704E 01	1.419E 01	1.419E 01	1.008E 03	~4.697E 0	3 p2.193E	03 #2.504E 03	3.309E 03	3.762E 01	1.9116-02	3.762E 01	1.911E=02
54/76E 01	1.029E 01	1.059E 01	1.0416 03	-4.792E 0	3 -2.225E	03 42.5678 03	3,402E 03	2.727E 01	1.385E-02	2.727E 01	1.385E-02
5.878E 01	6.037£ 00	6.037E 00	1.060E 03	-4.916E 0	\$ -2.267E	03 P2.650E 03	3.532E 03	1.600E 01	8.129E=03	1.600E 01	8 129L=03
6.079E 01	1.320E 01	1.950E 01	1.062£ 03	->.153E 0	3 -2.343L	03 -2.8108 03	3,790£ 03	3.49HE 01	1.7776-02	3.498E 01	1.777E=Q2
6.221£ 01	1.690E 01	1.690F 01	1.062E 03	-5.323E 0	3 -2.405E	03 -2.918E 03	3,972E 03	4.479E 01	2.275E=02	4.479E 01	2.2756-02
6.468E 01	5.015E 01	2.012E 01	1.062E 03	-5.066E 0	3 +2,558E	03 =3.108E 03	4,289E 03	5.332E 01	2.7096-02	5.332E 01	2.7096-02

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AZAC MUMIM 6 IVAL PHI ETAC GAMPA MOLINT SONV MACH VEL 5 #/A COMBUSTOR 0 38 31 7 1 97.965 3184 560.6(1245) 1.2868 19.799 3208 56.785 6.037 1631 -87.6(596) 1.3444 19.801 2346 2.439 5/22 2.722 0.27145 26.259 0.3777 5254 24.137 200.1 1.33 0.24 58,785 COMBUSTOR 0 39 32 6 60.795 53.404 4091 557.6(1628) 1.2348 20,601 3492 76,4(1176) 1,2769 20,637 307A 1,594 4907 2,646 0,28090 26,259 0,3650 5239 21,422 199.5 1,33 0,45 60.795 13.200 3080 COMBUSTOR 0 40 33 62.215 49.732 4384 551.2(1754) 1.2117 20.888 3556 16,900 3542 142,6(1394) 1,2509 20,462 3264 1,385 4520 2,667 0,28851 26,259 0,3553 5228 20,268 199,1 1,33 0,53 62.215 COMBUSTOR 0 41 34 4 44.403 4614 538,1(1853) 1.1886 21.134 3592 64.679 20,120 4061 216,2(1997) 1,2184 21,255 3402 1,180 4013 2,886 0,27348 26,259 0,3749 5208 17,057 198,3 1,33 0,61 64,679 COMBUSTOR 0 42 35 65.055 40.816 4676 535.8(1880) 1.1808 21.198 3599 20,543 4213 250,7(1664) 1,2049 21,330 3440 1,098 3777 2,896 0,25425 26,259 0,4032 5205 14,925 198,2 1,33 0,63 05.055 COMBUSTOR REGEN 43 36 21 65.055 40.816 4745 587.8(1912) 1.1762 21.160 3621 65.055 25.229 4372 347.1(1738) 1.1940 21.287 5492 0.994 3470 2.907 0.25425 26.259 0.4032 5231 15.711 194.2 1.33 0.63 44 37 NOZZLE AE 87.291 40,816 4676 \$35,8(1860) 1,1808 21,198 3599 87.291 1,200 2378 -607,7(864) 1,2914 21,427 2669 2,834 7565 2,896 0.05293 26,259 1,9371 6769 6,222 257,8 1,33 0,63 NOZZLE PO 45 38 40.816 4676 535.8(1860) 1.1808 21.198 3599 87.291 0.377 1817 -831.7(640) 1.3149 21,427 2355 3.513 8272 2.896 0.02382 26.259 4.3045 7168 3.062 273.0 1.33 0.63 87.291 NOZZLE AE REGEN 46 39 5 40.816 4745 587.8(1912) 1.1762 21.160 3621 87.291 1.228 2455 =575.9(895) 1.2885 21.427 2709 2.817 7631 2.907 0.05293 26.259 1.9371 6837 6.276 260.4 1.33 0.63 87.291 NOZZLE PO REGEN 47 40 5 40.816 4745 587.8(1912) 1.1762 21.160 3621 87.291 87.291 0.577 1869 =811.4(660) 1.3124 21.427 2386 3.507 8367 2.907 0.02342 26.259 4.3780 7252 3.045 276.2 1.33 0.63 FICTIVE COMBUSTR 67 60 0 65.055 194-299 5232 535.8(2125) 1.1793 21.707 3759 0.377 1447-1217.9(492) 1.3286 21.974 2086 4.491 9368 2.757 0.03473 26.259 2.9520 7931 5.056 302.0 1.33 1.00 65.055 FICTIVE NOZZLE 68 61 87.291 27-142 4605 503-7(1847) 1-1788 21-195 3569 87.291 1,452 2675 =484,0(987) 1,2806 21,427 2819 2,494 7030 2,927 0,05293 26,259 1,9371 6458 5,782 245,9 1,33 0,63

W MINUY DAVA IVAC PHI ETAC GAMMA MOLMT SONV MACH VEL S COMBUSTOR 0 19 12 21 47.310 94.114 2374 603.6(769) 1.3224 22.783 2617 47.310 75.391 2248 559.1(724) 1.3267 22.783 2551 0.586 1496 2.290 0.75463 25.738 0.1332 3768 17.540 146.4 0.67 0.00 COMBUSTOR 0 20 13 21 47.335 94.183 2300 605.40 766) 1.3227 22.777 2613 47.335 75,489 2241 558,9(722) 1,3270 22,777 2548 0,595 1491 2,289 0,75378 25,738 0,1333 3771 17,471 146,5 0,67 0,00 COMBUSTOR 0 21 14 5 48.116 90.229 2763 592.0(902) 1.3042 23.158 2781 48.110 68.705 2592 529.4(640) 1.3099 23.158 2700 0.656 1770 2.337 0.70316 25.738 0.1429 3931 19.342 152.7 0.67 0.14 COMBUSTOR 0 22 15 9 48.775 81.747 2615 642.3(1013) 1.3150 19.224 2982 48.775 53.047 2355 531.3(903) 1.3239 19.224 2840 0.830 2357 2.686 0.66059 26,259 0.1552 4032 24,198 15%,6 1.33 0.09 COMBUSTOR 0 23 16 81.670 2620 48.785 642.2(1015) 1.3148 19.229 2985 48.785 52,886 2359 530,5(905) 1.3237 19.229 2841 0.832 2365 2.687 0.65973 26.259 0.1554 4035 24.246 153.7 1.33 0.09 COMBUSTOR 0 24 17 77.943 2881 635.9(1122) 1.3026 19.436 3098 49.315 49.315 44.346 2522 480.3(968) 1.3147 19.437 2912 0.958 2790 2.722 0.61700 26.259 0.1662 4165 26.754 158.6 1.33 0.15 COMBUSTOR 0 25 18 50.725 72.582 3182 621.2(1246) 1.2882 19.699 3216 50.725 29.569 2568 360.6(990) 1.3083 19.700 2923 1.235 3611 2.758 0.52586 26.259 0.1950 4424 29.511 168.5 1.33 0.22 COMBUSTOR 0 26 19 5 52.825 64.558 3559 603.2(1404) 1.2687 20.043 3347 52.825. 244000 2864 289.0(1099) 1.2934 20.049 3031 1.308 3965 2.799 0.43100 26.259 0.2379 4698 26.556 178.9 1.33 0.31 COMBUSTOR 0 27 20 4 62.612 3660 599.3(1447) 1.2631 20.137 3378 53.325 53.325 23.487 2961 279.9(1139) 1.2885 20.146 3069 1.303 3998 2.809 0.41339 26.259 0.2480 _4755 25.684 181.1 1.33 0.33_ 954.075 54.075 0 28 21 4 61.294 3721 593.7(1472) 1.2595 20.201 3396 21.079 2959 244.1(1136) 1.2876 20.211 3061 1.366 4182 2.814 0.38967 26.259 0.2631 4834 25.328 184.1 1.33 0.35 COMBUSTOR 0 29 22 60.674 3759 588,3(1480) 1.2582 20.227 3401 54.835 54.835 18.637 2902 204.7(1111) 1.2892 20.238 3032 1.445 4381 2.816 0.36849 26.259 0.2782 4904 25.088 186.7 1.33_0.35 COMBUSTOR 0 30 23 55.760 58.834 3814 582.1(1511) 1.2536 20,304 3422 55.700 17:131 2934 176:3(1122) 1:2869 20:119 3039 1:483 4506 2:823 0:14599 26:259 0:2963 4978 24:230 189:6 1:33 0:37 COMBUSTOR 0 31 24 56.260 47,193 4290 579,1(1715) 1,2195 20,744 3541 56.260 16.316 3506 .183.6(1360) 1.2570 20.802 3245 1.371 4449 2.871 0.27874 26.259 0.3678 5168 19.271 196.8 1.53 0.49 COMBUSTOR 0 32 25 56.315 52.446 3957 578.8(1572) 1.2441 20.438 3461 56.315 12,670 2941 104,6(1122) 1.2844 20.463 3029 1.608 4870 2.843 0.27785 26.259 0.3690 5172 21.030 197.0 1.33 0.41 COMBUSTOR 0 33 26 56.455 52.291 3967 578.1(1576) 1.2435 20.448 3463 56.455 12.556 2945 101.3(1124) 1.2841 20.473 3031 1.612 4884 2.844 0.27586 26.259 0.3717 5182 20.940 197.3 1.33 0.41 COMBUSTOR 0 34 27 56.535 47.961 4280 577.6(1711) 1.2204 20.738 3539 56.535 15.869 3465 168.4(1342) 1.2590 20.795 3229 1.401 4526 2.869 0.27894 26.259 0.3675 5167 19.618 197.5 1.33 0.49 COMBUSTOR 0 35 28 3 56.815 48.517 4271 576.2(1707) 1.2212 20.732 3537 56.815 15.412 3426 154.4(1326) 1.2608 20.789 3214 1.429 4594 2.867 0.27802 26.259 0.3688 5205 19.850 198.2 1.33 0.49 COMBUSTOR 0 36 29 57.041 50.280 4177 575.0(1666) 1.2286 20.647 3515 57.041 14.194 3251 124.5(1251) 1.2695 20.692 5149 1.508 4748 2.859 0.27760 26.259 0.3693 5218 20.483 198.7 1.33 0.46 COMBUSTOR 0 37 30 59.716 3784 571.4(1498) 1.2552 20.298 3411 57.765 57.765 10.290 2581 28.1(972) 1.2993 20.312 2865 1.820 5214 2.818 0.27319 26.259 0.3753 5244 22.136 199.7 1.33 0.37

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SUMMARY REPHAT

CLS P T	н	GAMPA	WLFAL	งกะง	MACH	VEL	ş	n/A	H	A/AC	ROMIN	e	IVAC	PhI	ETAC
CO - IND TUNNEL 1	0 5	1 2040	AGA_AC	2550	•	•				•					
0.000 742.749 2917		1 3986	28.897	968	6.028	5637	1.820	0.10572	055,65	0.9314	4665	9.589	185.0		
SPIKE TIP NS - 2	0 5	• • • • •		-	•					,					
0.600 10.125 2917	545.3(771)	1,2958	28,697	2550											
0,600 16,454 2853	626,1(753)	1.2978	20.09/	2524	0,388	980	2.075	0.10572	25,220	n.9314	4694	1.011	186.1		
WIND TUNNEL 5	0 0														
0.000 /42./49 2917		1.2959	20.698	5550	6 0+4	Entr		0 10451	26 // 00	0.0314	70	6 - 50			
	#35.6(94)	1.2400	20.041	470	0.010	2032	14050	0.10021	\$2.404	6.4214	4700	9.059	10240		
SPIKE TIP NS 4 0.600 18.125 2917		1 2058	28.807	2550											
	025.8(752)	1.2979	28.897	2524	0.392	989	2.075	0.10651	25.409	0.9314	4700	1.637	185.0		
INLET THROAT 5	0 4						••••	****			,,,,,	• • • •	• • • • • •		
40.400 194.299 2809	612.7(739)	1.2993	28.897	2506											
40.400 17.610 1565		1.3449	28.897	1903	2,208	4505	1,901	0.88424	25.220	0.1114	3796	57.746	150,5		
INLET UPNRSK 6	0 3														
40,400 194.299 2809		1.2993	28.897	2506		4464			25 224		7047	CO 274	467 0		
40,400 15,011 1502	243.0(372)	1+3484	60.041	1007	2,504	4301	1,401	0,00385	42ª54n	0.1845	2043	53.734	124.4		
INLET DNNRSK / 40,400 107,581 2809	V 4	. 5001	38 HO7	ンニハム	,										
40.400 90.436 2698		1.3028	28.697	2450	0.521	1282	1.941	0.80385	25.220	0.1225	3843	16,021	152.4		
COMBUSTOR Q 8	1 4	,,,,,,,,	4440.1	4.77				,,,,,,	,, - , - , -	- 4 1 4 4 4	*	,,,,,,,	• • • • •		
40.410 193.912 2809	612,7(739)	1.2993	28,897	2506											
40.410 17.630 1566		1.3449	28.897	1904	5.206	4200	1,901	0.68413	25,220	0.1114	3795	57.710	150.5		
COMBUSTOR 0 9	2 4			_	•										
41.310 158.785 2797	609,3(736)	1,2997	28,897	2501											
	297:0(426)	1.5381	20.047	1480	1,947	3953	1.913	0.885/1	₹2.44¢.	0.1112	3000	54,412	147.9		
COMBUSTOR 0 10 41,375 156,702 2796	3 4 509 07 7161	1 2007	38 HQ /	2501											
	299.9(429)				1-981	2011	1.914	0.88705	25.220	0-1110	4670	54.217	145.5		
COMBUSTOR 0 11	4 4					-,			W-4				• - • •		
41.500 152,496 2794	600.5(735)	1,2998	28,897	2500											
	305:4(434)	1.3307	28.097	1997	1.951	3895	1.916	0.08726	25.220	0.1110	3653	53.700	144.8		
COMBUSTOR 0 12	5 3														
42,460 138,441 2778						70/-		a 47654	25 220		25.00	E . 778			
42,460 22,366 1790 COMBUSTOR 0 13	320.9(450) 6 8	1.3343	60.041	2421	1,000	3760	1.451	U . 0 / 0 3 4	23,240	0.1121	2707	51.338	142.3		
44.095 140.854 2743	-	1 3014	28.897	2418											
	301.0(430)				1.923	3823	1.916	0.84835	25.220	0-1161	3603	50.406	142.9		
COMBUSTOR 0 14	7 9	• •		•								•			
44,310 141,430 2737	591.5(719)	1.5016	28.897	2476											
	298,4(428)	1.3379	26.897	1983	1,931	3829	1.915	0.84687	25,220	0.1163	3603	50.396	142.9		
COMBUSTOR 0 15	8 21	. 7034	34. 00B												
44.800 142.676 2721					1 050	70/16		A 081E2	36 230	6	141.3	E (2 11 /s			
COMBUSTOR 0 16	292.0(421) 9 13	1.3340	20.041	1410	11730	3040	1.712	V # 0 4 3 3 /	23.220	0.1101	3005	50.344	146.0		
44.810 142.913 2721		1.3021	28.897	2469											
	591.6(421)				1.951	3642	1.912	0.84358	25.220	0.1167	3602	50.364	142.8		
	10 19		- '			-		 	•	,		,			
	620.1(801)														
	548.9(731)	1.3254	55.454	2559	0.737	1887	2.304	v.81152	25.738	0.1438	3603	23.602	140.0	0 = 67	0.05
COMBUSTUR 0 18 46,260 93,250 2465		1 4:27	ו כא נכ	3664	•										
	619.9(801) 549.1(730)				0.734	1887	2.500	0.81102	JK. 71H	h . t 270	3600	27.717	140.0	6.67	ده. ۵
-01500 001041 5501		* * * * * * * * * * * * * * * * * * * *			0 9 1 20 0	,003		ATOLINE		V4 (637	2004	29 1 2 1 2 1	* 40 6 0	A # G !	VOVE

Reading 71

t = 248.74 sec.

RAMUCT PERFORMANCE - -

دىك	KAMOET PERP	ORMANCE
384	ENGINE PERFORMANCE	INLET
	CALCULATED THRUST	ANGLE OF ATTACK
	MEASURED THRUST COEFFICIENT 0.5389	DELTA PT2
	REGENERATIVE+COOLED ENGINE PERFORMANCE CALCULATED	INLET PROCESS EFFICIENCY - SUBSONIC 0.8989 KINETIC ENERGY EFFICIENCY - SUPERSONIC 0.9035
	STREAM THRUST	KINETIC ENERGY EFFICIENCY - SUBSONIC 0.8685 ENTHALPY AT PO - SUPERSONIC
	MOMENTUM AND FORCES	COMBUSTOR
	INLET FRICTION DRAG	FUEL-AIR RATIO
	MEASURED LOAD CELL FORCE	
	STATIONS	FUEL INJECTORS
	NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A

x	DDRAG	CDRAG	CF	нс
4.040E 01	1.281E 02	1.281E 02	2.380F-03	4.485E-02
4.041E 01	1.756E-01	1.283E 02	2.666E-03	3.409E-02
4.130E 01	1.672E 01	1.450E 02	2.778E-03	4.030E-02
4.131E 01	1.754E-01	1.452E 02	2.563E-03	4.293E-02
4.138E 01	1.107E 00	1.463E 02	2.535E-03	4.370E-02
4.150E 01	2.070E 00	1.484E 02	2.547E-03	4.648E-02
4.246E 01	1.543E 01	1.638E 02	2.602E-03	5.462E-02
4.410E 01	2.222E 01	1.860E 02	2.751E-03	7.329E-02
4.431E 01	2.531E 00	1.885E 02	3.023E-03	6.616E-02
4.480E 01	5.881E 00	1.944E 02	3.035E-03	6.598E-02
4.481E 01	1.386E-01	1.946E 02	3.035E-03	6.598E-02
4.625E 01	1.736E 01	2.119E 02	3.374E-03	5.881E+02
4.626E 01	1.167E-01	2.120E 02	2.903E-03	6.996E+02
4.731E 01	1.094E 01	2.230E 02	2.850E-03	6.865E+02
4.734E 01	2.803E-01	2.233E 02	2.946E-03	6.621E+02
4.811E 01	7.928E 00	2,312E 02	2.902E-03	6.482E-02
4.878E 01	7.409E 00	2,386E 02	3.235E-03	5.383E-02
4.879E 01	1.147E-01	2,387E 02	2.841E-03	6.169E-02
4.932E 01	5.648E 00	2,444E 02	2.777E-03	5.852E-02
5.073E 01	1.432E 01	2.587E 02	2.716E-03	5.197E-02
5.283E 01	1.944E 01	2.781E 02	2.739E-03	4.441E-02
5.333E 01	4.465E 00	2.826E 02	2.904E-03	4.060E+02
5.408E 01	6.750E 00	2.895E 02	2.897E-03	3.785E-02
5.484E 01	6.720E 00	2.961E 02	2.883E-03	3.504E-02
5.576E 01	7.924E 00	3.040E 02	2.857E-03	3.314E-02
5.626E 01	2.632E 00	3.066E 02	2.837E-03	3.000E-02
5.632E 01	3.893E-01	3.070E 02	3.002E-03	2.459E-02
5.646E 01	1.020E 00	3.080E 02	2.844E-03	2.561E-02
5.654E 01	5.919E-01	3.086E 02	3.232E-03	2.602E-02
5.682E 01	2.063E 00	3.107E 02	2.995E-03	2.753E+02
5.704E 01	1.624E 00	3.123E 02	2.974E-03	2.674E-02
5.777E 01	5.330E 00	3.176E 02	2.905E-03	2.375E-02
5.879E 01	7.833E 00	3.255E 02	2.756E-03	1.637E-02
6.080E 01	1.421E 01	3.397E 02	2.373E-03	2.810E-02
6.222E 01	9.582E 00	3.493E 02	2.783E-03	2.857E-02
6.468E 01	1.642E 01	3.657E 02	3.012E-03	3.163E-02
6.506E 01	2.208E 00	3.679E 02	3.268E-03	2.882E+02
6.510E 01	2.276E+01	3.681E 02	3.361E-03	2.913E-02
6.530E 01	1.157E 00	3.693E 02	3.357E-03	2.905E-02
6,696E 01 6.763E 01 6.840E 01 6.912E 01 6.973E 01	1.008E 01 3.850E 00 4.082E 00 3.298E 00 2.463E 00	3.794E 02 3.832E 02 3.873E 02 3.906E 02 3.931E 02	3.204E-03 3.173E-03 3.105E-03 3.058E-03	2.184E=02 1.985E=02 1.529E=02 1.253E=02
7.068E 01 7.111E 01 7.264E 01	3.283E 00 1.308E 00 4.243E 00	3.963E 02 3.976E 02 4.019E 02	3.027E-03 2.976E-03 2.961E-03 2.933E-03	1.074E-02 8.280E-03 7.630E-03 6.579E-03
7.354E 01 7.354E 01 7.487E 01	3.663E-01 1.533E 00 2.515E-03 8.785E-01	4.023E 02 4.038E 02 4.038E 02 4.047E 02	2.922E-03 2.850E-03 2.849E-03 2.882E-03	6.234E-03 4.364E-03 4.353E-03 5.352E-03
7.772E 01	2.099E 00	4.068E 02	2.937E+03	7.661E-03
8.162E 01	2.289E 00	4.091E 02	2.861E-03	5.682E-03
8.443E 01	9.737E+01	4.100E 02	2.812E-03	4.689E-03
8.729E 01	4.223E-01	4.104E 02	2.856E-03	6.270E-03
8.729E 01	0.000	4.104E 02	2.856E-03	6.273E-03

	XABS	P⇒IB	P#08	PDA .	QΩX	Q+IB	Q~OB	CAWALL	P=IB/PS0	P.SIB/PTO	P-08/PS0	P-OB/PTO
دت	6.468E 01	1.844E 01	1.844E 01		-5.496E 03	-2.749E n	3 -2.747E 03	4.289E 03	4.899E 01	2.483E-02	4.899E 01	2.483E+02
- œ	6.506E 01	2.002E 01	1.932E 01				3 -2.777E 03	4.337E 03	5.320E 01	2.696E-02	5.132E 01	2.601E=02
N	6.510E 01	2.002E 01	1.941E 01				3 -2.781E 03	4.342E 03	5.320E 01	2.696E+02	5.157E 01	2.613E-02
	6.530E 01	1.906E 01	1.987E 01				3 -2.797E 03	4.368E 03	5.065E 01	2.567E-02	5.280E 01	2.676E-02
	6.696E 01	1.109E 01	8.710E 00				3 -2 918E 03	4.583E 03	2.946E 01	1.493£-02	2.314E 01	1.173E=02
		7.898E 00	8.887E 00				3 -2.963E 03	4.665E 03	2.098E 01	1.063E-02	2.361E 01	1.197E=02
	16.763E 01	4.230E 00	6.840E 00				3 -3.018E 03	4.760E 03	1.124E 01	5.695E-03	1.817E 01	9.209E=03
	6.840E 01		•				3 -3.074E 03	4.848E 03	8.807E 00	4.463E=03	1.308E 01	6.631E=03
	6.912E 01	3.315E 00	4.925E 00 4.069E 00				3 -3.122E 03	4.922E 03	6.748E 00	3.420E-03	1.081E 01	5.478E-03
	6.973E 01	2.540E 00					3 -3.189E 03	5.036E 03	4.956E 00	2.511E-03	7-266E 00	3.682E+03
	7.068E 01	1.865E 00	2.735E 00				3 -3.215E 03	5.088E 03	4.144E 00	2.100E÷03	6.788E 00	3.440E-03
	7.111E 01	1.560E 00	2.555E 00					5.273E 03	3.878E 00	1.965E-03	5.088E 00	2.578E-03
	7.264E 01	1.460E 00	1.915E 00				3 -3,281E 03		3.852E 00	1.952E=03	4.494E 00	2.278E-03
	7.279E 01	1.450E 00	1.692E 00				3 -3.285E 03	5.290E 03			1.528E 00	7.742E-04
	7.354E 01	1.392E 00	5.750E-01				3 -3,312E 03	5.374E 03	3.699E 00	1.875E-03		7.661E=04
	7.354E 01	1.392E 00	5.690E-01				3 -3.312E 03	5.375E 03	3.698E 00	1.874E-03	1.512E 00	
	7.487E 01	1.290E 00	0.000				3 ~3.366E 03	5.426E 03	3.427E 00	1.737E-03	0.000	0.000
	7.772E 01	2.100E 00	0.000				3 -3.366E 03	5.525E 03	5.579E 00	2.827E-03	0.000	0.000
	8.162E 01	1.420E 00	00000	1.736E 03	-6.329E 03	2.964E n	3 -3.366E 03	5.630E 03	3,773E 00	1.912E-03	0.000	0.000
	8.443E 01	1.110E 00	0.000	1.764E 03	-6.342E 03	-2.976E n	3 -3.366E 03	5.684E 03	2.949E 00	1.494E-03	0.000	0.000
	8.729E 01	1.640E 00	0.000	1.798E 03	#6.363E 03	72.997E √	3 -3,366E 03	5.707E 03	4.357E 00	2.208E=03	0.000	0.000
	8.729E 01	1.641E 00	0.000	1.798E 03	-6.363E 03	-2.997E 0	3 +3.366E 03	5.707E 03	4.360E 00	2.210E+03	0.000	0.000

XABS	P-18	P=OB	PDA	X00	0-1B	Q=0B	CAWALL	P-18/PS0	P-IB/PTO	P=08/PS0	P-08/PT0
									1.400E-03	0.000	0.000
6.981E-01	1.040E 00	0.000	-4.420E-01		0.000	0.000	2.470E-02	2.763E 00			
1.836E 01	1.040E 00	0.000	-3.463E 01		0.000	0.000	1.634E 02	2.763E 00	1.400E-03	0.000	0.000
3.070E 01	2.890E 00	0.000	-1.939E 02	0.000	0.000	0.000	5.053E 02	7.678E 00	3.891E+03	0.000	0.000
3.508E 01	3.899E 00	0+000	-4.139E 02		0.000	0.000	6.804E 02	1.036E 01	5.250E-03	0.000	0.000
3.519E 01	4.222E 00		-4.787E 02		0.000	0.000	6.855E 02	1.122E 01	5.684E=03	1.477E 01	7.487E-03
3.520E 01	4.239E 00		-4.788E 02		0.000	0.000	6.858E 02	1.126E 01	5,707E+03	1.470E 01	7.449E-03
3.555E 01	5.220E 00	3.864E 00	-4.918E 02	0.000	0.000	0.000	7,208E 02	1.387E 01	7.028E-03	1.027E 01	5.202E-03
3.587E 01	5.031E 00	2.350E 00	-5.131E 02	−3.9 35E 0	2 -3 .935E n	2 0.000	7.530E 02	1.336E 01	6.773E-03	6.243E 00	3.164E-03
3.606E 01	4.915E 00		-5.264E 02				7.727E 02	1.306E 01	6.617E-03	9.214E 00	4.669E+03
3.648E 01	4.239E 00		-5.458E 02				8.164E 02	1.126E 01	5.707E-03	1.567E 01	7.942E-03
								•			
3.701E 01	5.270E 00					2 -2.408E 01	8.722E 02	1.400E 01	7.095E-03	2.382E 01	1.207E#02
3.733E 01	4.938E 00	1.080E 01	L -5.804E 02	-4.606E 0	2 - 4.284E n	2 -3.220E 01	9.064E 02	1.312E 01	6.648E-03	2.869E 01	1.454E+02
3.803E 01	4.200E 00	1.447E 01	-5.944E 02	-4.969E 0	2 -4.471E c	2 -4.976E 01	9.832E 02	1.116E 01	5.655E-03	3.844E 01	1.948E-02
3.835E 01	8.005E 00		1 45.994E 02			2 -5.759E 01	1.019E 03	2.127E 01	1.078E-02	4.284E 01	2.171E-02
3,875E 01	1.285E 01					2 -6.748E 01	1.064E 03	3.413E 01	1.730E-D2	4.671E 01	2.367E+02
3.882E 01	1.365E 01										_(.
						2 -6.911E 01	1.072E 03	3.626E 01	1.838E-02	4.736E 01	2.400E-02
3,901E 01	1.597E 01					2 -7.381E 01	1.094E 03	4.243E 01	2.150E-02	4.688E 01	2.376E-02
3.933E 01	1.877E 01	1.735E 01	L ⇔6.565E 02	-5.794E 0	2 - 4.980E (2 -8.148E 01	1.130g 03	4.987E 01	2.527E+02	4.609E 01	2.336E-02
3.950E 01	2.038E 01					2 -8.562E 01	1.150E 03	5.393E 01	2.733E-02	3,487E 01	1.767E-02
3.982E 01	1.817E 01					2 +9.309E 01	1.187E 03	4.827E 01	2.446E-02	1.435E 01	7.270E-03
4.000E 01	1.694E 01										
4.040E 01						2 -9.732E 01	1.209E 03	4.500E 01	2.280E-02	1.373E 01	6.959E-03
	2.078E 01	4.0046 00	-1.0000E UZ	-0./33E U	2 -5,6625 (2 -1.071E 02	1.256E 03	5.521E 01	2.798E-02	1.239E 01	6.279E-03
4.041E 01	2.088E 01	4 651E U) - 7.542E 02	-6.743E 0	2 ~5.669E (2 -1.074E 02	1.257E 03	5.546E 01	2.811E-02	1.236E 01	6.262E-03
4.130E 01	2.945E 01	3.526E 00) - 8.632E 02	-7.903E 0	2 -6.361E (2 -1.543E 02	1.362E 03	7.823E 01	3.964E-02	9.367E 00	4.747E+03
4.131E 01	2.954E 01	3,513E 00	-8.646E 02	∵~7.919E 0	2 ⊶6.369E (2 -1.550E 02	1.363E 03	7.848E 01	3.977E+02	9.334E 00	4.730E-03
4.138E 01	3.017E 01	3.431E 00	-8.736F 02	-8.026F 0	2 -6.423E c	2 -1.603E 02	1.371E 03	8.014E 01	4.061E-02	9.116E 00	4.620E=03
4.150E 01	3.135E 01					2 -1.708E 02	1.386E 03	8.329E 01	4.221E-02	1.517E 01	7.690E-03
4.246E 01	2.659E 01					2 -2.760E 02	1.501E 03	7.063E 01	3.580E-02	6.239E 01	3.162E-02
4.410E 01	5.048E 01										
						2 -4.951E 02	1.699E 03	1.341E 02	6.797E+02	1.429E 02	7.242E-02
4.431E 01	5.360E 01	5.3432 01	1 -2009TE 05	. ***210E 0	3 49.845E	2 -5.252E 02	1.725E 03	1.424E 02	7.216E-02	1.419E 02	7.193E-02
4.480E 01	6.075E 01	5.260E 0	l -9.089E 02	-1.664E 0	3 -1. 063E (3 -6.017E 02	1.784E 03	1.614E 02	8.179E-02	1.397E 02	7.081E+02
4.481E 01	6.071E n1	5.258E 01	l - 9.097E 02	-1.668E 0	3 -1.064E (3 -6.037E 02	1.786E 03	1.613E 02	8.173E-02	1.397E 02	7.079E+02
4.625E 01	5.559E 01					3 +8.669E 02	1.963E 03	1,477E 02	7.485E-02	1.332E 02	6.751E-02
4.626E 01	5.556E 01					3 -8.689E 02	1.964E 03	1.476E 02	7.480E-02	1.332E 02	6.748E-02
4.731E 01	5.182E 01					3 -1.078E 03	2.094E 03	1.377E 02	6.977E=02	1.284E 02	6.509E-02
4.734E 01	5.185E 01	* 030E 0	1 - የያማማጨር ሀር 1ማ ልዕቴም ለጠ	- ~ F300C 0	3 -4 ACCC	3 -1.084E 03					
		440300 0.	1 -1.4461E UA	-2,559E 0	3 -1,455E (3 -1.0045 03	2.097E 03	1.377E 02	6.981E-02	1.283E 02	6.503E+02
4.811E 01	5.255E 01	4.1092 0	1 -0.433E UZ	-2.796E 0	2 -1.202F (3 -1.231E 03	2.194E 03	1.396E 02	7.075E-02	1.108E 02	5.613E-02
4.878E 01	3.599E 01	3.599E 0	l - 5,243E 02	: →3.002E 0	3 -1. 655E (3 -1.347E 03	2.277E 03	9.562E 01	4.846E-02	9.562E 01	4.846E+02
4.879E 01	3.591E 01	3.591E 01	l ~5.224E 02	: -3,005E C	3 -1.657E (3 -1.348E 03	2,278E 03	9,540E 01	4.835E-02	9.540E 01	4.835E-02
4.932E 01	3.138E 01	3.138E 01	L -4.294E 02	-3.159E 0	3 -1.726E (3 -1.433E 03	2.345E 03	8.336E 01	4.225E-02	8.336E 01	4.225E-02
5.073E 01	2.557E 01	2.557E 01	l -2.189 F 02	*3.528E (3 -1.900E /	3 -1.629E 03	2.5228 03	6.793E 01	3.442E-02	6.793E 01	3.442E-02
5.283E 01	2.111E 01	2.111E 01				3 -1.860E 03	2.789E 03	5.609E 01	2.842E=02	5.609E 01	2.842E-02
5.333E 01	2.022E 01	2.022E 01		=4.0835.0	3 -2 1765 6	3 -1.907E 03	2.852E 03	5.373E 01	2.723E-02	5.373E 01	2.723E-02
5.408E 01	1.819E 01	1.819E 01									
			1.0015 05	-4.222E (3 -2.244E (3 41.978E 03	2.948E 03	4.832E 01	2.449E-02	4.832E 01	2.449E-02
5.484E 01	1.612E 01	1.612E 01	1 2.320F 03	-4.355E (3 -2.310E (3 -2.045E 03	3.046E 03	4.284E 01	2.171E-02	4.284E 01	2.171E-02
5.576E 01	1.483E 01	1.483E 01	L 3.043E 02	! -4. 506€ (3 -2.383£ (13 -2.123E 03	3.164E 03	3.940E 01	1.997E=02	3.940E 01	1.997E-02
5.626E 01	1.413E 01	1.413E 01	L 4.707E 02	4.581E (3 -2.417E (3 -2.164E 03	3.209E 03	3.753E 01	1.902E-02	3.753E 01	1.902E-02
5.632E 01	7.912E 00	1.405E 01				3 -2.168E 03	3.216E 03	2.102E 01	1.065E-02	3.733E 01	1.892E=02
5.646E 01	7.912E 00	1.385E 01				3 -2.179E 03	3.234E 03	2.102E 01	1.065E-02	3.681E 01	1.865E-02
5.654E 01	1.374E 01	1.374E 0	4 803E 02	-4 610F C	3 -0 4335	13 -2.185E 03		3.651E 01	1.850E-02	3.651E 01	1.850E+02
5.682E 01	1.335E 01	1.335E 0	. TOTAL UZ	76UA7E (-1 4866 6	3 2 4400	10 TE . 100E US	3.245E 03				
				-4 4000	U #6.449E (3 -2.207E 03		3.547E 01	1.797E+02	3.547E 01	1.797E-02
5.704E 01	1.256E 01	1.256E 0				3 -2.225E 03	3.309E 03	3.338E 01	1.692E-02	3.338E 01	1.692E-02
5.777E 01	1.005E 01	1.005E 0				13 -2.281E 03	3.402E 03	2.670E 01	1.353E-02	2.670E 01	1.353E+02
5.879E 01	5.437E 00	5.437E 00	0 5.682E 02	4¦'889ε (3 -2.543E	3 -2.346E 03	3.532E 03	1.445E 01	7.321E-03	1.445E 01	7.321E-03
6.080E 01	1.017E 01	1.017E 0:	1 5.700E 02	-5.081E	3 -2.610E	13 -2.471E 03	3.790E 03	2.703E 01	1.370E-02	2.703E 01	1.370E-02
6,222E 01	1.271E 01	1.271E 0	1 5.700E 02	-5.222E	3 -2.654F	3 -2.568E 03	3.972E 03	3.376E 01	1.711E-02	3.376E 01	1.711E-02
l			 	· · ·							

A/AC MOMTM Q IVAC PHI ETAC GAMMA MOLWT SONV MACH VEL S W/A COMBUSTOR n 38 31 4 57.767 52.297 3578 510.5(1313) 1.2633 21.725 3216 10.050 2486 56.7(871) 1.3024 21.734 2721 1.751 4765 2.653 0.27100 26.048 0.3753 4824 20.069 185.2 1.05 0.40 57.767 COMBUSTOR 0 39 32 7 58,787 91.383-2935 506.3(1062) 1.2953 21.161 2989 5.437 1472 -59.7(499) 1.3521 21.161 2162 2.461 5322 2.549 0.26927 26.048 0.3777 4834 22.270 185.6 1.05 0.24 58.787 COMBUSTOR 0 40 33 6 54.337 3560 498,9(1305) 1.2640 21.734 3209 60.797 41.8(860) 1,3033 21.742 2706 1,767 4782 2.647 0.27864 26.048 0.3650 4823 20.709 185.2 1.05 0.40 60.797 10.175 2457 COMBUSTOR 0 41 34 49.554 3806 493.5(1402) 1.2495 21.979 3280 62.217 85.6(1012) 1.2859 21.997 2881 1.568 4518 2.670 0.28619 26.048 0.3553 4814 20.093 184.8 1.05 0.47 62.217 12.706 2855 COMBUSTOR 0 42 35 5 64.681 40.741 4287 483.0(1593) 1.2142 22.484 3393 18.441 3709 203.4(1349) 1.2430 22.544 3189 1.173 3740 2.710 0.27128 26.048 0.3749 4799 15.768 184.2 1.05 0.61 64.681 COMBUSTOR 0 43 36 4 65.657 37.366 4365 481.2(1624) 1.2067 22.569 3406 19,671 3902 248.1(1427) 1.2308 22.635 3248 1.052 3415 2.720 0.25220 26.048 0.4032 4797 13.386 184.1 1.05 0.64 65.057 COMBUSTOR REGEN 44 37 21 65.057 37,366 4572 603,5(1714) 1,1926 22,503 3471 65.057 18.147 4062 328.8(1495) 1.2193 22.610 3300 1.123 3708 2.748 0.25220 26.048 0.4032 4876 14.531 187.2 1.05 0.64 NOZZLE 45 38 5 87,293 37.366 4365 481.2(1591) 1.2067 22.569 3406 1,069 2096 -502.5(704) 1,3051 22.674 2449 2.865 7016 2.720 0.05250 26.048 1.9371 6210 5.724 238.4 1.05 0.64 87,293 46 39 NOZZLE 87.293 37.366 4365 481.2(1591) 1.2067 22.569 3406 0.376 1632 -672.3(535) 1.3265 22.674 2178 3.487 7597 2.720 0.02572 26.048 3.9545 6532 3.036 250.8 1.05 0.64 87.293 NOZZLE AE REGEN 47 40 5 87,293 37.366 4572 603.5(1714) 1.1926 22.503 3471 1.137 2285 -430.8(776) 1.2976 22.674 2550 2.821 7194 2.748 0.05250 26.048 1.9371 6388 5.870 245.3 1.05 0.64 87,293 NOZZLE PO REGEN 48 41 5 87.293 37.366 4572 603.5(1714) 1.1926 22.503 3471 0.376 1761 -625.9(581) 1.3200 22.674 2258 3.474 7843 2.748 0.02460 26.048 4.1340 6749 2.999 259.1 1.05 0.64 87.293 FICTIVE COMBUSTR 68 61 0 191,923 5246 481.2(1982) 1,1619 23.486 3592 65.057 0.376 1584-1208.5(501) 1.3152 24.004 2077 4.426 9195 2.595 0.03394 26.048 2.9963 7733 4.850 296.9 1.05 1.00 65.057 FICTIVE NOZZLE 69 62 0 27.161 4298 449.7(1596) 1.2072 22.573 3381 87,293 1.236 2290 -429.0(778) 1.2974 22.674 2552 2.598 6631 2.741 0.05250 26.048 1.9371 5982 5.410 229.6 1.05 0.64 87.293

89,671 2611 594,3(847) 1.3111 23.084 2716

85.623 2766 580.11 900) 1.3036 23.260 2776

85.547 2769 579.7(901) 1.3034 23.263 2777

45,427 3875 515,2(1431) 1,2454 21,998 3303

46.760 3814 514.0(1406) 1.2493 21.942 3286

0 37 30

GAMMA MOLWT SONV MACH VEI

W/A

52,841 2300 482.6(736) 1.3217 23.084 2559 0.924 2364 2.317 0.81137 25.742 0.1239 3568 29.806 138.6 0.65 0.09

50,085 2437 461.0(782) 1.3146 23.260 2617 0.933 2441 2.335 0.75494 25.742 0.1331 3661 28.636 142.2 0.65 0.16

50,075 2440 460,7(783) 1.3145 23.263 2618 0.932 2440 2.336 0.75388 25.742 0.1333 3662 28.590 142.3 0.65 0.16

13.350 3004 136.1(1071) 1.2802 22.020 2947 1.478 4356 2.685 0.27579 26.048 0.3688 4787 18.668 183.8 1.05 0.47

12.565 2891 116.8(1027) 1.2851 21.960 2900 1.537 4459 2.678 0.27537 26.048 0.3693 4798 19.080 184.2 1.05 0.46

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IVAC PHI ETAC

81.788 2927 569.7(955) 1.2958 23.436 2837 48.110 48,110 47.121 2576 441.2(828) 1.3076 23.436 2673 0.949 2536 2.353 0.70346 25.742 0.1429 3753 27.722 145.8 0.65 0.22 COMBUSTOR 0 23 16 77.144 2628 578.7(948) 1.3116 20.758 2873 48.777 35,994 2185 403.5(774) 1.3270 20.758 2635 1.124 2961 2.541 0.65528 26.048 0.1552 3828 30.151 147.0 1.05 0.12 48.777 COMBUSTOR 0 24 17 77,100 2629 578.6(948) 1.3115 20.760 2874 48,787 48.787 35,908 2185 402,9(774) 1.3269 20.760 2635 1.125 2965 2.541 0.65442 26.048 0.1554 3830 30.153 147.0 1.05 0.12 COMBUSTOR 0 25 18 4 74.794 2717 572.7(981) 1.3073 20.842 2911 49.317 31,379 2205 369,5(780) 1,3250 20.842 2640 1,208 3189 2.553 0.61204 26.048 0.1662 3917 30.328 150.4 1.05 0.14 49.317 COMBUSTOR 26 19 50.727 68.557 2951 558.5(1070) 1.2961 21.066 3004 25.569 2341 313.2(828) 1.3169 21.066 2697 1.299 3503 2.584 0.52163 26.048 0.1950 4113 28.399 157.9 1.05 0.21 50.727 ORIGINAL PAGE IS OF POOR QUALITY COMBUSTOR 0 27 20 5 60.560 3283 540.9(1199) 1.2797 21.391 3125 52.827 52.827 21.112 2588 254.6(918) 1.3036 21.394 2800 1.352 3785 2.622 0.42753 26.048 0.2379 4351 25.148 167.0 1.05 0.30 COMBUSTOR 0 28 21 59,043 3351 537.2(1225) 1.2762 21.459 3148 53.327 20.225 2636 241.3(936) 1.3010 21.463 2818 1.365 3848 2.629 0.41006 26.048 0.2480 4400 24.521 168.9 1.05 0.32 53.327 COMBUSTOR 0 29 22 54.077 57.862 3397 531.9(1243) 1.2737 21.512 3162 18,189 2623 211.4(930) 1.3006 21.516 2808 1.426 4004 2.634 0.38654 26.048 0.2631 4468 24.054 171.5 1.05 0.34 54.077 COMBUSTOR 0 30 23 3 54.837 57.364 3407 526.8(1246) 1.2730 21.532 3164 16.125 2565 178.8(906) 1.3024 21.537 2777 1.503 4173 2.635 0.36553 26.048 0.2782 4527 23.703 173.8 1.05 0.34 54.837 COMBUSTOR 0 31 24 55.760 55.619 3468 520.9(1270) 1.2696 21.601 3183 14.831 2586 154.8(913) 1.3007 21.606 2782 1.539 4281 2.641 0.34325 26.048 0.2963 4591 22.833 176.3 1.05 0.36 55.760 COMBUSTOR 0 32 56.262 44.078 3897 518.1(1439) 1,2439 22.013 3309 56,262 14.128 3082 160.8(1102) 1.2771 22.036 2980 1.419 4228 2.689 0.27640 26.048 0.3679 4755 18.163 182.5 1.05 0.48 COMBUSTOR 0 33 26 56.317 49.582 3585 517.8(1316) 1.2629 21.716 3220 56.317 95.7(906) 1.2994 21.725 2767 1.661 4596 2.659 0.27562 26.048 0.3690 4758 19.684 182.7 1.05 0.39 10.982 2574 COMBUSTOR 0 34 27 56.457 49.429 3593 517.0(1319) 1.2625 21.725 3222 56.457 92.8(907) 1.2992 21.734 2768 1.665 4608 2.660 0.27364 26.048 0.3717 4766 19.595 183.0 1.05 0.40 10.883 2578 COMBUSTOR 0 35 28 56.537 44.877 3885 516.6(1434) 1.2447 22.005 3305 56.537 13,742 3040 147.8(1086) 1.2788 22.027 2962 1.450 4296 2.686 0.27675 26.048 0.3675 4771 18.476 183.2 1.05 0.47 COMBUSTOR 0 36 29 3

COMBUSTOR

46.260

46.260 COMBUSTOR

47.310

47,310 COMBUSTOR

47.337

47.337

56.817

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57.043

57.043

COMBUSTOR

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0 22 15

SUMMARY REPORT

н GAMMA MOLWT SONV MACH VEL S A/AC MOMTM IVAC PHI ETAC WZA WIND TUNNEL 0 5 742.749 2910 643.1(769) 1.2961 28.898 2547 0,376 388 -35.8(93) 1,3986 28.897 966 6.032 5828 1.819 0.10573 25.230 0.9317 4661 9.577 184.7 SPIKE TIP NS 18,162 2910 643.1(769) 1.2960 28.897 2547 16.500 2846 0.600 624.0(751) 1.2981 28.897 2521 0.387 975 2.074 0.10573 25.230 0.9317 4702 1.602 186.4 WIND TUNNEL 0.000 742.749 2910 643.1(769) 1.2961 28.898 2547 0.382 390 -35.4(94) 1.3986 28.897 968 6.016 5827 1.819 0.10689 25.509 0.9317 4711 9.679 184.7 0.000 SPIKE TIP NS 18,162 2910 643.1(769) 1.2960 28.897 2547 0.600 16.458 2845 623.5(750) 1.2981 28.897 2521 0.392 988 2.074 0.10689 25.509 0.9317 4711 1.641 184.7 0.600 INLET THROAT 191.923 2821 40.400 616.4(743) 1.2989 28.897 2511 40.400 17.863 1583 264.7(394) 1.3440 28.897 1913 2.192 4195 1.903 0.88499 25.230 0.1113 3799 57.690 150.6 INLET UPNRSK 0 3 6 191,923 2821 616.4(743) 1.2989 28.897 2511 40.400 40.400 15,220 1519 247.7(377) 1,3474 28.897 1877 2,289 4295 1,903 0.80454 25.230 0,1224 3846 53,704 152.4 INLET DNNRSK 107.644 2821 616.4(743) 1.2989 28.897 2511 40.400 90.380 2709 583.1(710) 1.3025 28.897 2464 0.523 1290 1.942 0.80454 25.230 0.1224 3846 16.124 152.4 40.400 COMBUSTOR 0 в 1 21 40.410 161.025 2776 616.4(765) 1.3016 27.531 2554 12,764 1489 236.3(387) 1.3505 27.531 1906 2.289 4362 1.990 0.88833 25.329 0.1113 3798 60.212 149.9 0.13 0.07 40.410 COMBUSTOR 618.3(773) 1.3056 26.377 2580 41.302 127.068 2704 289.8(447) 1.3444 26.377 2038 1.990 4054 2.067 0.89316 25.417 0.1111 3672 56.272 144.5 0.24 0.04 16.486 1638 41.302 COMBUSTOR 0 10 3 21 41.312 132,206 2662 618.2(760) 1.3076 26.333 2563 41.312 16.528 1594 290.3(434) 1.3470 26.333 2013 2.012 4051 2.060 0.89388 25.417 0.1110 3670 56.276 144.4 0.24 0.01 COMBUSTOR 0 11 4 21 41.377 131,353 2654 617.8(758) 1.3079 26.326 2560 41.377 16,799 1598 293.5(435) 1.3469 26.326 2016 1.998 4029 2.059 0.89391 25.417 0.1110 3660 55.964 144.0 0.24 0.00 COMBUSTOR 0 12 5 21 617.0(757) 1.3080 26.325 2559 41.500 130.012 2650 306.3(448) 1.3448 26.325 2041 1.931 3943 2.060 0.89420 25.417 0.1110 3641 54.789 143.3 0.24 0.00 41,500 18.531 1641 COMBUSTOR 0 13 42.460 120,945 2626 609.3(749) 1.3088 26.325 2548 349.6(491) 1.3383 26.325 2125 1.696 3604 2.062 0.88536 25.417 0.1121 3566 49.594 140.3 0.24 0.00 42.460 25,036 1797 0 14 COMBUSTOR 592.5(904) 1.2845 26.930 2728 44.097 96,145 3139 44.097 52.136 2735 460.0(775) 1.2980 26.931 2560 1.006 2575 2.120 0.85540 25.417 0.1160 3583 34.224 141.0 0.24 0.47 COMBUSTOR 0 15 95.997 3140 590.0(905) 1.2843 26.939 2728 44.310 44.310 53,511 2753 463,1(781) 1,2973 26,940 2567 0.981 2520 2.120 0.85379 25.417 0.1162 3583 33.432 141.0 0.24 0.48 COMBUSTOR 0 16 44.800 95.668 3115 583.9(896) 1.2853 26.931 2719 56.673 2768 470.4(786) 1.2969 26.932 2574 0.926 2383 2.117 0.85039 25.417 0.1167 3577 31.498 140.7 0.24 0.47 44.800 COMBUSTOR 0 17 10 2 44.812 95.636 3114 583.8(896) 1.2853 26.930 2718 44.812 56.642 2767 470.2(785) 1.2969 26.931 2574 0.926 2383 2.117 0.85038 25.417 0.1167 3576 31.498 140.7 0.24 0.47 COMBUSTOR 0 18 11 11 46.250 89.706 2610 594.4(847) 1.3112 23.082 2715 46.250 52.867 2299 482.8(736) 1.3217 23.082 2558 0.924 2363 2.317 0.81179 25.742 0.1238 3567 29.812 138.6 0.65 0.09

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RAMJET PERFORMANCE

ယ	RAMJET PE	RFORMANCE
76	ENGINE OFFICIONANCE	INLFT
	CALCULATED THRUST	ANGLE OF ATTACK
	MEASURED THRUST COEFFICIENT	TOTAL PRESSURE RECOVERY - SUPERSONIC 0.2590 TOTAL PRESSURE RECOVERY - SUBSONIC 0.1451 INLET PROCESS EFFICIENCY - SUPERSONIC 0.8704 INLET PROCESS EFFICIENCY - SUBSONIC 0.8986 KINETIC ENERGY EFFICIENCY - SUPERSONIC 0.9052
	STREAM THRUST	KINETIC ENERGY EFFICIENCY - SUBSONIC 0.8701 ENTHALPY AT PO - SUPERSONIC
	MOMENTUM AND FORCES	COMBUSTOR
	INLET FRICTION DRAG	FUEL-AIR RATIO
	EXTERNAL FRICTION DRAG	VACUUM STREAM THRUST COEFFICIENT - C5 0.9607 NOZZLE COEFFICIENT - CT
	STATIONS	FUEL INJECTORS
	NOMINAL COWL LEADING EDGE	INJECTORS STATION VALVE 1A 40.400 A 1B 41.300 B 1C 44.360 2A 48.775 D 2C 46.250 E 3A 54.065 3B 56.250 4 44.800

x	DDRAG	CORAG	CF	нс
4.040E 01	1.279E 02	1.279E 02	2.381E-03	4.490E-02
4.041E 01	1.758E-01	1.281E 02	2.658E~03	3.407E-02
4.130E 01	1.671E 01	1.448E 02	2.779E-03	4.032E-02
4.151E 01	1.760E+01	1.450E 02	2.563E-03	4.297E-02
4.137E 01 4.150E 01	1.109E 00	1.461E 02	2.534E-03	4.377E-02
4.150E 01 4.246E 01	2.110E 00 1.556E 01	1.482E 02 1.638E 02	2.547E-03	4.638E=02
4.409E 01	2.273E 01	1.865E 02	2.601E-03 2.739E-03	5.288E=02 7.148E+02
4.431E 01	2.646E 00	1.892E 02	2.988E-03	6.519E-02
4.480E 01	6.110E 00	1.953E 02	3.001E-03	6.498E-02
4.481E 01	1.182E-01	1.954E 02	2.997E-03	6.505E-02
4.625E 01	1.847E 01	2.139E 02	3.258E-03	5,678E-02
4.626E 01	1.279E-01	2.140E 02	2.856E-03	6.556E-02
4.731E 01	1.233E 01	2.263E 02	2.784E-03	6.196E-02
4.733E 01	2.962E-01	2.266E 02	2.846E-03	6.054E-02
4.811E 01 4.877E 01	8.989E 00 7.877E 00	2.356E 02	2.804E+03	5.861E-02
4.878E 01	7.877E 00.	2.435E 02 2.436E 02	3.129E-03 2.788E-03	4.982E-02 5.594E-02
4.931E 01	5.705E 00	2.493E 02	2.7435-03	5.379E-02
5.072E 01	1.421E 01	2.635E 02	2.691E-03	4.700E-02
5.282E 01	1.916E 01	2.827E 02	2.698E-03	3.998E-02
5.332E 01	4.343E 00	2.870E 02	2.854E=03	3.714E-02
5.407E 01	6.512E 00	2.935E 02	2.861E=03	3.462E-02
5.483E 01 5.576E 01	6.456E 00	3,000E 02	2.852E-03	3.221E-02
5,626E 01	7.632E 00 2.529E 00	3.076E 02	2.829E-03 2.794E-03	3.000E=02
5.631E 01	3.735E-01	3.105E 02	2.948E-03	2.707E-02 2.200E-02
5.645E 01	9.727E-01	3.115E 02	2.775E-03	2.297E-02
5.653E 01	5.698E-01	3.121E 02	3.214E-03	2.312E-02
5.681E 01	1.995E 00	3,141E 02	2.932E-03	2.469E-02
5,704E 01	1,550E 00	3.156E 02	2.908E~03	2.437E-02
5.776E 01 5.878E 01	4.997E 00 7.413E 00	3.206E 02	2.866E-03	2.295E-02
6.079E 01	7.413E 00 1.360E 01	3.280E 02	2.792E-03 2.377E-03	1,495E+02 2,660E+02
6.221E 01	9.118E 80	3.507E 02	2.802E-03	2.649E-02
6.468E 01	1.569E 01	3.664E 02	3.015E-03	2.919E-02
6.505E 01	2,114E 00	3.685E 02	3.258E-03	2,659E-02
6.509E 01	2.184E-01	3.688E 02	3.349E-03	2,688E-02
6.529E 01	1.109E 00	3.699E 02	3.345E-03	2.681E-02
6.695E 01 6.762E 01	9.643E 00 3.683E 00	3.795E 02 3.832E 02	3.192E-03	2.035E-02
6.839E 01	3.922E 00	3.832E 02 3.871E 02	3.162E-03 3.092E-03	1.862E-02 1.442E-02
6.911E 01	3.173E 00	3.903E 02	3.041E-03	1.173E-02
6.972E 01	2.322E 00	3.926E 02	2.998E-03	9.531E-03
7.067E 01	2.854E 00	3.955E 02	2.913E-03	6.194E-03
7.110E 01	1.068E 00	3.965E 02	2.903E-03	5.903E~03
7.263E 01	3.779E 00	4.003E 02	2.911E-03	6.170E-03
7.278E 01 7.353E 01	3.521E-01 1.440E 00	4.007E 02 4.021E 02	2.899E-03	5.835E=03
7.354E 01	2.293E-03	4.021E 02	2.813E+03 2.812E-03	3.836E-03 3.825E-03
7.486E 01	7.504E-01	4.029E 02	2.816E-03	4.040E-03
7.771E 01	1.854E 00	4.047E 02	2.911E-03	7.029E-03
8.161E 01	2.156E 00	4.069E 02	2.832E-03	5.160E-03
ω 8.442E 01 ⊸ 8.728E 01	9,201E+01	4.078E 02	2.787E-03	4.349E-03
€1 8.729E 01	3.998E-01 0.000	4.082E 02	2.829E-03 2.829E-03	5.723E-03 5.726E-03
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	_+0E>E-03	047E0E=00

XABS	6-19	P⇔0B	PDA '	QOX	Q≠IB	9 ≠ 0 B	CAWALL	P-18/PS0	P-IB/PTO	P-OB/PSO	P=OB/PTO
6.468E 01	1.758E 01	1.758E 01	3.145E 02	-5.117E 03	-2.570E	(13 +2.547E 03	4.289E 03	4.662E 01	2.365E-02	4,662E 01	2.365E-02
6.505E 01	1.871E 01	1.839E 01	3.145E 02	-5.158 € 03	-2.585E	n3 →2.573E 03	4.337E 03	4.962E 01	2.517E+02	4.876E 01	2.473E-02
6.509E 01	1.871E 01	1.847E 01	3.145E 02	-5.162E 03	-2.586E	03 -2.576E 03	4.342E 03	4.962E 01	2.517E+02	4.898E 01	2.484E-02
6.529E 01	1.783E 01	1.890E 01	3.145E 02	-5.183E 03	-2.594E	n3 -2.589E 03	4.368E 03	4.729E 01	2.399E-02	5.012E 01	2.542E=02
6.695E 01	1.055E 01	8.600E 00	4.694E 02	-5.340E 03	-2,648E	n3 -2.692E 03	4.583E 03	2.798E 01	1.419E-02	2.280E 01	1.157E-02
6.762E 01	7.570E 00	8.835E 00	6.494E 02	-5.395E 03	-2.665E	n3 -2.730€ 03	4.665E 03	2.007E 01	1.0186-02	2.343E 01	1.188E-02
6.839E 01	4.145E 00	6.739E 00	8.354E 02	-5.458E 03	-2.680E	03 -2.778E 03	4.760E 03	1.099E 01	5.575£-03	1.787E 01	9.065E-03
6.9118 81	3.236E 00	4.786E 00	9.553E 02	-5.519E 03	-2.692E	n3 →2.827E 03	4.848E 03	8,580E 00	4.352E-03	1.267E 01	6.429E-03
6.972E 01	2.465E 08	3.486E 00	1.030E 03	-5,569E 03	-2.700E	03 -2.870E 03	4.922E 03	6.536E 00	3.315E-03	9.243E 00	4.688E-03
7.067E 01	1.825E 'Q0	1.470E 80	1.104E 03	-5,636E 03	-2.710E	ი3 −2. 926E 03	5.036E 03	4.8 39E 00	2.454E-03	3.898E 00	1.977E-03
7.110E 01	1.535E 00	1.556E 00	1.127E 03	45.660£ 03	-2.713E	n3 -2.947E 03	5.088E 03	4.07GE 00	2.065E+03	4.125E 00	2.092E-03
7.263E 01	1.426E 00	1.860E 00	1.203E 03	-5.726E 03	#2.724E	n3 -3. 002E 03	5.273E 03	3.781E 00	1.918E-03	4.932E 00	2.502E-03
7.278E 01	1.415E 00	1.636E 00			•	03 →3. 006E 03	5.290E 03	3.752E 00	1.903E-03	4.338E 00	2.200E-03
7.353E 01	1.246E 00	5.150E-01	1.249E 03	-5.758E 03	+2.730E	იპ - პ.029E 03	5.374E 03	3.303E 00	1.675E-03	1.366E 00	6.927E-04
7.354E 01	1.245E 00	5.090E-01	1.250E 03	-5.759E 05	⇒2.730E	03 - 3.029E 03	5.375E 03	3.300E 00	1.674E~03	1.350E 00	6.846E-04
7.486E 01	9.450E-01	0.000	1.273E Q3	-5,813E 03	-2.737E	n3 −3.076E 03	5.427E 03	2.506E 00	1.271E-03	0.000	0.000
7.771E 01	1.985E 00	0.000	1.332E 03	-5.826E 03	-2.750E	n3 ÷3.076E 03	5.525E 03	5.264E 00	2.6706-03	0.000	0.000
8.161E 01	1.325E 00	0.000				∩3 -3.076E 03	5.630E 03	3.513E 00	1.782E=03	0.000	0.000
8.442E 01	1.065E 00	0.000				n3 -3.076E 03	5.684£ 03	2.824E 00	1.432E-03	0.000	0.000
8.728E 01	1.540E 00	0.000	1.461E 03	-5.870E 03	-2.795E	n3 -3. 076E 03	5.707E 03	4.084E 00	2.071E-03	0.000	0.000
8.729E 01	1.541E 00	0+000	1,461E 03	-5.870E 03	-2.795E	n3 →3. 076E 03	5.707E 03	4.086E 00	2.073E-03	0.000	0.000

XABS	P-IB	P≂OB	PDA	Q0X	G-IB	Q=0B	CAWALL	P-18/PS0	P-IB/PTO	P=OB/PSO	P=08/PT0
6.981E-01	1.040E 00	0.000	-4.424E-01	0.000	0.000	0.000	2.470E-02	2.758E 00	1.399E=03	0.000	0.000
1.836E 01	1.040E 00	0.000	-3.464E 01	0.000	0.000	0.000	1.634E 02	2.758E 00	1.399€-03	0.000	0.000
3.070E 01	2.880E 00	0.006	-1.935E 02	0.000	0.000	0.000	5.053E 02	7.637E 00	3.874E-03		
3.508E 01	3.902E 00	0.000	-4.133E 02	0.000	0.000	0.000	6.804E 02	1.035E 01	5.249E~03	0.000	0.000
3.519E 01	4.214E 00		-4.780E 02	0.000	0.000	0.000				0.000	0.000
3.520E 01	4.231E 00	5.543F 00	-4.781E 02	0.000	•		6.854E 02	1.117E 01	5.668E-03	1.478E 01	7.495E-03
3.555E 01	5,200E 00	3.846F 00	-4.911E 02	0.000	0.000	0.000	6.857E 02	1.122E 01	5.690E-03	1.470E 01	7.455E-03
3.586E 01	5,030E 00	3.335E 00	-5.123E 02	0.000	0.000	0.000	7.209E 02	1.379E 01	6.994E-03	1.020E 01	5.173E-03
3,606E 01	4.925E 00	3.459E 00		-3.718E U	2 -3./18E n	2 0.000	7.529E 02	1.334E 01	6.766E-03	6.165E 00	3.127E-03
3.648E 01	4.252E 00	E 904E 00	-5.259E 02	-3. 134F A	< +3.759£ 0	2 0.000	7.729E 02	1.306E 01	6.624E-03	9.169E 00	4.651E-03
3.701E 01	5.260E 00	2.030E 00	-5.453E 02	-3,851E 0	2 -1.851E 0		8.164E 02	1.127E 01	5.719E-03	1.563E 01	7.930E+03
3.732E 01		8.9/2E 00	-5.677E 02	-4.209E 0	2 -3.972E ()	2 -2.363E 01	8.726E 02	1.395E 01	7.075E-03	2.379E 01	1.207E-02
3.803E 01	4,917E 60	1.000E 61	-5.798E 02	-4.363E Q	2 -4.047E 0:	2 -3.154E 01	9.063E 02	1.304E 01	6.614E=03	2.864E 01	1.453E-02
	4.150E 00	1.448E 01	5.933E 02	-4.712E 0	2 -4. 224E ni	2 -4.882E 01	9.834E 02	1.100E 01	5.582E-03	3.840E 01	1.948E-02
3.834E 01	7.912E 00	1.612E U1	. - 5.977E 02	-4.879F O	2 -4.314F a:	2 -5.685F ni	1.018E 03	2.098E 01	1.064E-02	4.276E 01	2.169E-02
3.875E 01	1.275E 01	1 • / 5 / 5 / 4	. *6.186E 02	-5.116E 0	2 ≓4.454E n:	2 - 6.621F 01	1.064E D3	3.382E 01	1.715E+02	4.659E 01	2.363E-02
3.881E 01	1.353E 01	1.78GE 01	6.224E 02	~5.157E ∩	2 =4.479F of	2 ⇔6.776F 01	1.072E 03	3.587E 01	1.820E-02	4.720E 01	2.394E-02
3.901E 01	1,586E 01	1.7626 01	-6.335E 02	~5.284E 0	2 ≒4.560E n:	2 -7.243F ni	1.094E 03	4.206E 01	2.133E-02	4.672E 01	2.370E=02
3.932E 01	1.866E 01	1./32E UL	. - 6.546E 02	~5.505 £ 0	2 ⇒ 4.786€ n:	2 -7.991E A1	1.130E 03	4.949E 01	2.510E-02	4.594E 01	2.330E=02
3.950E 01	2.022E 01	1.304E 01	. - 6.677E 02	~5.636E 0	2 ~4.79 6E ni	2 -8. 404E 01	1.150E 03	5.363E 01	2.720E-02	3.459E 01	
3.981E 01	1.811E 01	5.350E 00	-6.957E 02	~5.888F 0	2 -4 975F of	2 -9.133E 01	1.187E 03	4.801E 01	2.435E-02		1.754E-02
4.000E 01	1.686E 01	5.121E 00	-7.129E 02	-6.046F 0	2 +5.090E 0	2 -9.554E 01	1.209E 03			1.419E 01	7.196E-03
4.040E 01	2.074E 01	4.626E 00	-7.508F 02	-6.409F 0	25 3575 A	2 -1.052E 02	1.256E 03	4.471E 01	2.268E+02	1,358E 01	6.887E-03
4.041E 01	2.084E 01	4.613E 00	-7.517F 02	=6.418F 0	- 70.00 E ()	2 -1.054E 02	1 0575 03	5.501E 01	2.790E-02	1.227E 01	6.221E+03
4.130E 01	2.948E 01	3.512E 00	+8.607E 02	-7 SOTE 0	2 24 0005 0	2 -1.505E 02	1.257E 03	5.526E 01	2.803E-02	1.223E 01	6.205E-03
4.131E 01	2.958E 01	3.499F 00	₩8.620E 02	-7.542E A	- 40.0225 U	2 -1.512E 02	1.362E 03	7.817E 01	3.965E-02	9.312E 00	4.723E-03
4.137E 01	3.021E 01	3.419F 00	+8.7105 02	-7 644E 0	0.030E ();	2 -1.562E 02	1.363E 03	7.843E 01	3.978E-02	9.279E 00	4.706E-03
4.150E 01	3.142E 01	5.469F 00	-8 882E 02	-7 BUSE 0	- 90.00ZE 0	2 -1.562E 02	1.371E 03	8.011E 01	4.063E-02	9.065E 00	4.598E-03
4.246E 01	2.629E 01	2.119F 01	-0.537E 02	-7,040L U	* *0.183E 0	2 -1.664E 02 2 -2.672E 02	1.386E 03	8.333E 01	4.227E-02	1.450E 01	7.356E+Q3
4.409E 01	4.885E 01	4.707E 01	-D 389E 00	-9./JIE 0.	47.059E 0	2 -2.672E 02	1.501E 03	6.971E 01	3.536E-02	5.619E 01	2.850E=02
4.431E 01	5.181E 01	4.731E 01	-0 300E 02	-1.302F 0	-9.023E 0	2 -4.794E 02	1.699E 03	1.295E 02	6.570E-02	1.272E 02	6.451E-02
4.480E 01	5.857E 01	401572 01	-0 40EF 42	-1,442E 0	-9.329E 0	2 -5.092E 02	1.725E 03	1.374E 02	6.969E-02	1.252E 02	6.349E-02
4.481E 01	5.850£ 01	4 505E 01	-0 COOK 44	-1.291E 0	-1.006E 0	5-5.841E 02	1.785E 03	1.553E 02	7.878E+02	1.206E 02	6.117E=02
4.625E 01	4.716E 01	4 0 3 7 C 0 L	49.500E 02	-1.594E 0	-1.008E 0	5-857E 02	1.786E 03	1.551E 02	7.868E-02	1.205E 02	6.113E-02
4.626E 01	4.708E 01	4.0315 01	9,200E 02	-2.008E 0	-1.224E n.	3 -8.439E 02	1.963E 03	1.250E 02	6.343E-02	1.071E 02	5.430E-02
4.731E 01	3.881E 01	4.0346 01	43.50SE 05	-\$10\JE 0	-1.225E n	3 -8.458E 02	1.964E 03	1.248E 02	6.332E-02	1.070E 02	5.425E-02
4.733E 01	3.876E 01	3.0045 01	98.417E U2	-5.453E 0	372E 0	3 -8.458E 02	2.094E 03	1.029E 02	5.220E+02	9.715E 01	4.928E-02
4.811E 01	3.725E 01	J+000E 01	-8,405E 02	-2.431E 0	=1.375E n	3 -1.056E 03	2.097E 03	1.028E 02	5.214E~02	9.692E 01	4.916E-02
4.877E 01	3.043E 01	3.3235 01	~/.59/E U2	-2.678E 0	≥ -1.479E n:	3 -1.200E 03	2.194E 03	9.877E 01	5.010E-02	8.818E 01	4.473E-02
4.878E 01		3.043E U1	-6.608E 02	-2.874E 0	5 +1.563E n3	3 -1,310E 03	2.277E 03	8.068E 01	4.092E-02	8.068E 01	4.092E+02
4.931E 01	3.038E 01	3.U38E U1	-6.592E 02	-2.877E 0	-1.565E n	3 -1.312E 03	2.278E 03	8.057E 01	4.087E-02	8.057E 01	4.087E-02
	2.813E 01	2.8135 01	-5.784E 02	-3.051E 0	-1.630E 0	3 -1.391E 03	2.345E 03	7.459E 01	3.783E-02	7.459E 01	3.783E+02
5.072E 01	2,264E 01	2.264E U1	-3.907E 02	-3.364E 0	-1.792E n	3 -1.573E 03	2.522E 03	6:004E 01	3.046E-02	6.004E 01	3.046E-02
5.282E 01	1.856E 01	1.000E U1	-1.638E 02	-3.784E N.	5 →2 DDJF D.	5 w1.7x1x nx	2.789E 03	4.922E 01	2.497E-02	4 922E 01	2.497E-02
5.332E 01	1.823E 01	1.023E U1	-1.16UE 02	-3.872F N	-2.04AF A	3 -1 ROUE 03	2.852E 03	4.833E 01	2.452E-02	4.833E 01	2.452E-02
5.407E 01	1.659E 01	1.659E, U1	-4.865E 01	-3.998E 0	. →2.112E n3	3 -1.886F 03	2.948E 03	4.398E 01	2.231E-02	4.398E 01	2.231E+02
5.483E 01	1.492E 01	1.445E 01	1.243E 01	~4.117E O.	2.172F ∩3	5 -1.94KF 03	3.046E 03	3.958E 01	2.007E-02	3.958E 01	2.007E-02
5.576E 01	1.342E 01	1.342E 01	1.811E 01	-4.252E 0) -2.248€ n3	5 -2. 012E n3	3.164E 03	3.558E 01	1.805E=02	3.558E 01	
5.626E 01	1.260E 01	1.260E 01	2.226E 02	-4.318E 0	5 -2.271 E n3	5 -2 -047E n3	3.209E 03	3.342E 01	1.695E-02		1.805E-02
5.631E 01	6.862E 00	1,251E 01	2,262E 02	-4.325E 0	-2.274E 03	-2.050E 03	3.216E 03	1.820E 01	9.230E=03	3.342E 01	1.695E-02
5.645E 01	6.862E 00	1.229E 01	2.343E 02	-4.342E 0	າ +2.282E ດິ	3 -2. 060E n3	3.234E 03	1.820E 01	9.230E+03	3.318E 01	1.683E-02
5.65 3 E 01	1.216E 01	1.216E 01	2.392E 02	-4.351F n	-2.286F A	3 -2.065E 03	3.245E 03			3.258E 01	1.653E-02
5.681E 01	1.170E 01	1.170E 01	2.548E 02	-4.385F n	3 =2.301F 03	3 -2.084E 03	3.280E 03	3.223E 01	1.635E~02	3.223E 01	1.635E-02
5.704E 01	1.133E 01	1.133E 01	2.660E 02	-4.411F 0	-2 312F A	3 -2.099E 03	3.309E 03	3.102E 01	1.574E+02	3.102E 01	1.574E-02
5.776E 01	1.012E 01	1.812E 01	2.950F 02	-4 493F n	2 346F A	3 -2.147E 03		3.003E 01	1,523E-02	3.003E 01	1.523E-02
5.878E 01	5.175E 00	5.175E 00	3.127F 02	-4.59nF n	3 32 326E A	5 -2.203E 03	3.402E 03	2.685E 01	1.362E-02	2.685E 01	1.362E=02
6.079E 01	1.005E 01	1.005E 01	3.145F 02	-4.757E 0		5 -2.310E 03	3.532E 03	1.372E 01	6.960E-03	1.372E 01	6.960E=03
6.221E 01		1.231E 01	3.145F 02	-4.881E 0		3 -2.310E 03	3.790E 03	2.665E 01	1.352E-02	2.665E 01	1.352E-02
- ***			042.UE UZ	. FOOTE U	, 400E ()	2 -5 + 3 A D F 6 13	3.972E 03	3.265E 01	1.656E-02	3.265E 01	1.656E+02